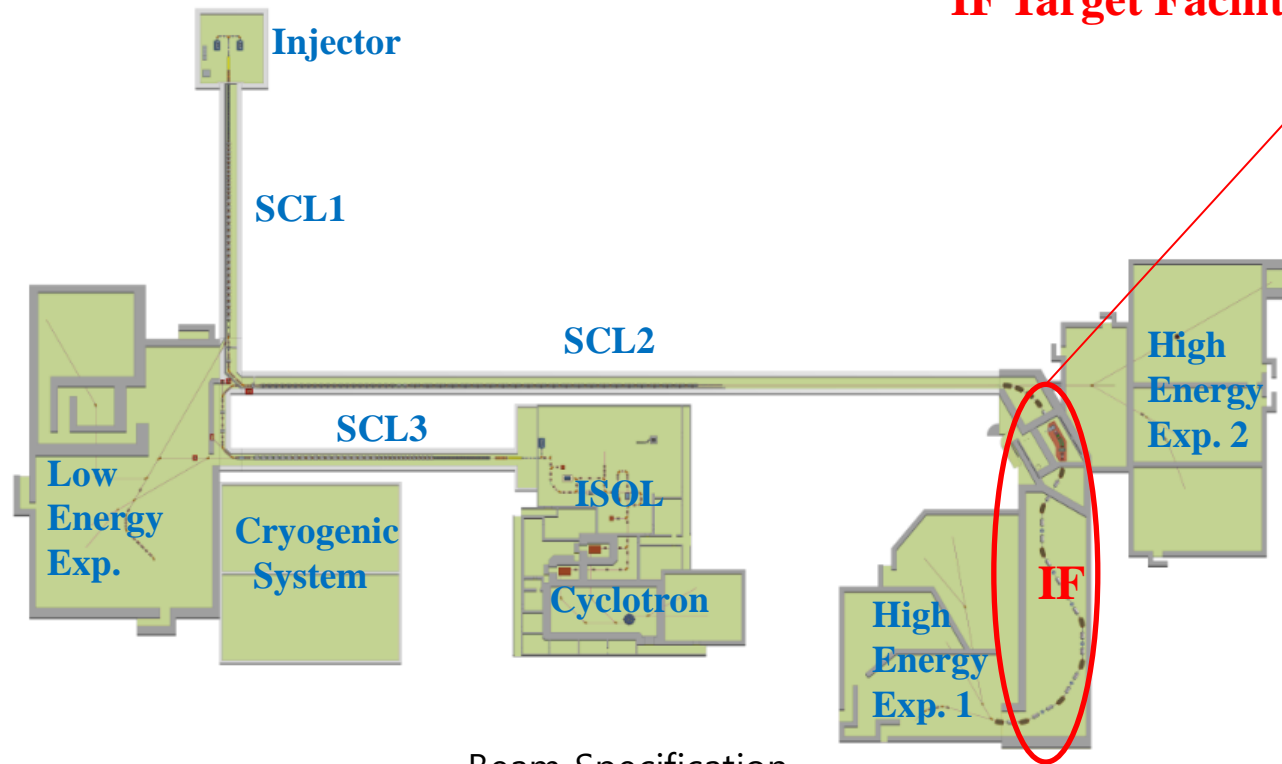


Radiation Transport Calculation for the In-Flight Fragment Separator of RISP



Rare Isotope Science Project(RISP)
Institute for Basic Science(IFS)
Mijung Kim

Raon Accelerator Layout

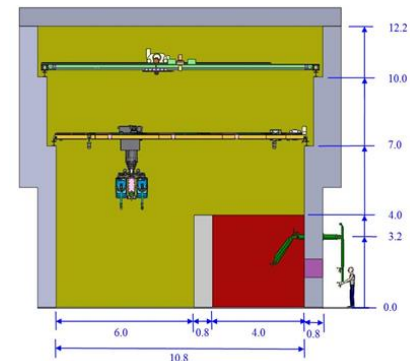
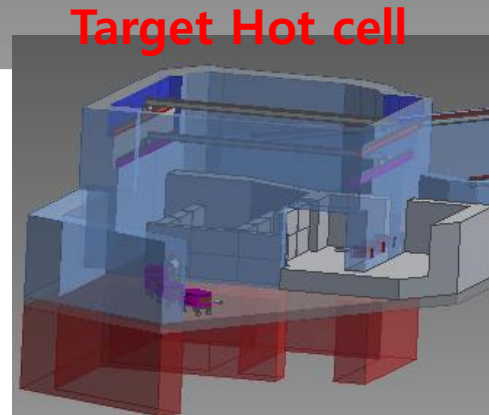
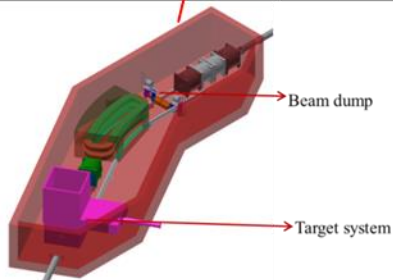
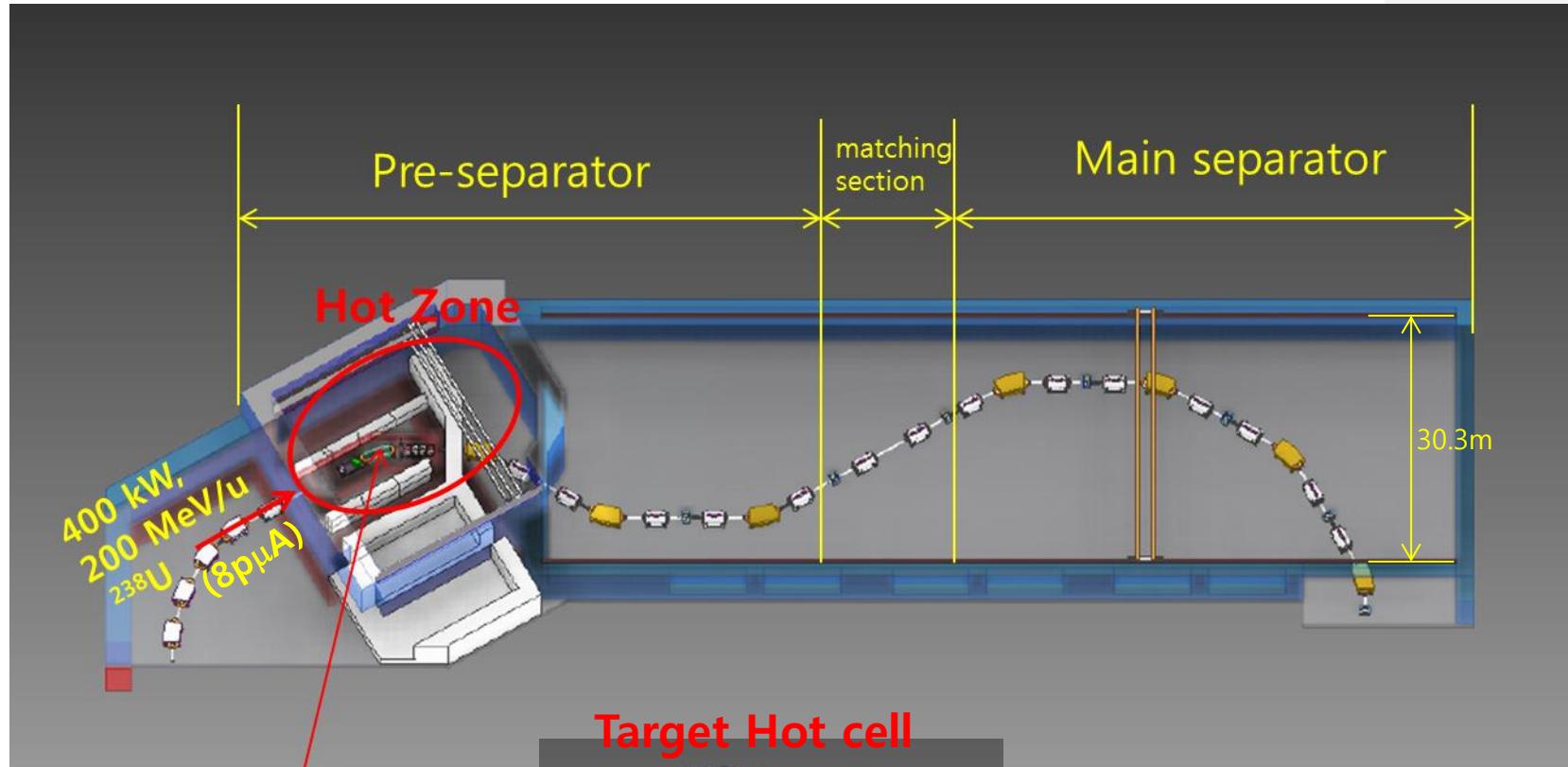


