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HTS Vibration Experience – Sources & Mitigation

Jeremiah Holzbauer Resonance Control Group - Technical Division October 8th, 2015 Microphonics Workshop

Synopsis

- Resonance Control Group has conducted several rounds of testing at HTS and discovered a quite sizable amount of microphonics disturbance
 - Notable sidebands at 30, 50 Hz and harmonics
- Larry D. and Brian C. attempted to control the cavity but were unable to because the detuning was so large
- Early attempts at diagnosis and mitigation revealed some obvious sources, and the environment was improved to the point testing was reasonable
- Further studies have proved relatively fruitful (Warren's Presentation)
- The results of this study and the resulting mitigation proposals will be presented here

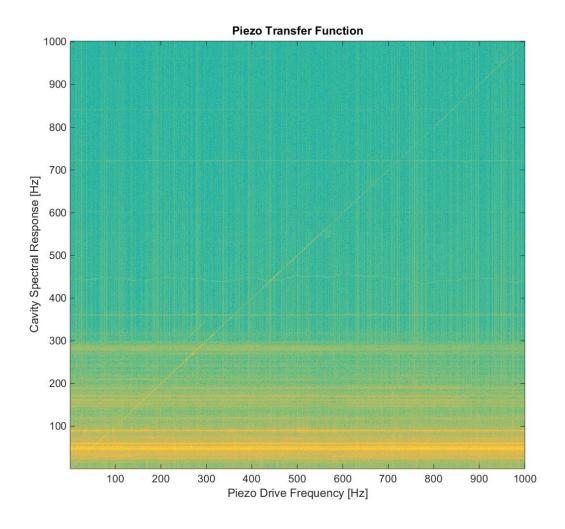


Testing Setup

- Measuring voltage driven across the cavity piezoelectric tuners gives a measurement of the cavity mechanical vibration
- Because the cavity it warm, it cannot easily be correlated with absolute frequency detuning, but the spectral information is still quite useful for diagnosis of vibrational sources
- A pair of geophones was used in the cave at large to measure surface vibrations
- Data was taken for 1 second periods, and the spectral powers were averaged over a number of data sets, usually close to 10
- Caveat: 120 Hz line is almost certainly electrical noise

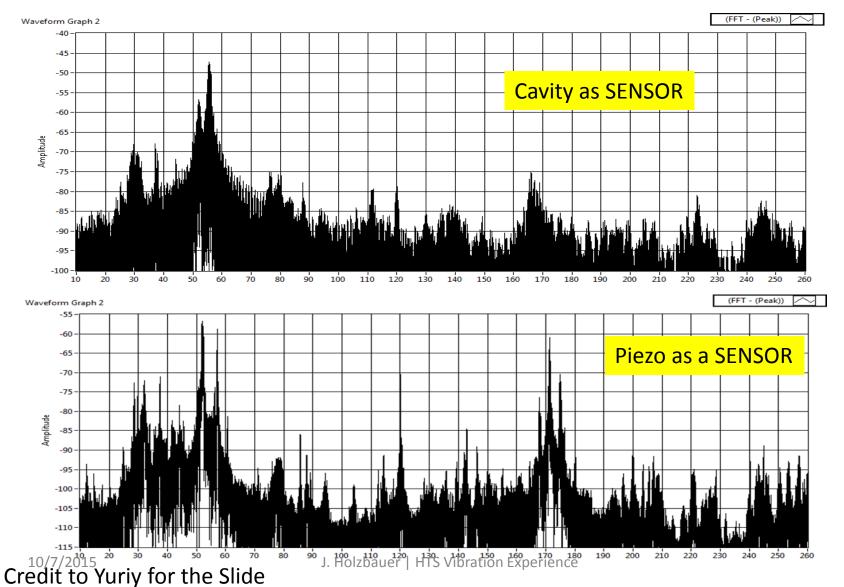


Cold HTS Transfer Function Data





Measurements of cavity vibration (microphonics) using (1) RF signal from cavity & (2) piezo signal/piezo as a sensor



