Detectors for e^+/e^- Identification in FGT

R. Petti

University of South Carolina, USA

DUNE ND Working Group Meeting December 3, 2015

Roberto Petti anticologia di un secondo all'estimato di un secondo all'estimato di un secondo all'estimato di u

THE DUNE FGT CONCEPT

- ✦ Evolution from the NOMAD experiment
- ✦ High resolution spectrometer $B = 0.4$ T
- ✦ Low density "transparent" tracking $\rho \sim 0.1 g/cm^3 \quad X_0 \sim 5m$
- ◆ Combined particle ID & tracking for precise reconstruction of 4-momenta
	- Transition Radiation $\Longrightarrow e^-/e^+$ ID, γ
	- $dE/dx \Longrightarrow$ Proton ID, $\pi^{+/-}$, $K^{+/-}$
- \blacklozenge Tunable thin target(s) spread over entire tracking volume \implies target mass \sim 7t
- \triangleq 4 π ECAL in dipole B field
- \blacklozenge 4 π μ -Detector (RPC) \Longrightarrow μ^+/μ^-

"ELECTRONIC BUBBLE CHAMBER" WITH $\mathcal{O}(10^8)$ EVENTS

DETECTION OF e^-/e^+ IN FGT

- ← Key feature reconstruction of e^-/e^+ as single CHARGED TRACKS, as opposed to compact electromagnetic showers:
	- Require low density (< 0.1 g/cm³) tracking with thickness $\sim 1X_0$ and track sampling $\mathcal{O}(10^{-3})$;
	- Require magnetic field to separate e^+ from e^- and reconstruct γ converted in tracking volume \Rightarrow With B=0.4 T e^-/e^+ tracks can be reconstructed down to \sim 80 MeV
	- Provide accurate 4-momentum measurement of e^-/e^+ (measure both \vec{p} and E)
- ✦ Continuous e[−]/e⁺ identification fully integrated into tracking volume:
	- Transition Radiation (TR) only produced by e^-/e^+ with $\gamma > 1000$;
	- Ionization dE/dx provides additional e/π separation in the DUNE energy range;

 \implies Measurement of energy deposition in active straws sensitive to both

- ← Matching of extrapolated e^-/e^+ tracks with ECAL electromagnetic showers (clusters):
	- Energy deposition in ECAL powerful e/π rejection;
	- Transverse and longitudinal profile of electromagnetic showers (clusters) in ECAL provides additional e/π rejection;
	- Reconstruction of Bremsstrahlung γ 's emitted by e^-/e^+ in the bending plane from ECAL and STT (conversions).

THE STRAW TUBE TRACKER

✦ Main parameters of the STT design:

- Straw inner diameter 9.530 ± 0.005 mm;
- Straw walls $70 \pm 5 \mu m$ Kapton 160XC370/100HN $(\rho = 1.42, X_0 = 28.6$ cm, each straw $< 5 \times 10^{-4} X_0$);
- \bullet Wire W gold plated 20 μ m diameter;
- \bullet Wire tension around 50g;
- Operate with $70\%/30\%$ Xe/CO₂ gas mixture.
- Straws are arranged in double layers of 336 straws glued together (epoxy glue) inserted in C-fiber composite frames;
- Double module assembly $(XX+YY)$ with FE electronics (each XX+YY tracking module $\sim 2 \times 10^{-3} X_0$);
- Readout at both ends of straws (IO & FE boards on all sides of each $XX+YY$ STT module);
- 160 modules arranged into 80 double modules over ~ 6.4 m (total 107,520 straws).
- \implies Total tracking length $\sim 0.3 X_0$
- \triangle Add dedicated (anti)neutrino thin target(s) to each STT double module keeping the average STT density ~ 0.1 g/cm³ for required target mass.