Beam Specification

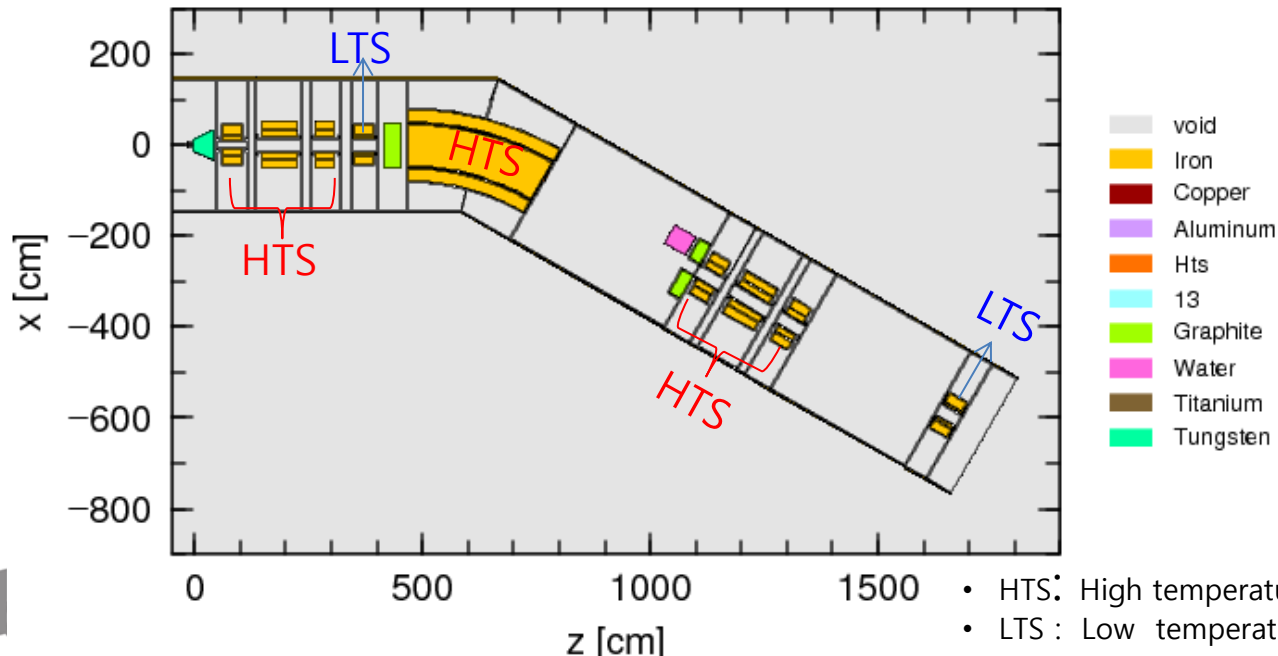
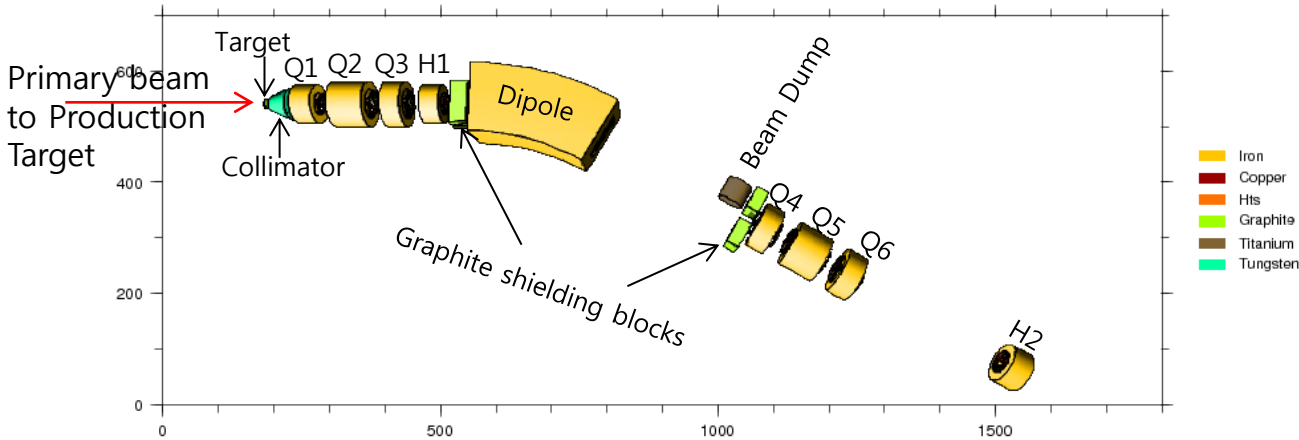
Accelerator	Driver Linac			Cyclotron
particle	proton	Xe ⁺⁵⁴	U ⁺⁷⁹	proton
Beam energy(MeV/u)	600	251	200	70MeV
Beam current(pμA)	660	11	8.3	1mA
Power on target(kW)	400	400	400	70 kW



IF Separator Layout



Model for PHITS Calculation



- HTS: High temperature superconducting
- LTS: Low temperature superconducting

Raon resource summary

resource	description
computing 30 node	Node[01-30]
CPU	2.9Ghz (16core per node)
Memory	64G(4G per core)
shared filesystem	/home(84TB)

Calculation condition

version: PHITS2.64

- Heavy ion: JAM/QMD+GEM
- Neutron($E > 20\text{MeV}$): JAM/QMD+GEM
- Neutron($E \leq 20\text{MeV}$): ENDF/B-VI, ENDF/B-VII, JENDL-3.3, JENDL-4.0

HTS Coil specification & Design

◆ Basic specifications of HTS coil

- Operating temperature : ~ 50 K
- Operating current : Amount equivalent to the field gradient of 15 T/m
($<$ critical current of HTS coil)
- Coils shape : Racetrack, Pancake
- Number of HTS coils : 1~4 single pancake (or, 1~2 double pancake)
- **HTS wire : 2nd Generation HTS Tape (ReBCO coated conductor-
GdBCO was used for the PHITS calculation)**
(width of tape = 12 mm)
- Electric insulation between turns : Metal insulation (**stainless steel tape**)

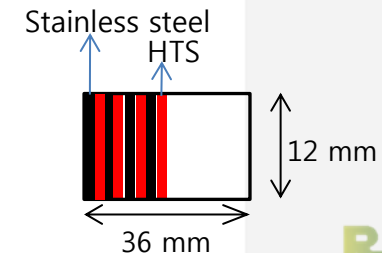
◆ HTS wire

- Two candidates : SuperPower, SuNam

◆ Number of HTS coils, Critical current and Operating current

-Basic shape of HTS coil

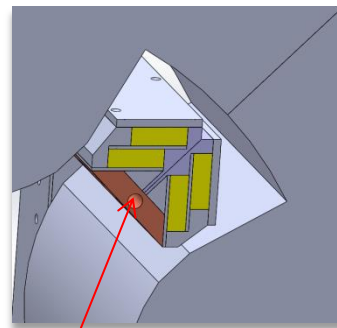
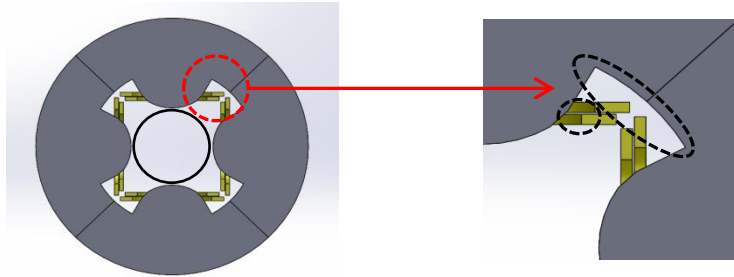
- **Cross-sectional dimension of single pancake = 36 mm X 12 mm**
(considering the acceptability in the yoke space)
- HTS tape : 12 mm width x 0.1 mm thickness
- Thickness of stainless steel insulator = 0.05 mm



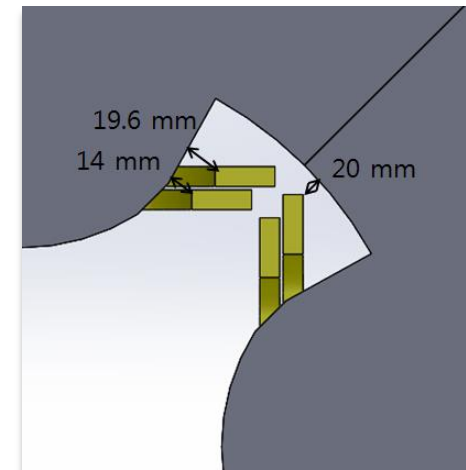
Iron Yoke Design

◆ Shape of iron yoke

1. Magnetic field performance of magnet (Field gradient, uniformity...)
 - Dominantly **depends on the shape of Iron Yoke**
2. **Space** for thermal insulation, mechanical structures for coil support and GHe cooling channels.
 - Size and shape of the space also affects the performance of magnet

