

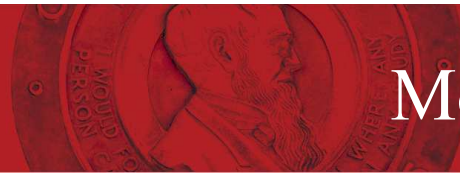
Determination of Magnetic Axis in a Sextupole magnet using Vibrating Wire Technique*

Alexander Temnykh* and Animesh Jain⁺

*Cornell University, Ithaca, New York 14850, USA

+Brookhaven National Laboratory, Upton, New York 11973-5000, USA

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- Work was motivated by NSLS-II project requirement of precise alignment of a string of quadrupole and sextupole magnets on a ~ 6 m long girder within a tight tolerance of ± 10 - 20 microns.
- Similar requirement is anticipated for ILC damping ring.



- Sextupole magnetic field:

$$B_y(x, y) = b_3(x^2 - y^2); \quad B_x(x, y) = -2b_3xy$$

- Horizontal scan:

$$B_y(x, y = y_{off}) = b_3x^2 - b_3y_{off}^2; \quad B_x(x, y) = -2b_3xy_{off}$$

- Vertical scan:

$$B_y(x_{off}, y) = -b_3y^2 + b_3x_{off}^2; \quad B_x(x, y) = -2b_3x_{off}y$$

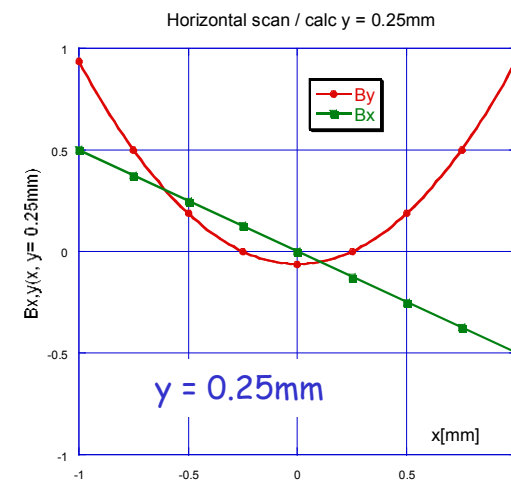
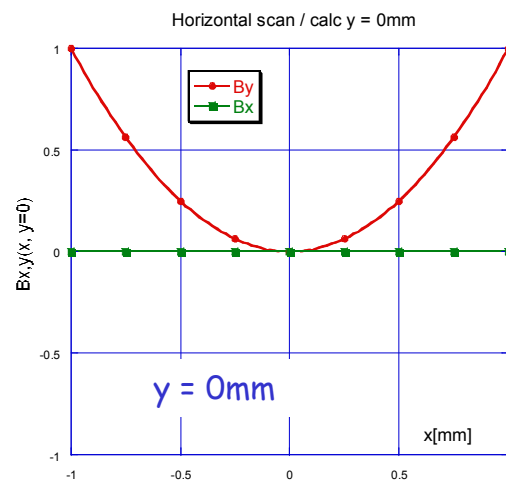
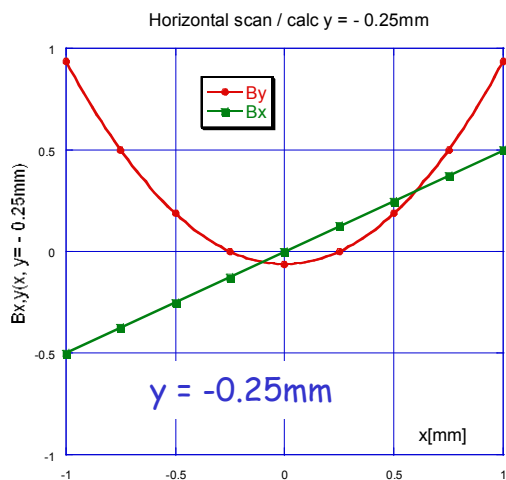
- The term which couples horizontal to vertical beam particles motion:

$$a_2(y_{off}) = \frac{\partial B_x(x, y_{off})}{\partial x} = -2b_3y_{off}$$

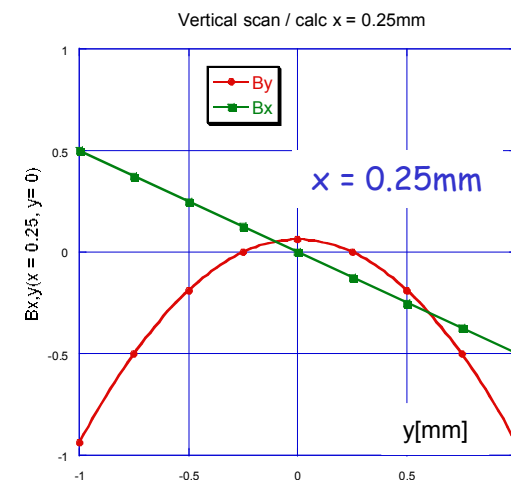
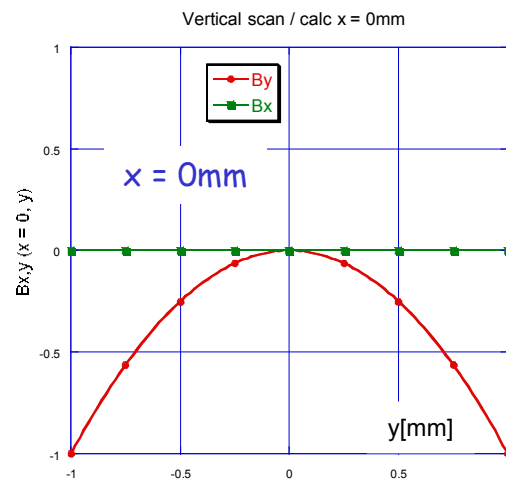
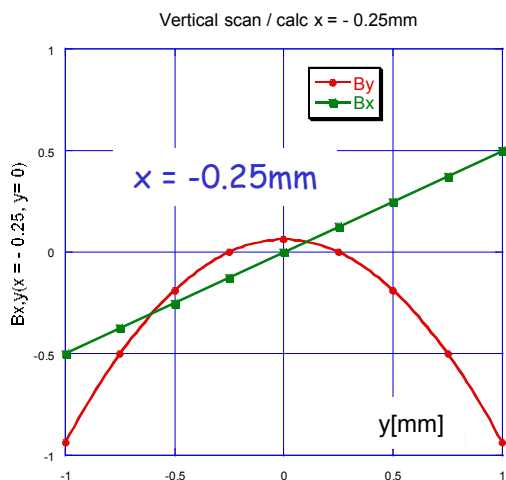


Sextupole magnet field properties

Horizontal
scan



Vertical
scan





- Algorithm for magnetic center finding from **horizontal scan**:

$B_{x,y}(x)$ - horizontal and vertical field components measured as a function of horizontal position.

$$B_y(x) = m_2 x^2 + m_1 x + m_0 = b_3 (x - x_c)^2 - b_3 y_c^2;$$

$$B_x(x) = n_1 x + n_0 = 2b_3 x y_c;$$

$$x_c = -\frac{m_1}{2m_2}; \quad y_c = \frac{n_1}{2m_2}$$



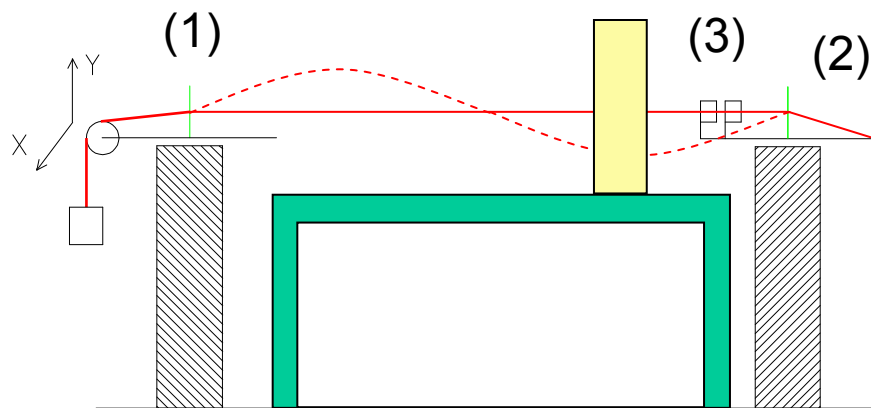
- Algorithm for magnetic center finding from the **vertical scan**:

$B_{x,y}(x)$ - horizontal and vertical field components measured as a function of vertical position.

$$B_y(x) = m_2 y^2 + m_1 y + m_0 = b_3 x_c^2 - b_3 (y - y_c)^2;$$

$$B_x(x) = n_1 y + n_0 = 2b_3 x_c y;$$

$$x_c = -\frac{n_1}{2m_2}; \quad y_c = -\frac{m_1}{2m_2}$$



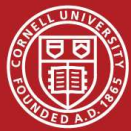
Vibrating Wire:
Length $\sim 2200\text{mm}$
Driving current $\sim 60\text{mA (RMS)}$
Fundamental freq $\sim 47\text{Hz}$
For measurement used 2-nd vibrating mode

- (1) Stage with tension mechanism
- (2) Stage with wire position sensors
- (3) Horizontal and vertical wire position sensors (LED-Phototransistor assemblies)



