

# Microphonics and Transient Effects

T. Powers

LCLS II Microphonics Workshop 1

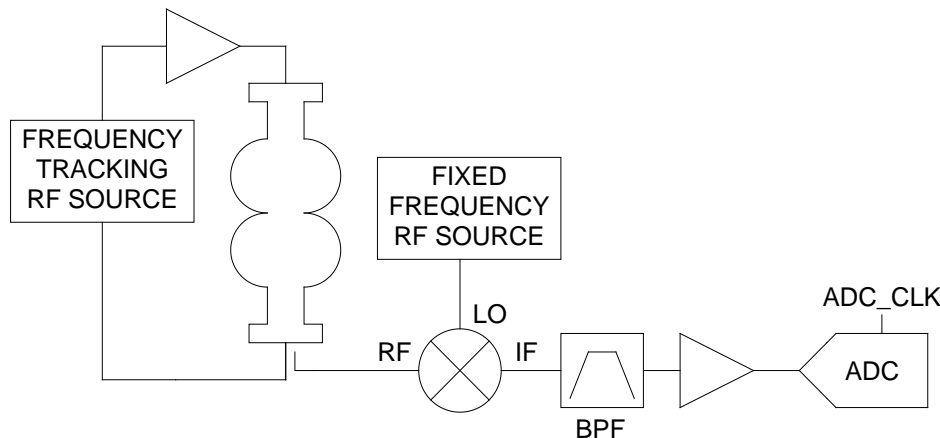
Oct. 2015

# Simple Microphonics Acquisition Scheme

If the RF IF frequency is not precisely related to the sample frequency by the ratio 4, 1/1.25, 1/2.5, 1/5 . . . the I and Q signals will have the form:

$$I(t) = V_{Peak} \cos(\omega_1 t + \varphi(t)) \quad Q(t) = -V_{Peak} \sin(\omega_1 t + \varphi(t))$$

Where  $\omega_1$  is the difference frequency between the ideal IF frequency and the actual IF frequency. One can implement such a system using a simple mixer to down convert the RF signal to an IF frequency as shown below to collect the data.



**Example Parameters:**

**IF = 400 kHz,**

**ADC clock = 320 kHz**

**Filter BW = 200 kHz**

**OR**

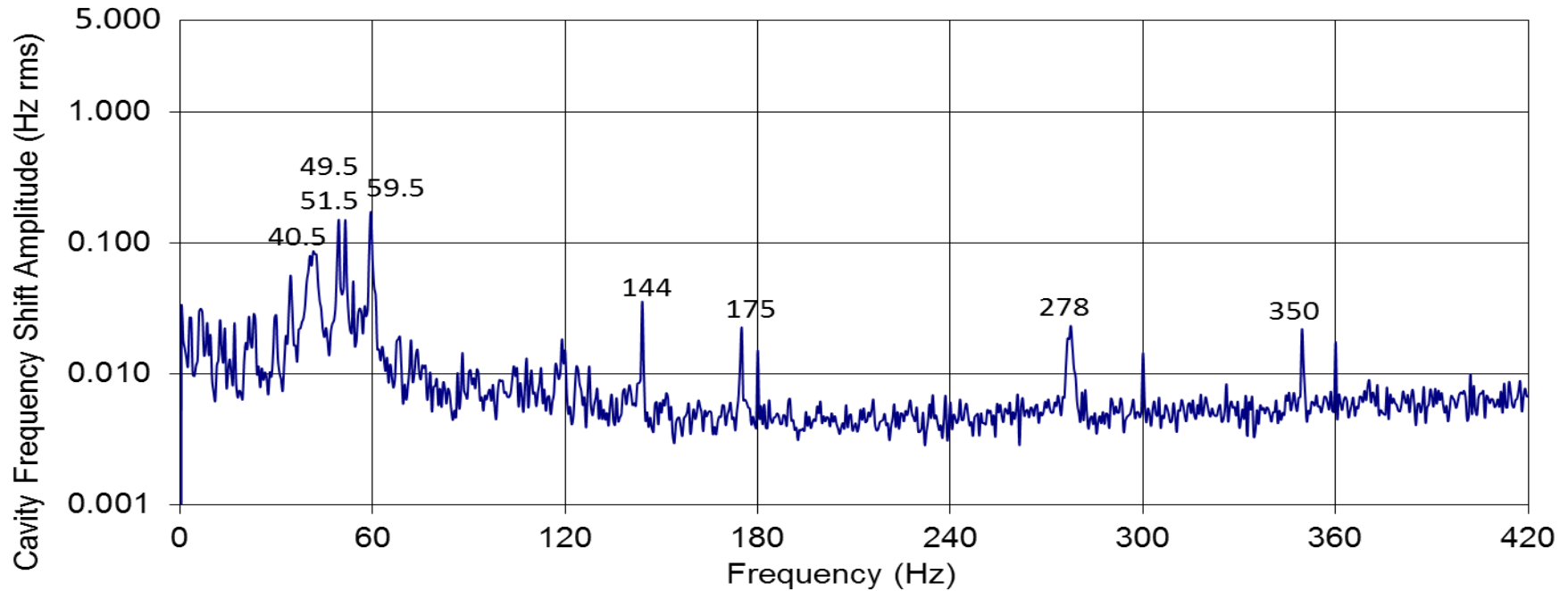
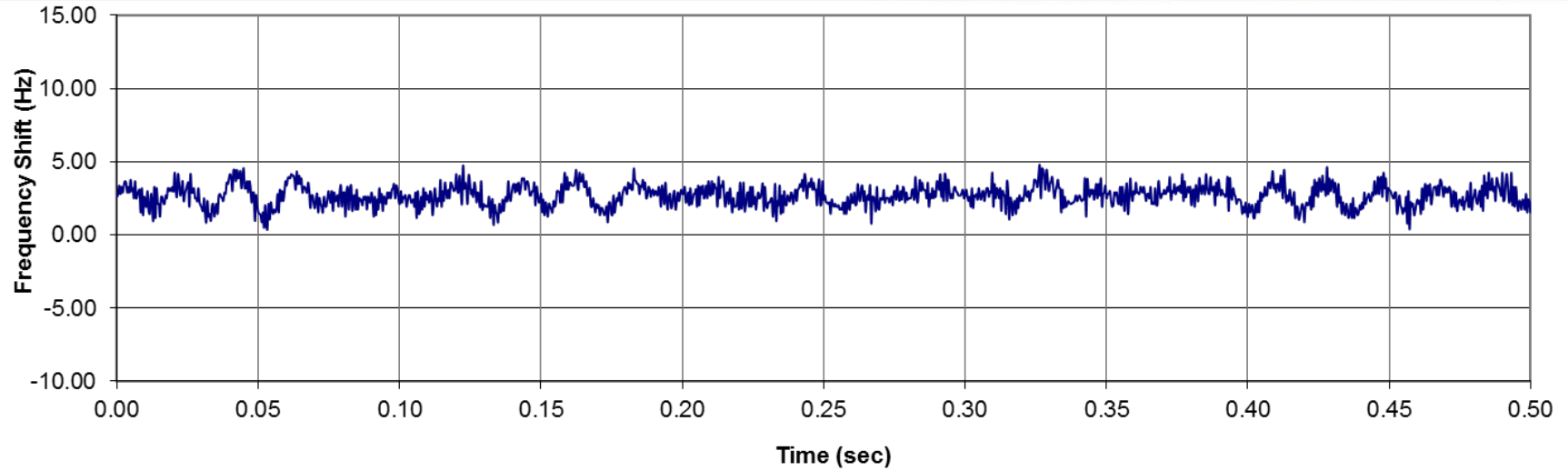
**IF 25 kHz**