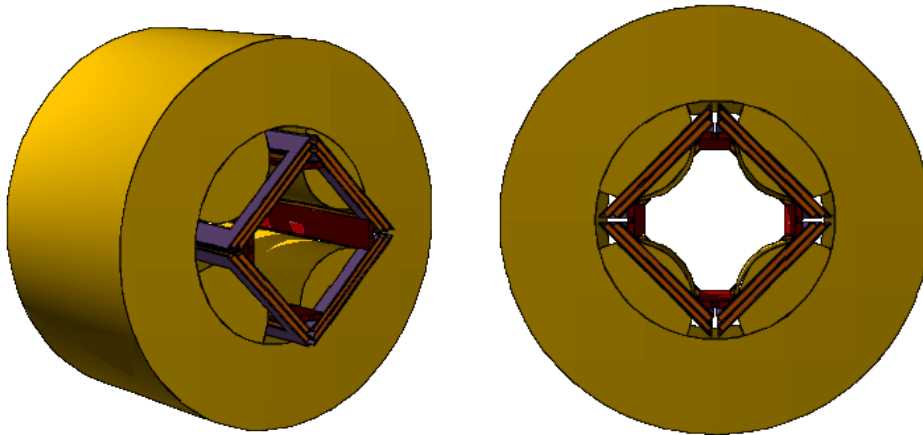


GHe cooling channel

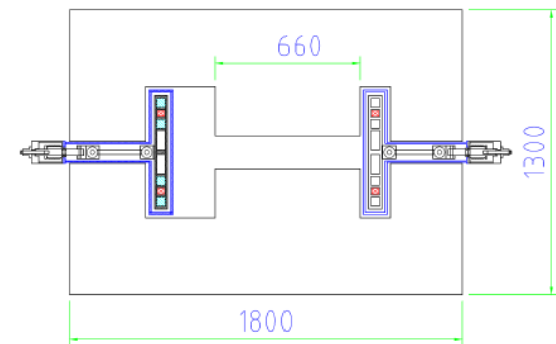
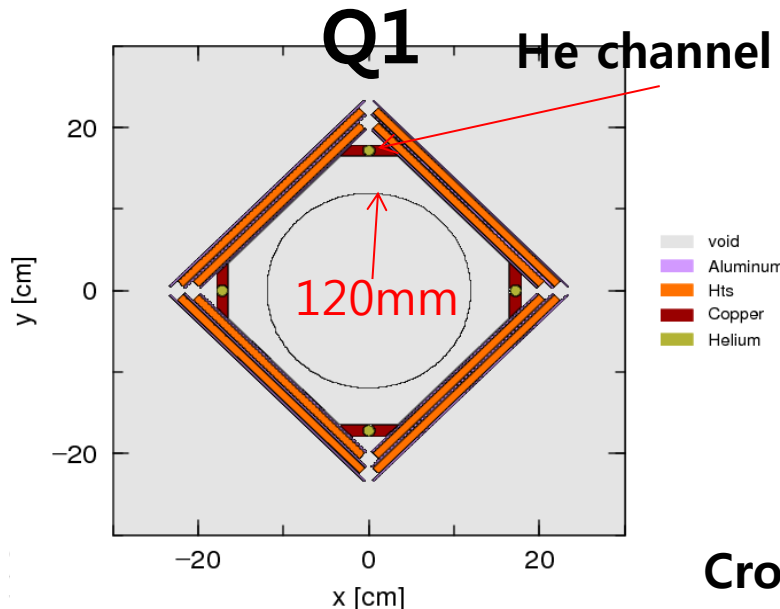
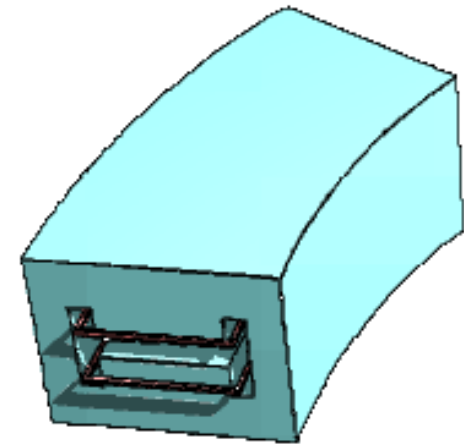


Magnet Model for PHITS calculation

Quadrupole



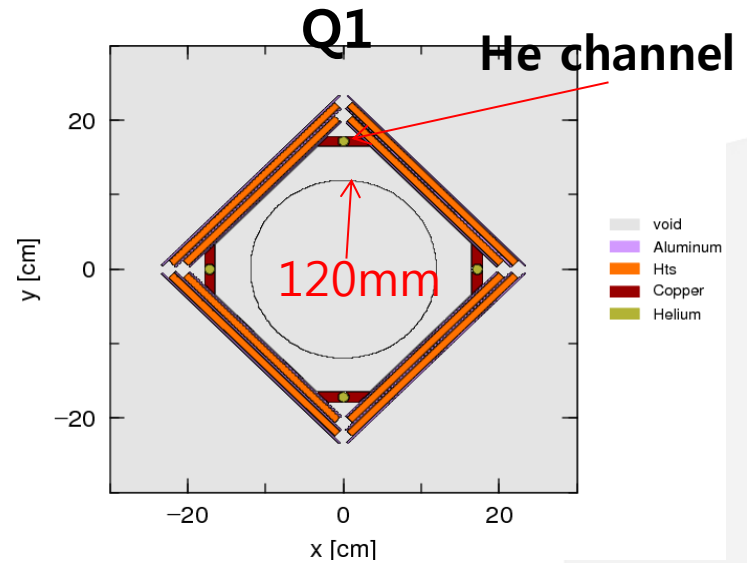
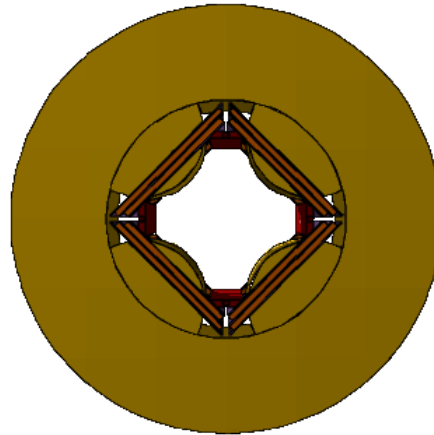
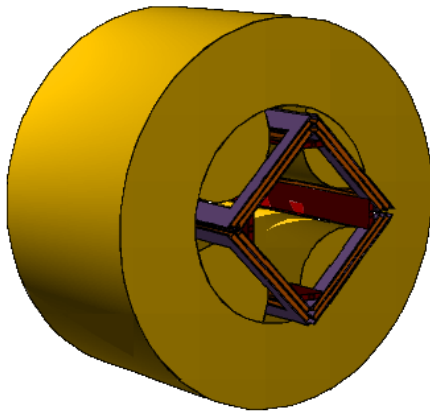
Dipole