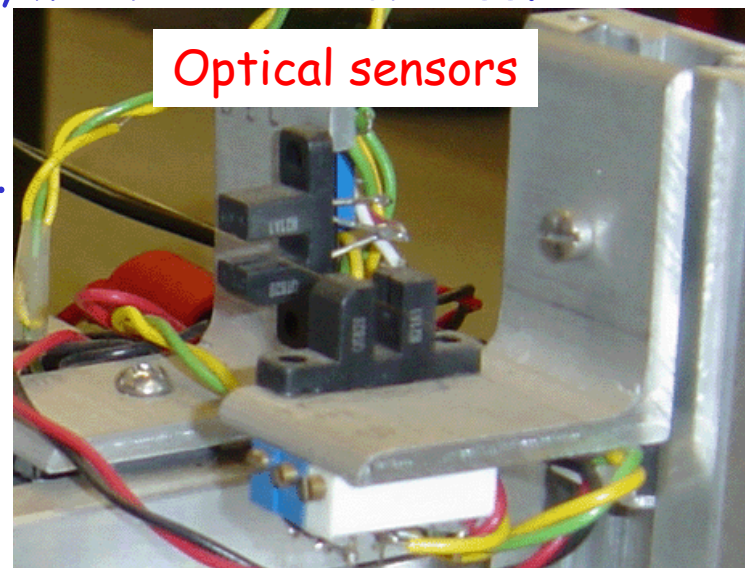
Sextupole magnet

$b_3l \sim 10.9\text{Gm/cm}^2$
Length $\sim 24\text{cm}$
Bore radius $\sim 5.5\text{cm}$



Experimental Setup

- In the VW technique the wire motion in vertical (horizontal) plane caused by the Lorentz forces between current flowing through the wire and horizontal (vertical) magnetic field.
- To separate horizontal and vertical field components measurement one should measure the wire motion in vertical and horizontal planes.
- The used assembly of the optical sensors show $\sim 10\%$ coupling between vertical and horizontal wire motion, we need $\sim 1\%$ or less.
- In a sextupole magnet, a X-Y coupling has the same effect as a roll of the magnet.
- Solution - assembly should be calibrated.





Optical wire position sensors calibration/decoupling procedure

- Stage (1) has been used for precise wire displacement (horizontal and vertical) at optical sensors and the sensors responses was measured.

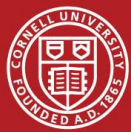
$dS_{x,y}$ - horizontal/vertical sensor responses in Volts

dx_w, dy_w - horizontal and vertical wire displacement in mm

$$\begin{pmatrix} dS_x \\ dS_y \end{pmatrix} = M \begin{pmatrix} dx_w \\ dy_w \end{pmatrix}; \quad M = \begin{pmatrix} 1.43 & 0.116 \\ -0.045 & 1.32 \end{pmatrix}$$

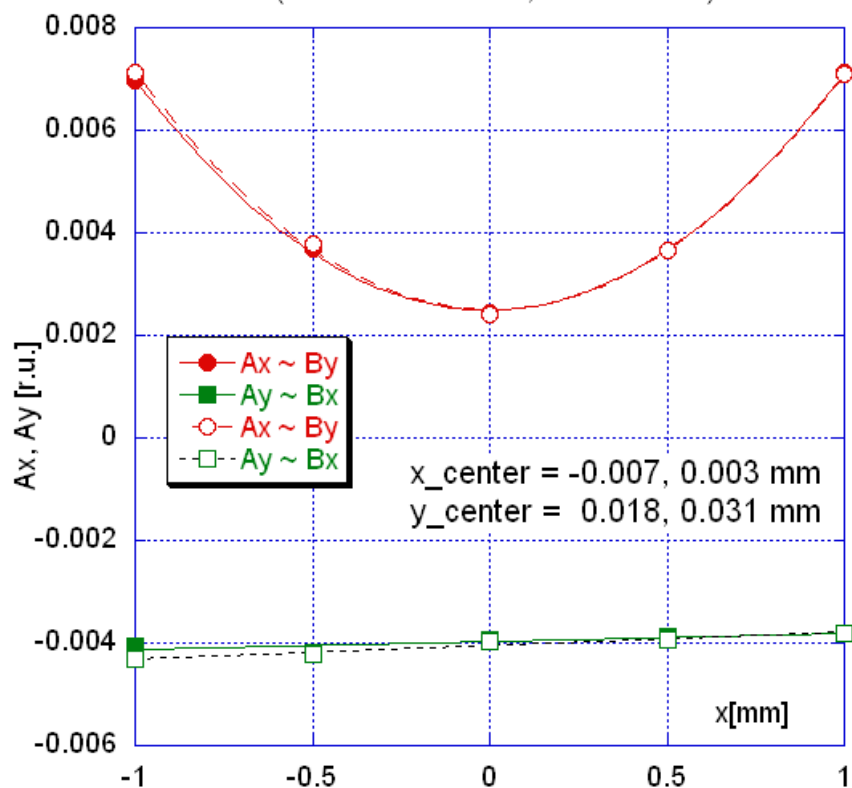
- In the course of measurement the sensor signals were converted to the wire displacement:

$$\begin{pmatrix} dx_w \\ dy_w \end{pmatrix} = M^{-1} \begin{pmatrix} dS_x \\ dS_y \end{pmatrix} = \begin{pmatrix} 0.697 & -0.061 \\ 0.024 & 0.755 \end{pmatrix} \begin{pmatrix} dS_x \\ dS_y \end{pmatrix}$$

