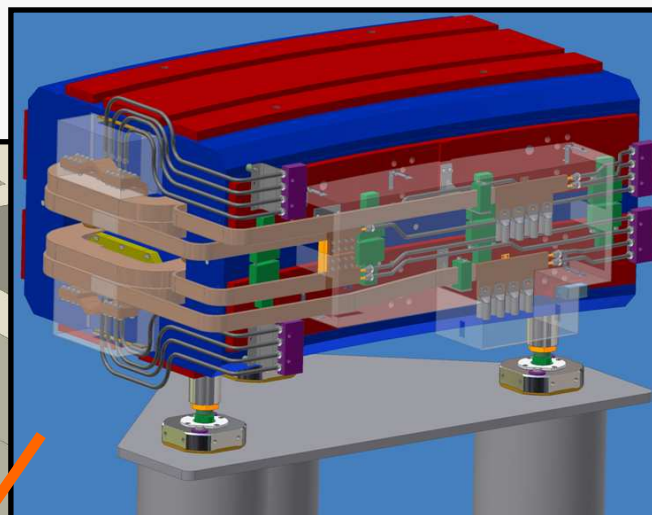
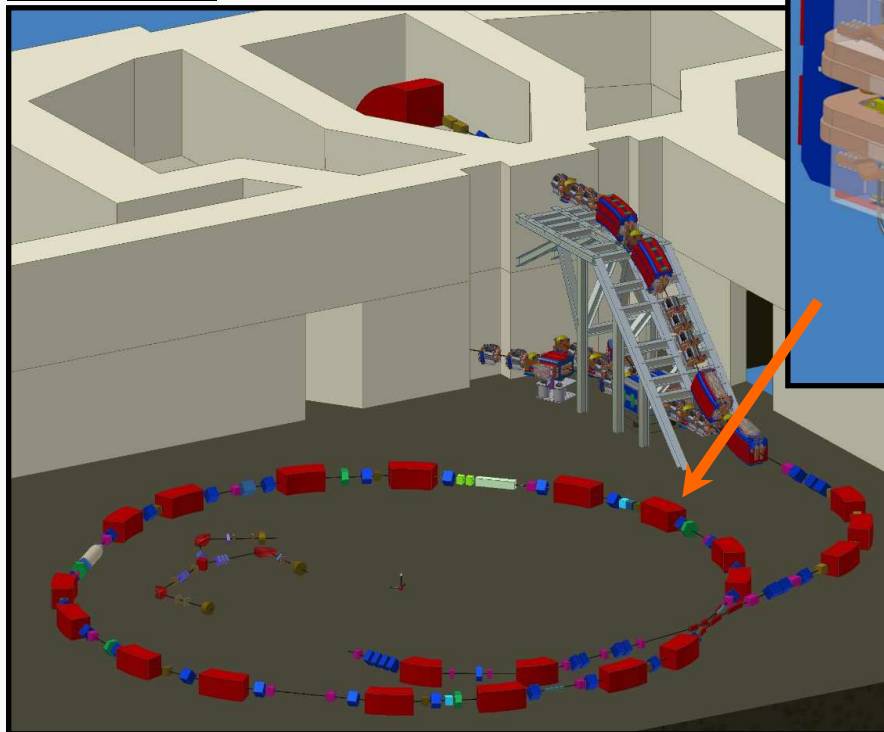


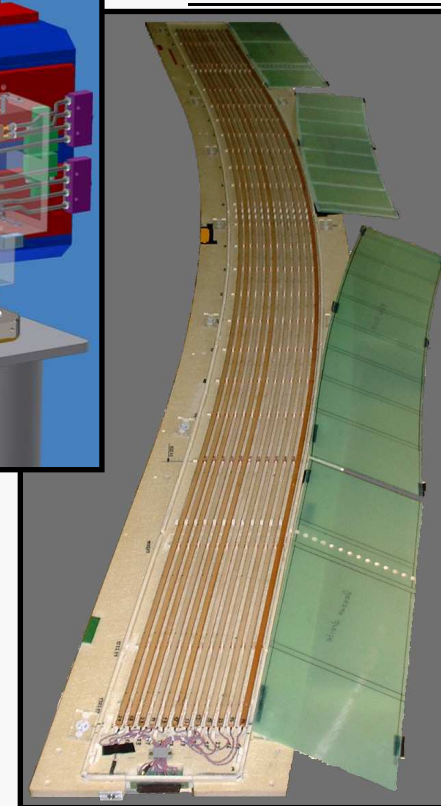
## Curved fluxmeter for static and dynamic characterization of pulsed CNAO magnets

CNAO project



CNAO curved dipole

Curved fluxmeter



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## CNAO measurements: 26 curved dipoles



■ Nominal maximum field [T]	1.4992
■ Bending radius [m]	4.231
■ Bending angle [deg]	22.5
■ Magnet gap height [mm]	72
■ Magnetic length (@ max.) [m]	1.6772
■ Overall length [m]	1.9046
■ Good field region [mm]	$\pm 60$ (hor); $\pm 28$ (vert)
■ Field Quality [ $\Delta B/B_{nom}$ ]	$\pm 2 \cdot 10^{-4}$
■ Nominal Current [A]	2800
■ Maximum Current [A]	3000
■ I nominal / I injection ratio	17
■ Field stabilization time	500 ms

### ■ Curved fluxmetre choice :

⇒ designed to measure integrated field and its uniformity along the bent beam path.