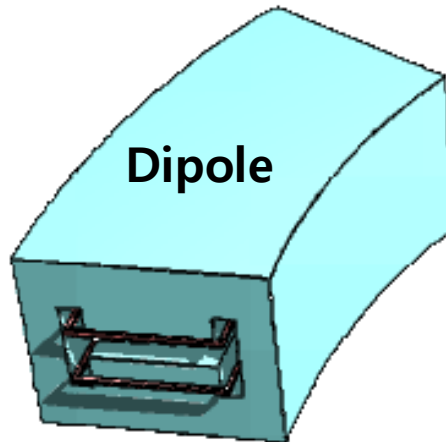
Cross sectional view

Magnet Model for PHITS calculation

Quadrupole



Dipole

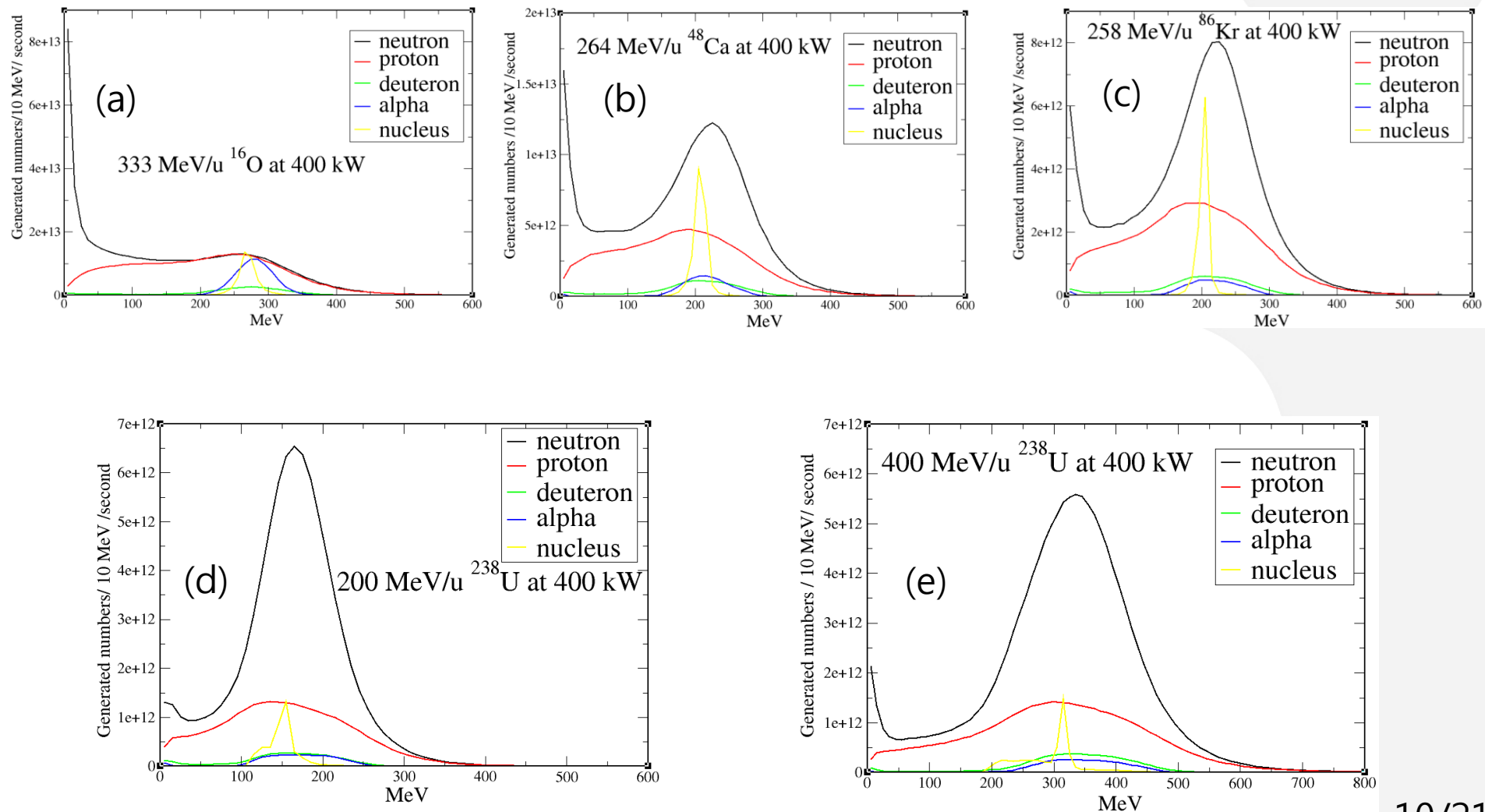


Used Primary beams and conditions

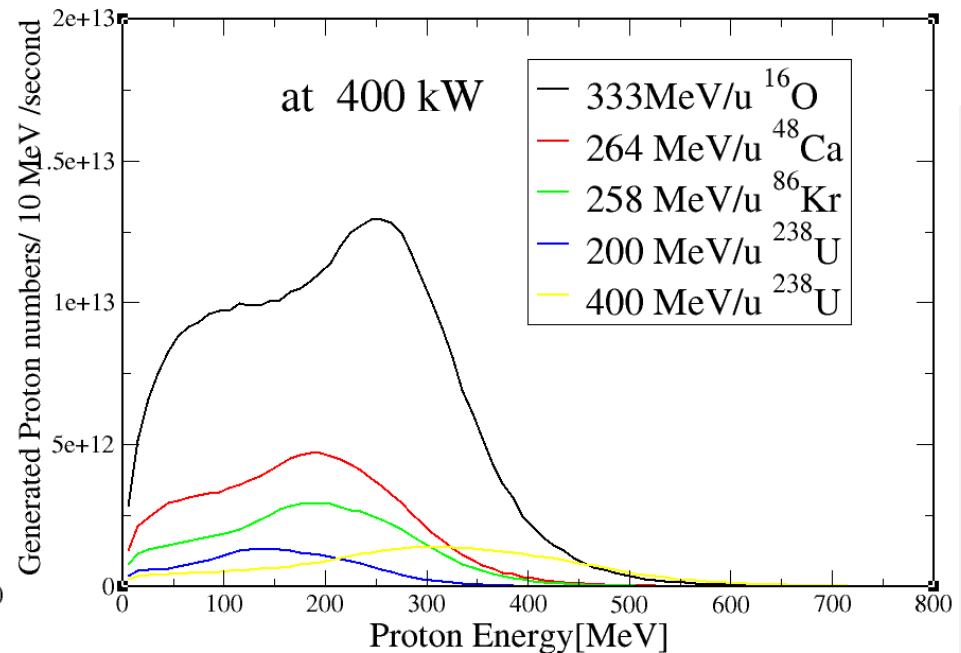
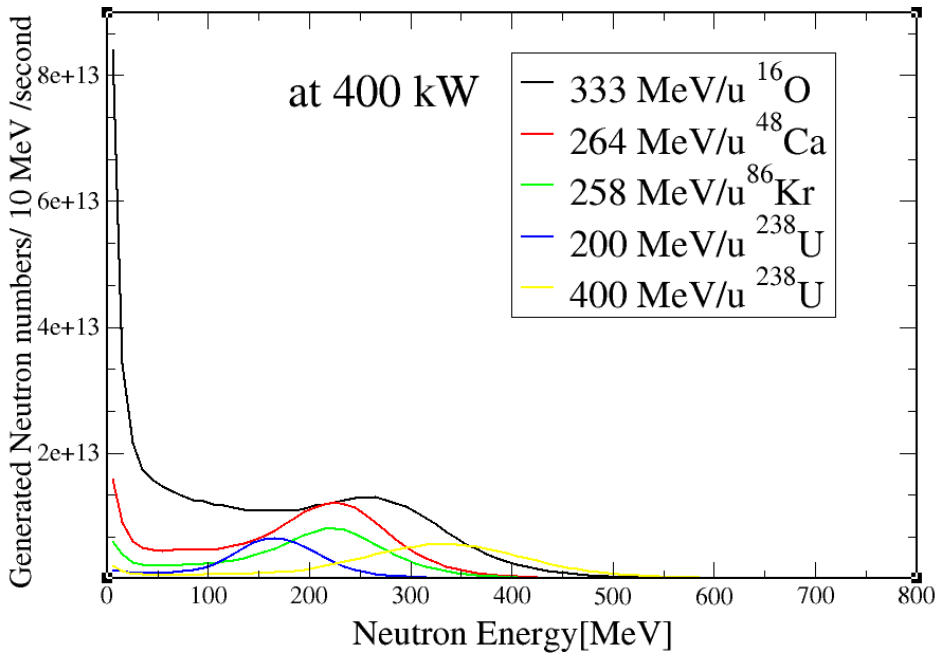
Primary beam	Projectile energy (MeV/u)	Graphite Target thickness (cm)	Beam intensity (pps)	wanted RI Frag.
^{16}O	333	2.298	4.692×10^{14}	^{12}N
^{48}Ca	264	0.752	1.973×10^{14}	^{16}C
^{86}Kr	258	0.406	1.127×10^{14}	^{77}Co
^{238}U	200	0.136	5.252×10^{13}	^{132}Sn
^{238}U	400	0.374	2.626×10^{13}	^{132}Sn