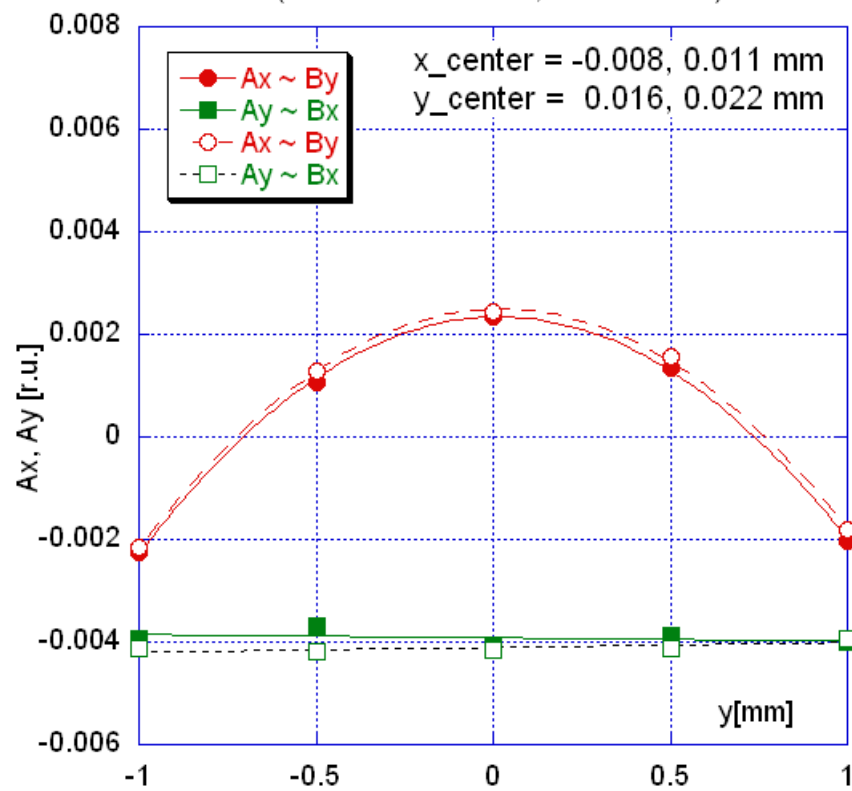


Horizontal and vertical scans near sextupole magnetic center

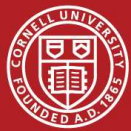
VW scan in **horizontal** plane near $y=0$
(files: hor scan 15,16 07/26/07)



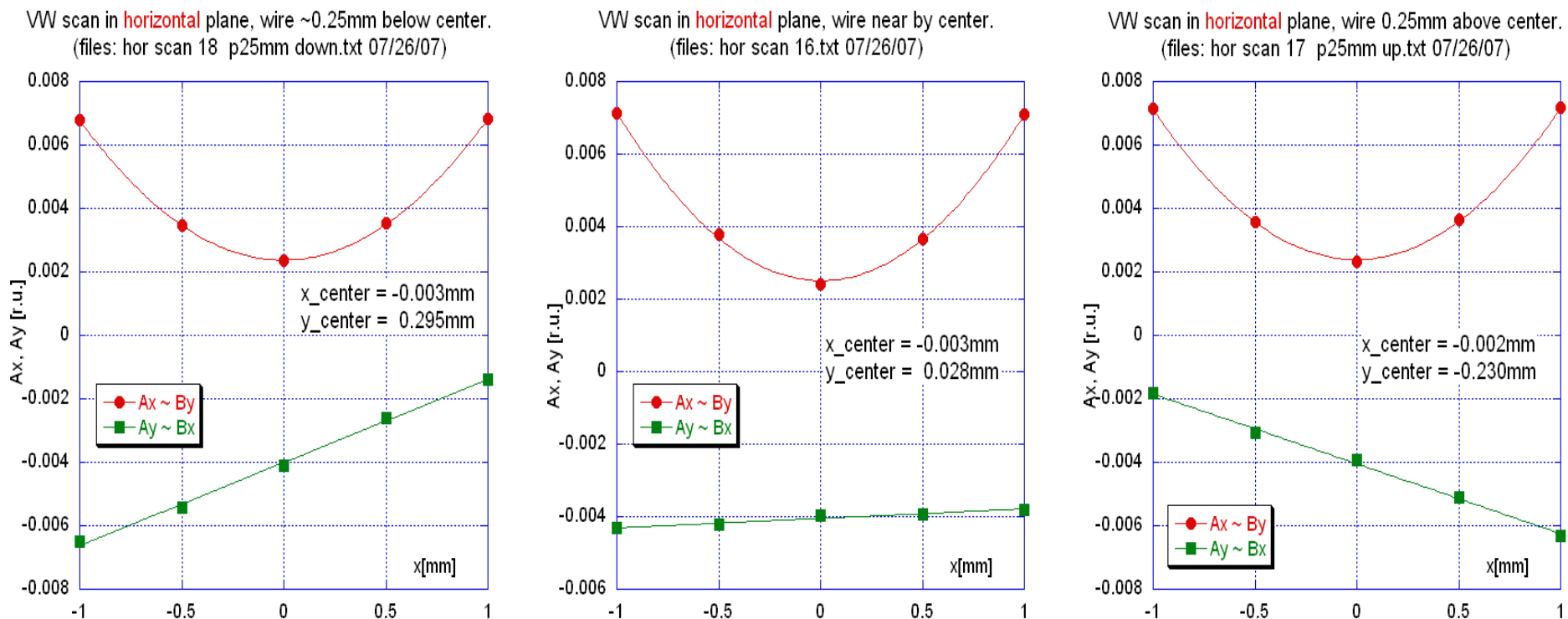
VW scan in **vertical** plane near $x = 0$
(files: vert scan 12,14 07/26/07)



