

# CW Cryomodule testing at DESY - differences from pulsed tests

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1. Introduction
2. Differences in the test equipment
3. Differences in parameters and in cool-down
4. Complementarity of results
5. Example of the sp and cw/lp test
6. Final remarks

# 1. Introduction

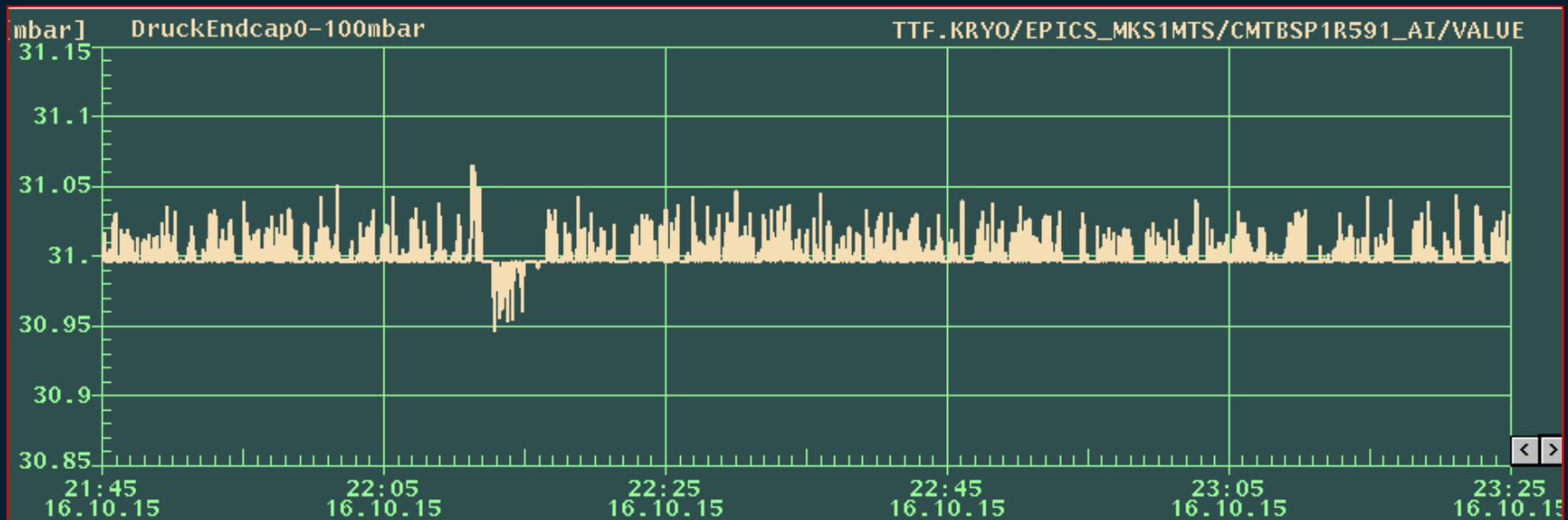
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## General remarks

- ❖ We test E-XFEL CMs (prototypes and production) at CMTB in the cw/lp mode always after they were conditioned and tested in the sp mode.
  
- ❖ The cw/lp operation is mainly:
  - to measure dynamic heat load vs Eacc and/or DF
  - to test performance of the FPC- and HOM couplers for these modes
  - to test performance of the slow and fast tuners for these modes
  - to study and adapt the E-XFEL LLRF for cw/lp operation
  - to study cool-down procedures and their impact on Qo.
  
- ❖ In this presentation, recent (preliminary!) test results for the XM4 cryomodule are used as an example.

# 1. Introduction, cont.

- ❖ Many previous and XM4 cw/lp tests could be conducted without LLRF (RF- and piezo feedback). It was and is possible because:
  - Helium pressure at CMTB is very stable, usually better than  $\pm 50\mu\text{Bar}$ , which cause small  $\Delta f$  of  $\pm 2.5\text{ Hz}$ .



- Microphonics caused by vacuum pumps is has been significantly suppressed by placing the pumps on a foam mat.

## 2. Differences in the test equipment

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	Short pulse	Long pulse	CW
RF-source	10 MW Klystron	105 kW IOT	
Peak Pin/cavity	-> 750 kW	-> 12 kW	
Duty Factor	-> 1.4%	-> 100%	
Rep. rate	10 Hz	usually 1Hz	-
Max. RF-pulse length	1.4 ms	-> cw	

The same RF-distributions system is used for both tubes. The RF-power at CMTB is theoretically “equally” distributed between cavities.

## 2. Differences in the test equipment, cont.

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- ❖ LLRF used for the sp test is a copy of what will be used for the E-XFEL accelerator.

The LLRF used for the cw/lp operation is in an R&D stage.

- The R&D LLRF program has been initiated at DESY to integrate the RF- and piezo feedback, and to compensate the Lorentz Force Detuning at loaded  $Q_s \geq 10^7$ . This seems complicated especially for the lp mode.
- The goal is to reach the sp mode spec for the vector sum stability;  $10^{-4}$  and  $0.01^\circ$  for amplitude and phase respectively.