Target thickness, beam intensity, magnetic field were obtained from LISE++

Particles and Nuclei from the Target

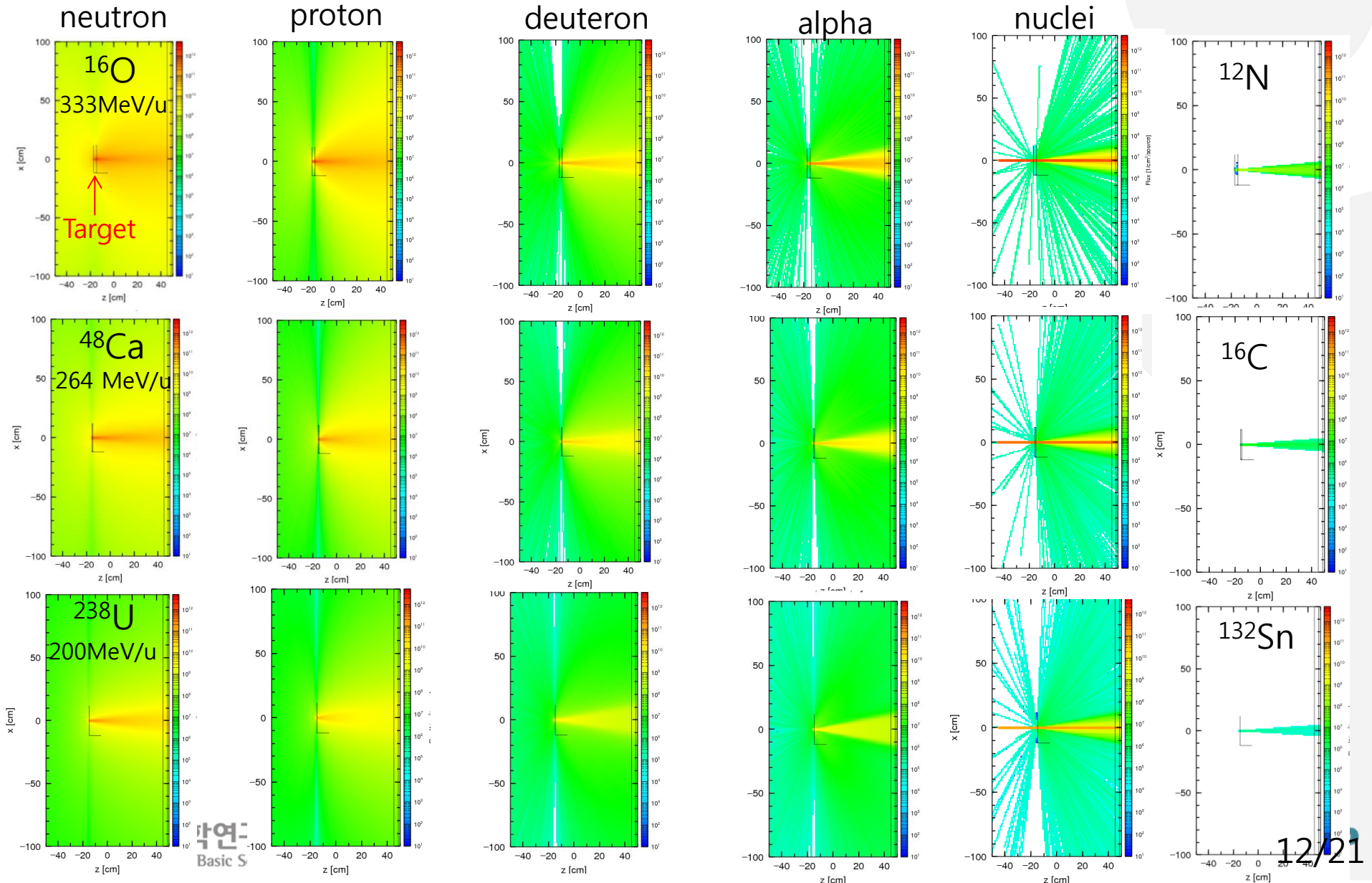


Neutrons and Protons from the Target



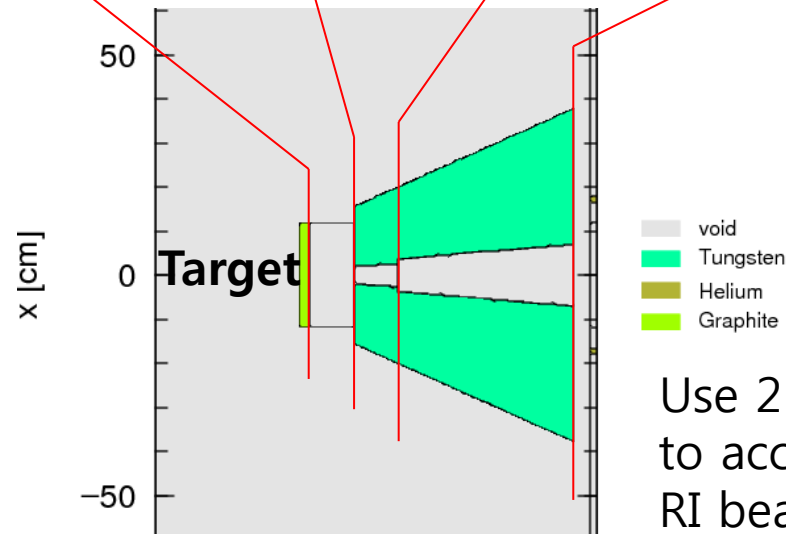
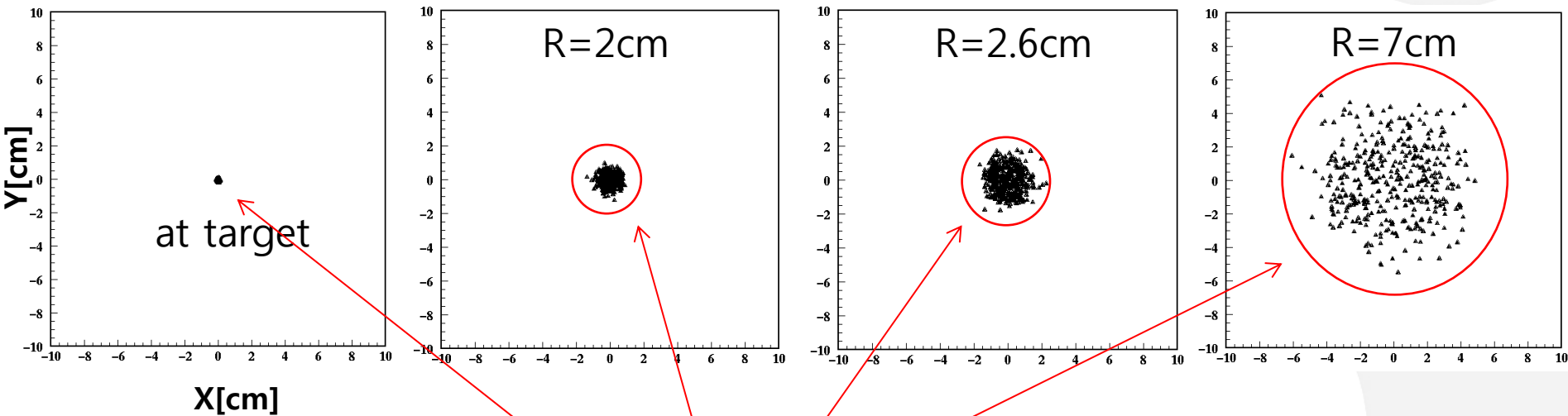
Flux Distribution [1/cm²/second]

at 400 kW

Other
nuclei

Collimator aperture(^{16}O beam for ^{12}N)

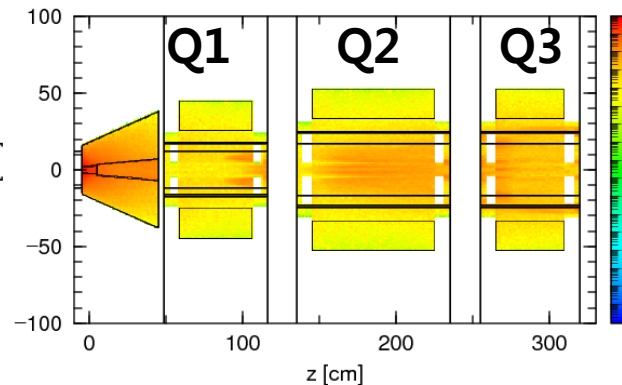
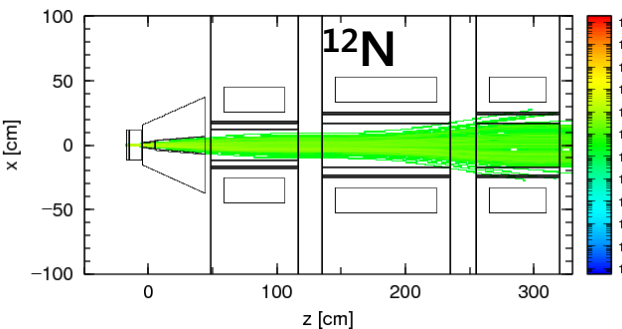
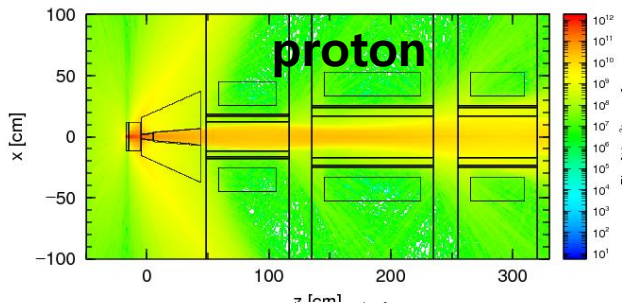
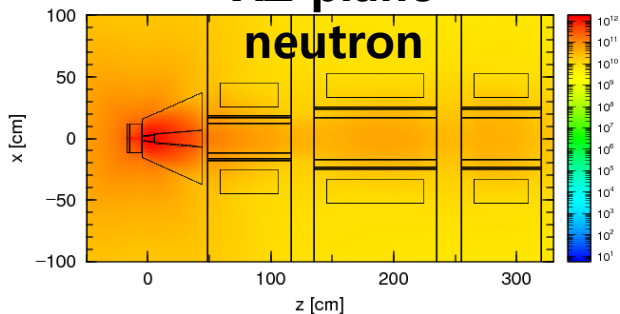
^{12}N distribution



Use 2 step of tapered aperture to accept diverging wanted RI beam

XZ plane

neutron



Target Area

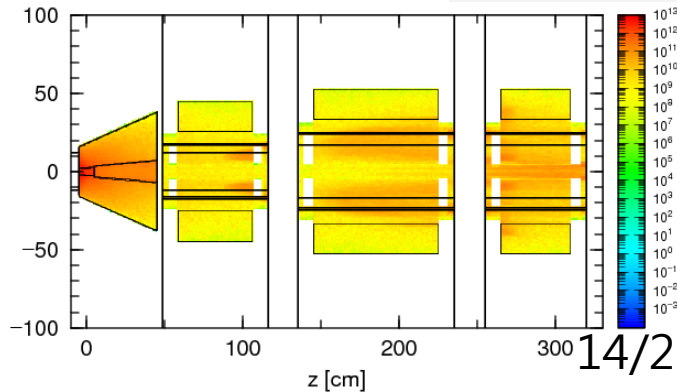
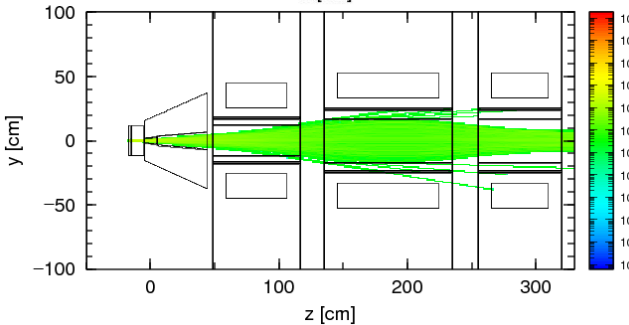
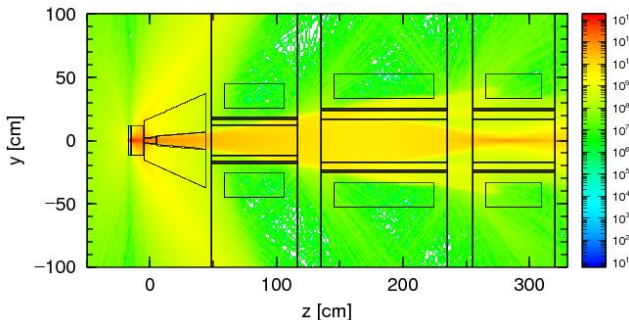
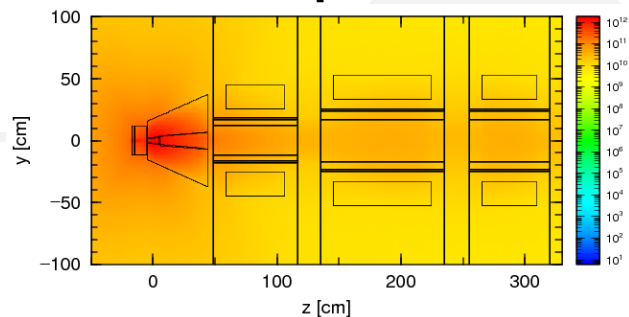
with collimator