Two independent runs are shown



Horizontal scans at different vertical position

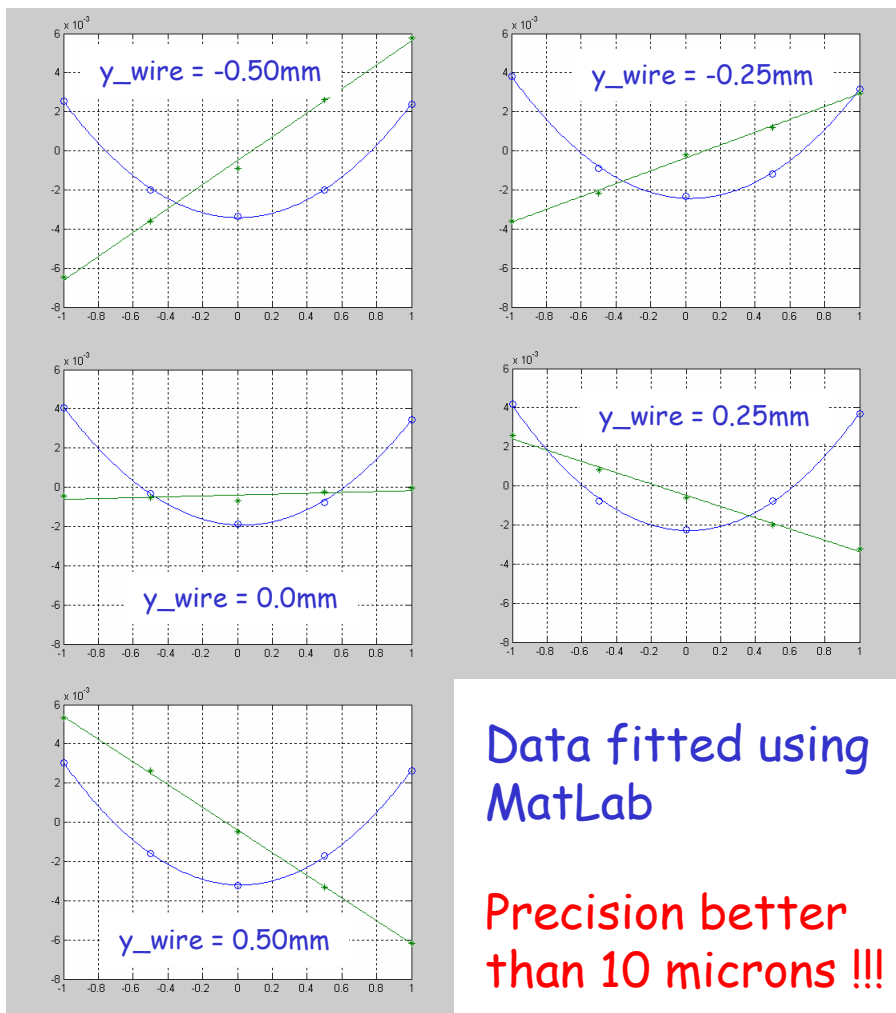


It is well consisted with theoretical prediction



Experimental results

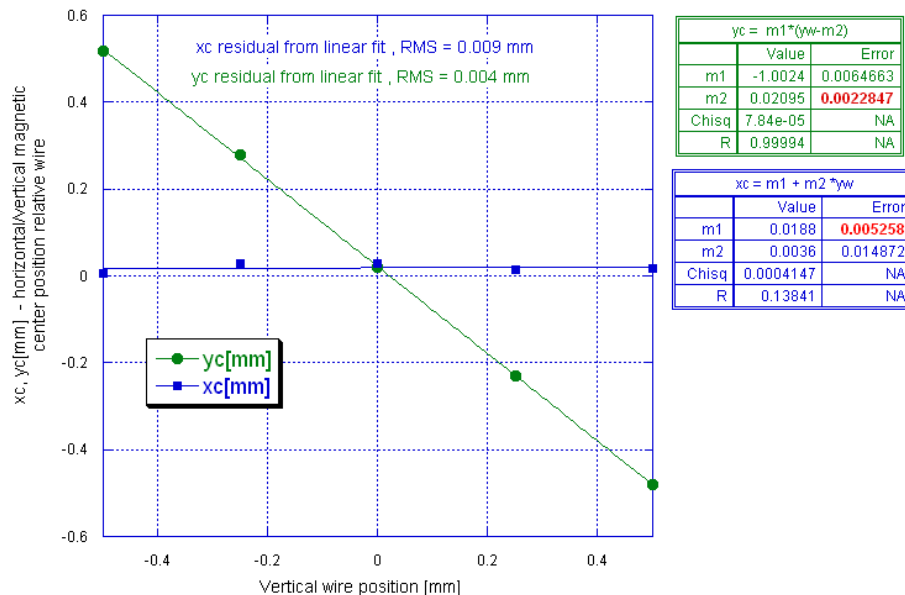
Precision test: Horizontal scans at different vertical position