**ADC clock 100 kHz**

**LPF 5 MHz (for high freq.)**

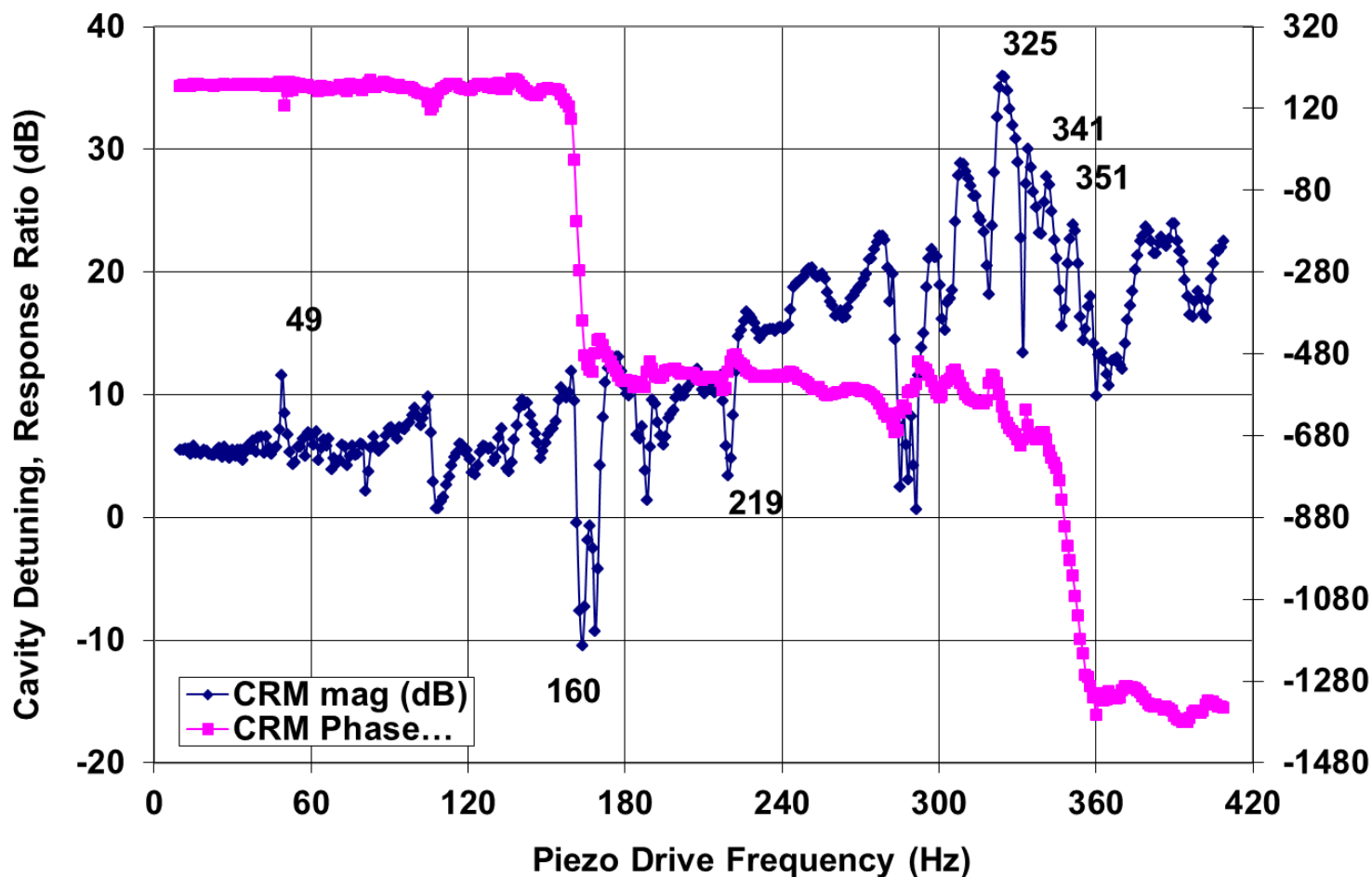
**LPF 40 kHz**

# FEL3-6 Microphonics

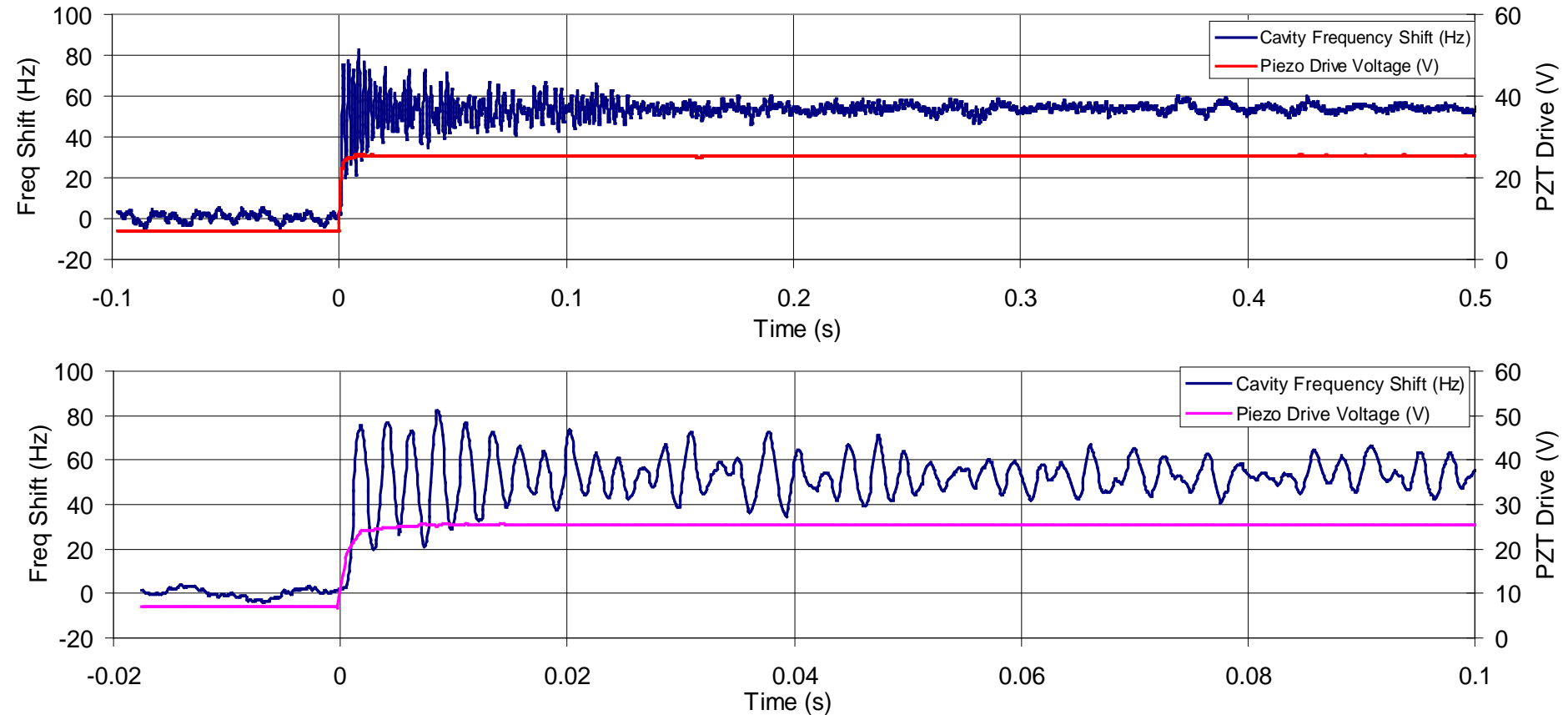


# FEL03-6, Piezo Transfer Function

## FEL03-6, Piezo Transfer Function

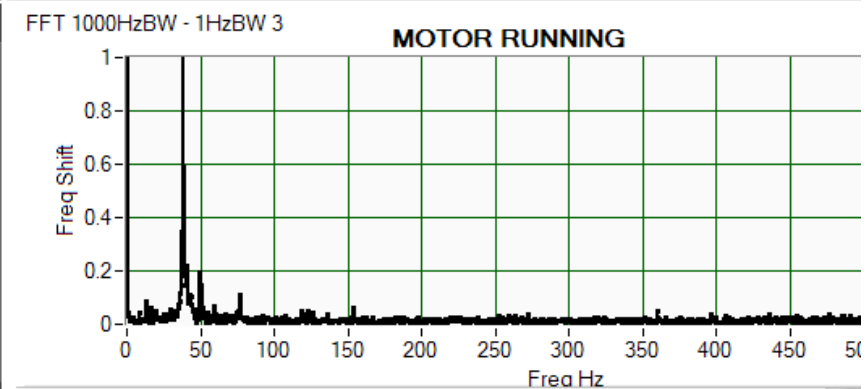
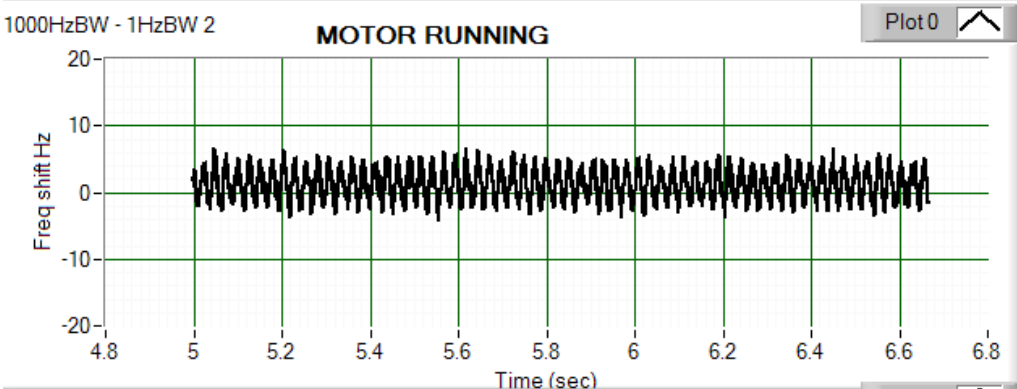
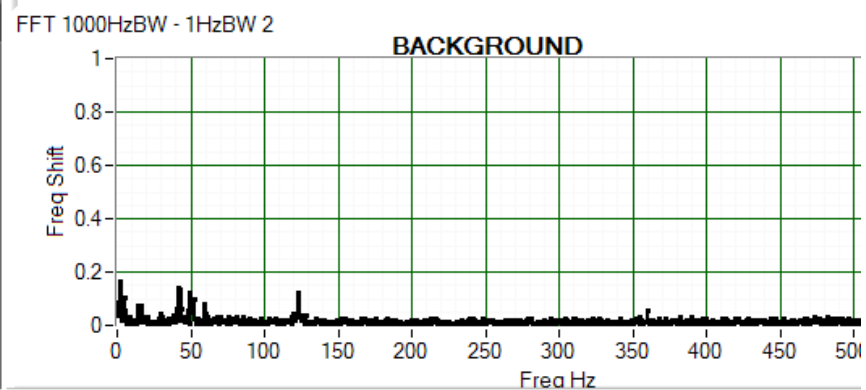
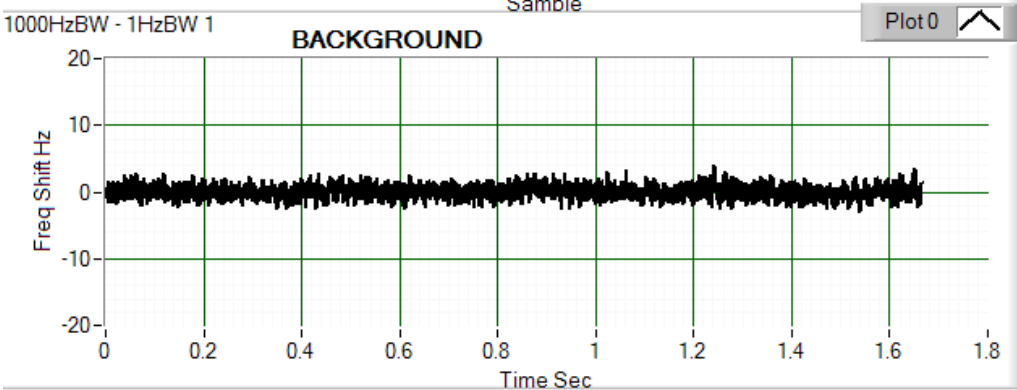
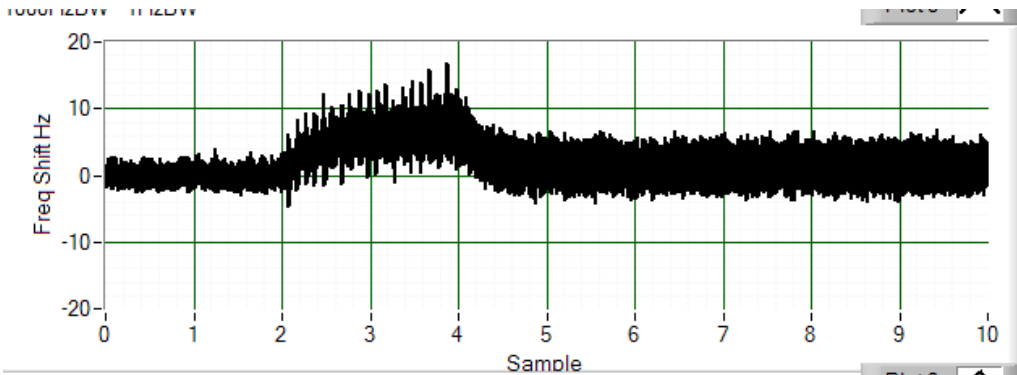


# FEL3 PZT Step Response



Step response of a cavity excited by a by a 50 Hz step in the piezo tuner controls.  
The total range of this tuner was 550 Hz.

# FEL3-5 Tuner Running 2 steps/full step

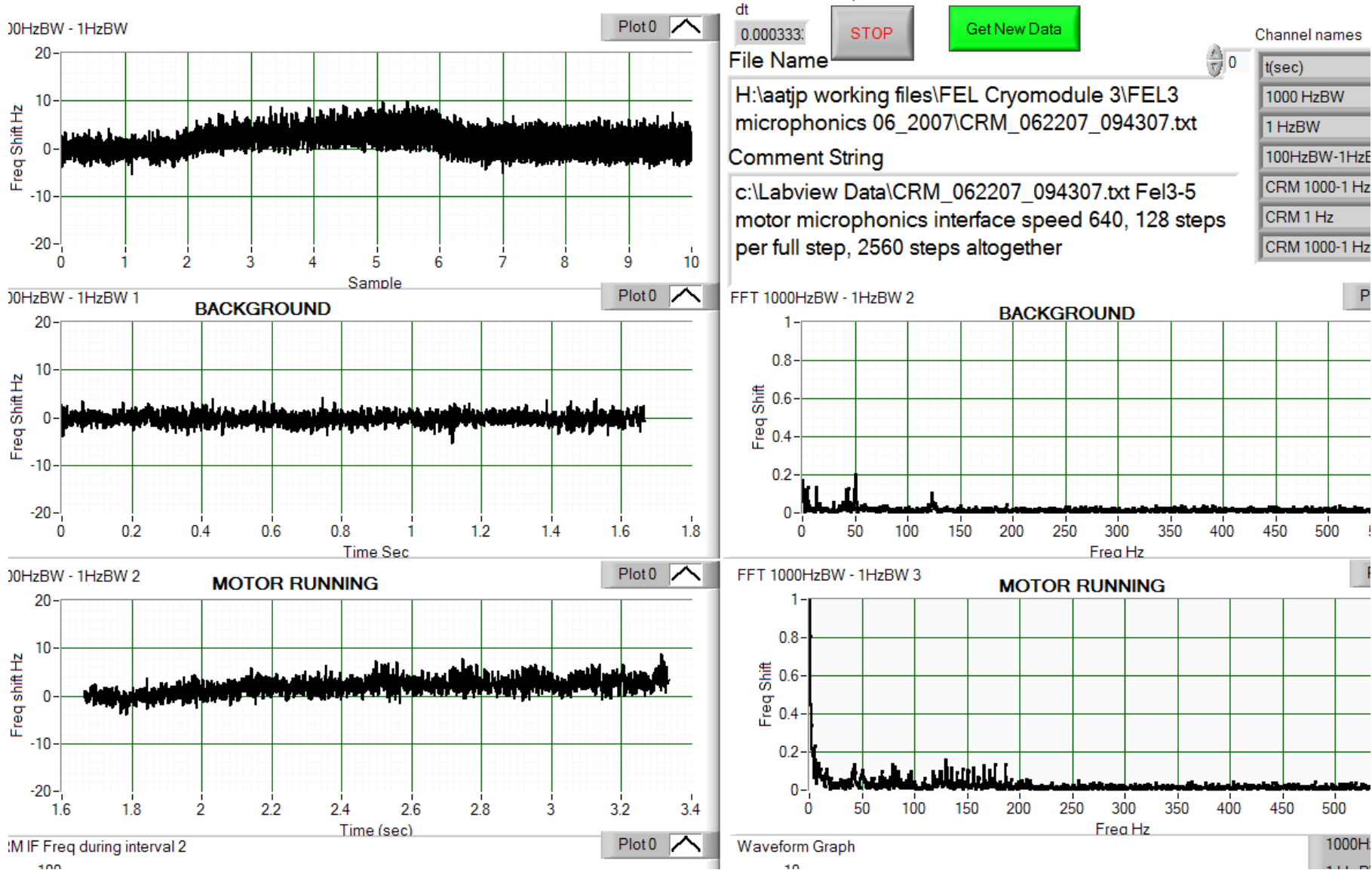


CRM IF Freq during interval 2

Waveform Graph

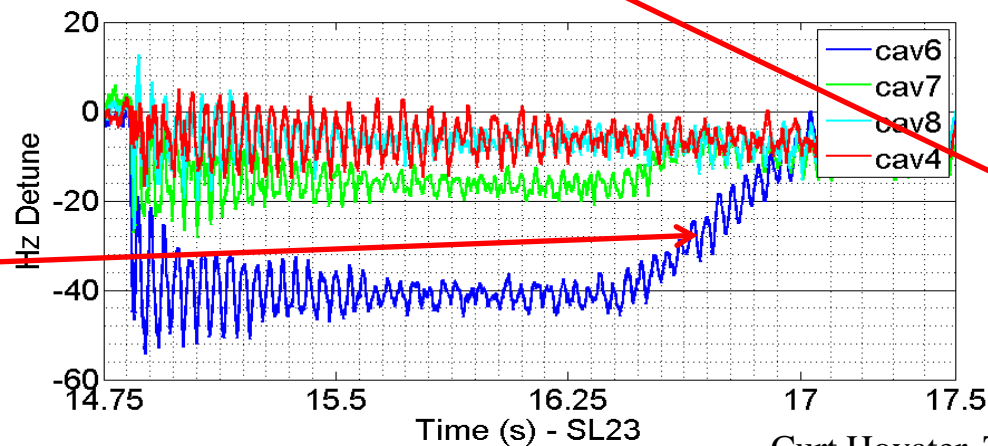
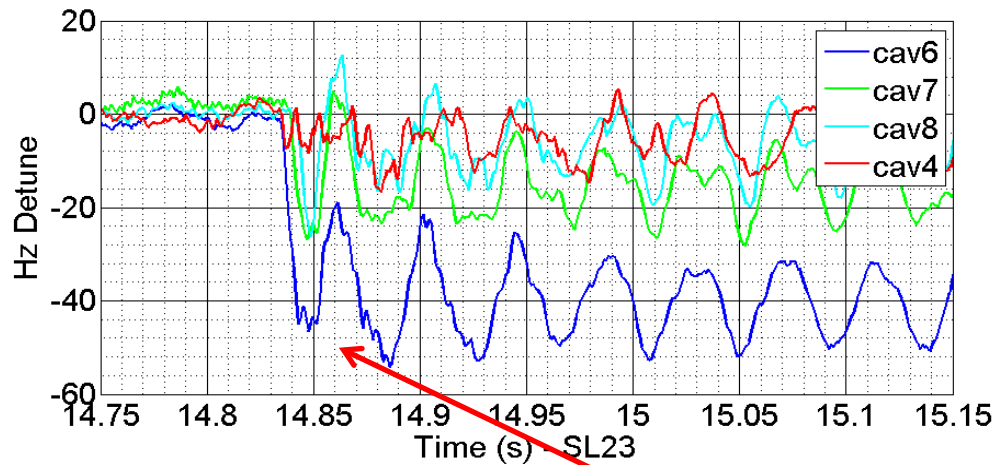


# FEL3-5 Tuner Operations 128 microsteps/step



# DYNAMIC COUPLING BETWEEN CAVITIES

C100-4 Cavities 4, 6, 7, 8 responding to an applied PZT step control voltage change from 52 to 39 volts (130 Volt range) in cavity 5



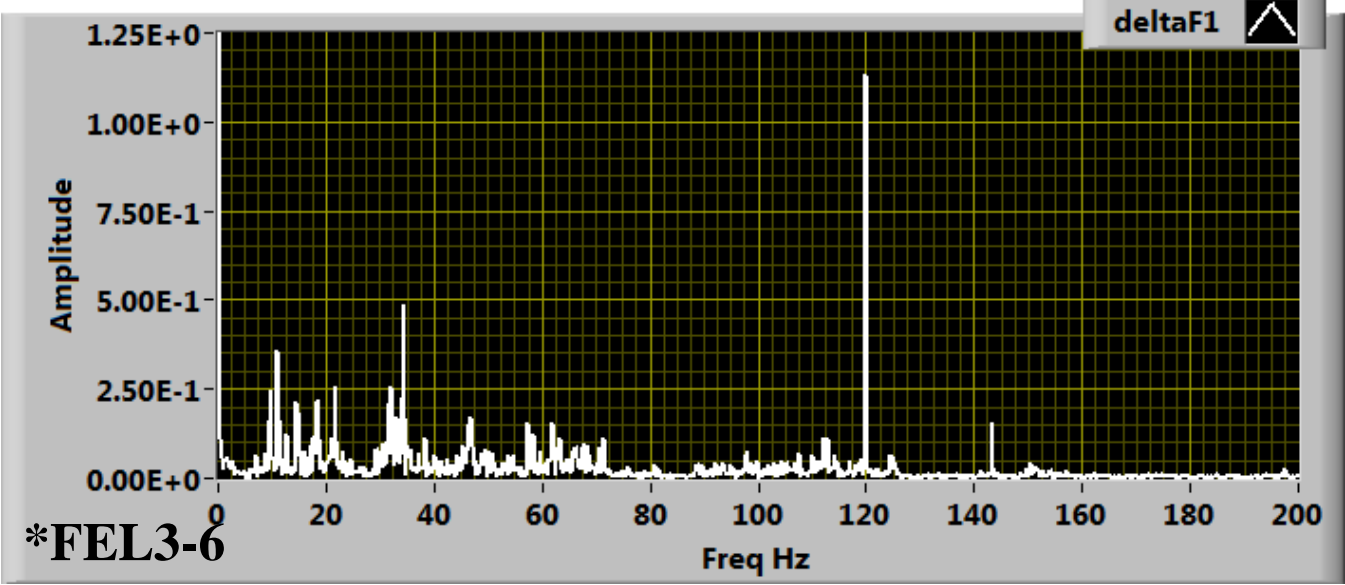
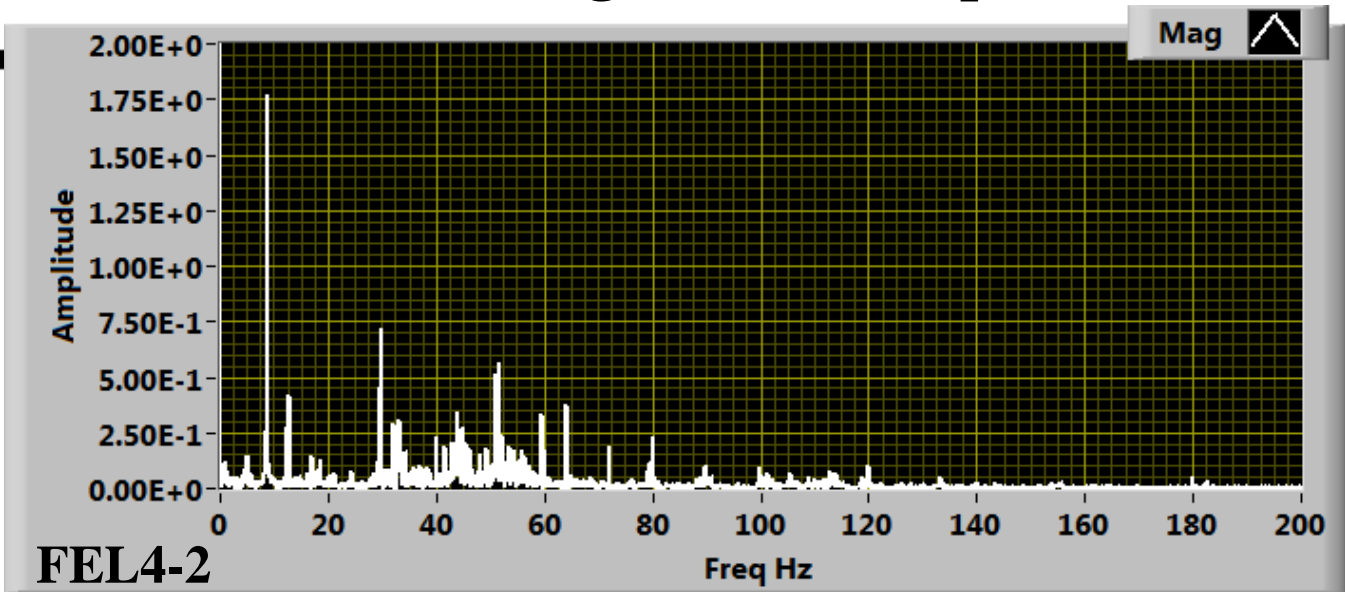
- **Adjacent Cavity coupling is ~ 10% between 1-4 and 5-8 cavities**
- **Cavities 4 and 5 have a “quasi” mechanical support between them.**
- **Ringings is the 21 Hz mechanical Mode**