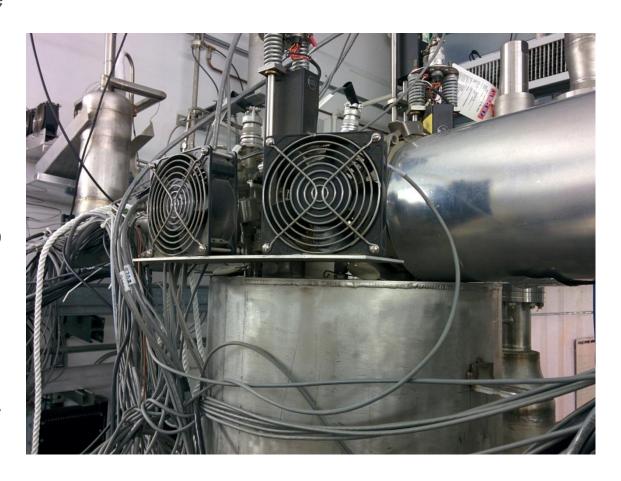
Insulating Pump Stack





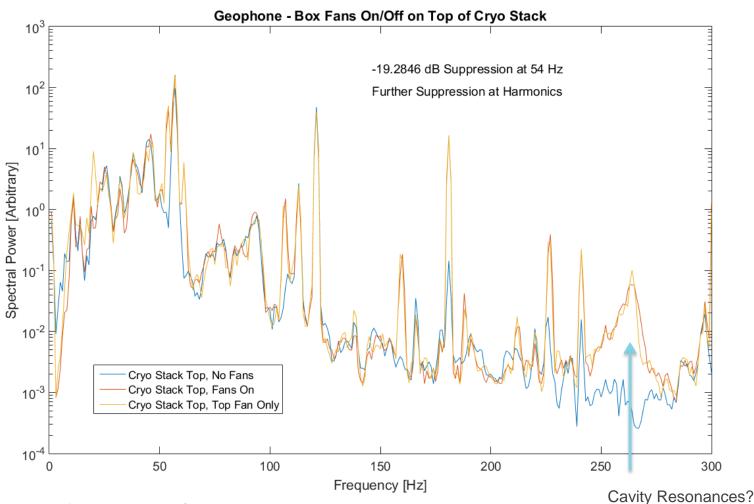
AD Cryo Box Fans

- Two box fans on a plate to mitigate valve heat leak, large vibration source
- Initially hard mounted, now soft mounted through grommets
- Heat leak is too large to have them off for more than a couple hours without significant icing
- AD cryo should be able to modify/replace with a non-vibrational heat source





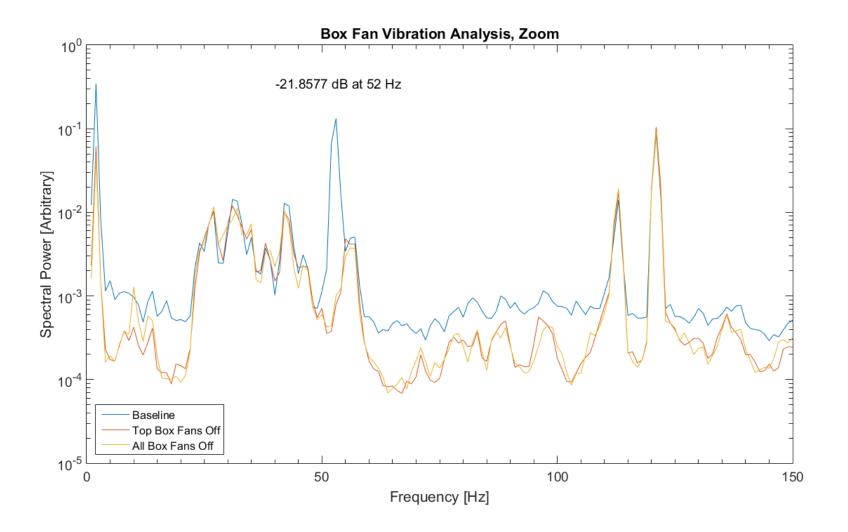
AD Cryo Box Fans – Geophones Next to Source