⇒ allows small difference between the measured integrated field and the integrated field on the real trajectories of the beam.

⇒ method based on bucked signals appears to be the most appropriate for the high homogeneity of the field requested.

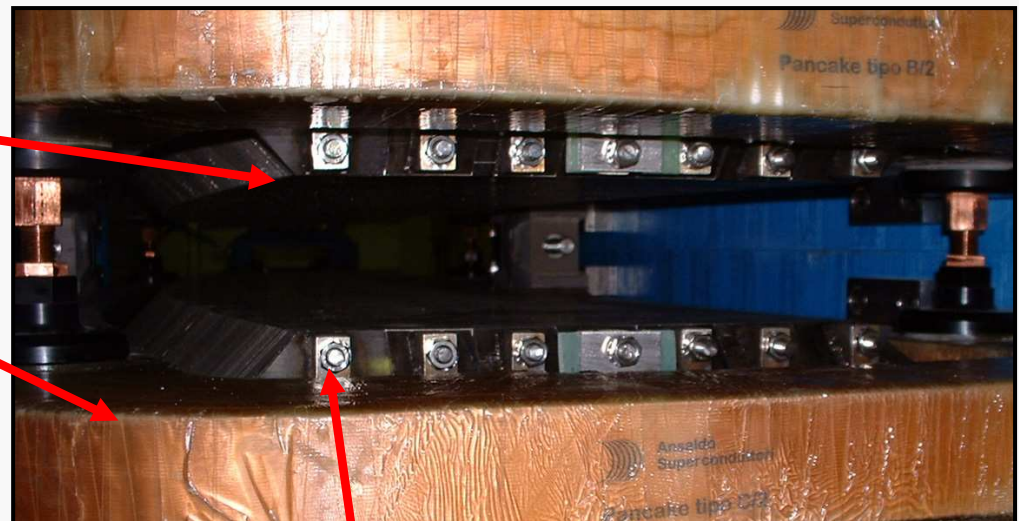
## Magnet specificity: optimal homogeneity

- Optimal homogeneity for injection current (168A) and nominal current (2800A) in the 2D design.

### Due to:

Minimun pole profil compensation to optimize homogeneity at low current.

Coils positioned close to the poles to compensate the saturation of the poles at nominal current.



### Disadvantage:

Limited accessibility for the shimming due to the coil positioning.

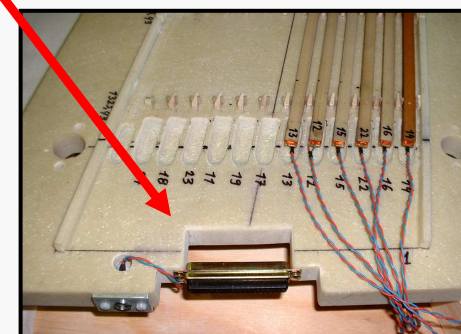
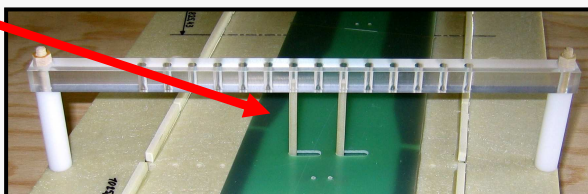
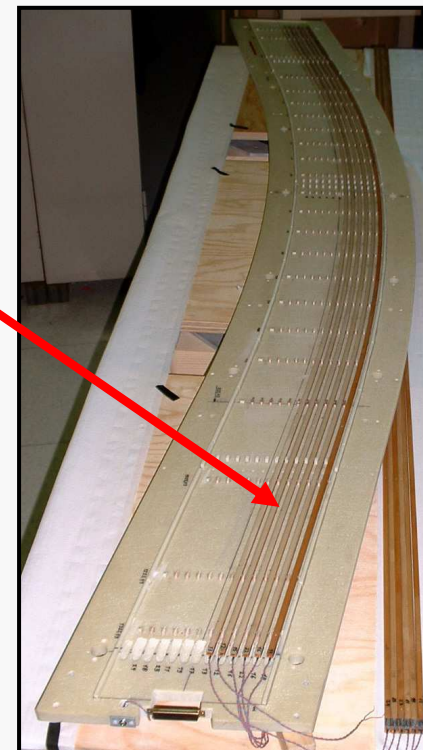
## Fluxmeter making

### Fluxmeter

- 11 curved coils (+ 1 spare ) - Coils size = 6 x 8 x 2755 mm.  
Mounted on a rigid support, and maintained by glass fiber pins (15 mm spacing).
- A cover protect the coils  $\Rightarrow$  the reference coil can slide on it without creating any vibration on the fluxmeter's coils.
- 14 Delrin wheels  $\Rightarrow$  to roll the fluxmeter longitudinally.
- Connections of the coils with twisted pair cables to a CANNON connector.