Curt Hovater, Tomasz Plawski,, Michael Wilson, Rama Bachimanchi

- **Cavity 5 PZT moved 460 Hz.**
- **Locked in GDR Mode**
- **Because of 10 MV/m operating point, the klystron had the overhead to keep cavities locked**
- **Stepper Motor operated to tune the cavities**



# Excessive Background microphonics

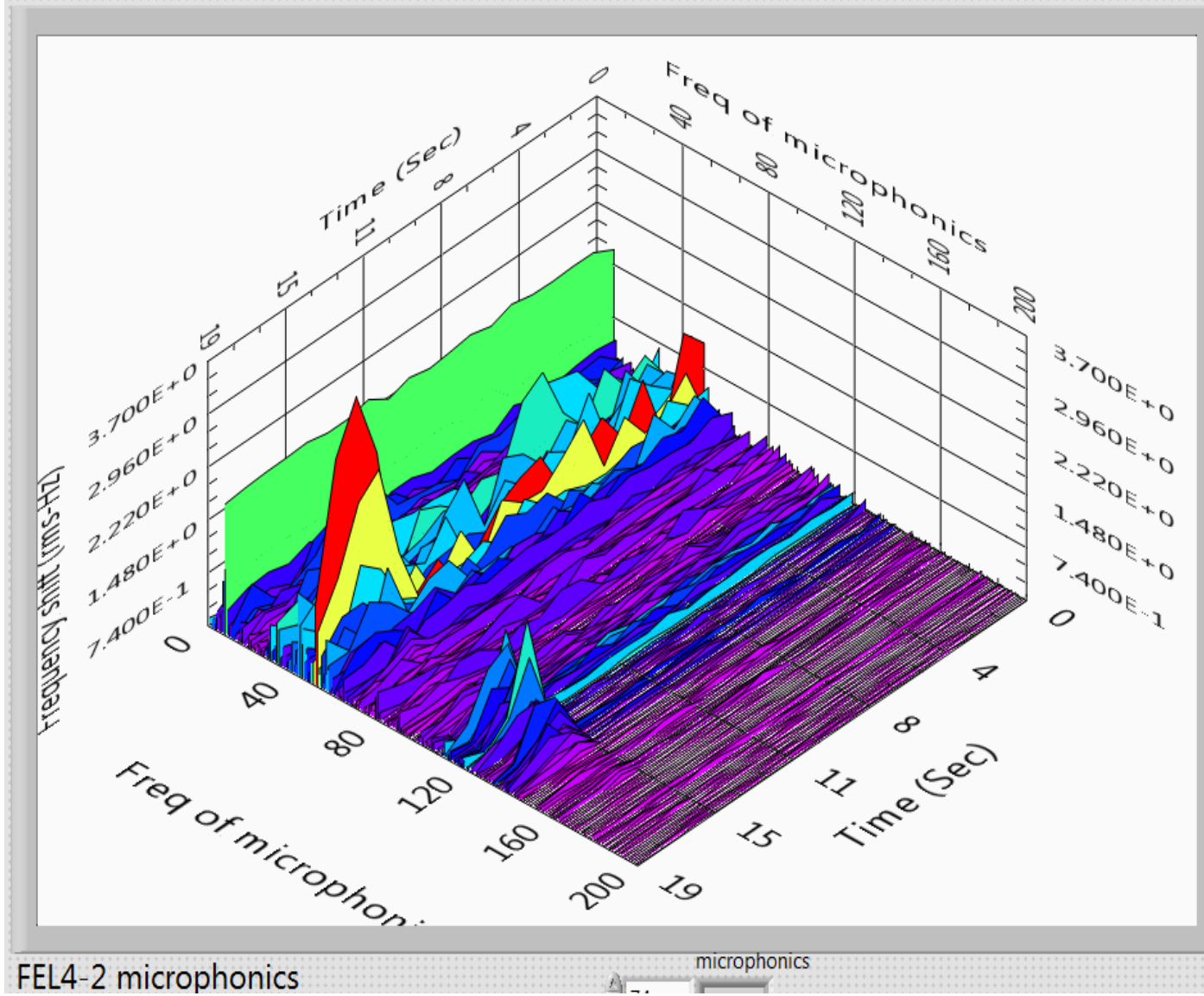


- Data taken during USPAS school.
- FEL4-2 Data taken with kystron at a few MV/m.
- FEL3-6 data taken with a 1W amplifier and a top hat.

\*Cryomodule replaced with former SL21 CM

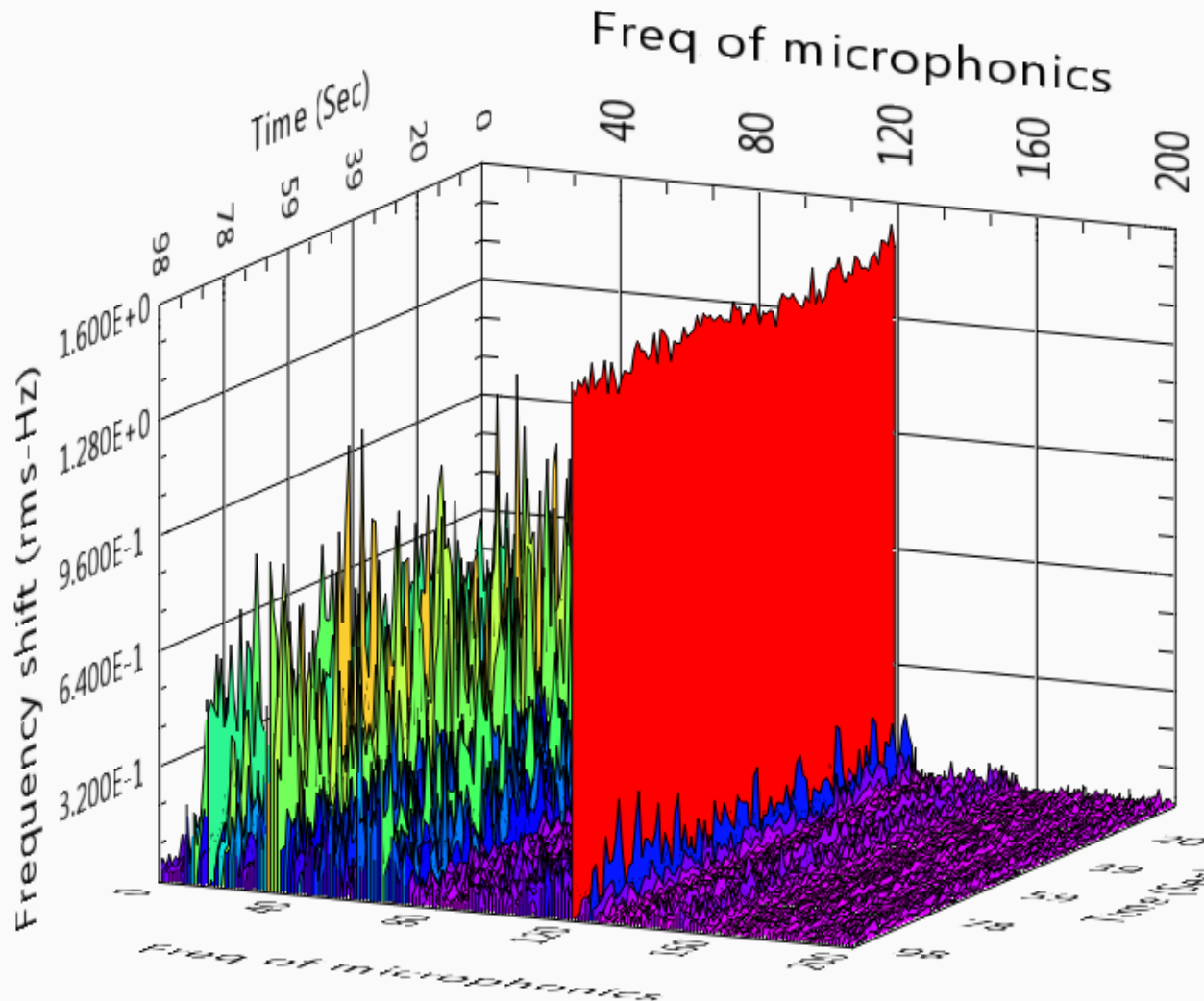


# FEL4-2 Frequency vs Time data



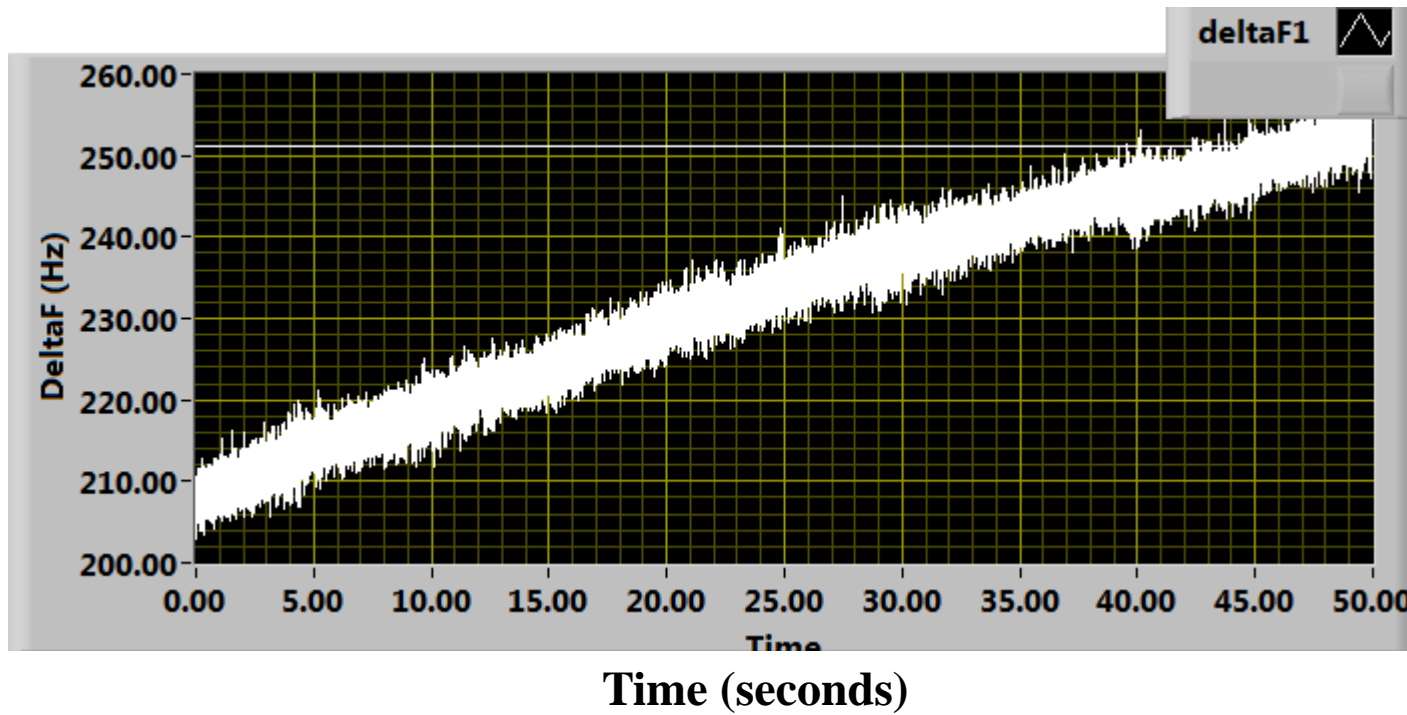
**8 Hz  
perturbation  
due to poorly  
mounted beam  
line ion pump  
(over extended  
jack stand).**

# FEL3-6 Frequency vs Time Data



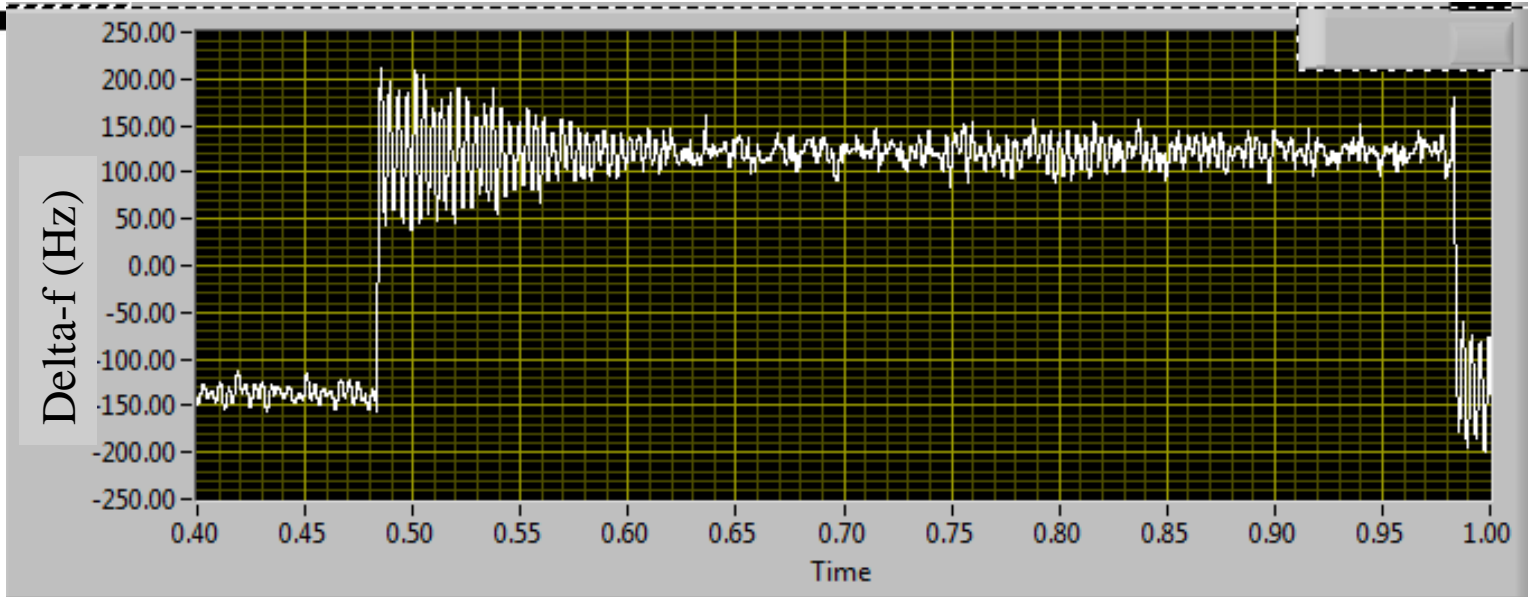
**120 Hz noise due to insulating vacuum turbo pump backing pump coupled in through corrugated hose.**