**333MeV/u
¹⁶O at 400 kW**

**Flux
Distribution
[1/cm²/second]**

**Heat deposition
Distribution
[MeV/cm³/second]**

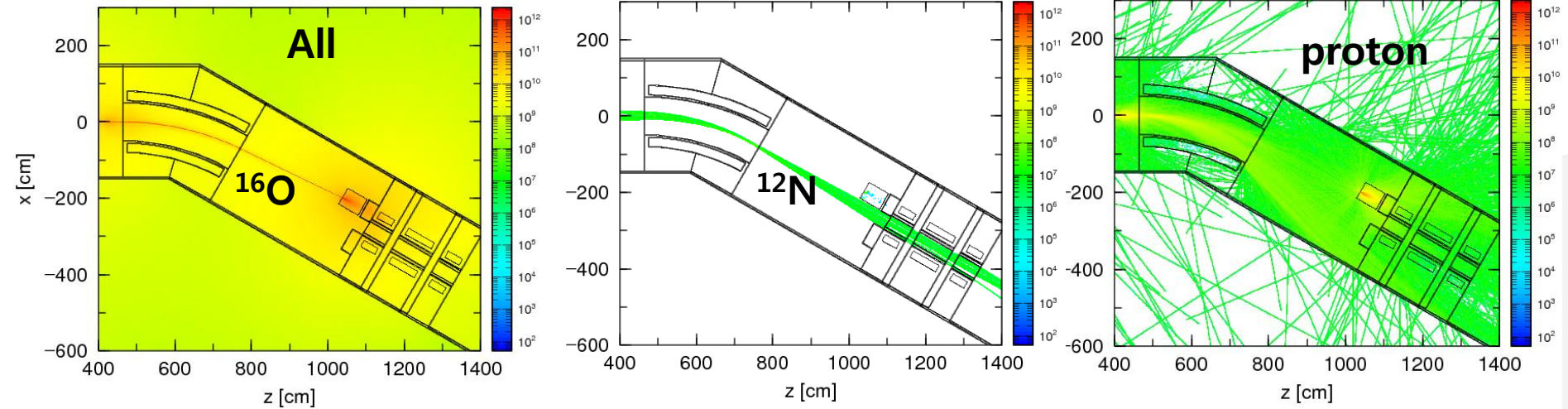
YZ plane



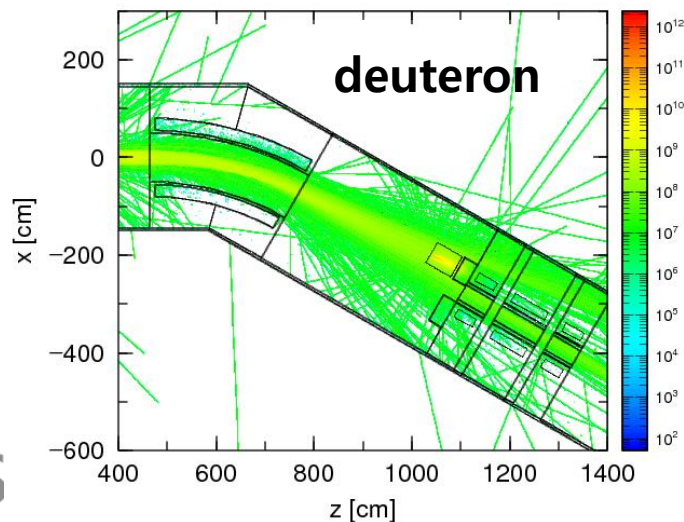
Dipole and Beam Dump area

For 333 MeV/u, ^{16}O
at 400 kW

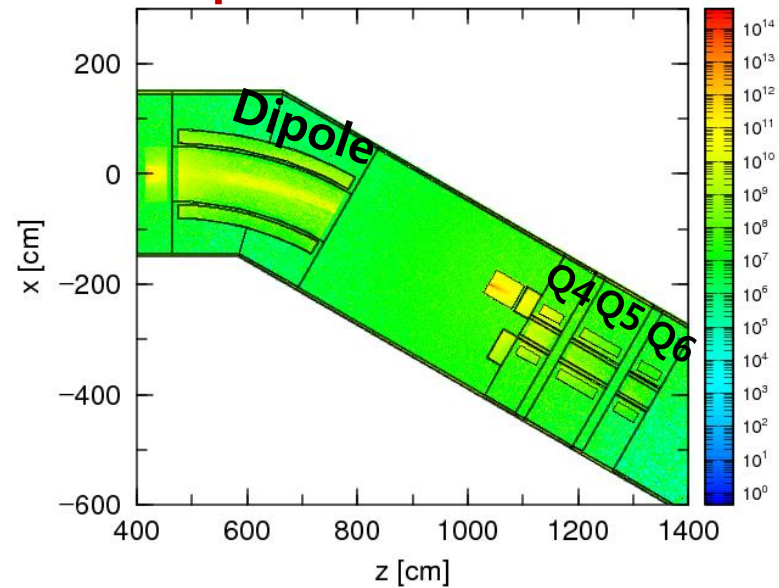
Flux Distribution [1/cm²/second]



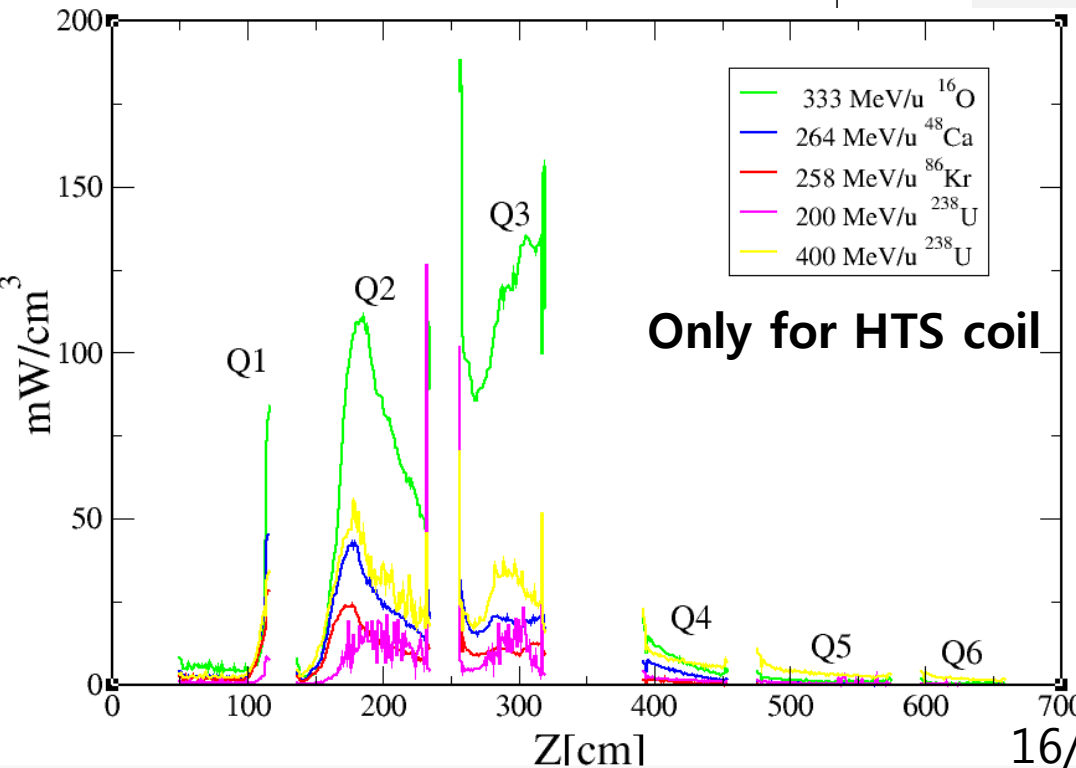
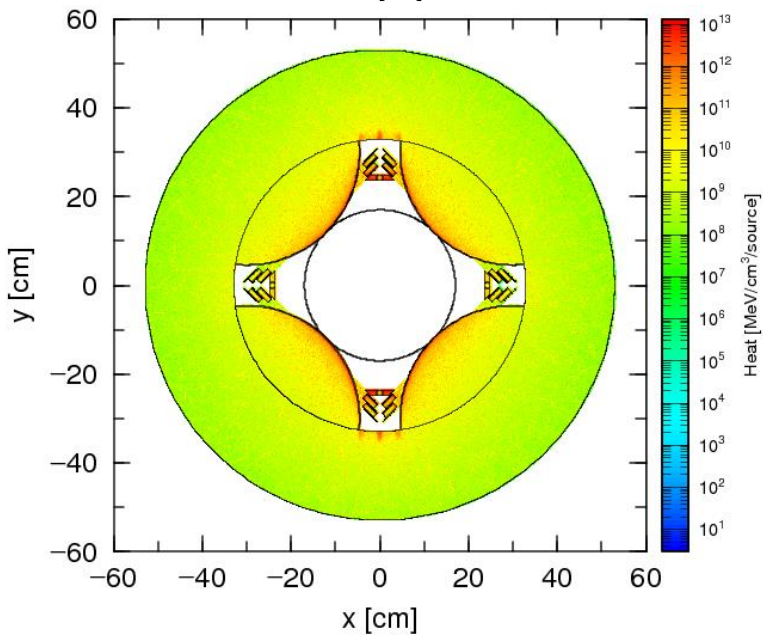
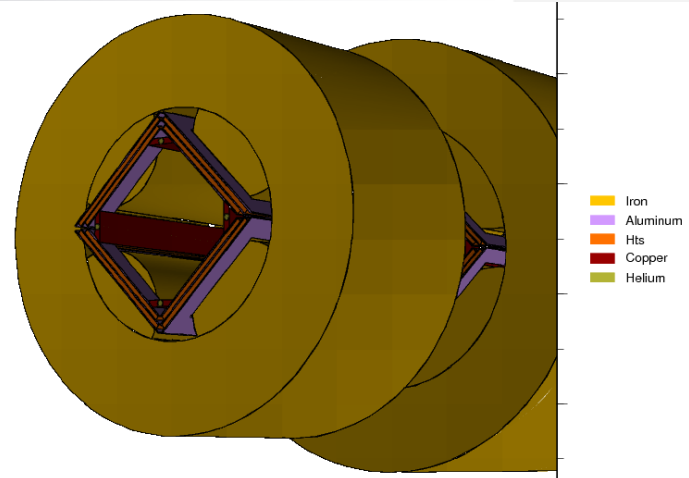
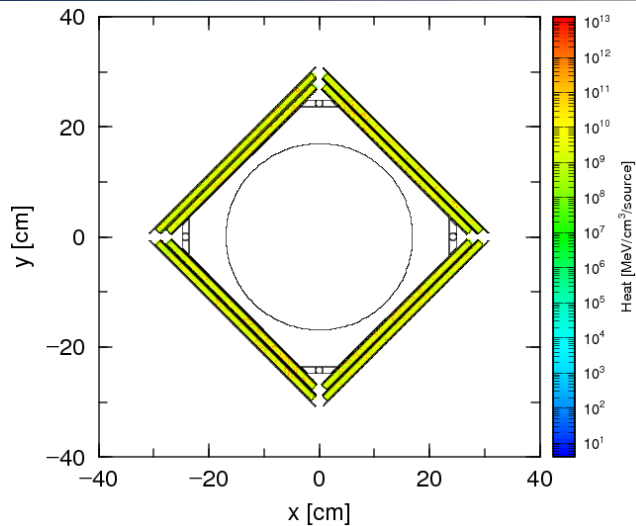
Flux Distribution [1/cm²/second]