## 2. Differences in parameters and in cool-down

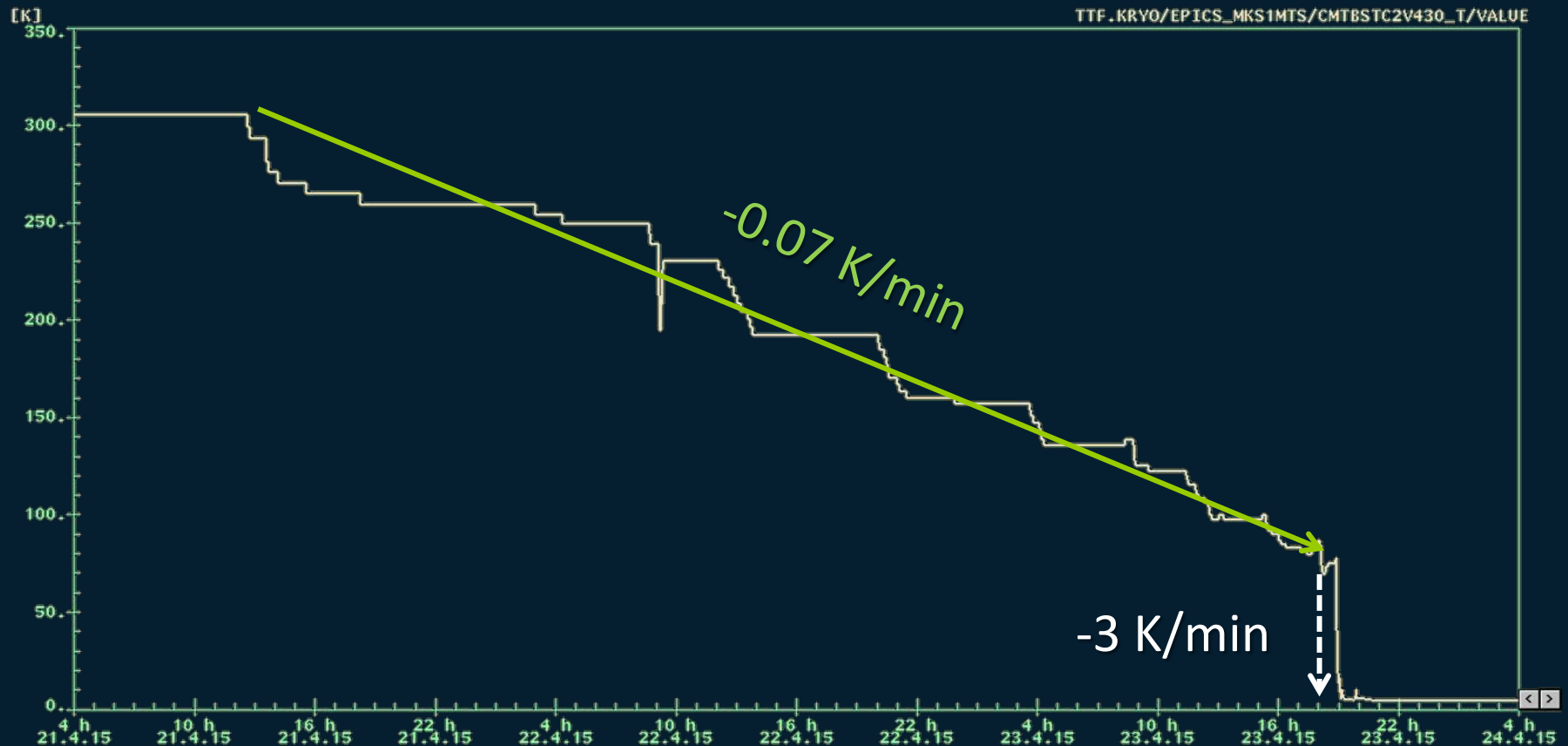
### Loaded Q and T

	Short pulse	Long pulse	CW
$Q_{\text{load}}$	$3.0-4.6 \cdot 10^6$	$1.5 \cdot 10^7$	$1.5 \cdot 10^7$
$\Delta f_{3\text{dB}}$	283 Hz->	87 Hz	87 Hz
Filling time	->750 $\mu\text{s}$	up to 150 ms	-
Flattop	650 $\mu\text{s}$	up to 850 ms	-
Max Eacc	-> 40 MV/m	19 MV/m	15 MV/m
Max LFD	-1600 Hz	-361 Hz	-225 Hz
Temperature	2K	1.8 K and 2 K	

## 2. Differences in parameters and in cool-down

### Cool-down:

- For sp test, we always apply the “fast” cool-down DESY procedure
- For cw/lp tests, we apply first the fast cool-down. Slow cool-down was performed for LG cavities (XM-3) and is planned for XM4.





## 4. Complementarity of the results

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### Short pulse tests

- High available  $P_{in}$  allows for FPCs and cavities conditioning, and to determine max Eacc for every cavity.
- Low  $Q_{load}$  makes sp tests less sensitive to microphonics.
- LFD needs more attention due to high gradients.
- Calorimetric measurements of  $Q_0$  is challenging, because the dynamic cryo-loads are rather small (few watts).

### Long pulse/cw tests

- High  $Q_{load}$  makes tests more sensitive to microphonics (observed in the past).
- Low  $P_{in}$  (few kW), in general, does not cause an electron activity in FPCs nor quenches in cavities. Less radiation.
- Measurements of cryoload gives reasonable results already at low Eacc.

## 5. Example of the sp and cw/lp test

XM4 is the first production cryomodule installed at CMTB for cw/lp test.



*Courtesy D. Kostin)*

It was fast cooled down in May 2015:

- 300 K  $\rightarrow$  80 K with rate - 0.07 K/min
- 80 K  $\rightarrow$  4.2 K with rate - 3 K/min

## 5. Example of the sp and cw/lp test

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XM4, cont.

- It houses 8 TESLA cavities made of polycrystalline Nb.
- All HOM couplers are equipped with high conduction feedthroughs.
- During tests at AMTF in 2014, four FPCs (Cav# 1, 2, 3, 4) were heavily overheated and burned. This happened due to improper assembly of inner conductors of warm parts . All 4 warm parts have been exchanged.
- Two HOM couplers have detuned filters:

Cav#1 HOM2  $Q_{\text{ext}} = 6.9\text{E}10$

Cav#2 HOM1  $Q_{\text{ext}} = 1.4\text{E}10 !!$

## 5. Example of the sp and cw/lp test

### Short pulse test (D. Kostin)

cavity	FE onset [MV/m]	$X > 10^{-2}$ [MV/m]	$E_{acc,max}$ [MV/m]	$P_{in,max}$ [kW]	$X_{max,G}$ [mGy/min]	$X_{max,D}$ [mGy/min]	Limit	$E_{oper}$ [MV/m]	Op.Limit
1.CAV00626	33.5	33.5	33.5	420	0.3	$10^{-5}$	BD_FE	31.0	PWR
2.CAV00607	32.0	34.8	34.8	530	0.01	$10^{-5}$	BD_FE	31.0	PWR
3.CAV00556	23.0	—	31.1	390	0.007	$10^{-5}$	BD_FE	30.6	BD
4.CAV00597	23.0	29.9	34.5	470	0.09	$5 \times 10^{-4}$	BD_FE	29.9	XRAY
5.CAV00606	36.5	—	39.0	685	0.002	$2 \times 10^{-5}$	BD_FE	31.0	PWR
6.CAV00621	—	—	24.4	220	—	—	BD	23.9	BD
7.CAV00592	—	—	22.0	180	—	—	BD	21.5	BD
8.CAV00594	30.0	—	35.1	480	$4 \times 10^{-4}$	$4 \times 10^{-4}$	BD_FE	31	PWR

- Cav#1  $P_{HOM2} = 17 \text{ W}$  at  $E_{acc} = 33.5 \text{ MV/m}$ , Cav#2  $P_{HOM1} = 90 \text{ W}$  at  $E_{acc} = 34.8 \text{ MV/m}$ , which for DF of ca. 1% does not lead to thermal issue in the cable, but may cause a discharge in connectors.
- The lowest X-ray onset is at 23 MV/m. The lowest quench gradient is at 22 MV/m.

## 5. Example of the sp and cw/lp test

### Short pulse test, cont.

2 K	static	dynamic		comment
$\langle E_{\text{acc}} \rangle$ [MV/m]		15	20.5	
Cryo-losses [W]	8 ÷ 9	1.01	2.02	all 8 cavities tuned
$Q_0$		$2.4 \times 10^{10}$	$2.3 \times 10^{10}$	



$Q_0$  seems high (small heat load)