# FEL3-6 with fan blowing on beam line

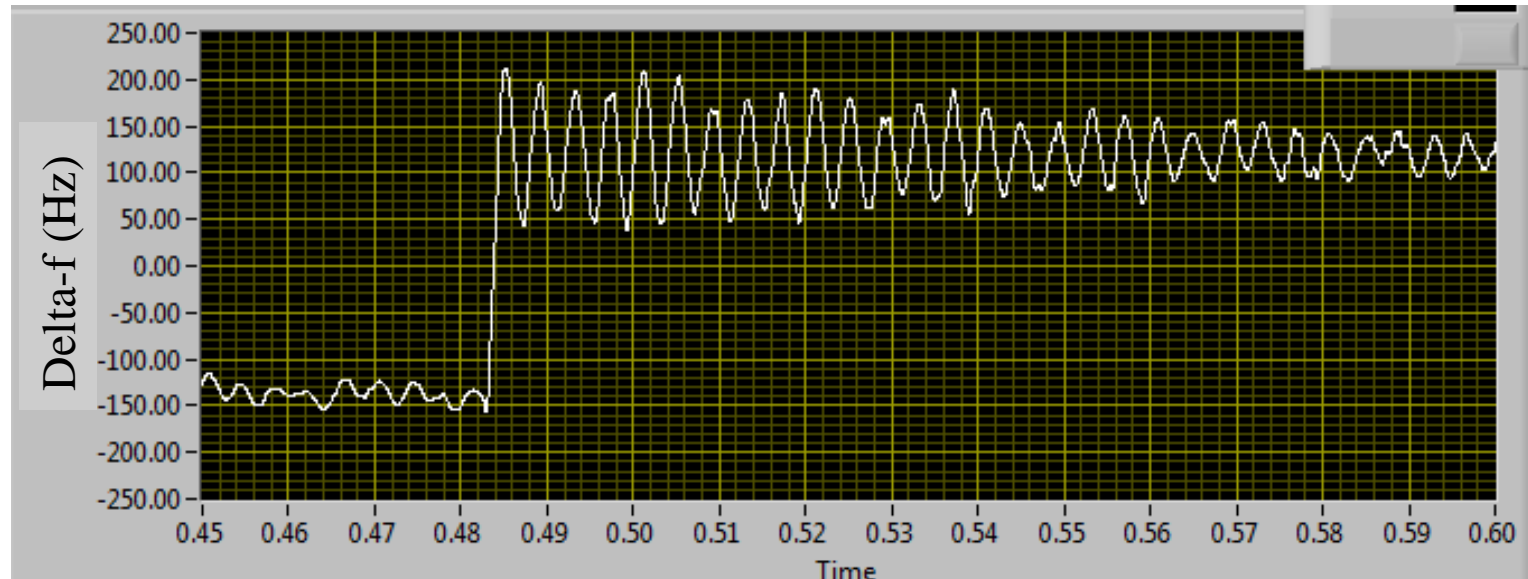


- Fan blowing on inner cryomodule girder caused slow temperature shift of about 200 Hz. Removal of the fan caused the frequency to restore to the previous value.
- Similar continuous (hours and hours) detuning has been seen in cryomodules operated at constant gradient overnight.

# Transient Frequency Shift Oscillation Due to Step Change in Gradient



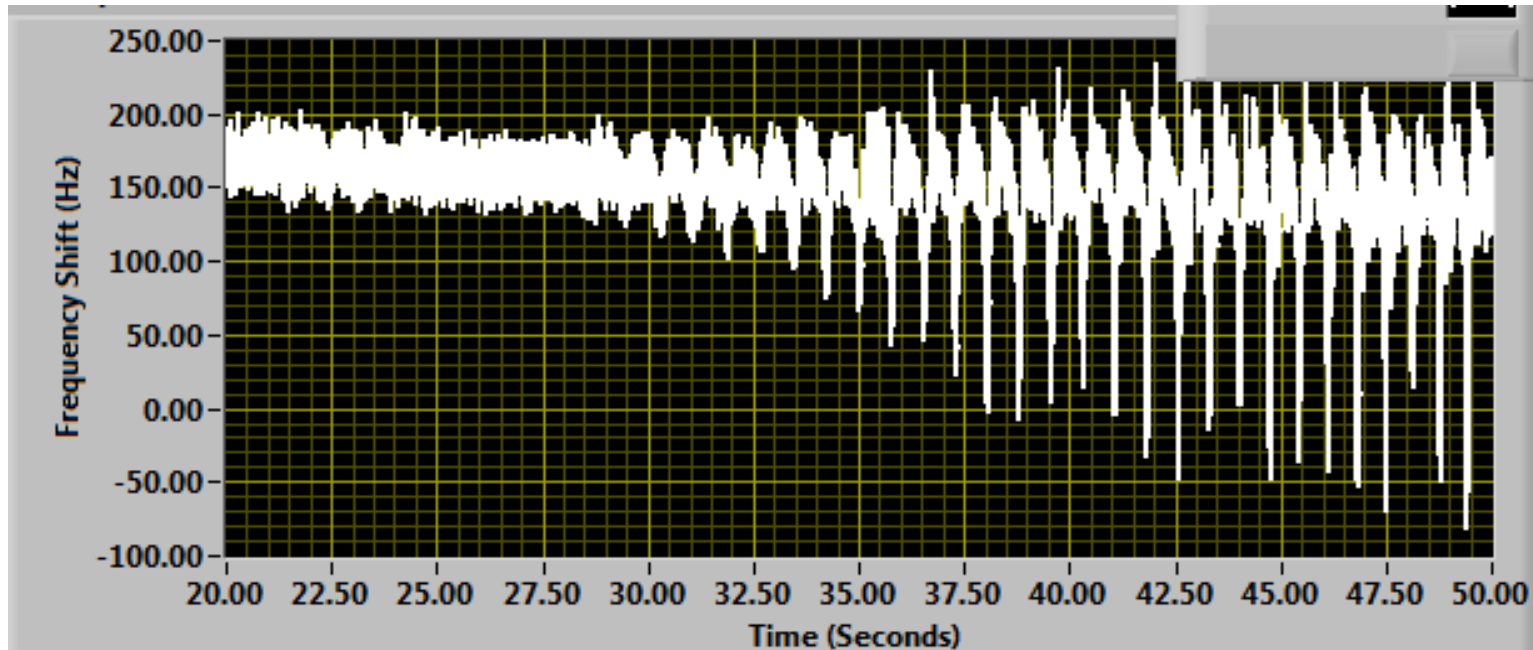
**IHEP  
HWR  
structure**



**Frequency of  
oscillation is  
appx. 250 Hz**

**Do not reprint this  
slide without  
permission**

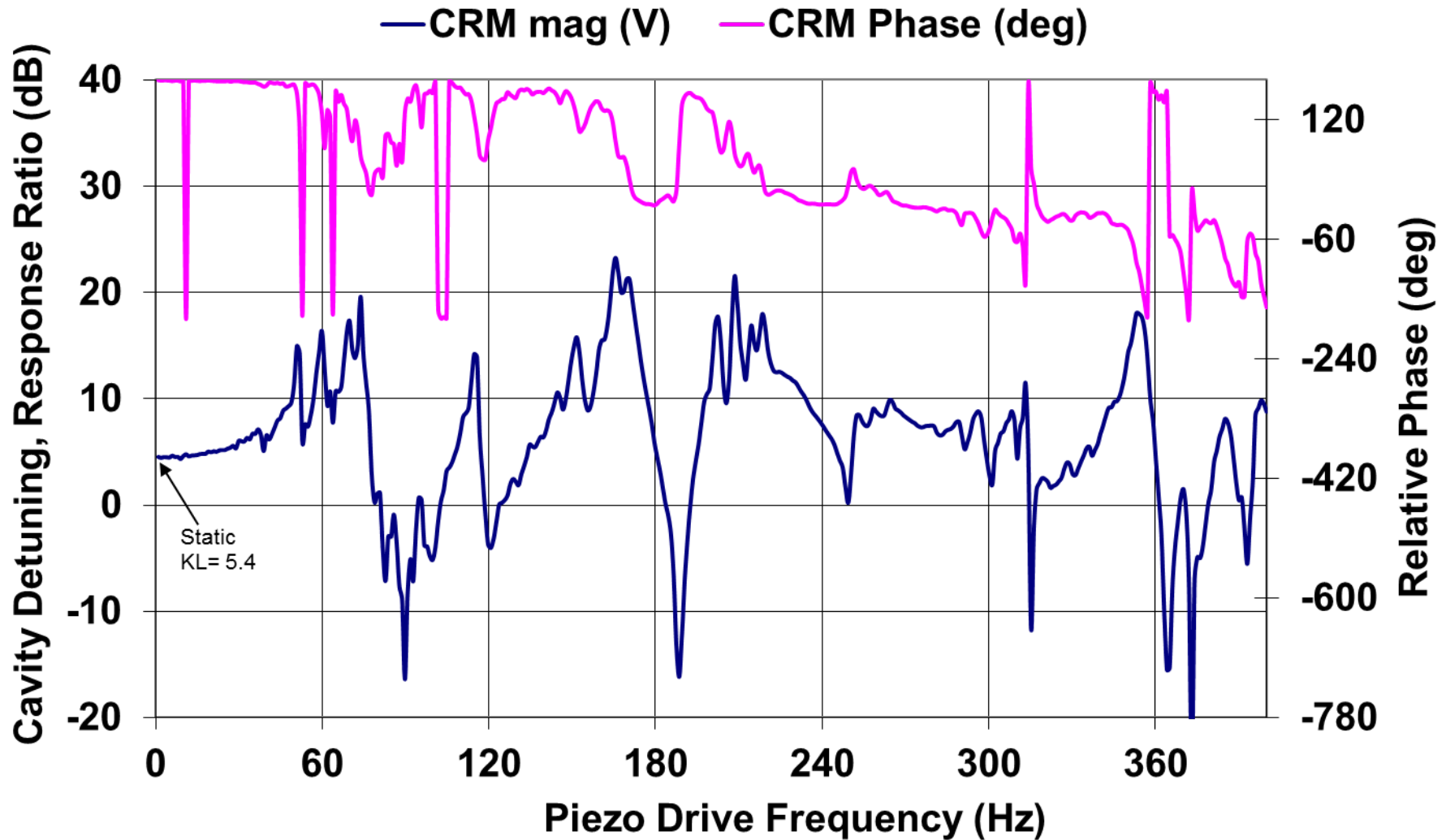
# Construction Noise Source



**IHEP spoke cavity 1  
excited by jack hammer on  
roof of building**

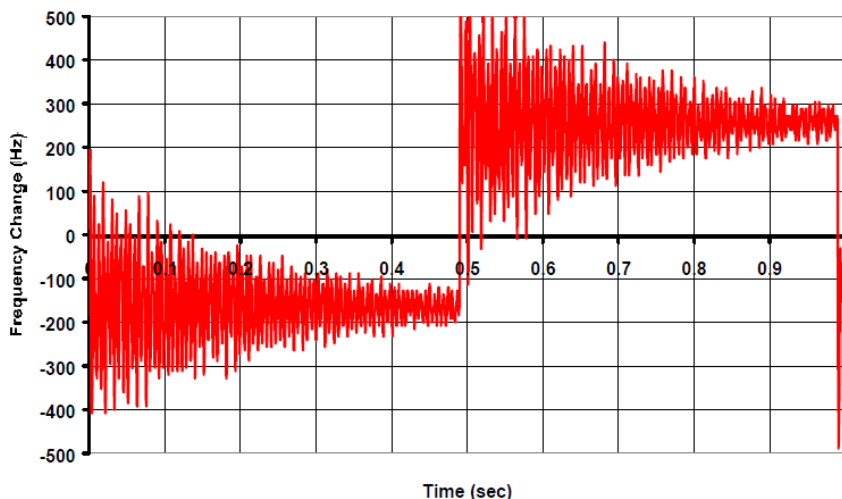
**Do not reprint this  
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permission**

# SNS MB1 Cavity 2, PZT Transfer Function

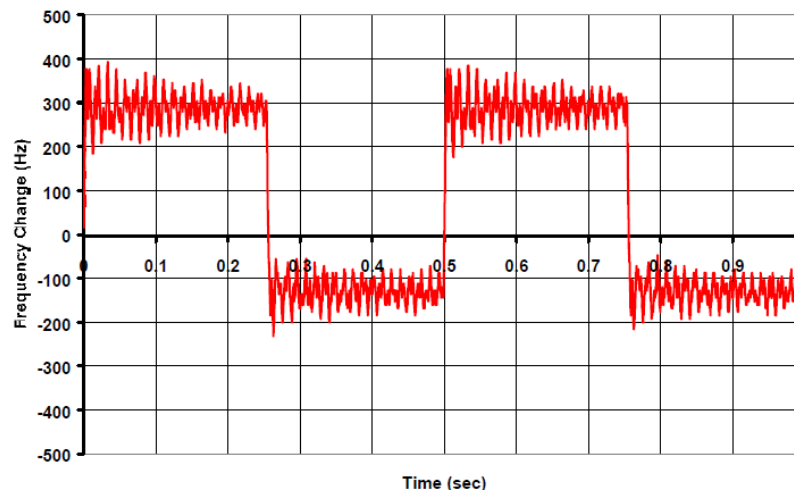


# Varying PZT ramp time SNS MB Cavity

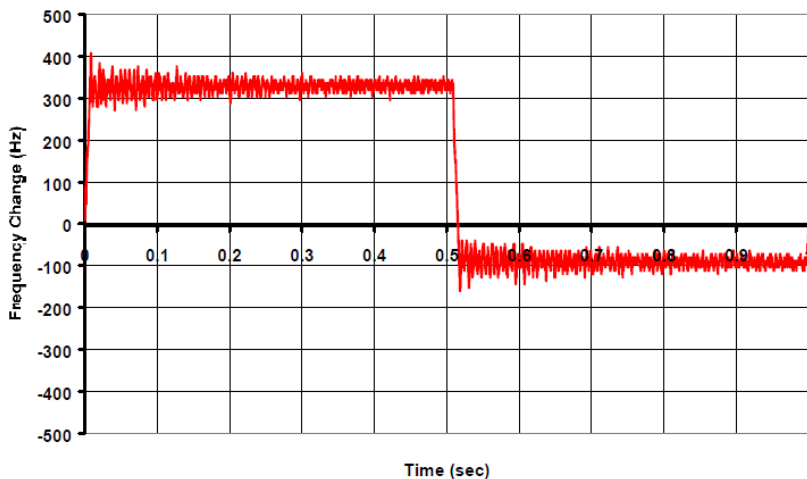
Cavity Pos. 2 Piezo Response, 1 Hz Square Wave