### Reference coil

- Reference coil curved in the same way as the fluxmeter's coil.
- Stability guaranteed by its glass fibre support (116 mm width, 10 mm height).
- Precise positioning of the reference coil on each coil of the fluxmeter with a system based on vertical rods .





## Calibration method

The fluxmeter is cross-calibrated with respect to the additional curved reference coil.

(For CNAO application we don't need absolute field values, but a relative comparison between the 26 dipoles and the reference magnet.)

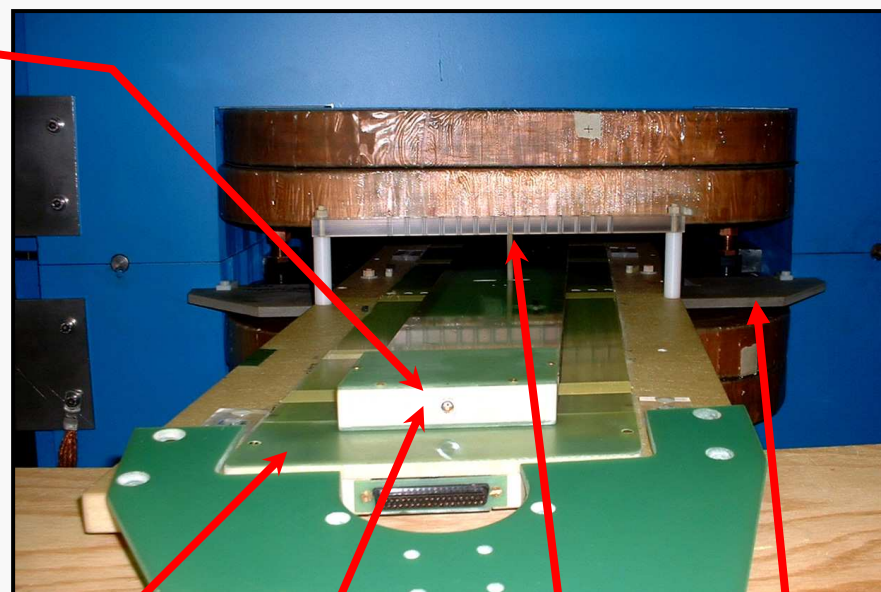
### ABSOLUTE VALUES

Long curved coils cannot be calibrated a CERN (calibration magnet with aperture large enough not available) so absolute accuracy is limited to few  $10^{-3}$ .

Their areas taken into account are their surfaces before being bent.

### RELATIVE VALUE

By comparison with a reference coil, which can be placed next to any other, the relative accuracy of all coils is better than  $10^{-4}$ .