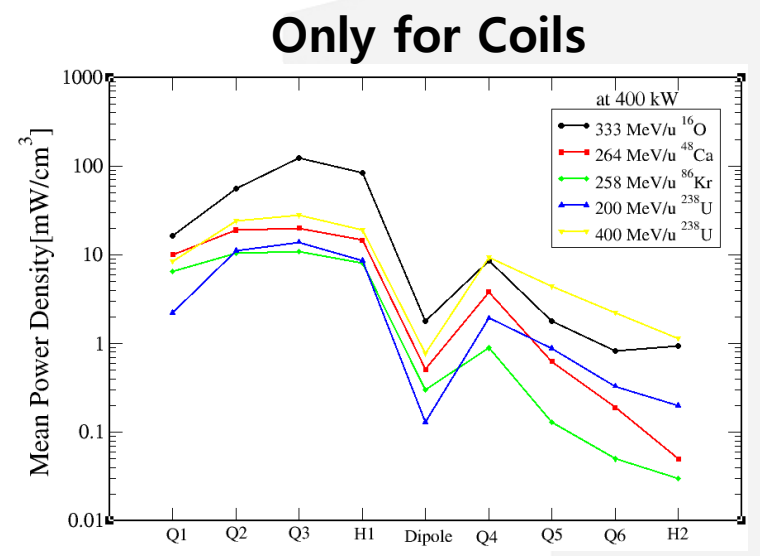
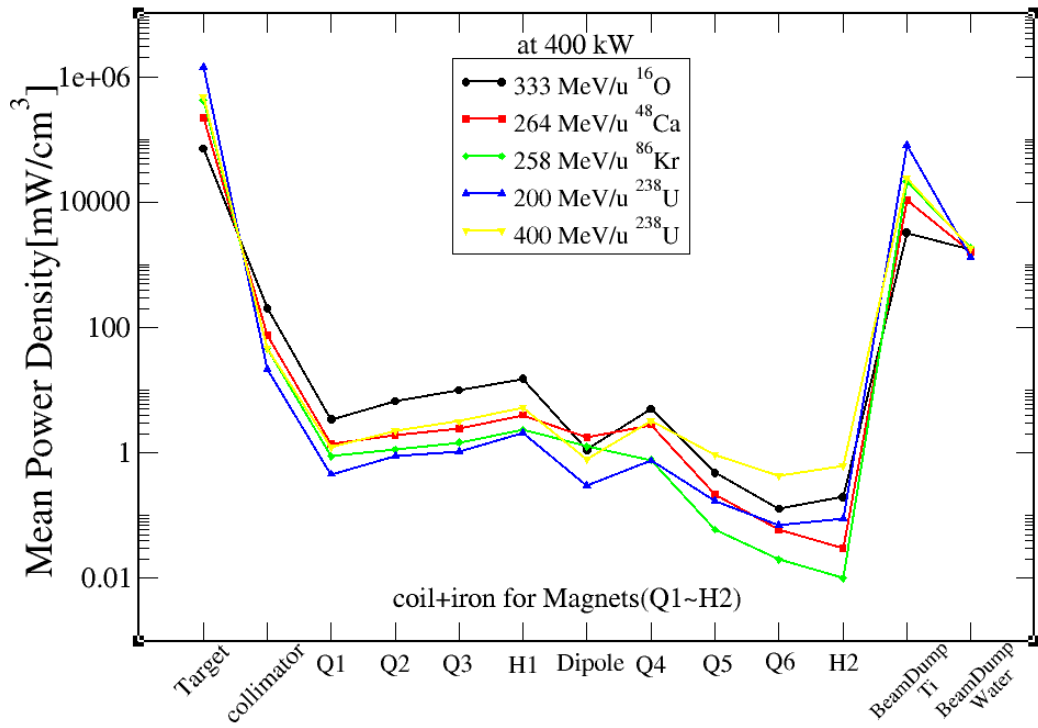
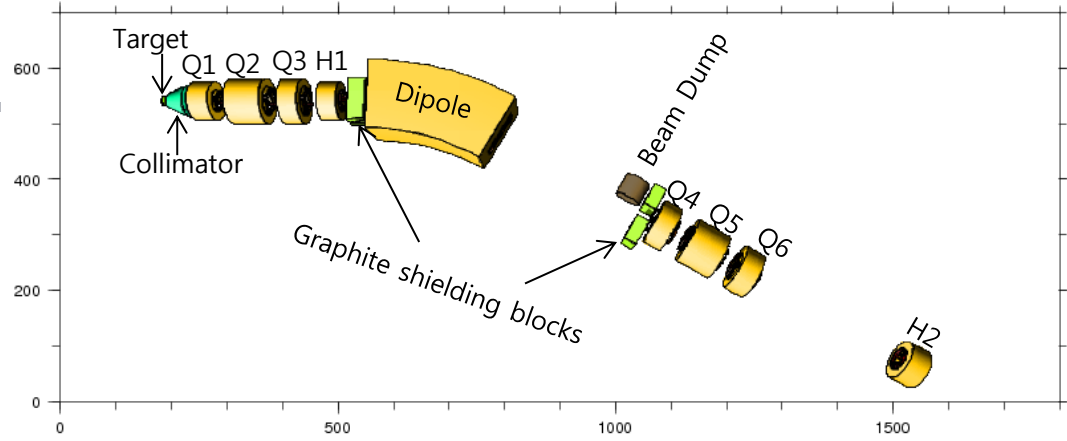
Heat Deposition Distribution [1/cm³/second]



Deposited Heat Distribution and Power Density

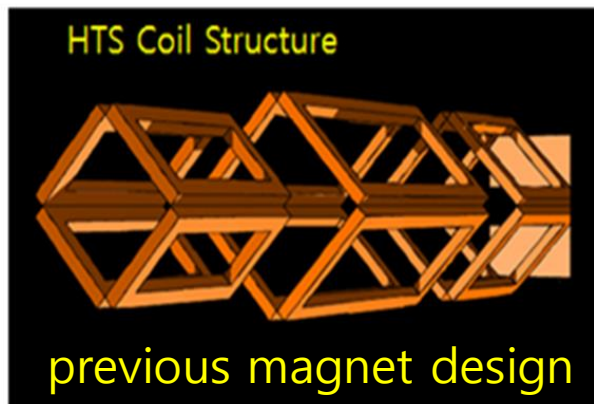
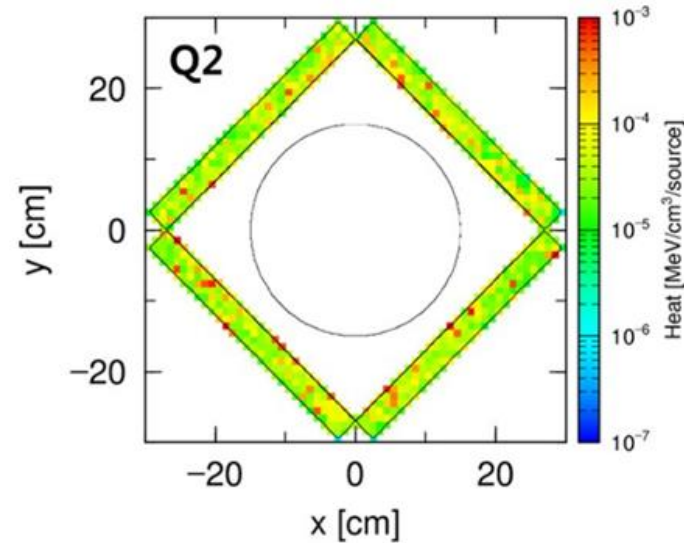
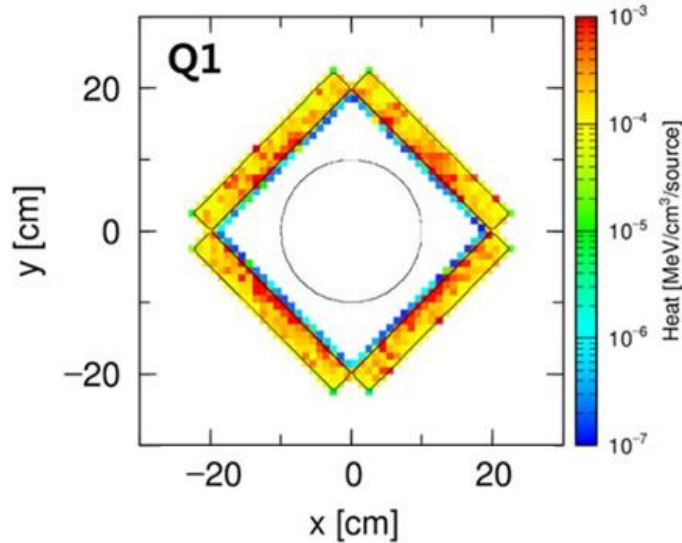


Mean Power Density [mW/cm³]



How to extract Peak power density of HTS coils ?