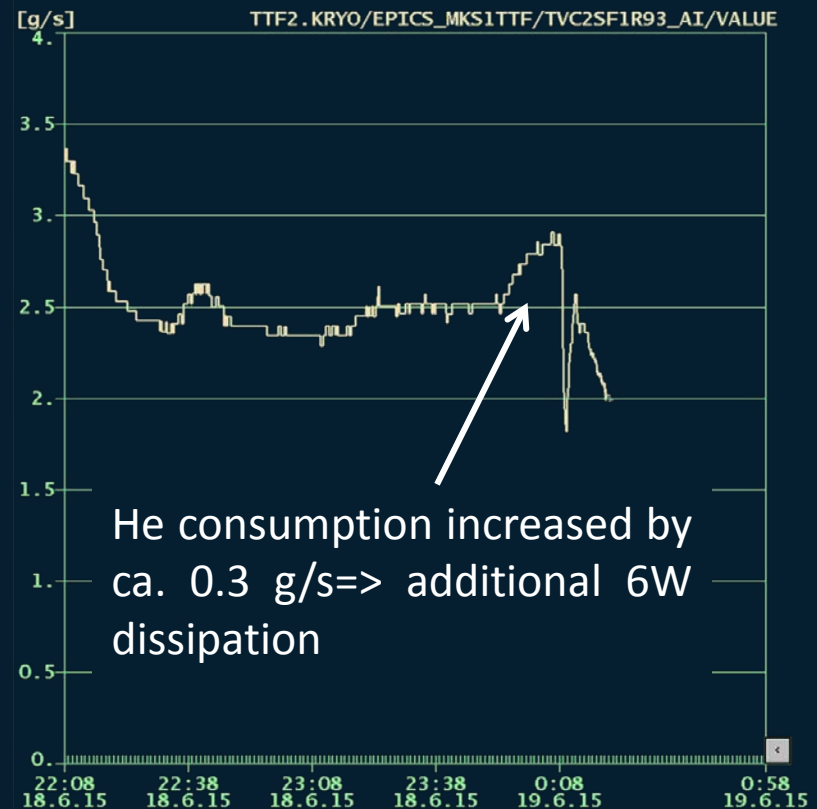
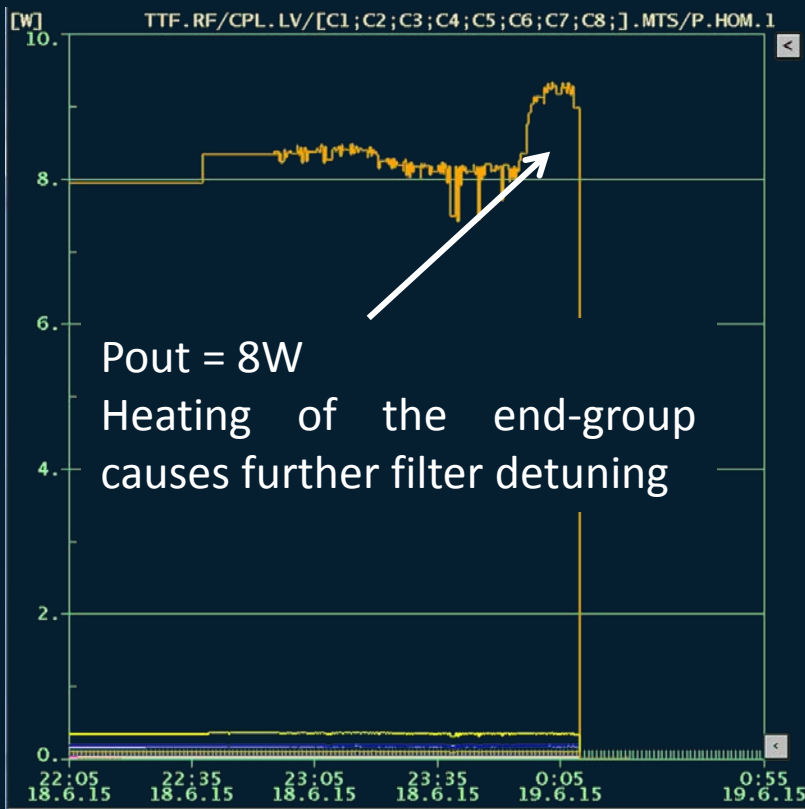
These values do not match the vertical test values, which are lower.

## 5. Example of the sp and cw/lp test

### cw/lp test

#### I. Thermal issues, not detected in the sp test

- Heating of the HOM1 coupler of cavity 2.  
Cav#2 can operate stable cw up to 8 MV/m. Heating of the end group at 11+MV/m:

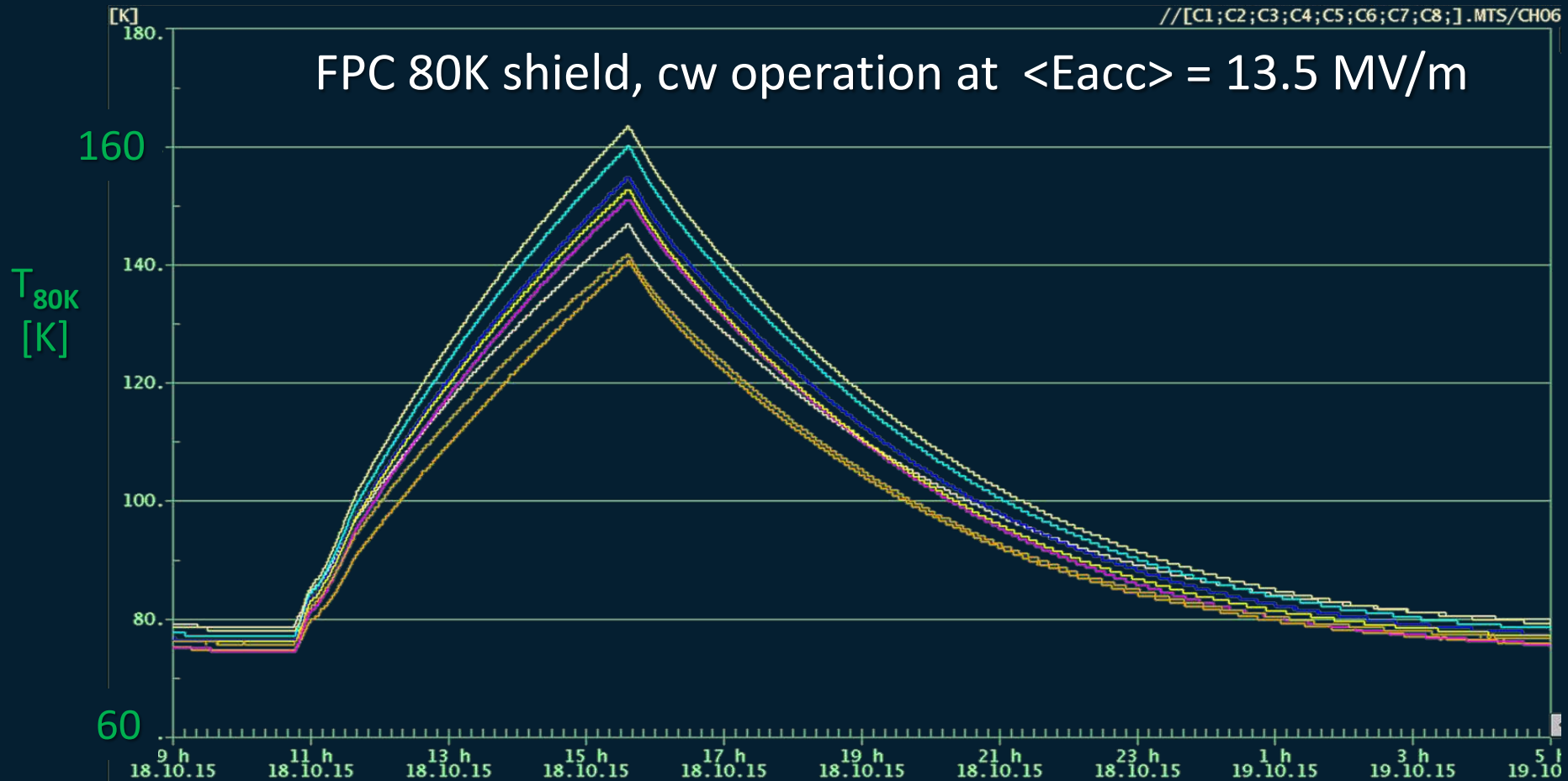


## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

## II. Thermal issues, not detected in the sp test

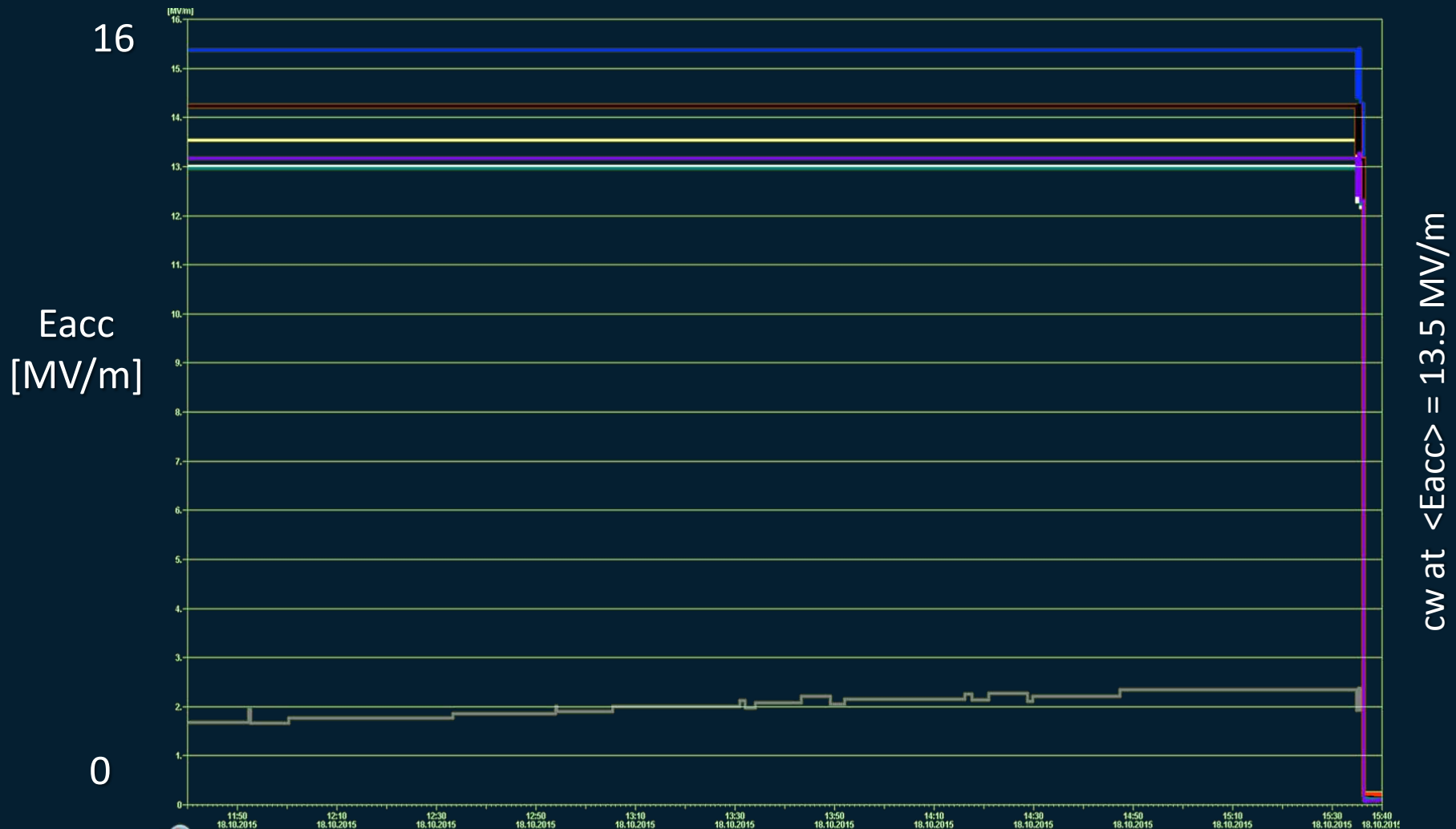
- Heating of FPCs causing change of  $Q_{load}$ . It is a very slow thermal process:



## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

- Over more than 4 hours Eacc stays constant

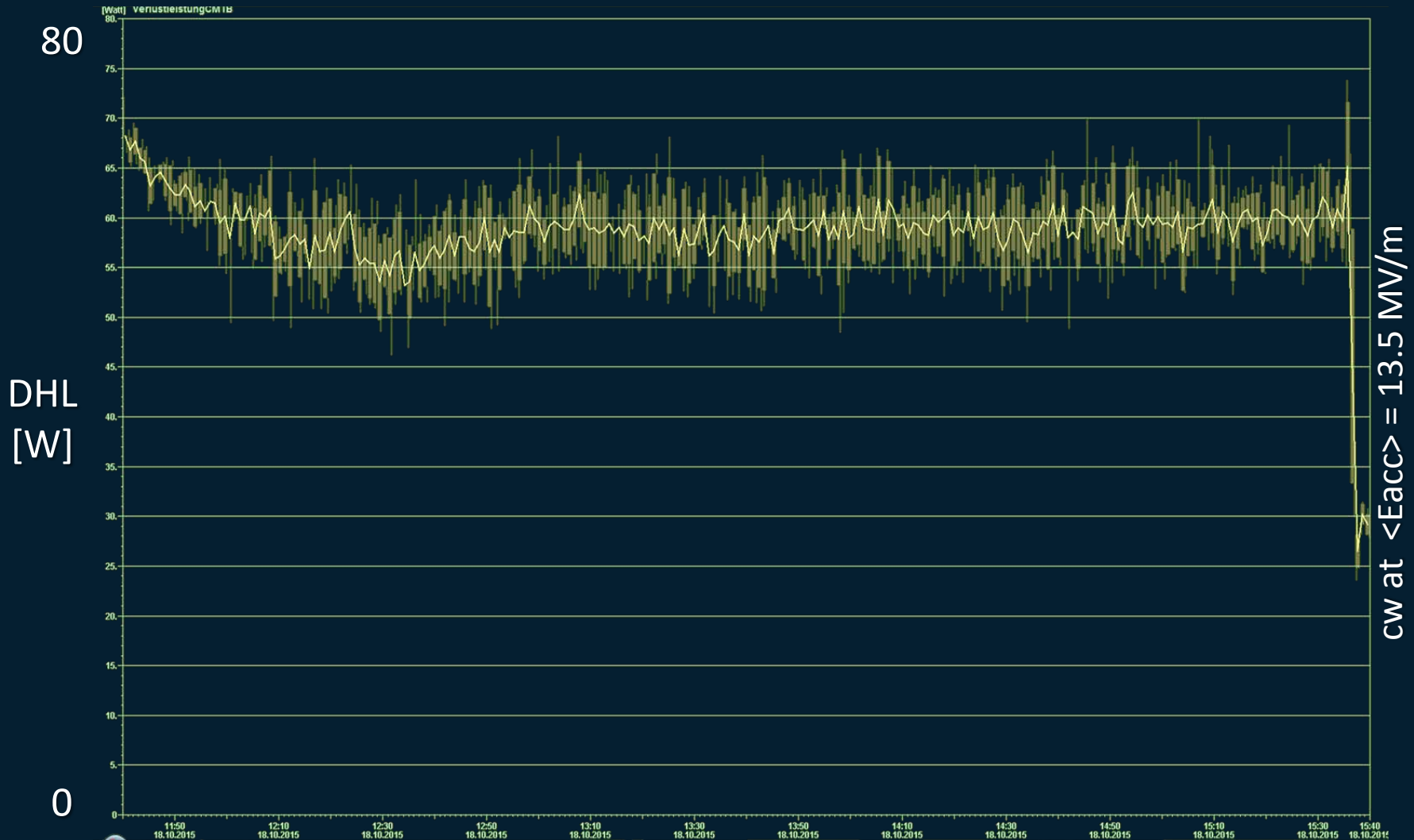




## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

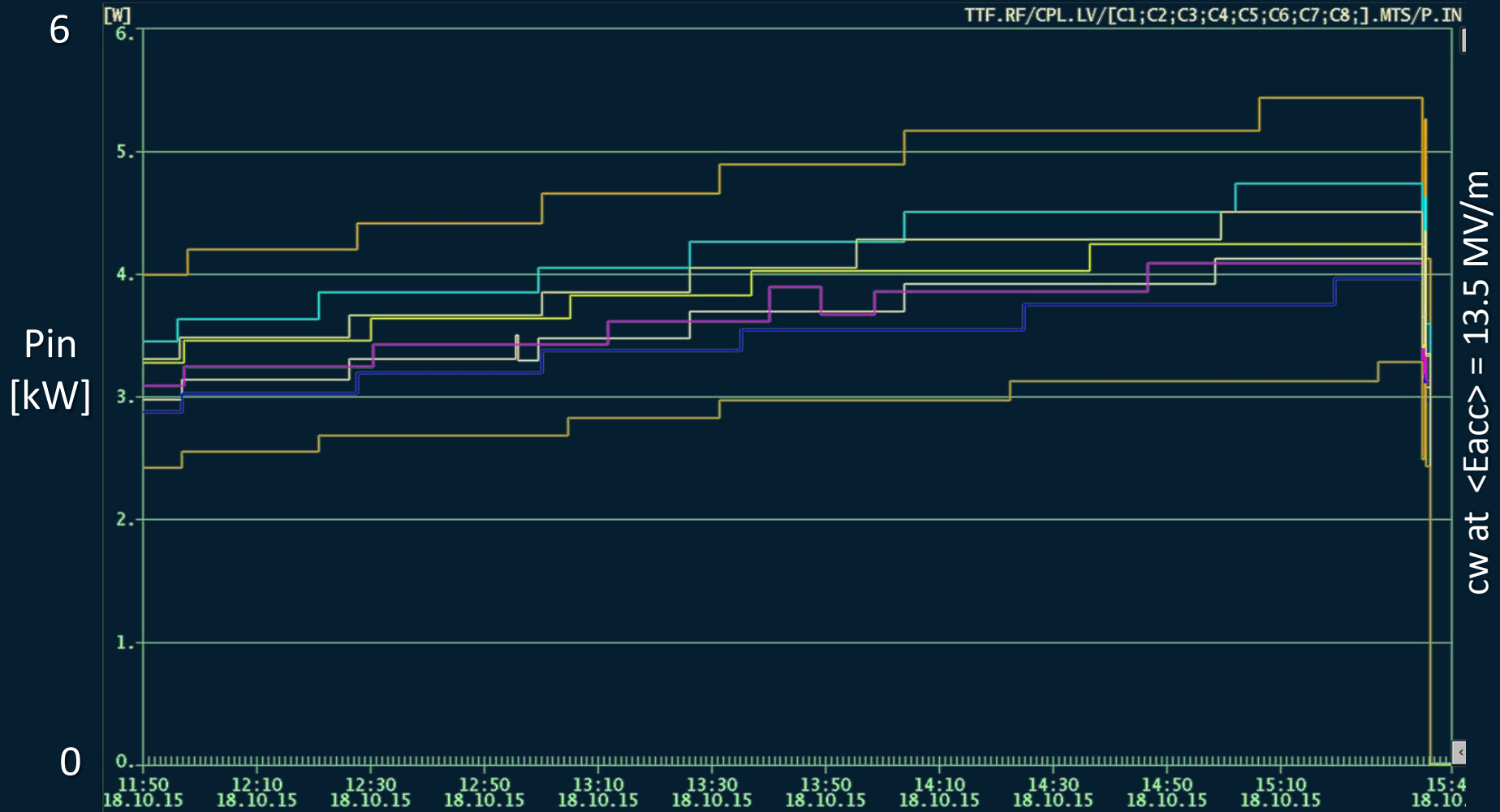
- Dynamic Heat Load (DHL) stays constant



## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

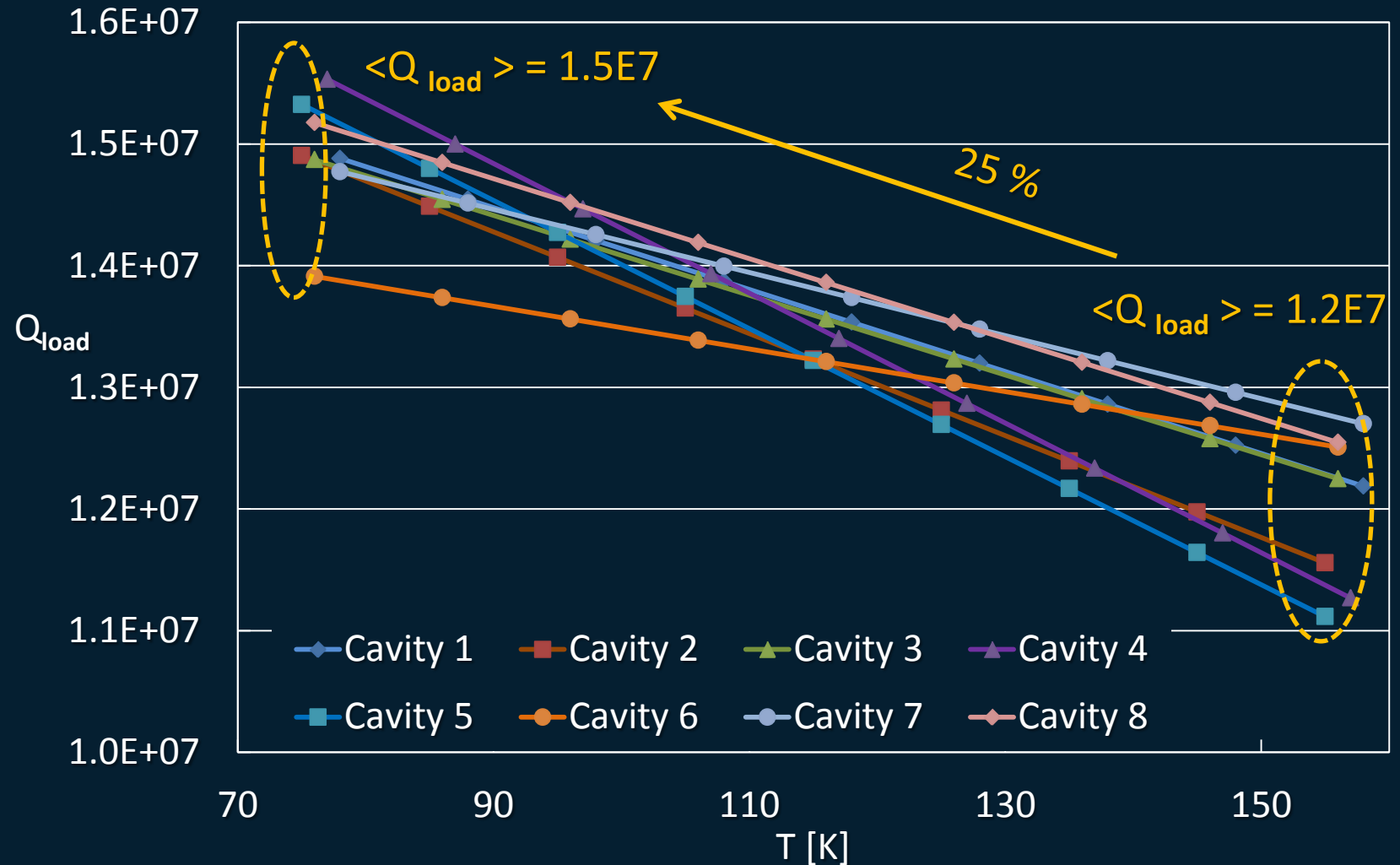
- The input power  $P_{in}$  increased significantly (by ca. 30%) during the 4h test:



## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

- Linear approximation of the measured  $Q_{\text{load}}$  vs  $T_{80\text{K}}$



## 5. Example of the sp and cw/lp test

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### cw/lp test, cont.