^{*}Again, be wary of 120 Hz peak/harmonics

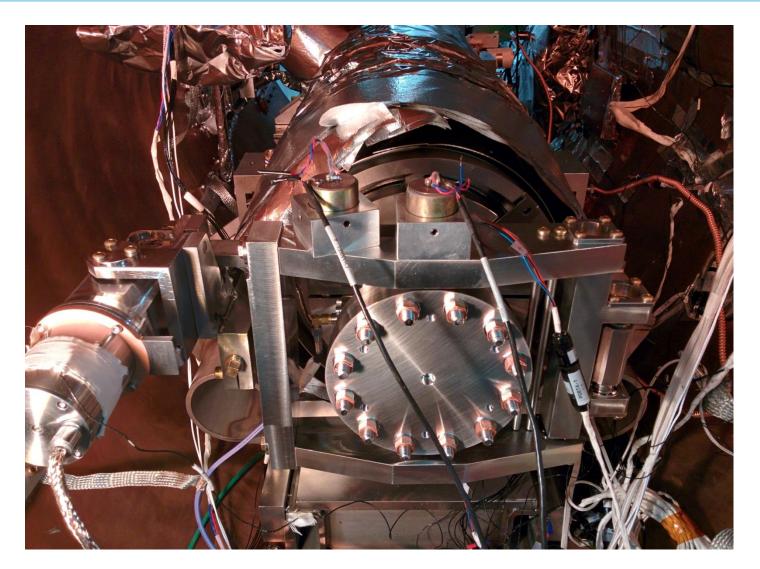


AD Cryo Box Fans – Piezo Data



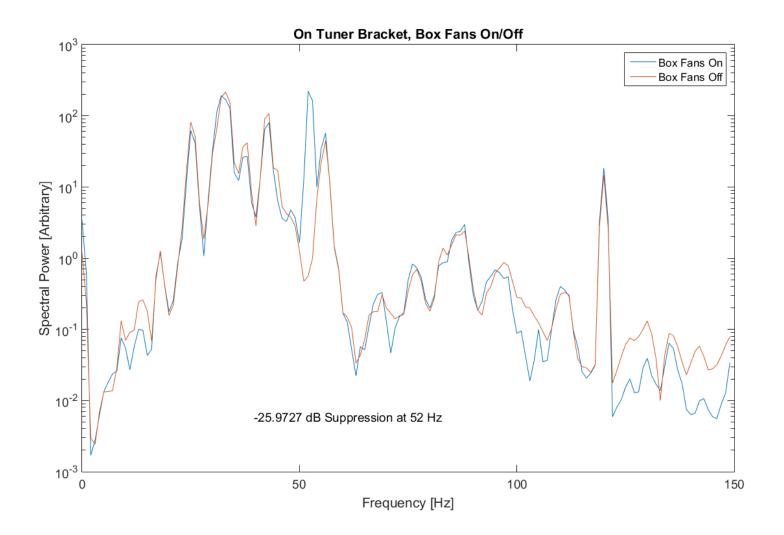


Geophones on Tuner Bracket





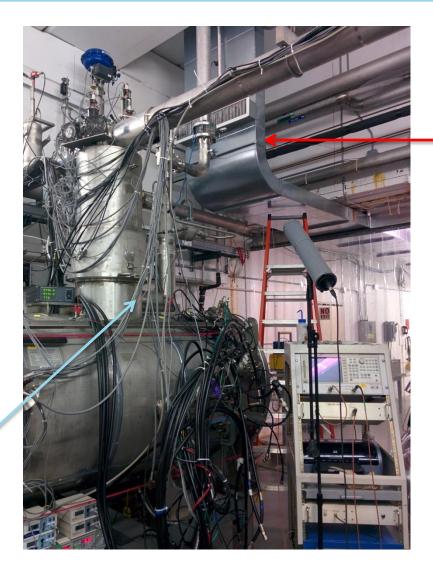
AD Cryo Box Fans – Geophone Data





ODH Blowers/HVAC Duct

- Ventilation in the HTS cave is run by two systems in parallel
- HVAC is (theoretically) controlled by a thermostat outside the cave
- ODH ventilation blowers run 24/7 when the cave is unsecured
- ODH blowers should be off when cave is secured
- Primary vent blows directly onto a cryo relief stack which hard-connects to the HTS stack