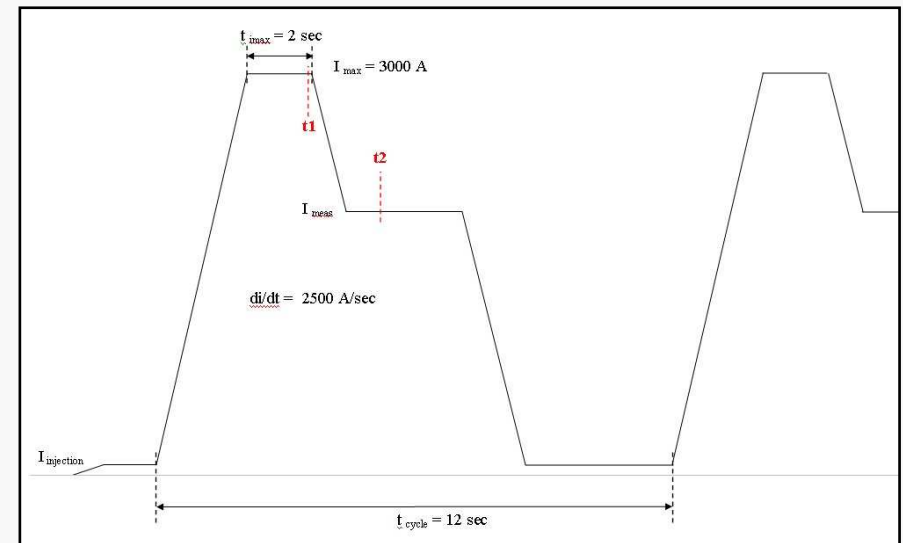
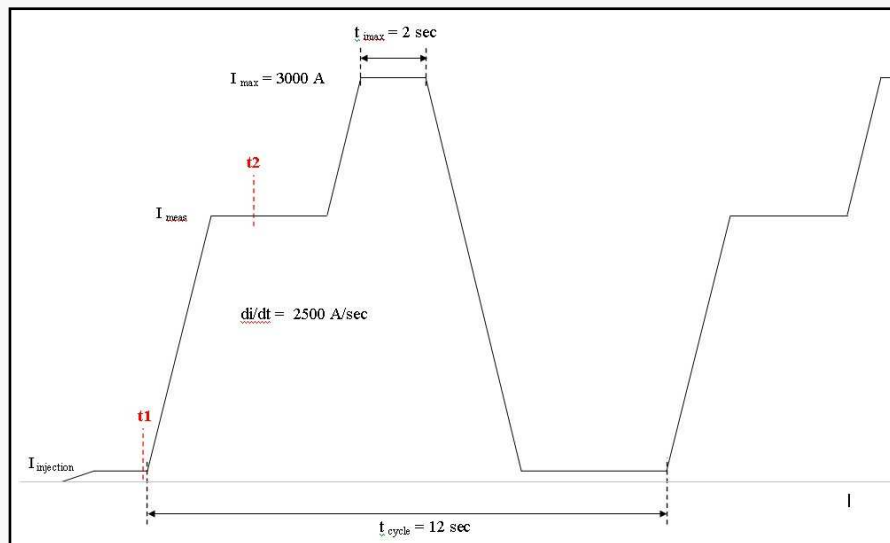
Fluxmeter with 12 coils

Positioning system for reference coil

Mobile reference coil

Plate for a precise fluxmeter's positioning

## Current measurement cycles used



- Field measurement done between **t1** and **t2** to study dynamic effects for ramp up and ramp down current.
- For every measurement the current is ramped up to the maximum current  $I_{\max}$  during the cycle  $\Rightarrow$  the same hysteresis cycle followed for any measurements.
- Timing precision = 1 ms (Timings handled with a VME crate).

## Shimming

- Different shimming configurations tested:

⇒ shims with **straight edge**

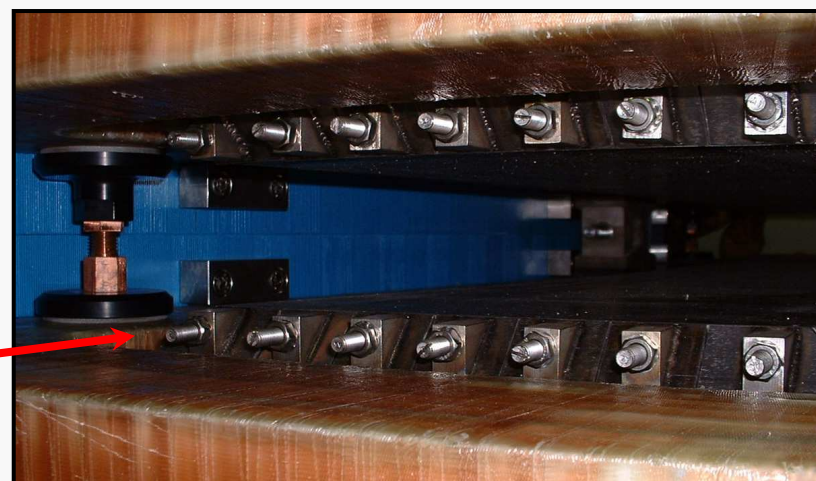
⇒ shims with **45° chamfers**

- With **45° chamfers** ⇒ improvement for field homogeneity over straight edge. They reduce peak fields near the end plates ⇒ but not as good as expected.

- Original shimming bolts (**magnetic**) did perturb low field close to the poles (Due to the bolt head volume).

- Non magnetic (**stainless steel**) bolts did not allow to obtain an homogeneity within the specifications close to the poles (Lack of magnetic volume in the holes).

- **Bi-metal bolts (Fe-Inox)** did allow to fulfill the homogeneity in the total good field region.



## Bi-metal bolts effect on shimming

Bi-metal bolts:

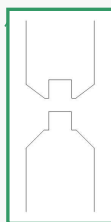
⇒ allow  $\pm 10^{-4}$  field homogeneity adjustment (We couldn't obtain it only with shimming plates).

⇒ allow the magnet to fulfill the specifications for both I injection and I nominal.