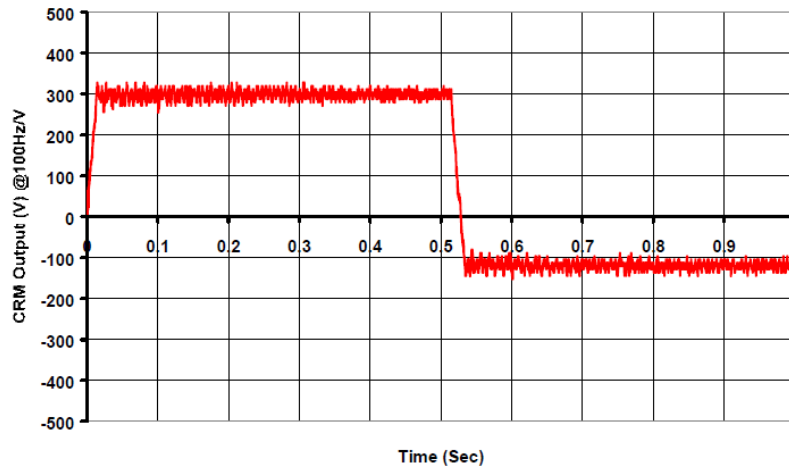
Cavity Pos. 2 Piezo Response @ 5ms rise time; 2 Hz



Cavity Pos. 2 Piezo Response at 10 ms rise time; 1 Hz



Cavity Pos. 2 Piezo Response at 20 ms rise time; 1 Hz



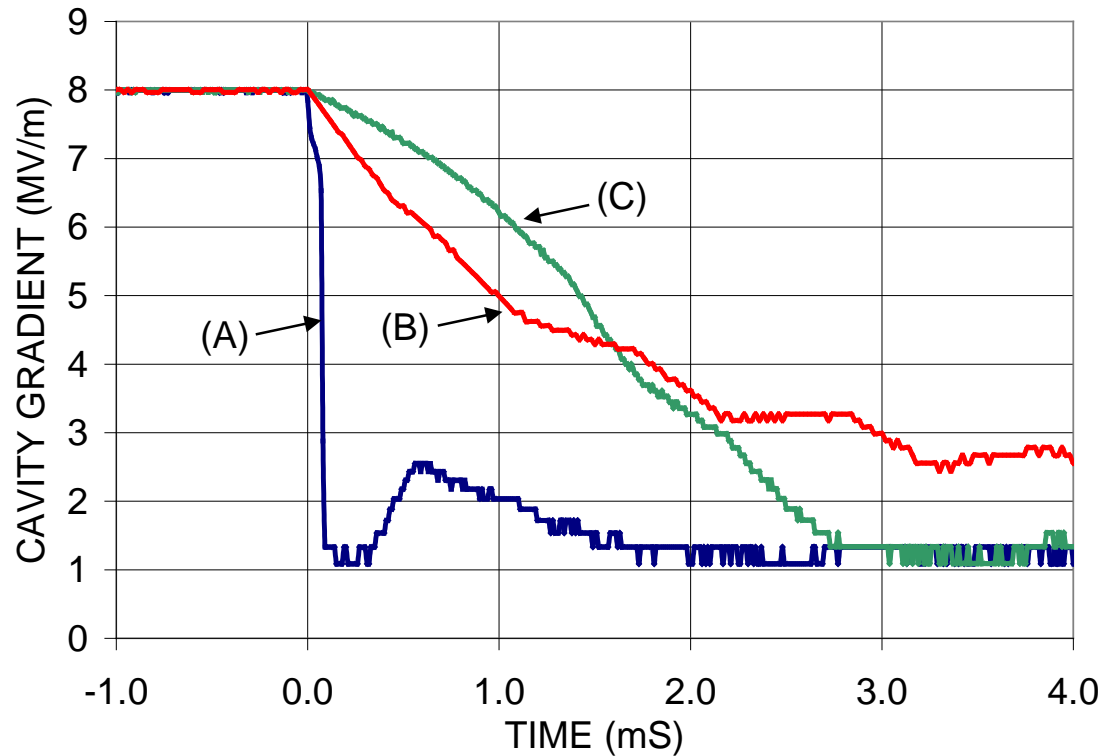
JLAB TN-02-049, Delayen, et. al. Frequency Measurements on Prototype SNS Medium- $\beta$  Cryomodule Under Pulsed and CW operations.



# Types of Arc Events

1. Waveguide Arc
  - Occur in the vacuum space between warm and cold windows
  - Gradient decay time  $\sim 1 - 2$  msec
2. “Electronic Quench”
  - Occur in vacuum space on the cavity side of the cold window
  - Gradient decay time  $< 200$   $\mu$ sec

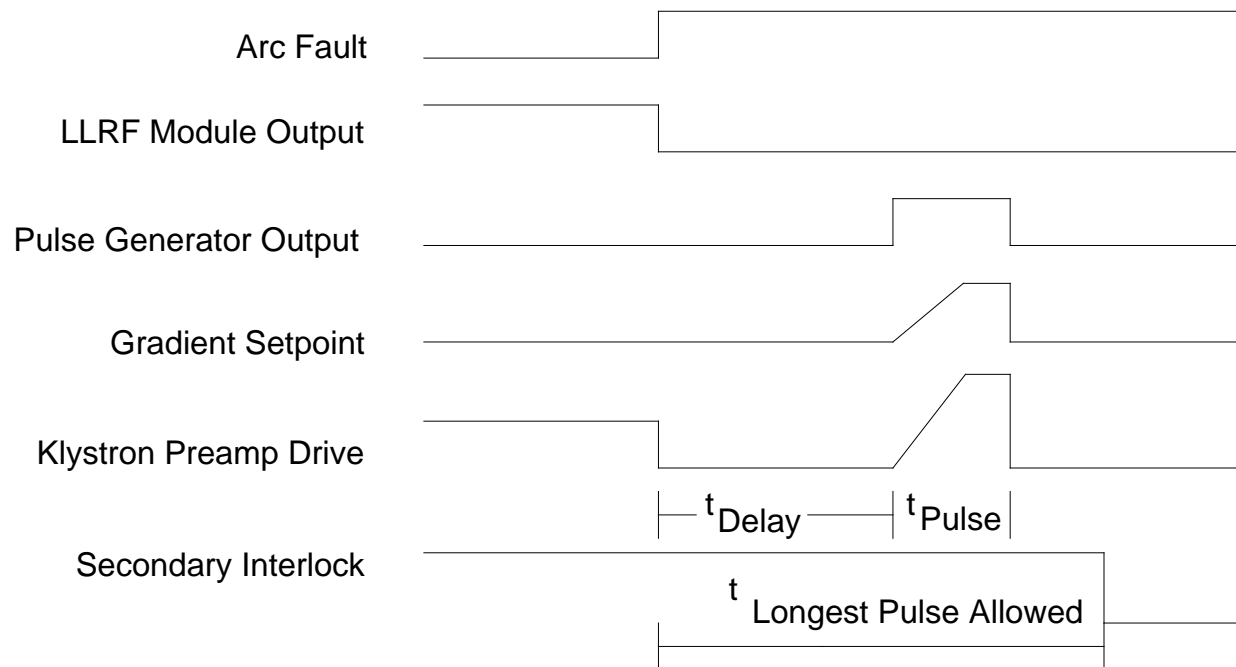
# System Response to Arc Events



- A. “Electronic Quench”
- B. Waveguide Arc
- C. Normal Response

# Experimental Overview

- Induce arc events using the existing LLRF system
- Apply a secondary RF pulse following a delay
- Measure system response
- Vary delay and ramp-up time of secondary RF pulse
- Maintain machine protection via hardware interlocks



# Open Loop Test Results at 7.7 MV/m

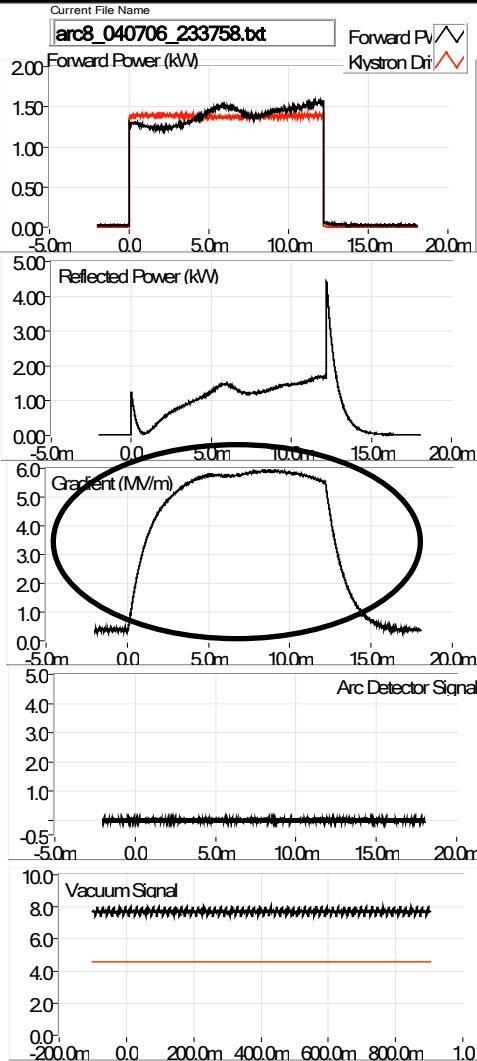
Forward Power

Reflected Power

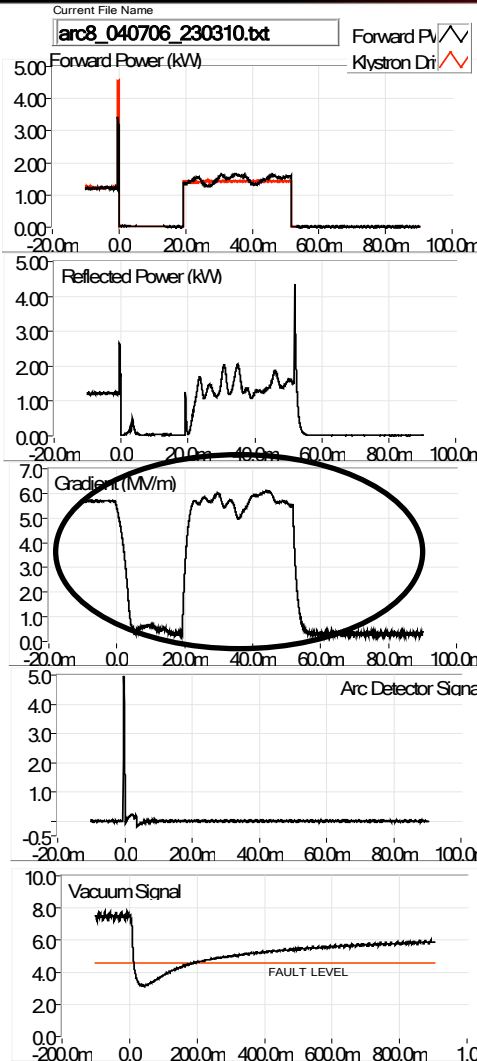
Gradient

Arc Detector

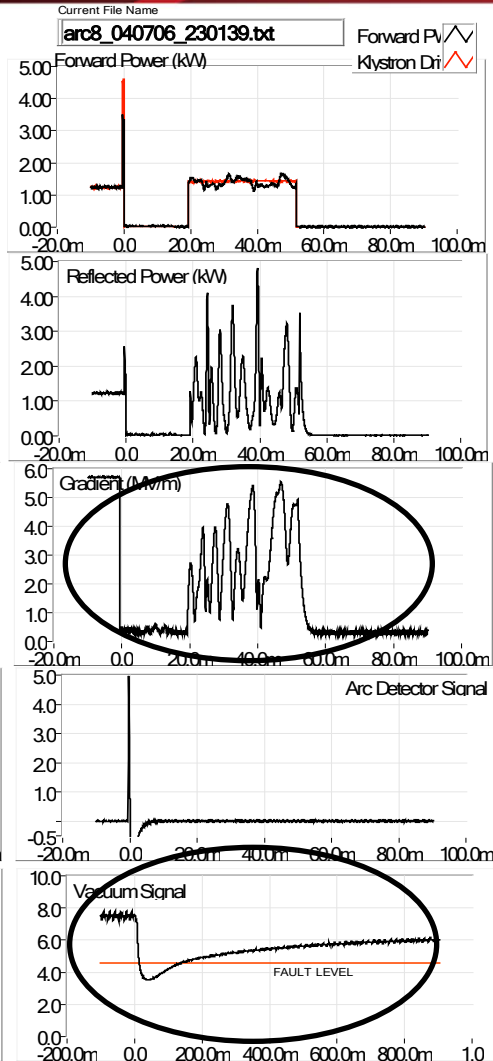
Vacuum



Normal Pulse  
(no event)



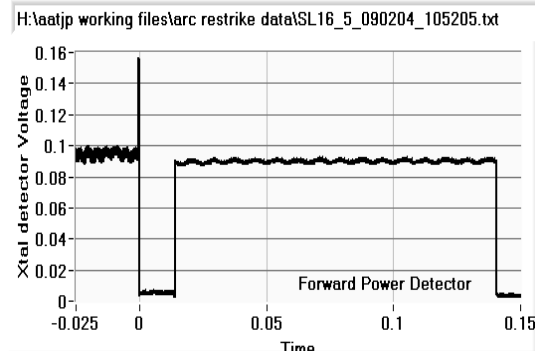
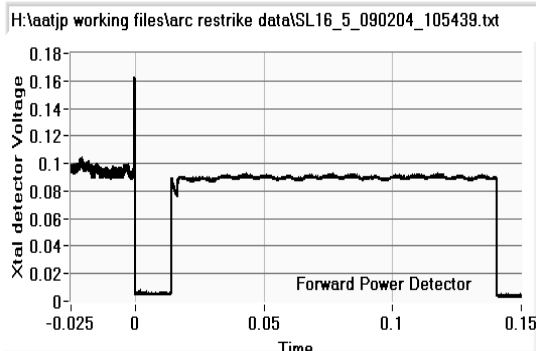
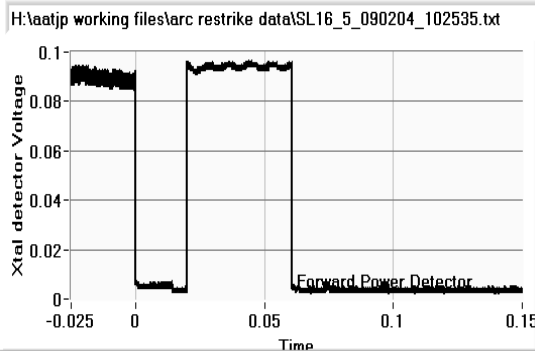
Pulse following  
Waveguide Arc



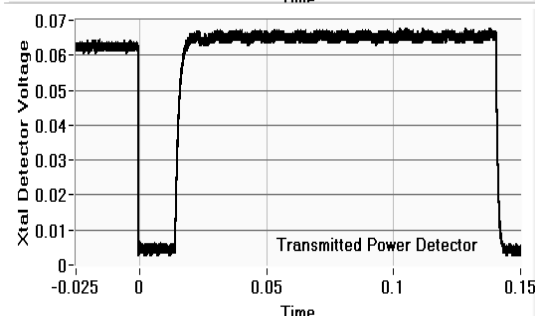
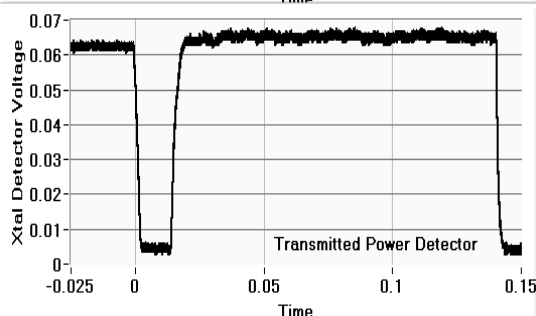
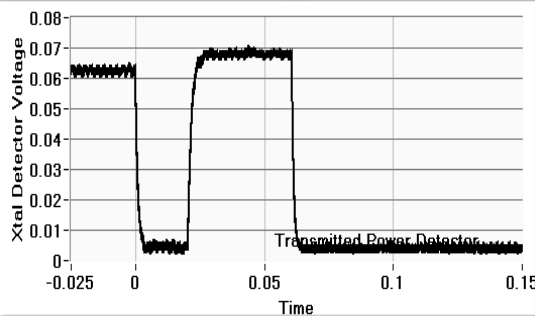
Pulse following  
"Electronic Quench"