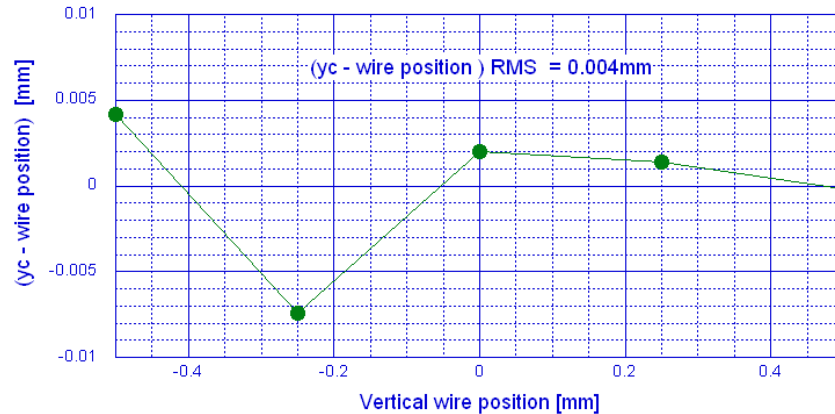
Data fitted using
MatLab

Precision better
than 10 microns !!!

Sextupole magnetic center position relative wire as a function of the vertical wire position, files: hor scan (15, ... 19) 5/7/07



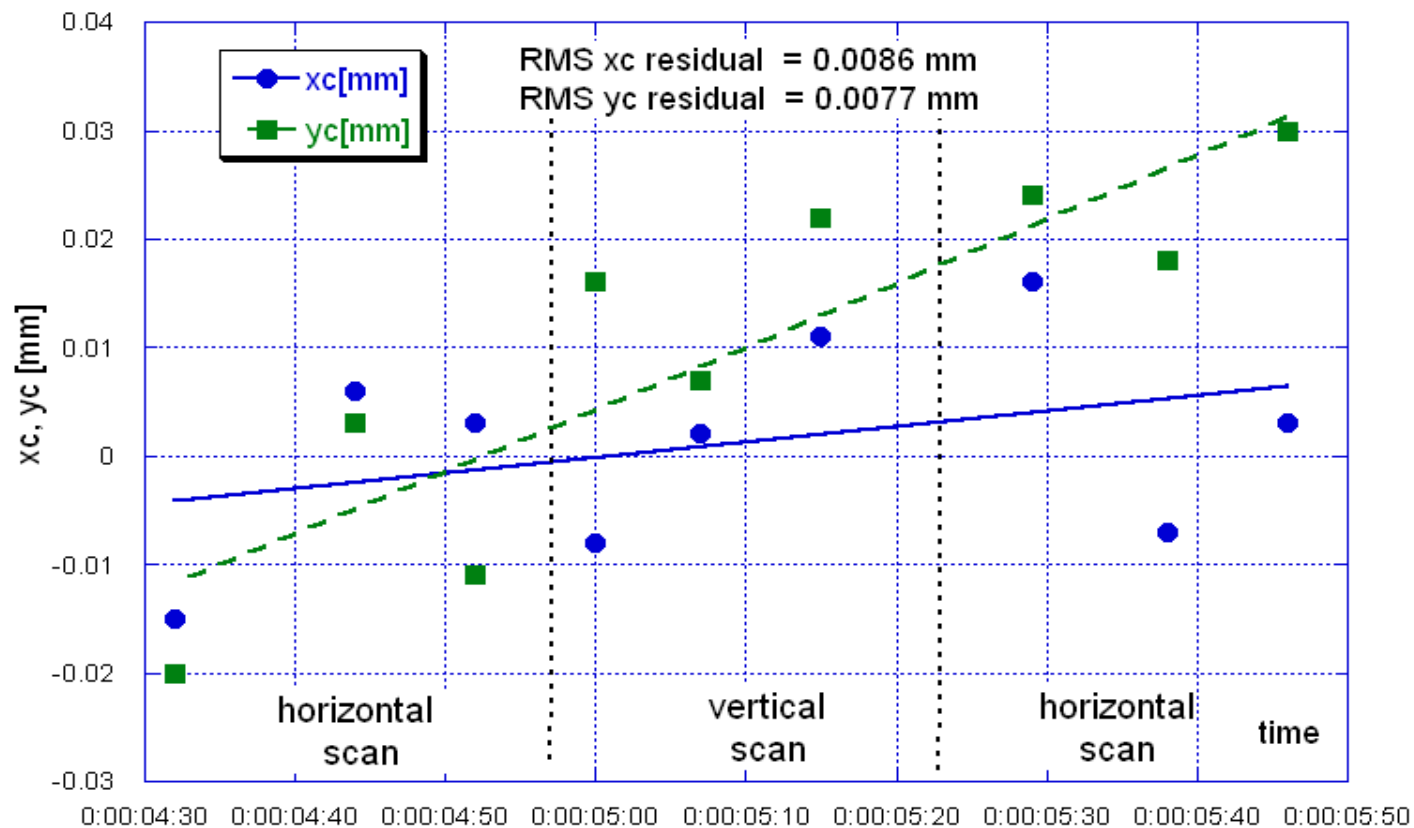
Sextupole center vertical position in the frame coupled with magnet