For 400 kW, 200MeV/u ^{238}U

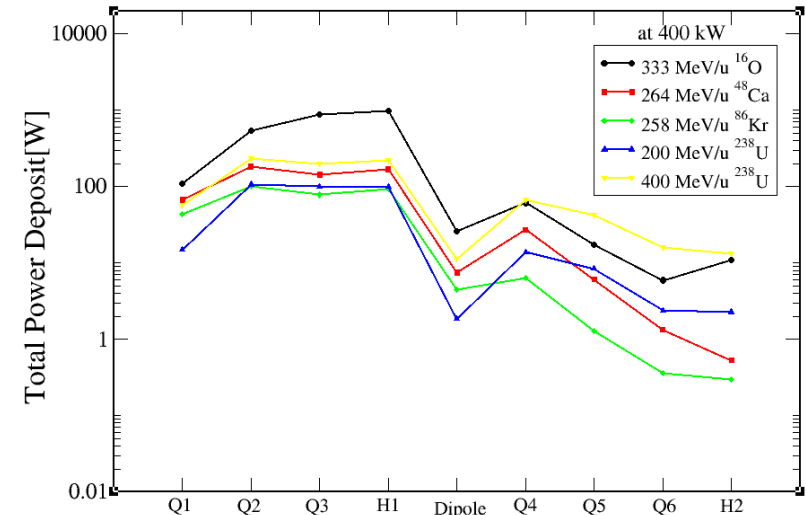
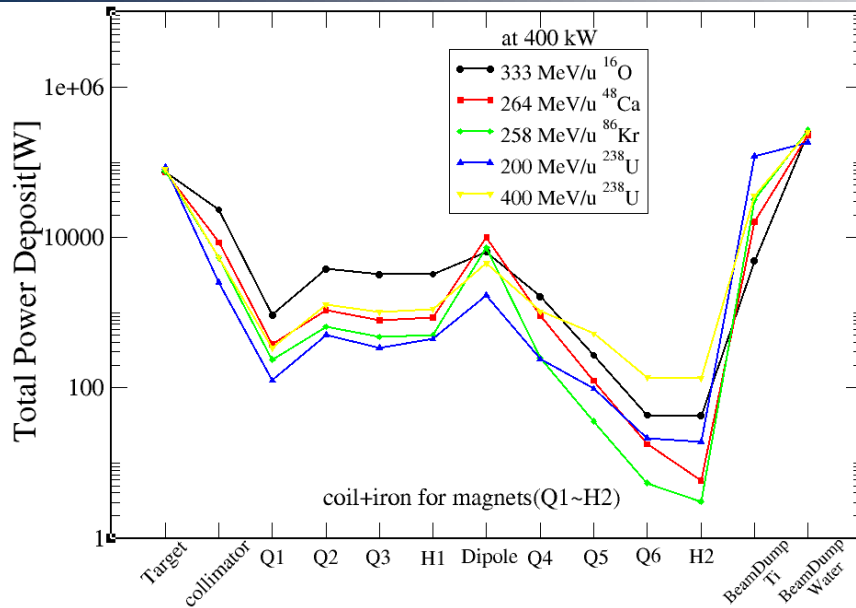


averaging the beam energy in the mesh of 1 cm square in the transverse direction and of 1 cm in the beam direction

Peak power density calculation is ongoing with new design

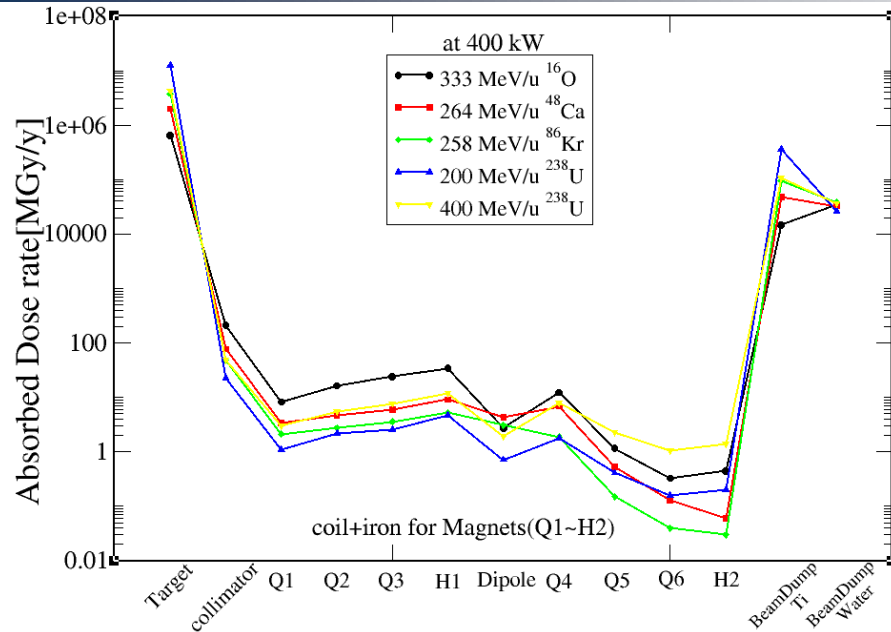
Total Power Deposit[W]

Only for Coils

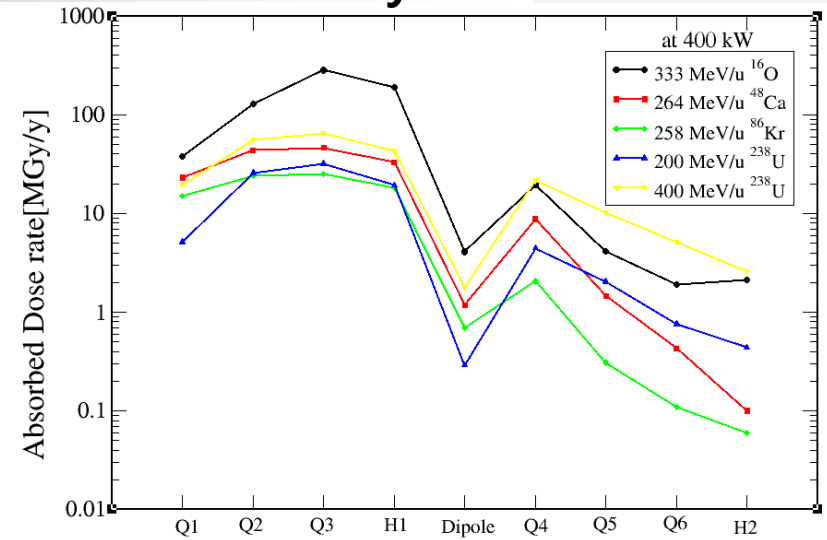


Beam ion	Target [kW]	Collimator [kW]	Coil [kW]	Iron [kW]	Beamdump (Ti+Water)[kW]	Target + Beamdump [kW]
^{16}O	74.26	23.50	2.63	17.06	4.90+ 246.45	325.60
^{48}Ca	75.05	8.65	0.61	13.73	16.21+228.36	319.62
^{86}Kr	76.08	5.34	0.33	9.12	31.68+268.17	375.94
$^{238}\text{U}_{200}$	86.07	2.52	0.35	3.15	119.85+185.13	391.05
$^{238}\text{U}_{400}$	80.45	5.40	0.86	9.29	35.81+ 252.54	368.79

Absorbed Dose Rate[MGy/y]



Only for Coils



HTS Coil Lifetime [y]

Radiation resistance:100MGy
operation time : 5600hrs/year

Magnets	¹⁶ O	⁴⁸ Ca	⁸⁶ Kr	²³⁸ U_200	²³⁸ U_400
Q1	2.6	4.3	6.7	19.5	5.1
Q2	0.8	2.3	4.1	3.9	1.8
Q3	0.4	2.2	4.0	3.1	1.5
Dipole	24.4	84.7	142.9	344.8	56.2
Q4	5.1	11.4	48.5	22.5	4.6
Q5	24.2	68.5	322.6	49.3	9.8
Q6	52.4	232.6	909.1	131.6	19.4

Summary

- Radiation Transport calculation was performed for the components of target and beam dump area of RISP IF separator system using PHITS code
- The production yields of particles and nuclei at the target and their flux distribution and heat deposition on the components are checked for the ^{16}O , ^{48}Ca , ^{86}Kr , 200 MeV/u ^{238}U and 400 MeV/u ^{238}U beams
- Total power deposition for the each component was extracted
- Absorbed dose rate and HTS coil life time were obtained from the mean power density
→ The calculation of peak power density is ongoing.
- In target area, to protect first quadrupole triplet(Q1 ~ Q3) much stronger shielding is needed

**Thank you very much
for your attention!**