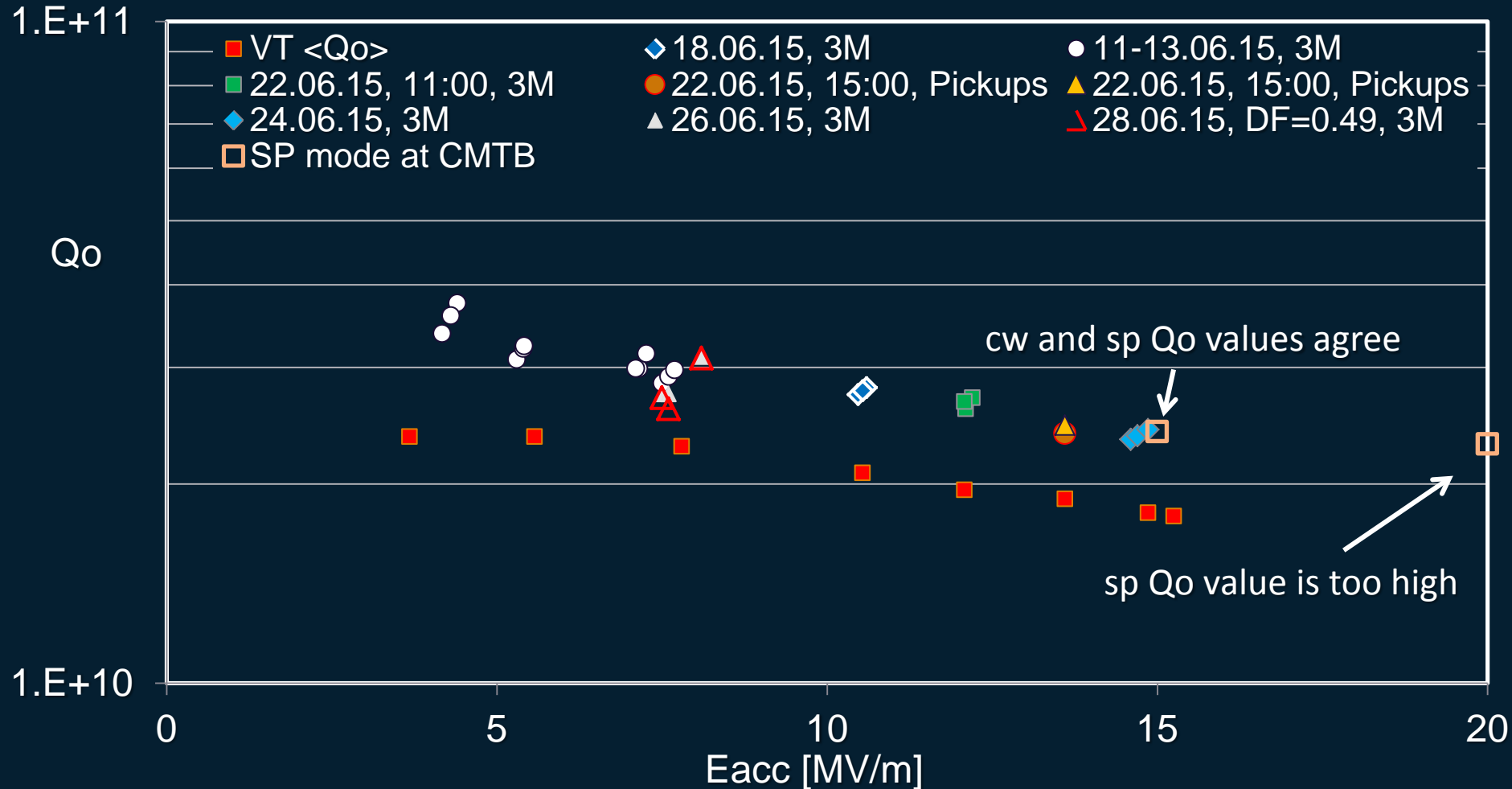
#### III. Qo test; general remarks

- For the cw/lp operation, measured DHL is significantly larger than the DHL measured in sp mode, for which the DF is  $\sim 1\%$ .
- In general, the accuracy of the calorimetric measured DHL is better for large DHL.
- In most runs 3 methods were used to determine  $E_{acc}$  (to minimize an error):
  - a. Read out of pickups which were calibrated for the sp mode.
  - b.  $P_{in}$  for each cavity (the directivity of the waveguide couplers is crucial).
  - c. IOT output power ( $P_{IOT} * 0.95/8$ ).
- We calibrated with the end-cup heater the DHL measurement. The calibration has confirmed values measured when RF was on.

## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

#### Qo vs. Eacc

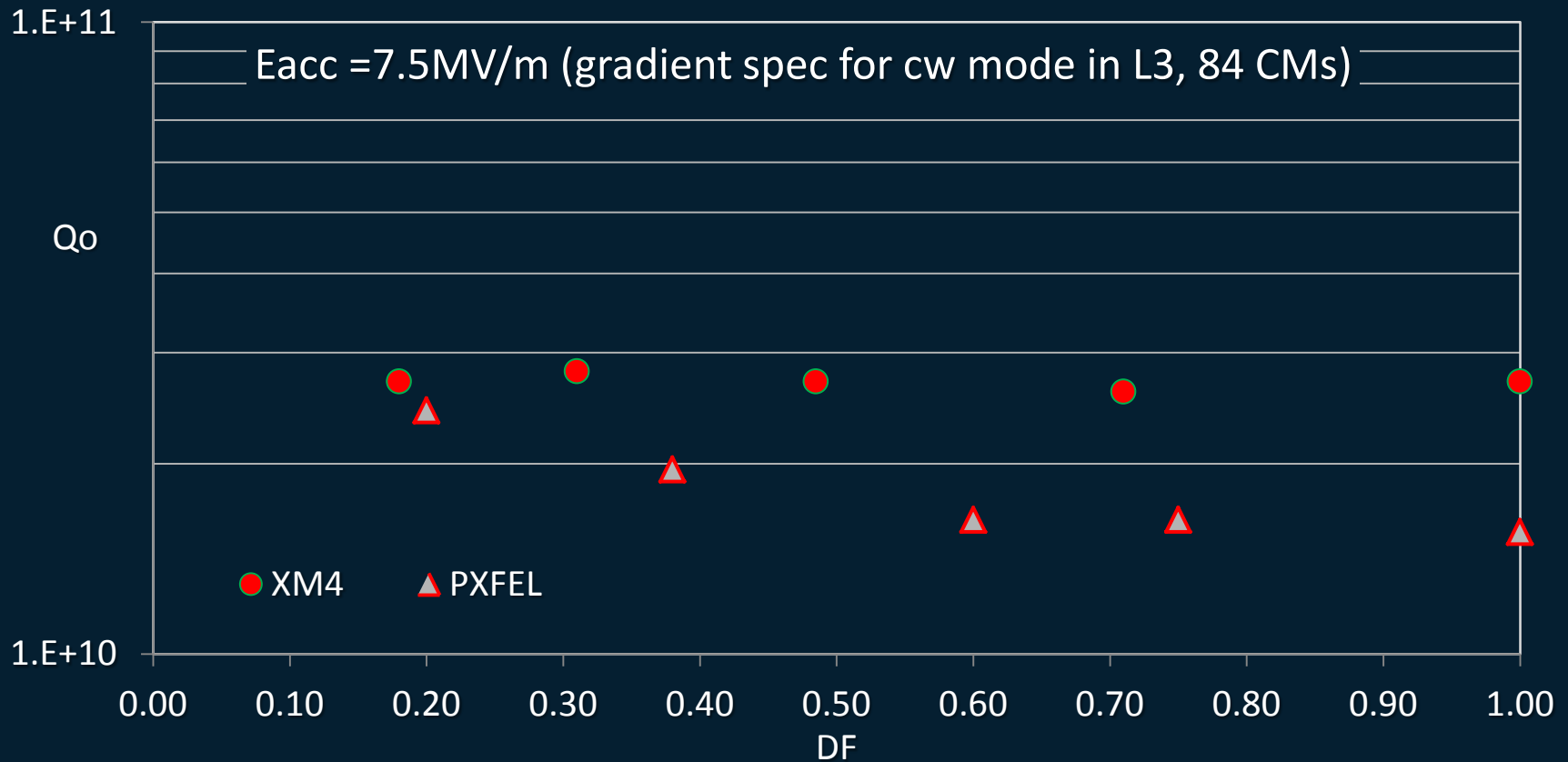


## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

#### IV. Indication of the end group heating

- Production E-XFEL CMs do not have temperature sensors on HOM couplers.
- Test of the  $Q_0$  vs DF can help to “detect” heating of end groups (a cavity or CM):