Stability test

Sextupole magnet magnetic center
measurement statistics, st 07/26/07



Position drift: vertical plane ~ 35 micron per hour
horizontal plane ~ 5 micron per hour



Sextupole magnet magnetic axes finding in the presence of the field errors

\tilde{b}_i, \tilde{a}_i - field errors, R - reference radius

$$B_y + iB_x = (\tilde{b}_1 + i\tilde{a}_1) + (\tilde{b}_2 + i\tilde{a}_2) \left(\frac{x+iy}{R} \right) + (b_3 + i\tilde{a}_3) \left(\frac{x+iy}{R} \right)^2$$

$$B_y = \tilde{b}_1 + \frac{\tilde{b}_2 x - \tilde{a}_2 y}{R} + b_3 \frac{x^2 - y^2}{R^2} - \tilde{a}_3 \frac{2xy}{R^2};$$

$$B_x = \tilde{a}_1 + \frac{\tilde{a}_2 x + \tilde{b}_2 y}{R} + b_3 \frac{2xy}{R^2} + \tilde{a}_3 \frac{x^2 - y^2}{R^2};$$

Magnetic center position from B_y measurement

(extrim in quadratic fit):

a) x_c from horizontal scan, \tilde{y} – wire position in vertical plane.

$$\frac{\partial B_y}{\partial x} = \frac{\tilde{b}_2}{R} + b_3 \frac{2x_c}{R^2} - \tilde{a}_3 \frac{2\tilde{y}}{R^2} = 0 \Rightarrow$$

$$x_c = -\frac{\tilde{b}_2}{2b_3} R + \frac{\tilde{a}_3}{b_3} \tilde{y} \approx -\frac{\tilde{b}_2}{2b_3} R$$

b) y_c from vertical scan, \tilde{x} – wire position in vertical plane.

$$\frac{\partial B_y}{\partial y} = -\frac{\tilde{a}_2}{R} - b_3 \frac{2y_c}{R^2} - \tilde{a}_3 \frac{2\tilde{x}}{R^2} = 0 \Rightarrow$$

$$y_c = -\frac{\tilde{a}_2}{2b_3} R - \frac{\tilde{a}_3}{b_3} \tilde{x} \approx -\frac{\tilde{a}_2}{2b_3} R$$

Magnetic center position from B_x measurement

("zero" sloop):

a) x_c from vertical scan, \tilde{y} – averaged vertical wire position (small).

$$\frac{\partial B_x}{\partial y} = \frac{\tilde{b}_2}{R} + b_3 \frac{2x_c}{R^2} - \tilde{a}_3 \frac{2\tilde{y}}{R^2} = 0 \Rightarrow$$

$$x_c = -\frac{\tilde{b}_2}{2b_3} R + \frac{\tilde{a}_3}{b_3} \tilde{y} \approx -\frac{\tilde{b}_2}{2b_3} R$$

b) y_c from horizontal scan, \tilde{x} – averaged horizontal wire position (small)

$$\frac{\partial B_x}{\partial x} = \frac{\tilde{a}_2}{R} + b_3 \frac{2y_c}{R^2} + \tilde{a}_3 \frac{2\tilde{x}}{R^2} = 0 \Rightarrow$$

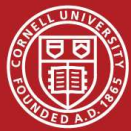
$$y_c = -\frac{\tilde{a}_2}{2b_3} R - \frac{\tilde{a}_3}{b_3} \tilde{x} \approx -\frac{\tilde{a}_2}{2b_3} R$$

Conclusion:

Both methods should give the same results. It can be used for cross checking.



- Vibrating wire technique has been applied to sextupole magnet magnetic axes finding.
- Demonstrated precision, ~ 10 microns, is adequate to the alignment requirement of NSLS - II project and, very likely, of ILC damping ring.