# Frequency Shift Measurements at 7.7 MV/m

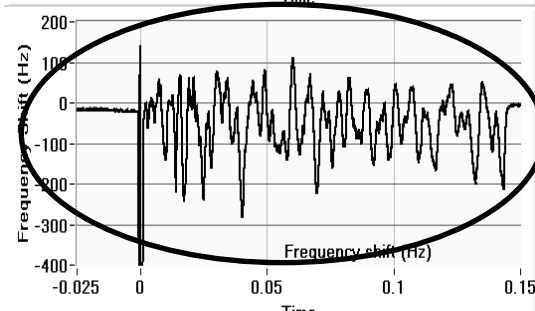
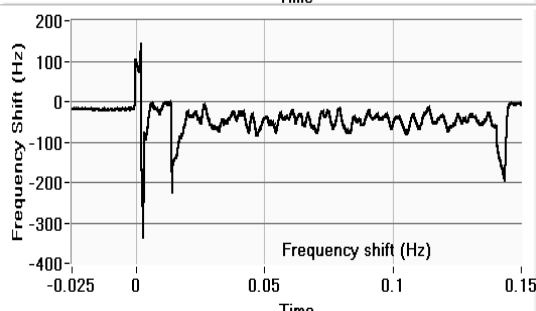
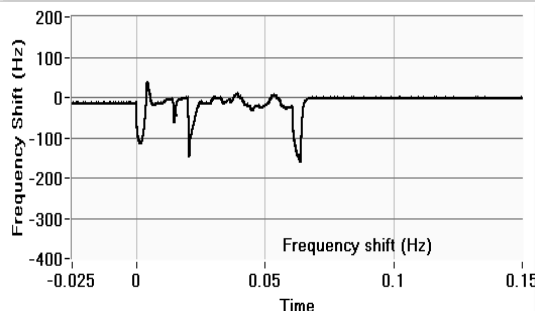
Forward Power



Transmitted Power (Gradient)



Frequency Shift



Normal Pulse  
(no event)

Pulse following  
Waveguide Arc

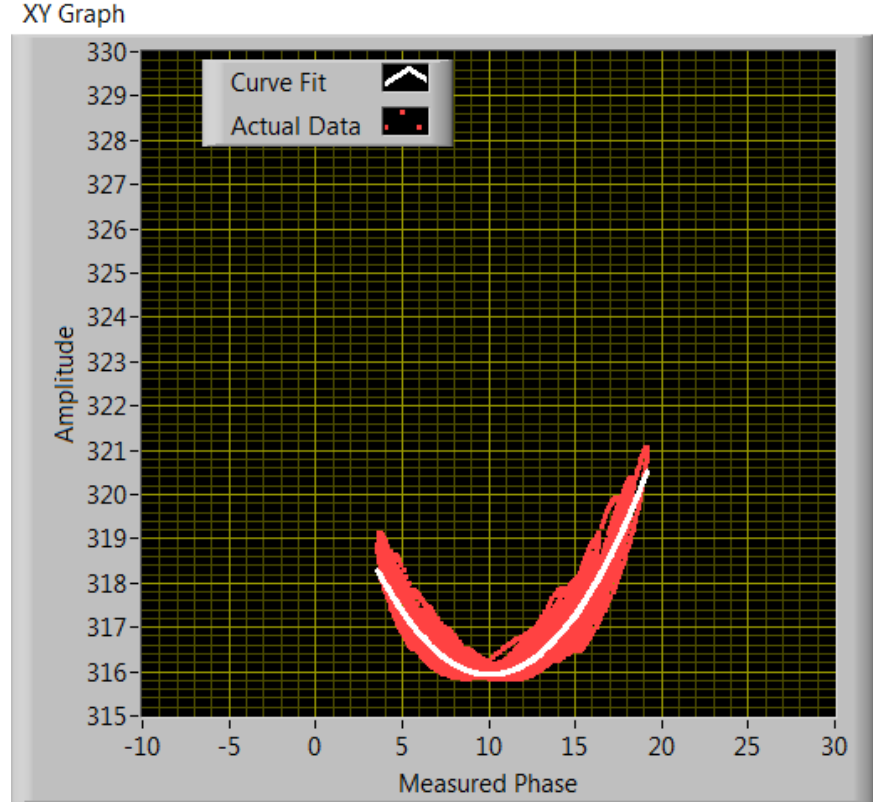
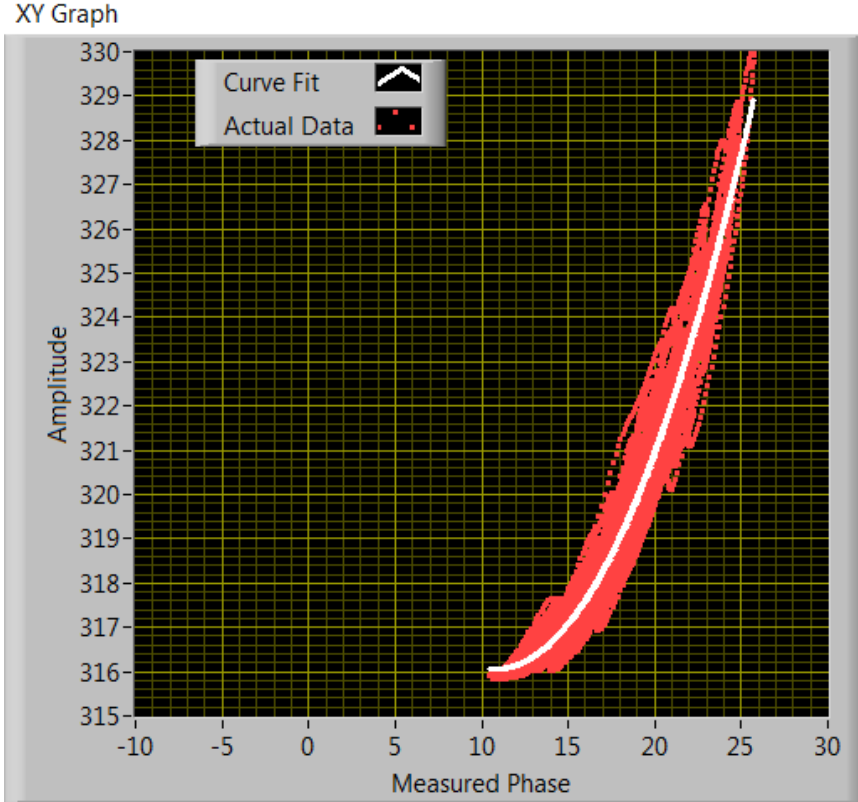
Pulse following  
“Electronic Quench”

# Backup Slides

# Automatically Determining TPOFF

- Using a digital LLRF system one can record the forward RF voltage (magnitude of the I/Q signal) and the difference between the transmitted power phase and the forward power phase for several seconds.
- The microphonics noise in the system will introduce spread in the data.
- If a second order fit (X value is the phase difference and the Y value is the RF voltage) is applied to the data the minimum will occur when  $TPES = TPOFF$ .
- This process is valid in GDR mode both with and without CW beam.
- It not valid during pulsed beam operation.

# Maintaining Proper Value of TPOFF



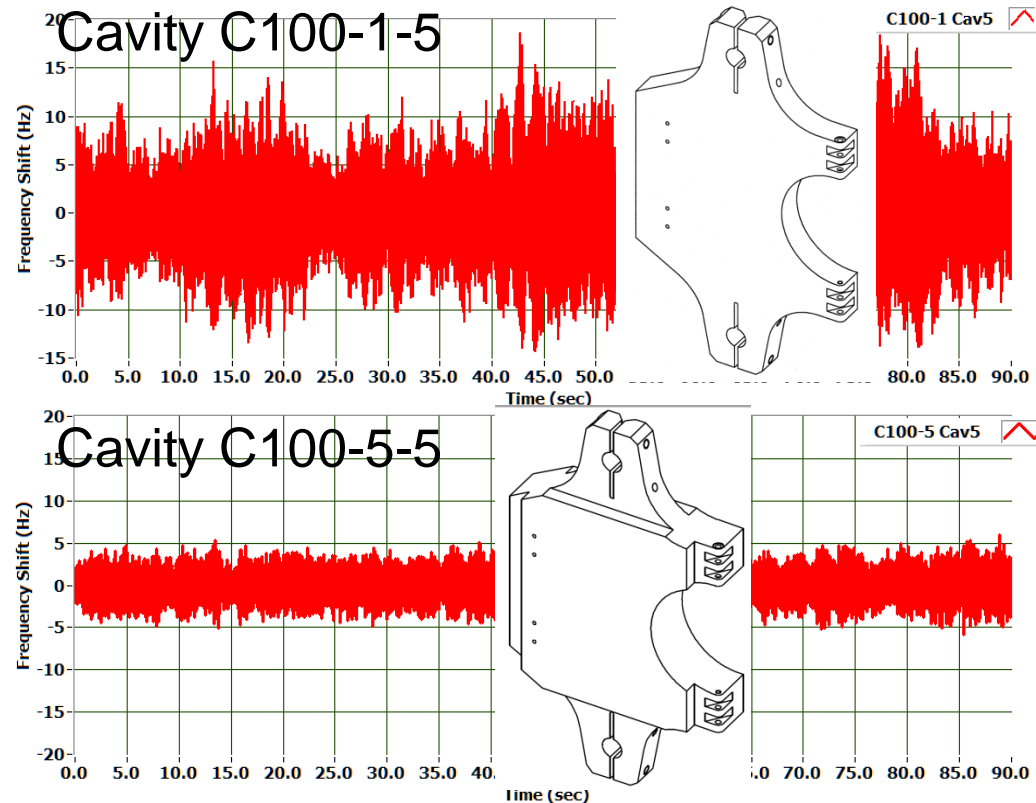
**Curve fitting for measured microphonics data with a peak to peak value of 15 Hz and a cavity that off resonance with a detune offset of  $10^\circ$  and (right) curve fitting for measured microphonics data with a peak to peak value of 15 Hz and a cavity that is close to on resonance. In both cases the data indicates that the proper detune offset is approximately  $10^\circ$ .**



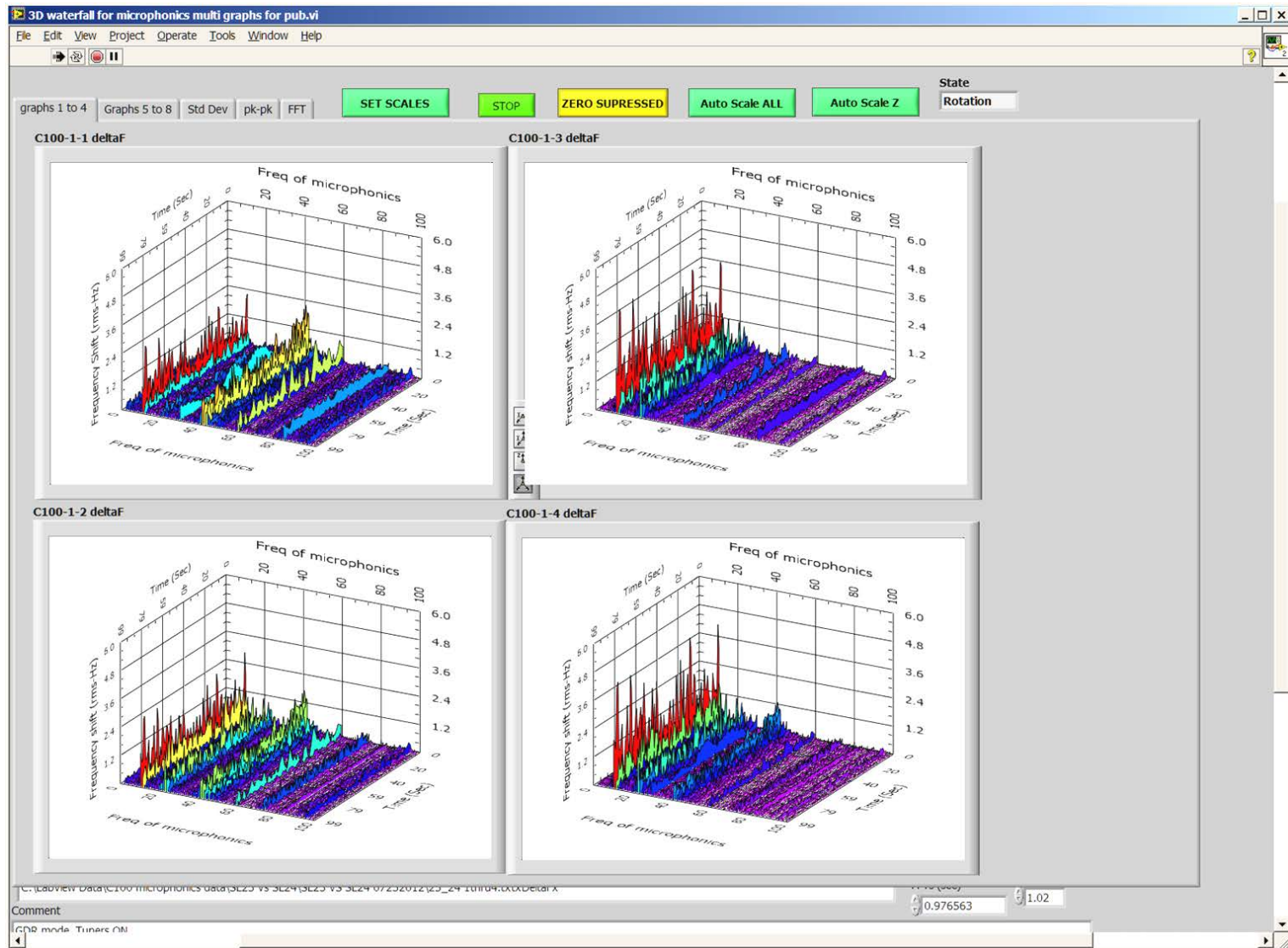
# C100 Cryomodule Fix

- Design allows for 25 Hz Peak Detuning
- Actual peak detuning (**21 Hz**) was higher than expected in first cryomodules
- A detailed vibration study was initiating which led to the following design change.
- A minor change to the **tuner pivot** plate substantially improved the microphonics for the CEBAF C100 Cryomodules.
- While both designs meet the overall system requirements the improved design has a larger RF power margin

Microphonic Detuning*	C100-1	C100-4
RMS (Hz)	2.985	1.524
6 $\sigma$ (Hz)	17.91	9.14