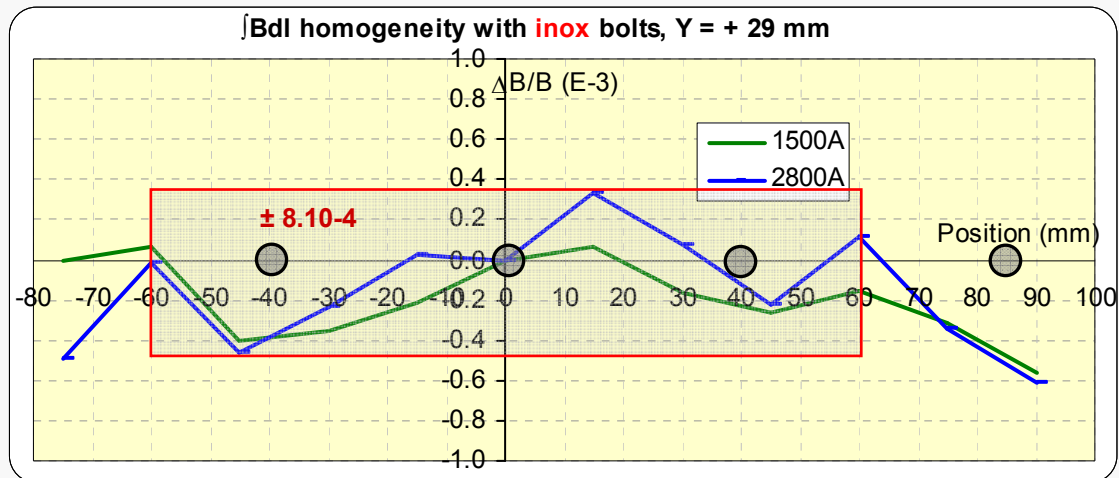
⇒ widen the good field area on the Y axis.



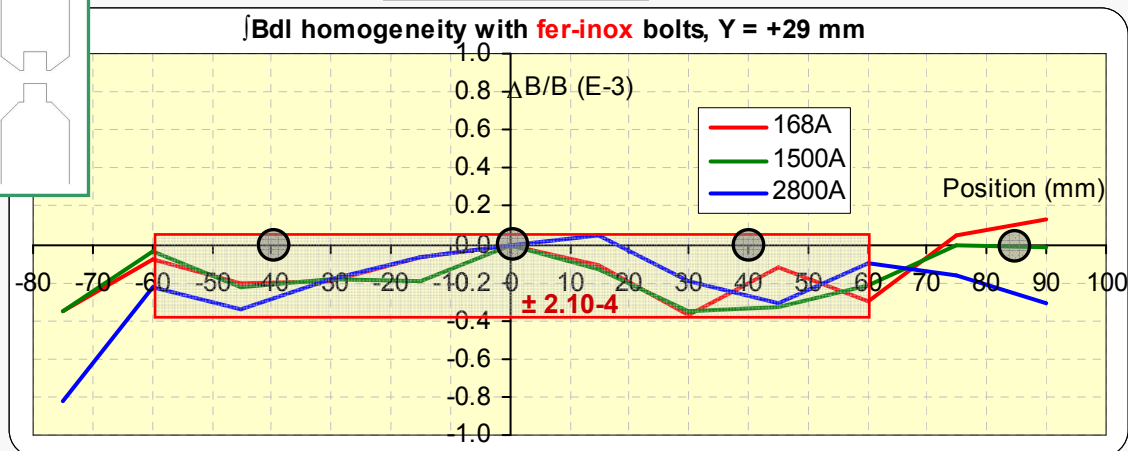
← Welding



### Inox bolts



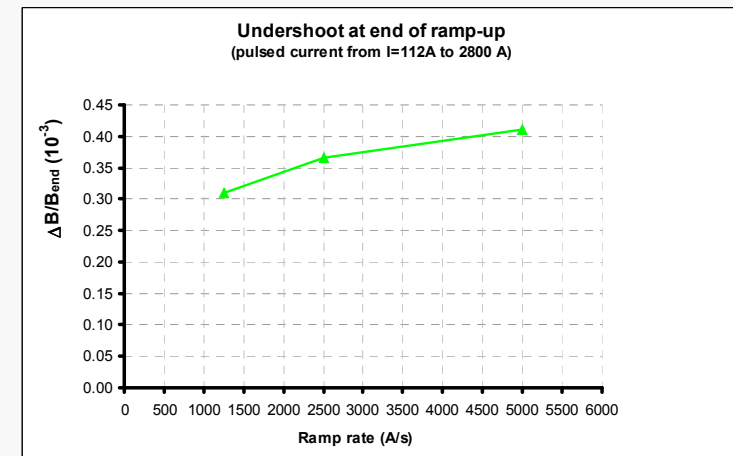
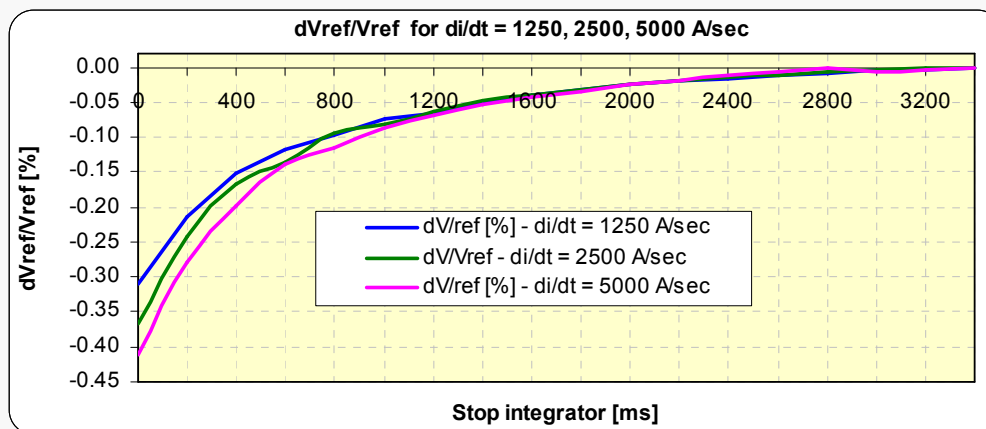
### Fe-Inox bolts