The field error effect

Sextupole magnet magnetic axes in the presence of the field errors

5/23/07

General case, including mixed terms; 5/23/07 (6)

$$(By + iBx) = (B_1 + iA_1) + (B_2 + iA_2) \left(\frac{x + iy}{R_{ref}} \right) + (B_3 + iA_3) \left(\frac{x + iy}{R_{ref}} \right)^2$$

$$B_y = B_1 + (B_2 x - A_2 y) / R_{ref} + B_3 \left(\frac{x^2 - y^2}{R_{ref}^2} \right) - 2A_3 \left(\frac{xy}{R_{ref}^2} \right)$$

$$B_x = A_1 + (A_2 x + B_2 y) / R_{ref} + B_3 \left(\frac{2xy}{R_{ref}^2} \right) + A_3 \left(\frac{x^2 - y^2}{R_{ref}^2} \right)$$

The "center" is defined as a point where B_2 & A_2 terms are zero:

$$B_2 + iA_2' = (B_2 + iA_2) + 2 \left(\frac{x_c + iy_c}{R_{ref}} \right) (B_3 + iA_3) = 0$$

$$x_c + iy_c = - \frac{(B_2 + iA_2) R_{ref}}{2(B_3 + iA_3)}$$

$$x_c = - \frac{B_2 B_3 + A_2 A_3}{2(B_3^2 + A_3^2)} R_{ref}$$

$$y_c = - \frac{A_2 B_3 - B_2 A_3}{2(B_3^2 + A_3^2)} R_{ref}$$

if $A_3 = 0$, $x_c = -\frac{1}{2} (B_2/B_3) R_{ref}$; $y_c = \frac{1}{2} (A_2/B_3) R_{ref}$

$$\left. \frac{dB_y}{dx} \right|_{y=y_0} = \frac{B_2}{R_{ref}} + 2B_3 \frac{x}{R_{ref}} - 2A_3 y_0 / R_{ref}^2$$

$$dB_y/dx = 0 \text{ at } x'_c = - \left[\frac{B_2 + 2A_3 (y_0/R_{ref})}{2B_3} \right] R_{ref}$$

neglecting A_3^2 in comparison to B_3^2 , $x_c \approx \left[-\frac{1}{2} (B_2/B_3) - \frac{1}{2} \left(\frac{A_2 A_3}{B_3^2} \right) \right] R_{ref}$

$$\therefore \text{error in } x_c = \Delta x_c \approx \left[+ \left(\frac{A_3}{B_3} \right) \left(\frac{y_0}{R_{ref}} \right) + \frac{1}{2} \left(\frac{A_2}{B_3} \right) \left(\frac{A_3}{B_3} \right) \right] R_{ref}$$

$\therefore \frac{1}{2} A_2/B_3 \approx y_c/R_{ref}$

$$\Delta x_c \approx \left(\frac{A_3}{B_3} \right) (y_0 - y_c)$$

The error is minimized if
i) either $A_3 \approx 0$
or ii) $y_0 \approx y_c$; i.e. dB_y/dx is evaluated at $y \approx y_c$.

$$\left. \frac{dB_y}{dy} \right|_{x=x_0} = -A_2/R_{ref} - 2B_3 y/R_{ref}^2 - 2A_3 x_0/R_{ref}^2$$

This is zero at $y = y'_c = - \left(\frac{A_2 + 2A_3 (x_0/R_{ref})}{2B_3} \right) R_{ref}$

neglecting A_3^2 in comparison to B_3^2 , $y_c \approx \left[-\frac{1}{2} \left(\frac{A_2}{B_3} \right) + \frac{1}{2} \left(\frac{B_2}{B_3} \right) \left(\frac{A_3}{B_3} \right) \right] R_{ref}$

$$\approx \left[-\frac{1}{2} \left(\frac{A_2}{B_3} \right) - \left(\frac{x_c}{R_{ref}} \right) \left(\frac{A_3}{B_3} \right) \right] R_{ref}$$

\therefore Error in y_c is

$$\Delta y_c = y'_c - y_c = \left(\frac{A_3}{B_3} \right) (x_c - x_0)$$

once again, the error is negligible if either
i) $A_3 \approx 0$
or ii) $x_0 \approx x_c$; i.e. $\frac{dB_y}{dy}$ is evaluated at $x_0 \approx x_c$.

$$\left. \frac{dB_x}{dx} \right|_{y_0} = \frac{A_2}{R_{ref}} + 2B_3 y_0 / R_{ref}^2 + 2A_3 x / R_{ref}^2$$

it can be seen that $\left. \frac{dB_y}{dy} \right|_{x_0, y_0} = - \left. \frac{dB_x}{dx} \right|_{x_0, y_0}$, as expected.

dB_x/dx is zero at $x = A$ for a given y_0 , $\left(\frac{dB_x}{dx} \right)$ is not strictly constant (i.e. B_x is not linear with x) due to the A_3 term.

for $2A_3 x/R_{ref} \ll \frac{A_2}{R_{ref}} + 2B_3 y_0/R_{ref}^2$

$$x \ll \left(\frac{A_2}{2A_3} \right) R_{ref}$$

$$\left. \frac{dB_x}{dx} \right|_{y_0} = \frac{A_2}{R_{ref}^2} + 2B_3 y_0 / R_{ref}^2 \left[1 + \left(\frac{A_3}{B_3} \right) \left(\frac{x}{y_0} \right) \right]$$

This can be large, specially near $y_0 \approx 0$
 $\therefore y_0 \approx 0$ should be avoided for studying $\frac{dB_x}{dx}$.