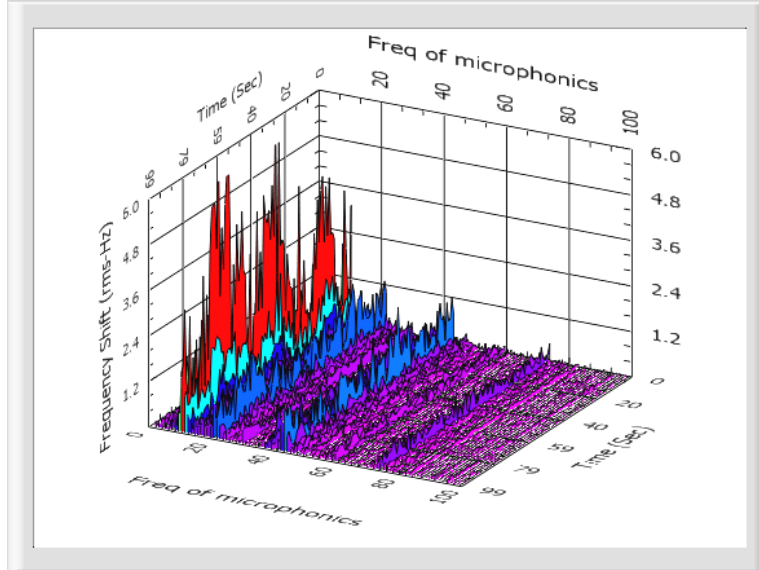


# C100-1 Microphonics

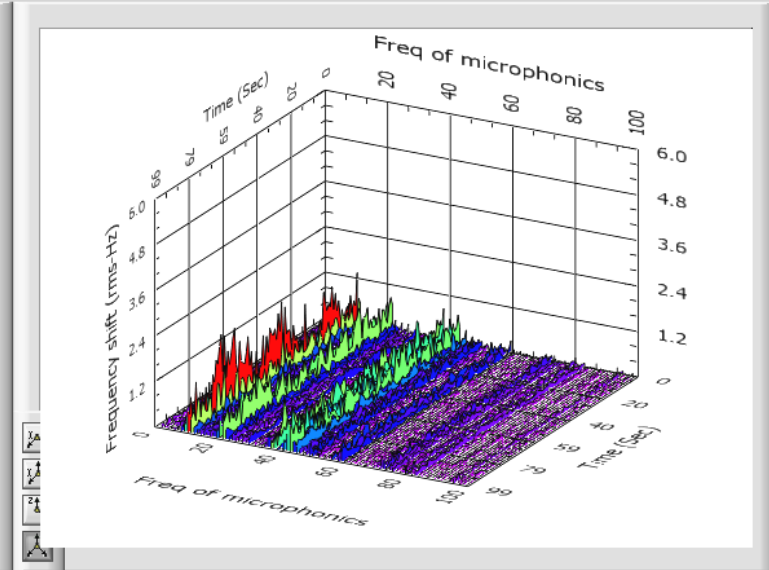


# C100-1 Microphonics

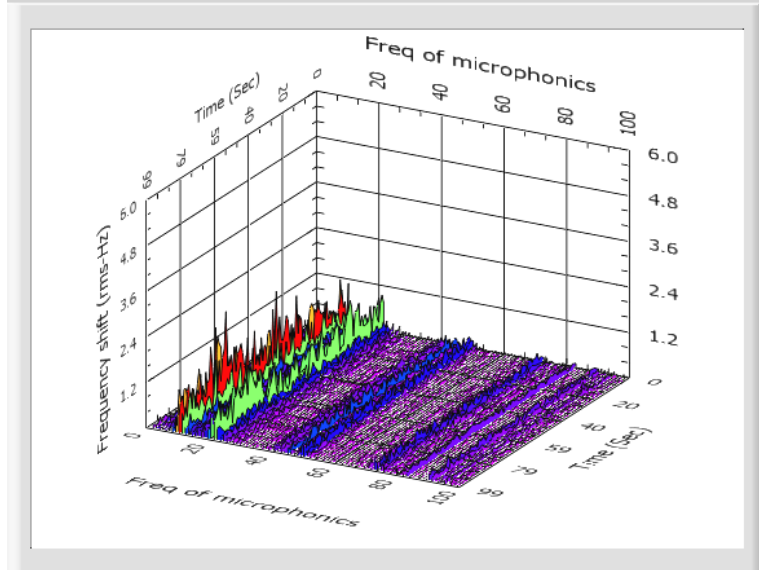
C100-1-5 deltaF



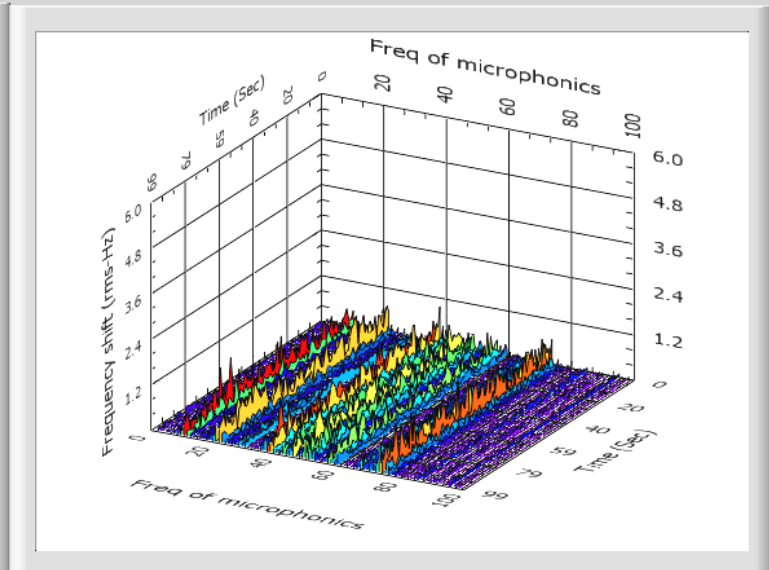
C100-1-7 deltaF



C100-1-6 deltaF

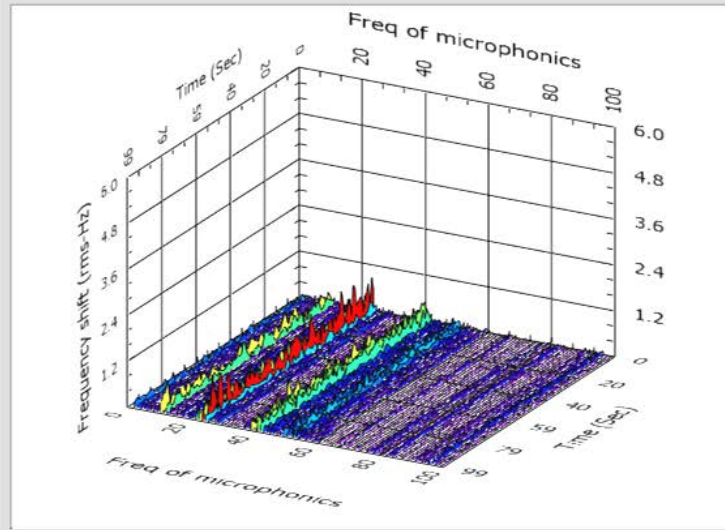


C100-1-8 deltaF

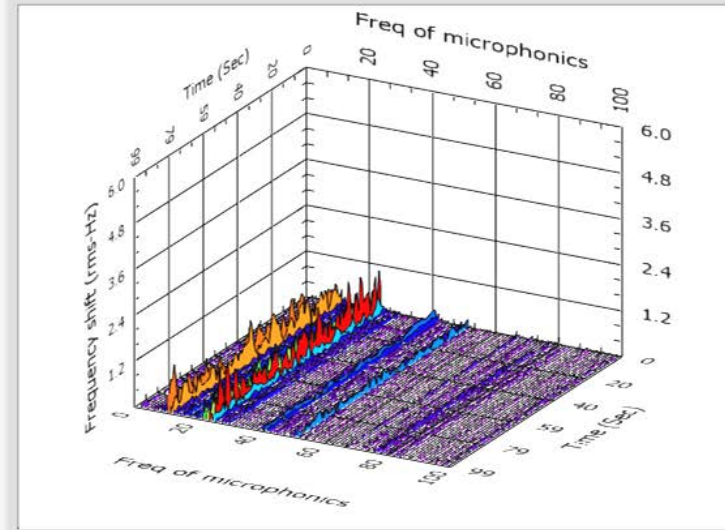


# C100-5 Microphonics

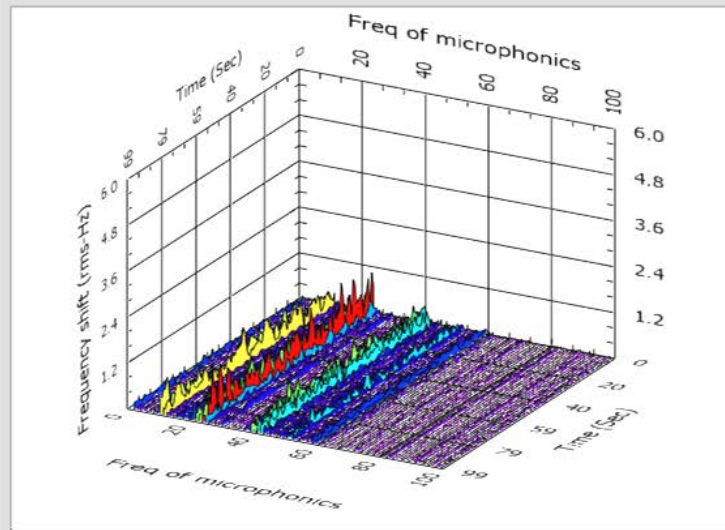
C100-5-1 deltaF



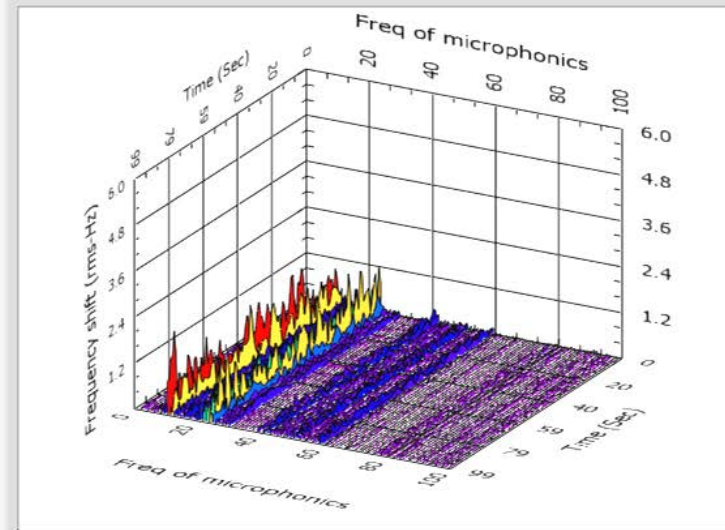
C100-5-3 deltaF



C100-5-2 deltaF

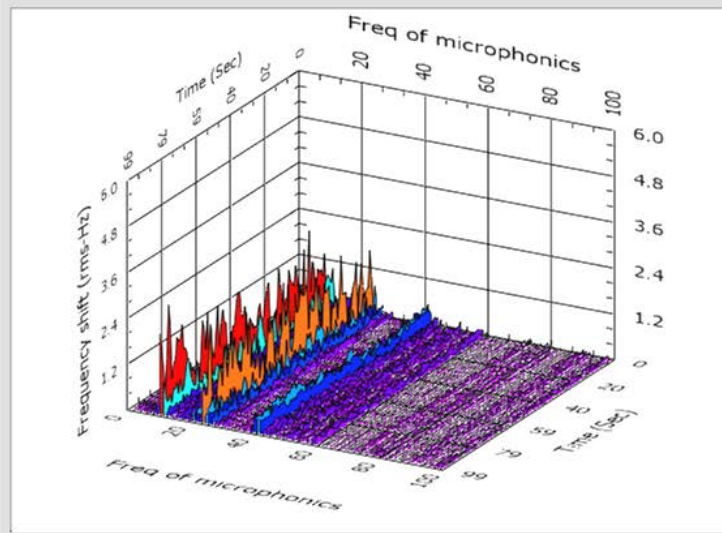


C100-5-4 deltaF

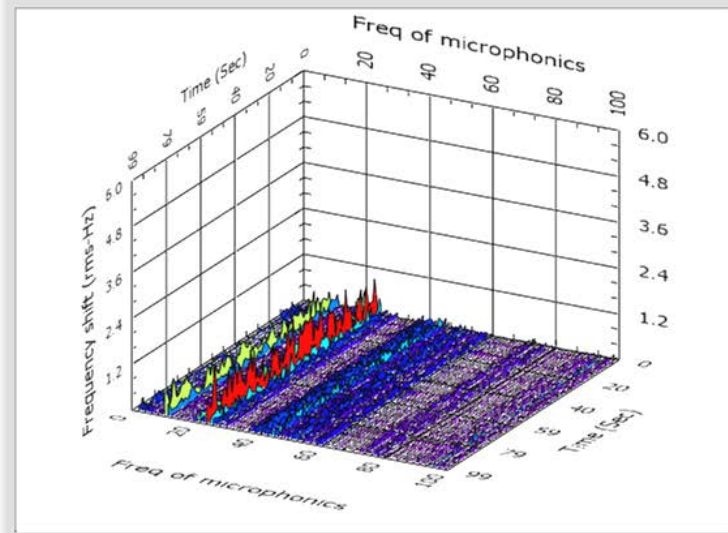


# C100-5 Microphonics

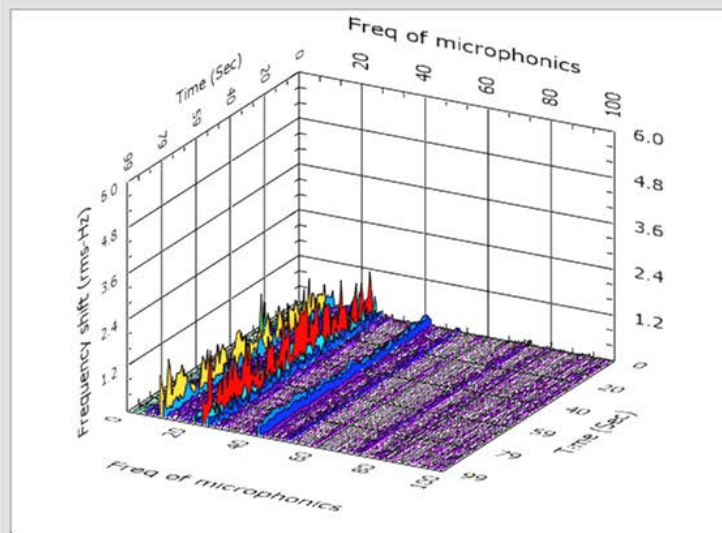