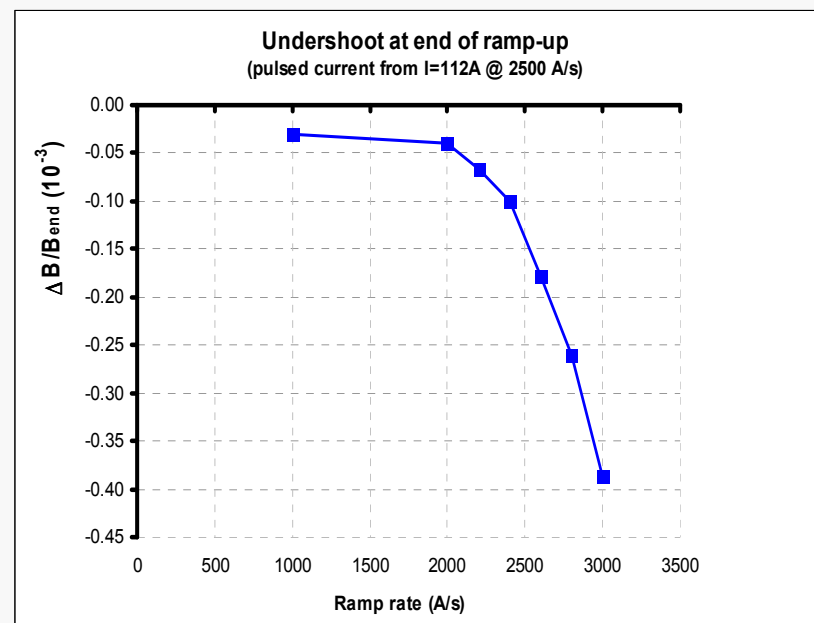
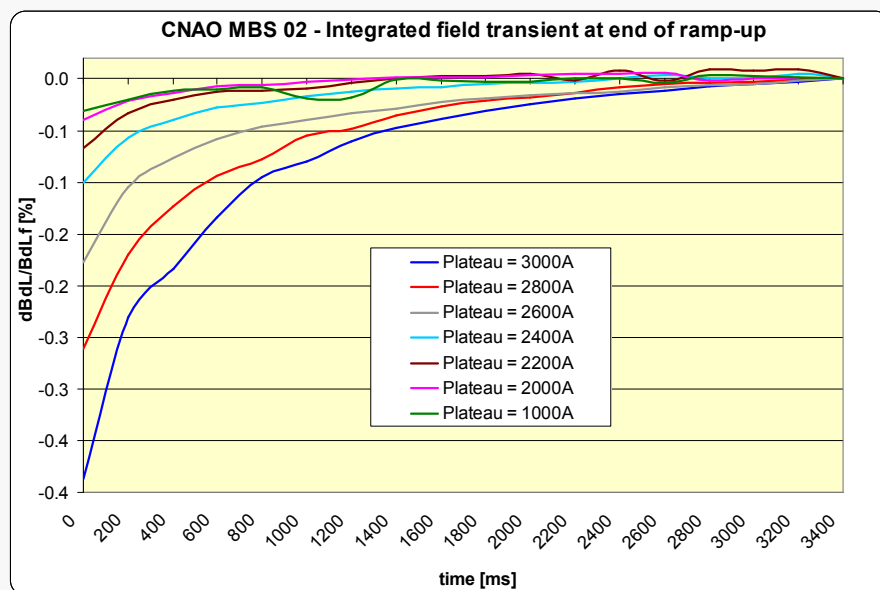
## Magnet dynamic behavior

- Strong Eddy current effects, field stabilized more than 2 seconds after the current flat-top start, with growing current.
- Even with phosphated metal sheets. (2<sup>nd</sup> prototype)
- Eddy current not proportional to  $di/dt$  (curves below)  $\Rightarrow$  CNAO magnet behaves like a short magnet.
- Needs at least 30 cycles to stabilize the remanent field  $\Rightarrow$  Problem due to the only hot-rolled yoke metal sheets ?  
(CNAO magnets are built using only hot-rolled metal sheets, without a following cold-rolled process as on other former magnets).