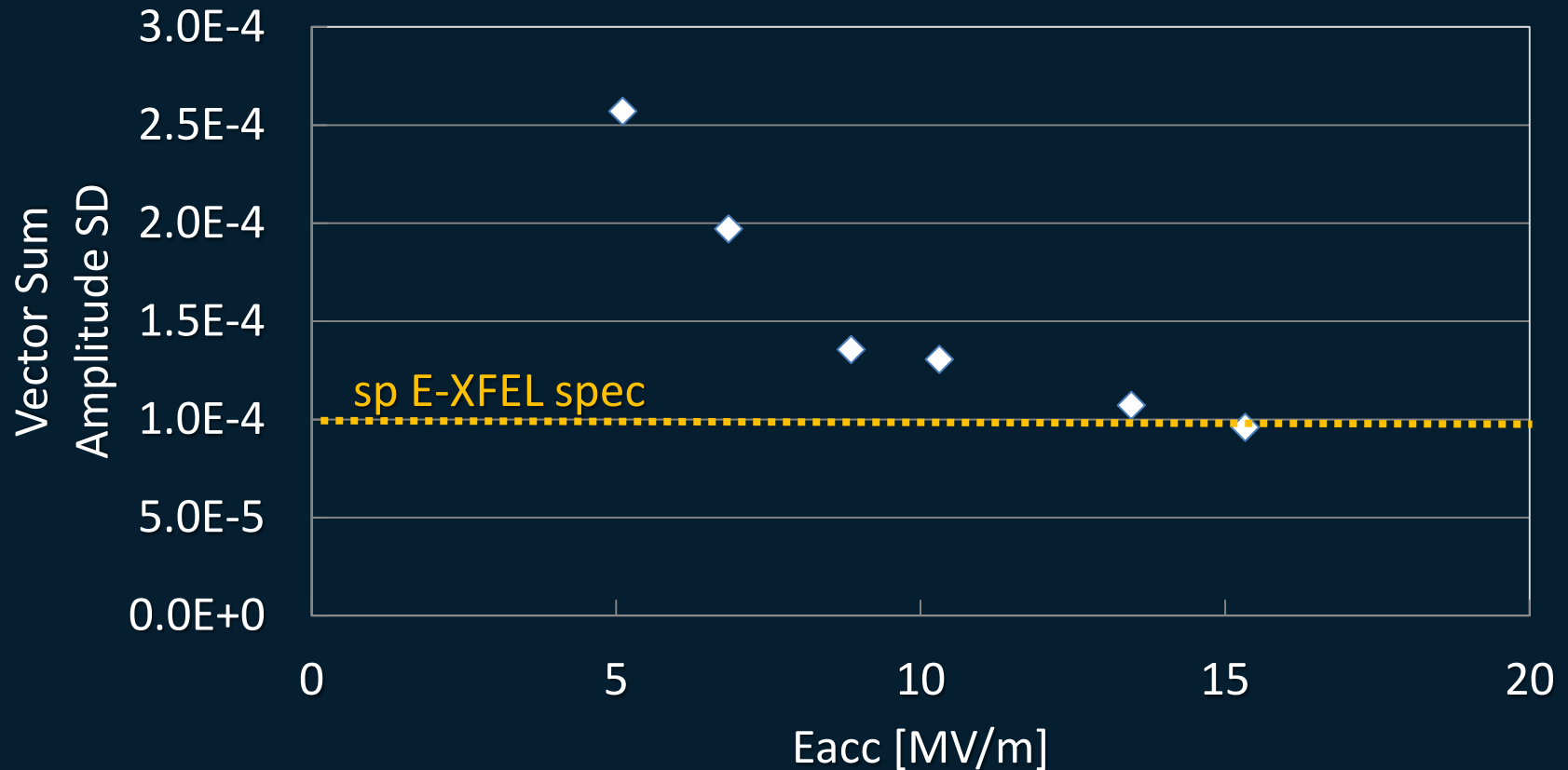


## 5. Example of the sp and cw/lp test

### cw/lp test, cont.

#### V. VS amplitude stability vs Eacc for $Q_{load}$ of $1.5E7$ (cw mode)

The VS amplitude stability in cw mode has been demonstrated. In this test the RF-feedback, Piezo-bias and Integral part of the piezo-feedback were on.



## 6. Final remarks

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1. SP and cw/lp tests are complementary and give together more complete picture of a CM performance.
2. E-XFEL CMs are first conditioned and tested with high peak power klystron in SP nominal mode and then thermally conditioned and tested with 105kW IOT in the cw/lp mode.
3. We have observed two thermal issues when a CM operates in cw mode, which may constrain the cw operation of an accelerator:
  - a. Heating of FPCs causing  $Q_{load}$  drop, which in turn causes that the LLRF rises the input power to keep the gradient, and thus increases the heating. The process can be stopped by remotely adjustable  $Q_{load}$  or with “pre-heating” of the FPCs. The latter will need some hours to stabilize thermally the system, after the input power was changed to match new setting e.g. beam current or Eacc.



## 6. Final remarks, cont.

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- b. End-group heating caused by HOM coupler which rejection filter is not properly tuned. This can limit the operational gradient of a cavity.
4. Dark current? There is a progress on these measurements. Nick Walker is helping to get the sp AMTF data calibrated. Once the AMTF system will be calibrated, we will install one at CMTB. The remaining open question is the phasing of cavities for the dark current measurement.
5. The statistics DESY has for cw/lp tests is still rather poor, especially for the production CMs, but for the E-XFEL cavities the statistics is 8 times better, so observed phenomena and performance of cavities are more sound.

## Acknowledgments

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I want to express my gratitude to all Colleagues supporting and contributing to the cw/lp experiments:

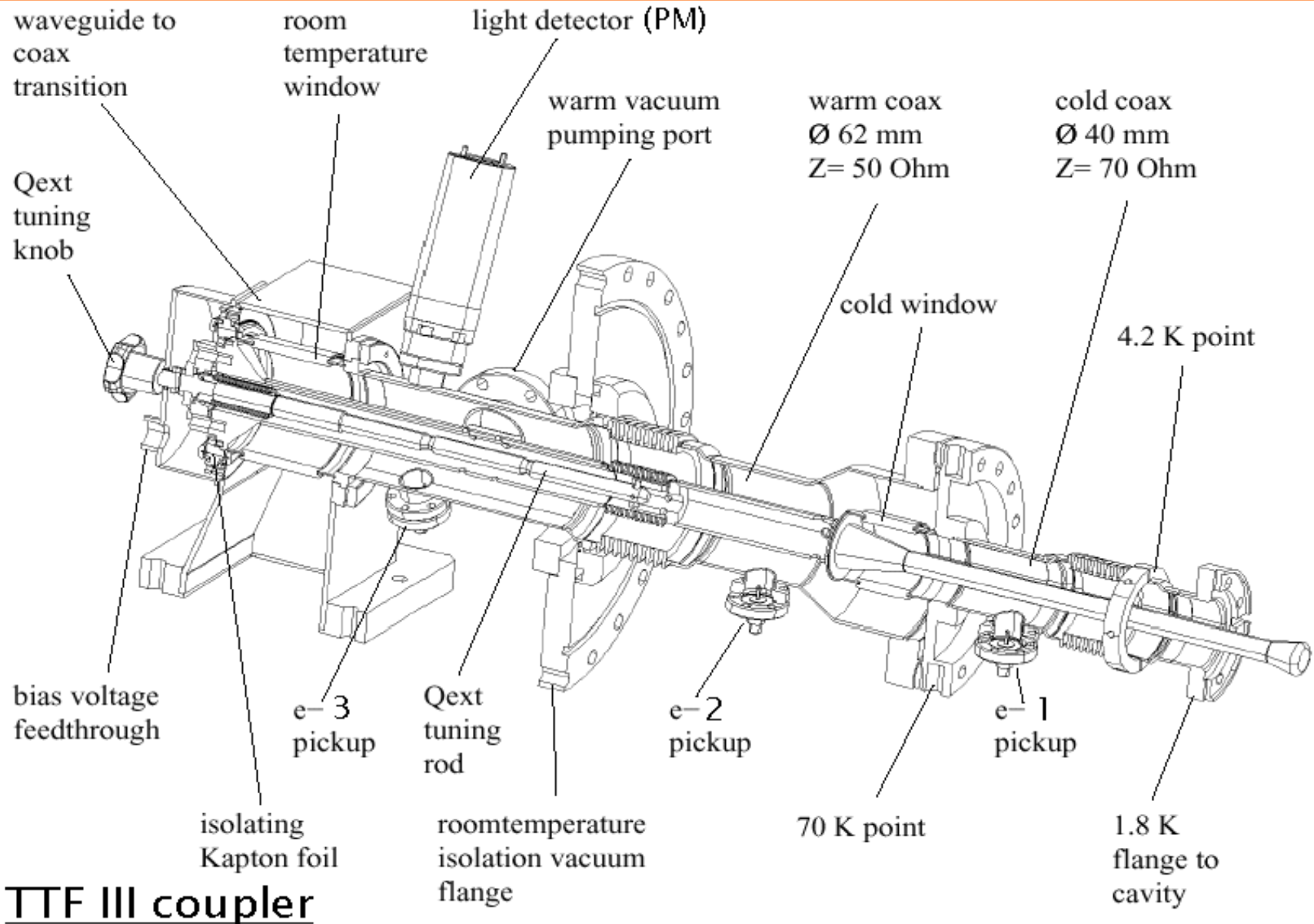
DESY: V. Ayvazyan, J. Branlard, T. Büttner, M. Ebert, J. Eschke, T. Feldmann, A. Gössel, D. Klinke, D. Kostin, L. Lilje, F. Mittag, W. Merz, W.-D. Möller, C. Müller, R. Onken, B. Petersen, D. Reschke, R. Rybaniec, I. Sandvoss, A. Sulimov and R. Brinkmann and H. Weise