C100-5-5 deltaF



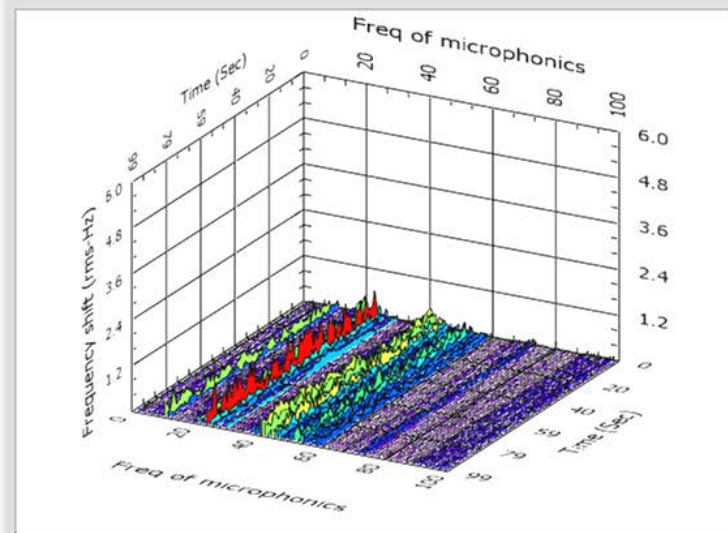
C100-5-7 deltaF



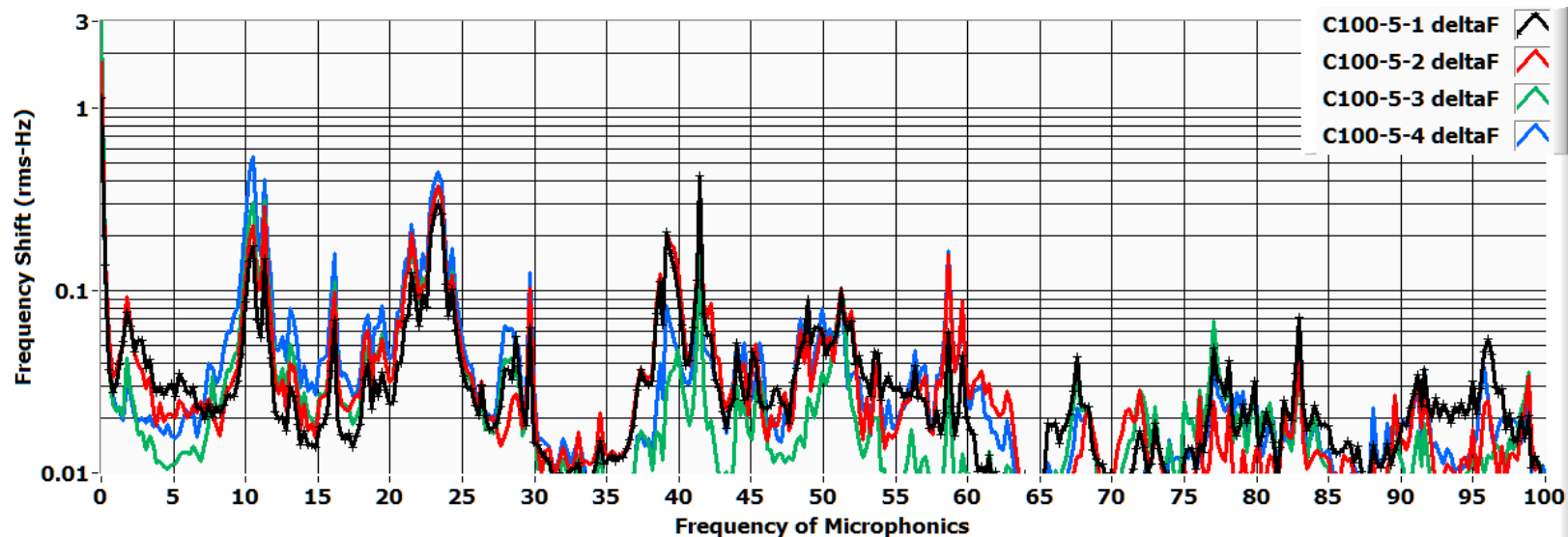
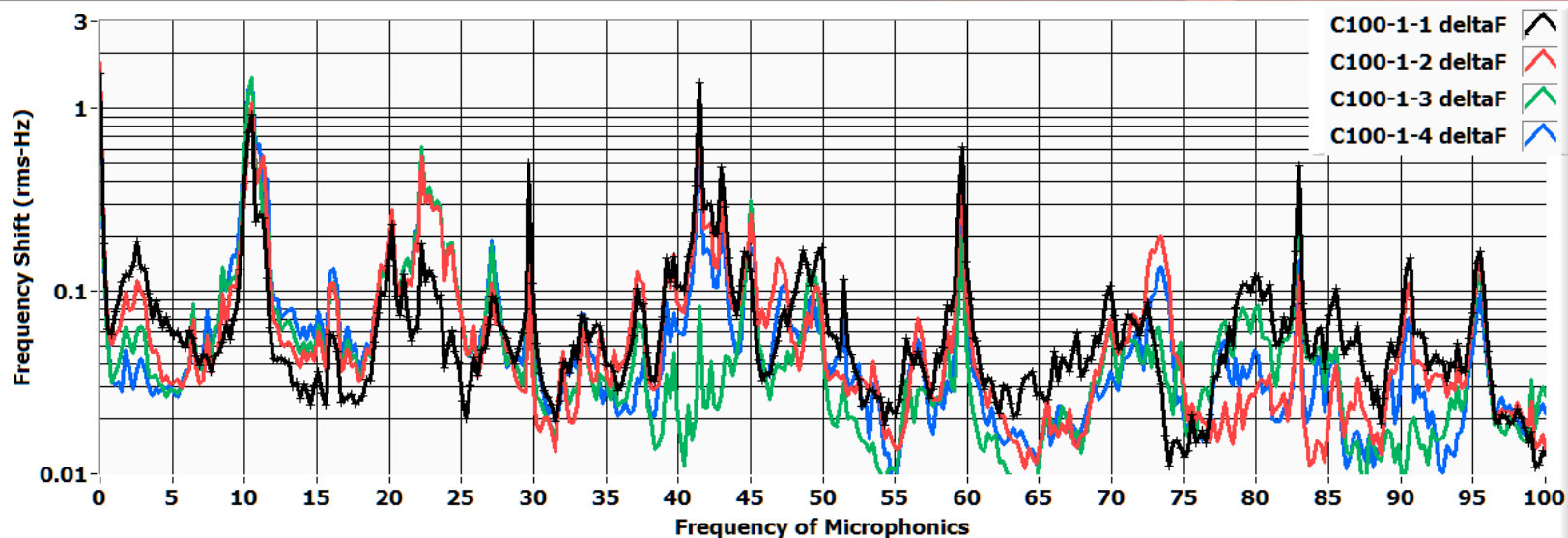
C100-5-6 deltaF



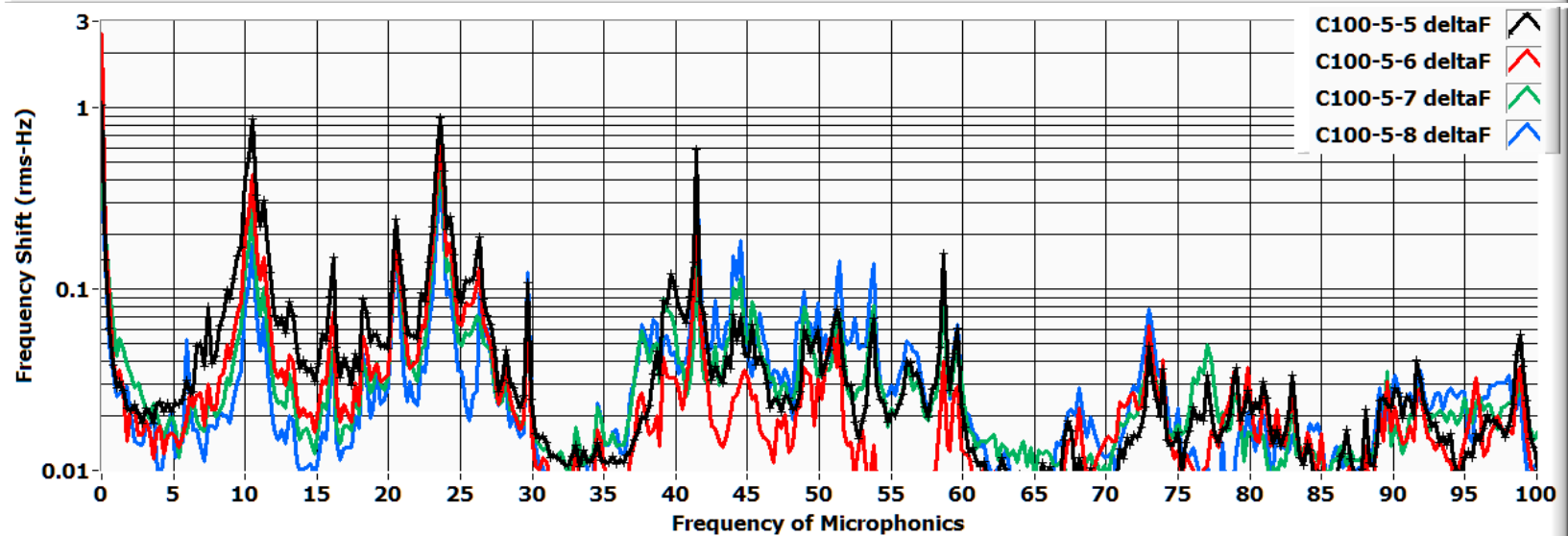
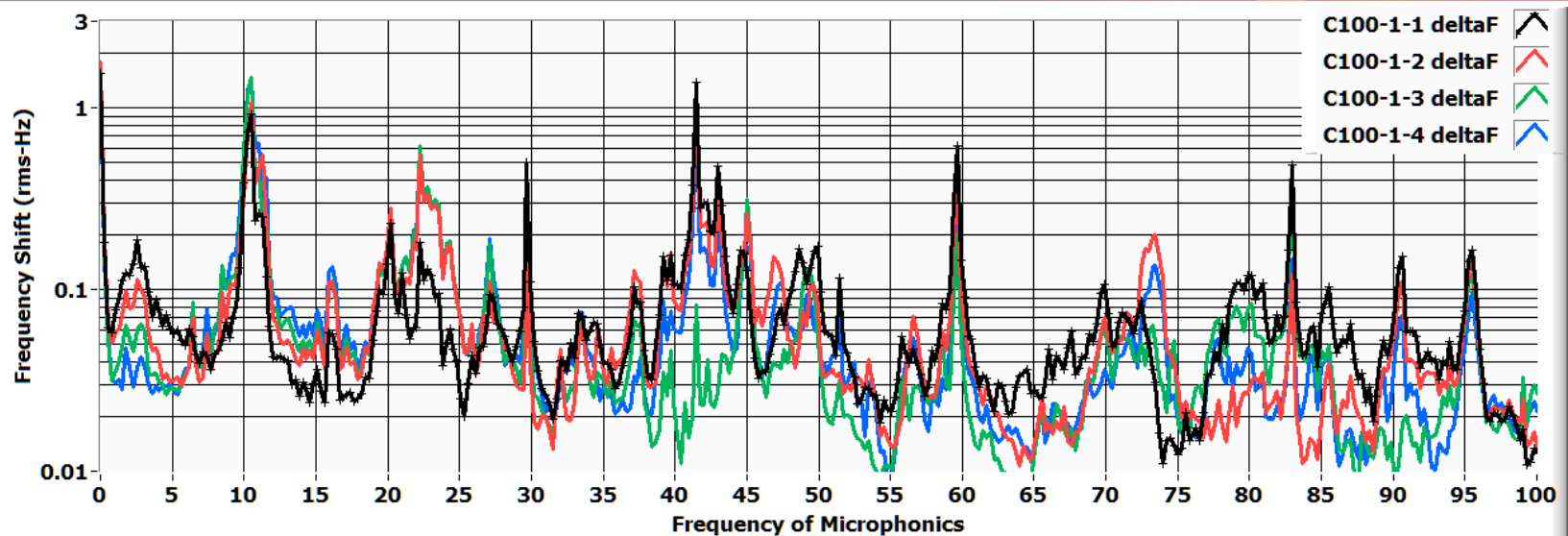
C100-5-8 deltaF



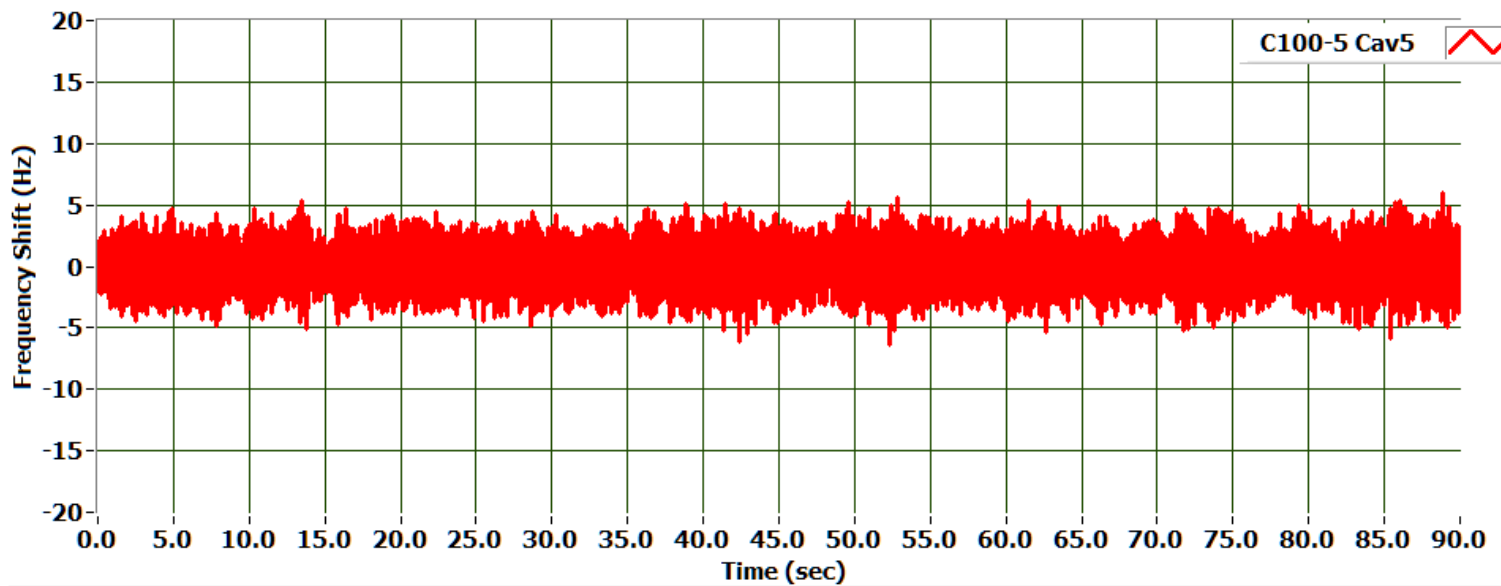
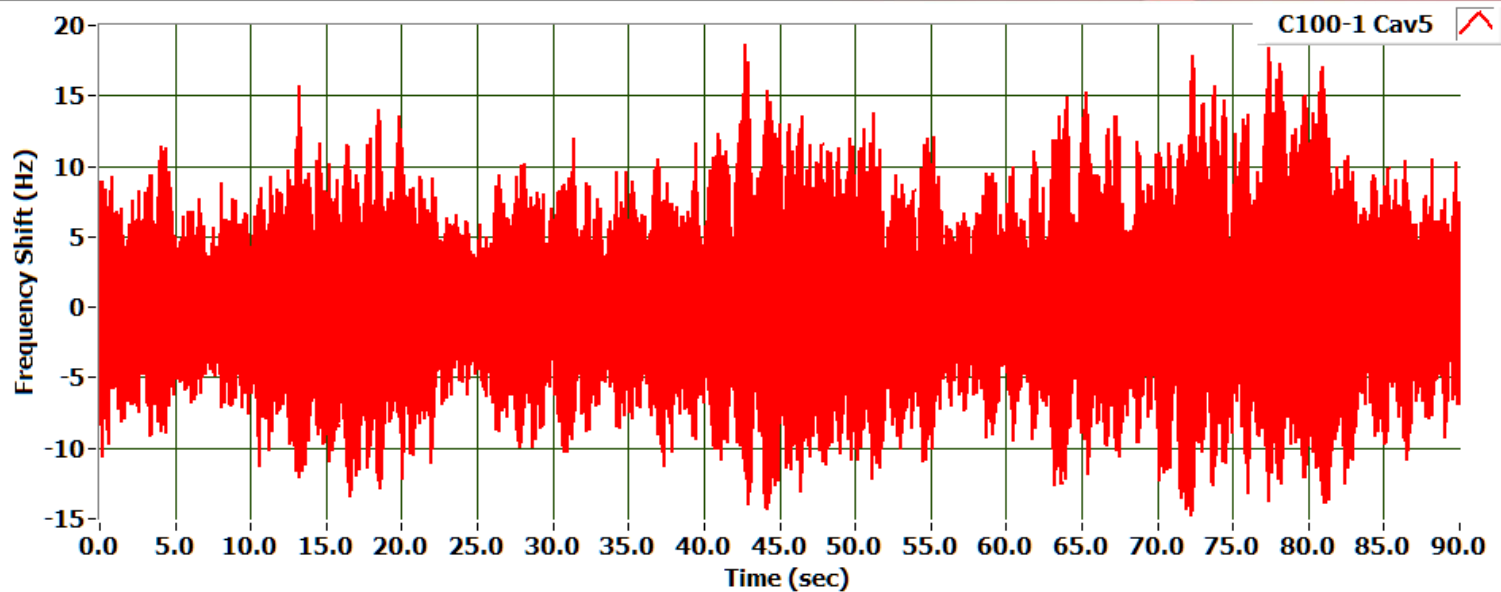
# Background spectrum for Original (C100-1) and Stiffened (C100-5)



# Background spectrum for Original (C100-1) and Stiffened (C100-5)



# Background Time Domain for Original (C100-1) and Stiffened (C100-5)





# Background spectrum for Original (C100-1) and Stiffened (C100-5)