## Magnet dynamic behavior

- Amplitude of the transient at the end of ramp-up (undershoot) vs. flat-top level
- The time constant does not depend on either ramp rate or flat-top level



## Eddy current with growing and decreasing current

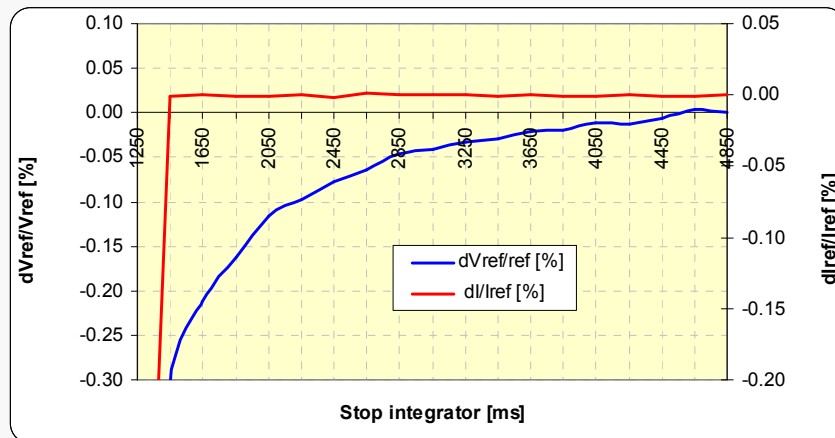
- With decreasing pulsed current, Eddy current effects are much less important. It takes 4 times less to be within  $2 \cdot 10^{-4}$  of the stabilized field.

- Due to the steel permeability curve:

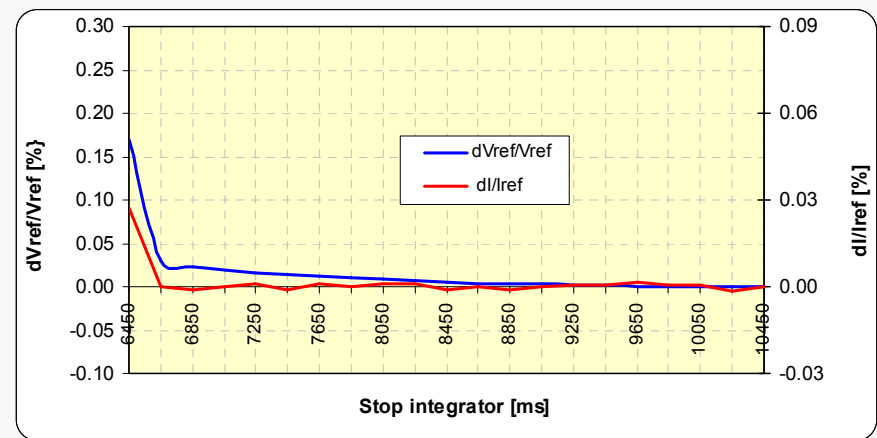
3000 A  $\Rightarrow$  low permeability  $\Rightarrow$  long Eddy current effects

168 A  $\Rightarrow$  higher permeability  $\Rightarrow$  short Eddy current effects

Eddy current with **growing** current from 168 to 3000 A (  $\int Bdl$  )

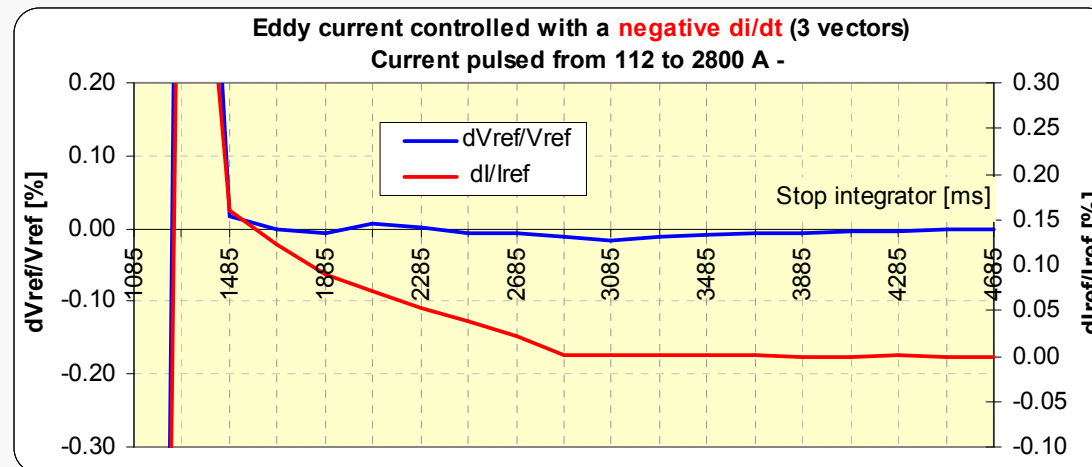


Eddy current with **decreasing** current from 3000 to 168 A (  $\int Bdl$  )