TUL: W. Cichalewski, A. Piotrowski, K. Przygoda

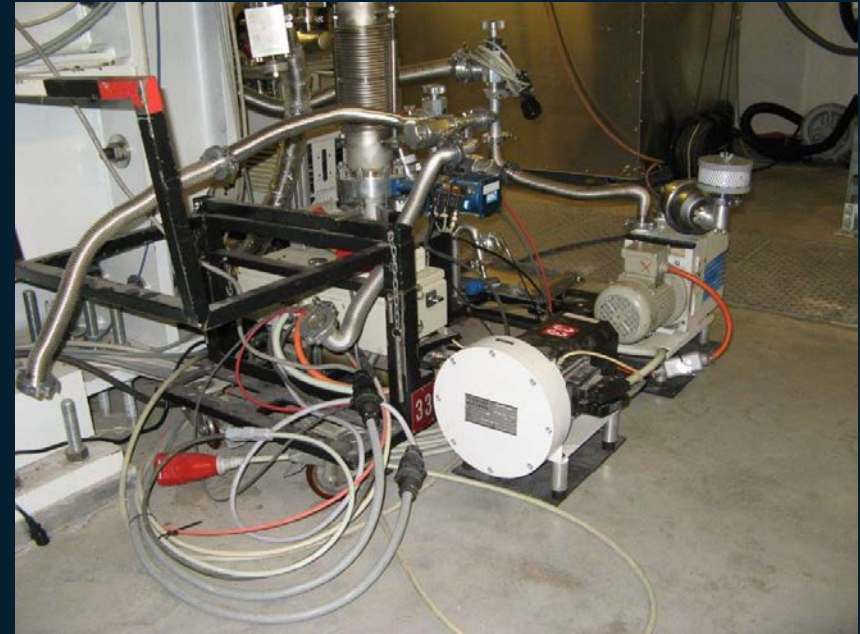
WUT: K. Czuba

IFJ-PAN: S. Myalski, M. Sienkiewicz, M. Wiencek

Thank you for your attention



# Backup: gradients for stability test 16/17.10.2015 (pumps)



# Backup: LP shape

## CW/LP operation

**SP**

RFGate  ON      FF enable  ON

Amplitude SP  MV

Phase SP  deg

**Pulse phases duration in % of 1s**

Delay  %

Filling  %

Flat-top  %

**RF FeedBack**      FeedBack gain

ON

**Piezo BW**

ON     

Piezo FB  OFF

Expert Piezo

Piezo plots

Detuning (model)

Probes

Forward

Reflected

FF A/P

GP I/Q

ERR I/Q

OUT A/P

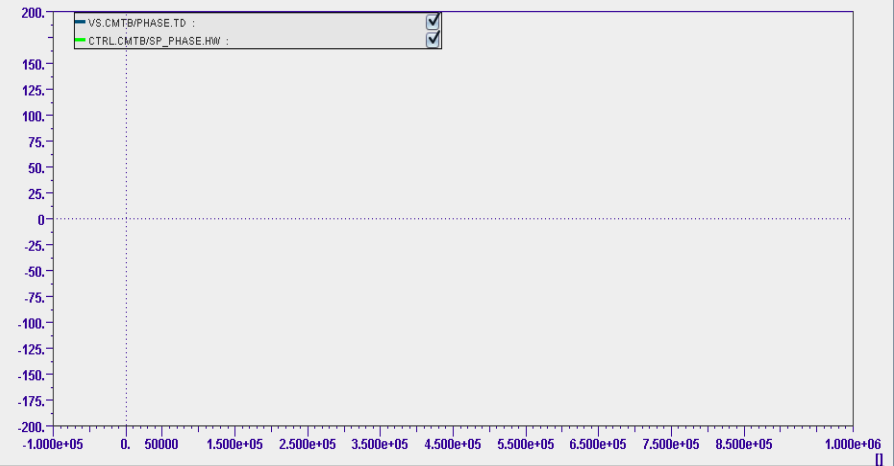
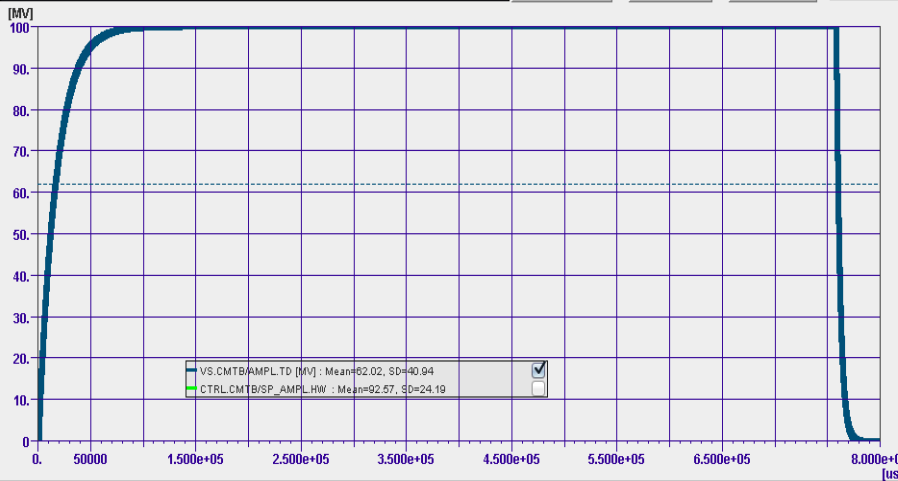
VM A/P

HPC

VS I/Q

VSSP A/P

	Piezo FF (DC bias) [V]	Status	Gain P	Gain I	FB	Relay
C1	ON + 3.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	0
C2	ON +14.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	0
C3	ON + 9.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	1
C4	ON - 4.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	0
C5	ON -13.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	0
C6	ON + 9.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	0
C7	ON + 9.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	0
C8	ON +15.00 H	ENABLED	+ 0 + 0	+ 0 + 0	OFF	0



	C1	C2	C3	C4	C5	C6	C7	C8	Module cryo loss	timing	Motors
FOR power [kW]	1.956	1.874	1.77	2.468	2.151	1.905	2.375	1.862	18.92		
Gradient [MV/m]	10.41	10.01	10.03	11.79	10.77	9.78	10.40	9.78			