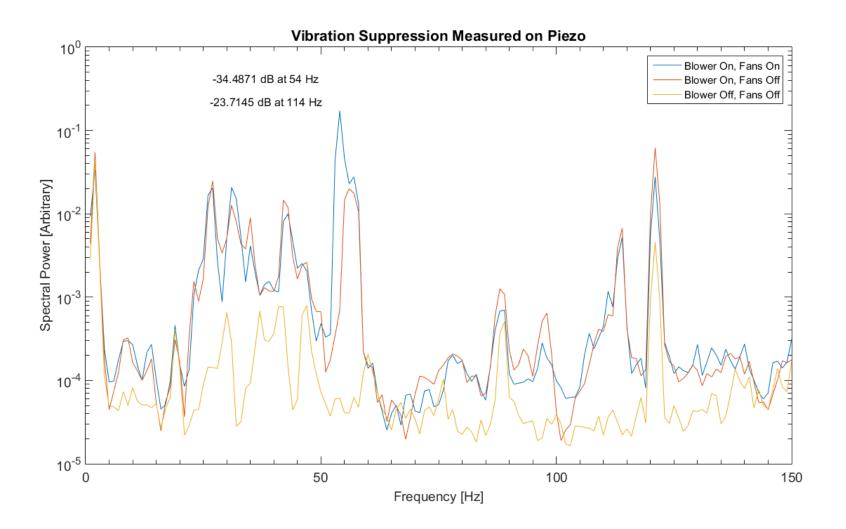


Cryo Relief Stack



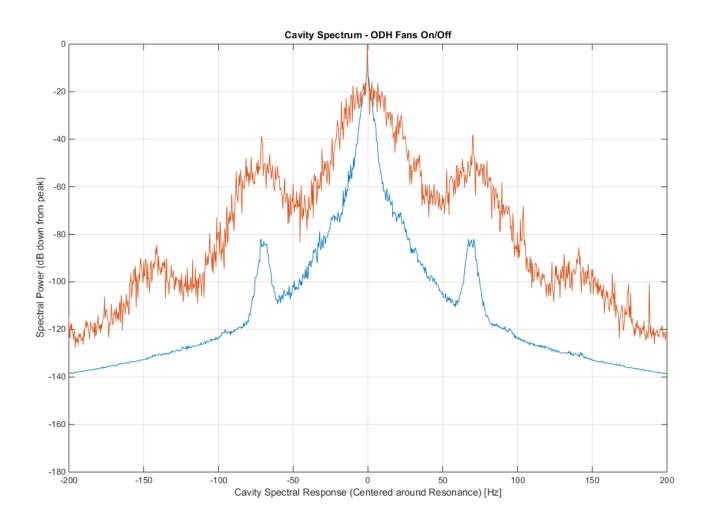
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HVAC/ODH Blower is a large noise source





Probe Spectrum Noise ON vs. OFF





Mitigation Conclusions

- ODH blower, HVAC, and AD cryo box fans seem to be the dominant sources of noise
- All spectral lines between 50 and 55 Hz (the dominant sources) seem to be suppressed or removed by these changes
- The ODH should no longer be a problem as it should shut off when the cave is interlocked (the original intention, and now restored)
- The HVAC can be turned off for periods of time when needed (summer is harder)
- The AD cryo box fans were just turned off, and the Cryo guys keep an eye on the valve icing



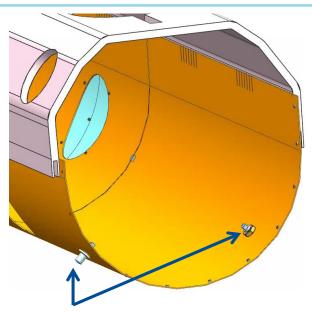
Future Work - Conclusions

- Passive mitigation is only one aspect of microphonics stability
 - Cavity/Tuner Design (excellent work done on df/dP for SSR1)
 - Cryogenics/Cryomodule Design (bath pressure environment, mechanical modes)
- My motto: "Passive mitigation first, last, and always."
- Good news: Vibration sources/issues are often obvious in retrospect
- Bad news: That retrospect part
- A centralized effort must be made to think about these issues ahead of time (my opinion)

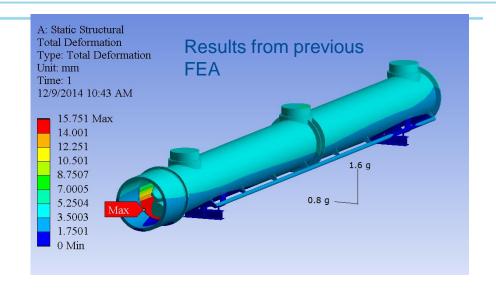


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Changes to FEA thermal shield model



- G10 support rods (newly added in 3D model), two on each end of lower shield
- ➤ To restrict the motion, in case of seismic event the lower shield cannot move further due to the G10 rods getting in contact with the inside of the vacuum vessel
- Plan to leave a gap between the inside of the vacuum vessel and the tip of these G10 rods, for thermal leak & shrinkage



Material properties of thermal shield:

- > EN AW-1050A, AI 99.5%
- > The extruded tube material: EB AW-6060 AlMgSi0.5

Table I. Mass Distribution of Finite Element Model (kg)

cold mass						
	cavity stri	ng	509.93			
	shield		2061.5	K		
				Evpor	stad to be	lower
				Exped	cted to be	e lower
Гable II. De	ensity and	Modulus o	of model p	arts		

Part	density (kg/m^3)	modulus (GPa)
shield	13815	207