## Eddy current effects controlled with a negative $di/dt$

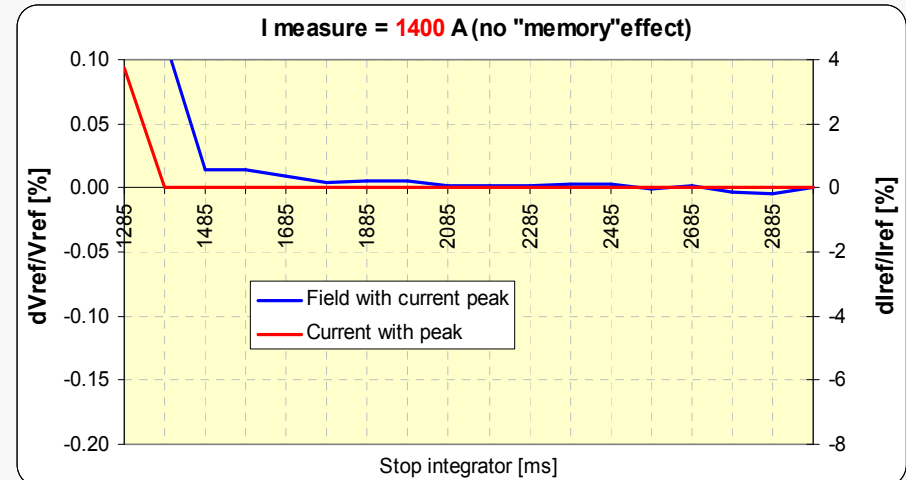
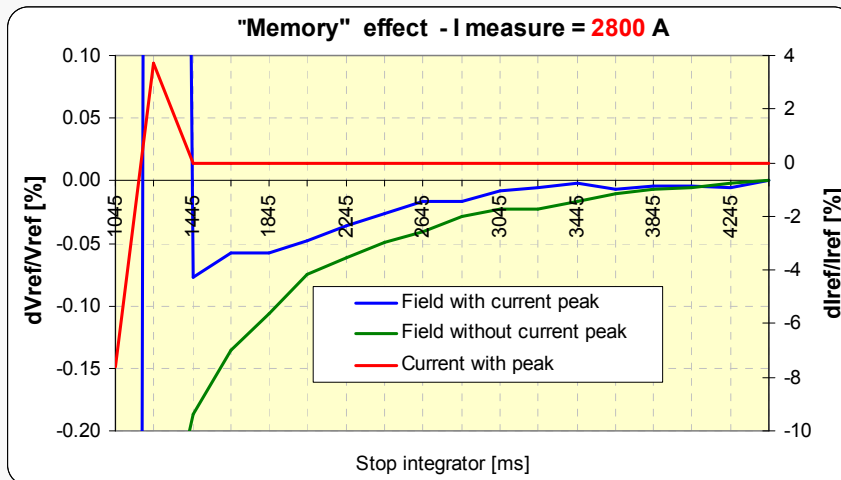
- Eddy current effects can be limited with an “over current peak” and a controlled negative  $di/dt$  (curves below).
- Limitation  $\Rightarrow$  each current flat-top needs its own peak et negative  $di/dt$  curve for an efficient Eddy current control.
- Finally not applicable to CNAO project because of the variety of pulsed current.





## “Memory” effect

- Left curve below: magnet pulsed from 168 to 3000 A ( $di/dt$  5000 A/sec), immediately followed with a negative ramp ( $di/dt$  - 5000 A/sec) from 3000 to 2800 A.
- After this current peak, the field curve general shape is the same than for a measure without any peak current.
- The magnet did act as if there was a “memory” effect of the Eddy currents.
- In non saturated state (1400 A curve) we can partly compensate the ramp up Eddy currents by a similar ramp down, but in a saturated state (2800 A curve) there is a “memory” of the highest Eddy currents.



## Conclusion

### The B-train solution for Eddy current control

- Real-time field measurement fed back to machine control system (closed loop).
- Real-time field adjustment  $\Rightarrow$  allows to always obtain the wanted field, independently of the last current cycle used.
- Automatic compensation of short term as well as long term drifts and better reproducibility.
- Eddy current control for faster operation.
- More safety for patients

### Efficiency of bi-metal bolts for high quality homogeneity adjustment

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