RADIATOR TARGETS

- ✦ Design and physics performance (Transition Radiation) of radiator targets optimized (docdb $\#$ 9766) \implies Mechanical engineering model available
- ✦ Radiator targets integrated at both sides of each STT (double layer) module to minimize overall thickness (foils could be removed if needed):
	- Embossed polypropylene foils, $25 \mu m$ thick, $125 \mu m$ gaps;
	- Total number of radiator foils 240 per XXYY module, arranged into 4 radiators composed of 60 foils each;
	- Total radiator mass in each XXYY module: 69.1 kg, $1.25 \times 10^{-2} X_0$.
	- \implies The radiator represents 82.6% of the total mass of each STT module
	- =⇒ Tunable for desired statistics & p resolution !"##

R. Petti University of South Carolina **Sketch of the embossing pattern for the polypropylene radiator foils**

 \bigcap

FGT G4 simulation: 1 GeV e^+

 $\emph{track sampling} \perp 0.95 \emph{cm} / 500 \emph{cm} = 0.19 \%$ $\rho = 0.1 \, \, g/cm^3, \, X_0 = 500 \, cm, \,\, track \,\, sampling \,\, 1.9 cm/500 cm \, = \, 0.38 \%$

FD G4 simulation: 1 GeV e^+

 $\rho = 1.4 \, \, g/cm^3, \, X_0 = 14 \, cm, \,\, track \,\, sampling \,\, 4.667 mm/140 mm = 3.33\%$

TR photons emitted within a cone $1/\gamma < 1$ mrad from the track direction

Xe gas has an absorption length 10 times smaller than Ar and \ll straw diameter Use a proven gas mixture with 70% Xe and 30% CO_2 for TR detection about 1 GeV/c to 100 GeV/c or \mathcal{L} to 100 GeV/c or higher, the upper limit being determined not only by para-

Need closed gas system to minimize Xe leakage (Xe is expensive) and avoid Xe content in gas volume outside straws (flush with CO $_2)$

TRANSITION RADIATION

- HiresMy March 1996 ✦ Simulation of Transition Radiation (TR) based on formalism by Garibian (1972), Cherry (1975) \implies Narrow energy range \sim few keV
- ◆ Radiator design optimized for TR performance: 0.02 8
	- TR build-up over many interfaces;
	- Self-absorption of lower part of energy spectrum;
	- Need compact radiarors to keep large tracking sampling.
	- \Rightarrow Select 25 μ m foils, 125 μ m spacing
- detected in a single STT module from a 1 GeV e \triangle On average \sim 1 TR photon with $E > 5$ keV
- \triangleleft dE/dx in straws are of the same order as TR at energies of few GeV: a 5 GeV e(π) has a probability $\sim 41\% (18\%)$ of depositing $E > 6$ keV

Ionization dE/dx, E=5 GeV

COMPARISON WITH NOMAD

 \overline{D} ✦ Continuous TR+dE/dx detection over entire STT volume, NOMAD only limited forward coverage \implies Improved acceptance and e^+/e^- ID

✦ NOMAD TRD configuration:

- 9 radiators made of 315 $(C_3H_6)_n$ foils each;
- foils 15 μ m thick, with 250 μ m air gaps;
- 16 mm diameter straws without tracking capability.
- \implies Total 2,835 foils over \sim 154 cm length
- R. Petti each) to match the total foils of the NOMAD TRD ✦ Need ∼ 12 double STT modules (4 straw layers \implies More compact design with length \sim 92 cm

Opposite effects in STT:

- Smaller air gaps and thicker foils reduce TR production with respect to NOMAD;
- Lettency. • Larger Xe volume more uniformly distributed within radiator foils increases TR detection efficiency.

Fig. 8. Monte Carlo predicted electron efficiency ε_e corresponding to $\varepsilon_n = 10^{-3}$ as a function of the momentum of the particle

THE ELECTROMAGNETIC CALORIMETER

- Glo-Sci-51,23 measure absolute and relative ν_μ, ν_e and $\bar{\nu}_\mu, \bar{\nu}_e$ spectra separately. Glo-Sci-24 measure rates, kinematic distributions and topologies of bkgnd processes \implies reconstruction of $e^+/e^-, \gamma$ with accuracy comparable to μ^+/μ^- and FD \implies containment of $> 90\%$ of shower energy NDC-L2-29,37 \implies energy resolution $< 6\%/$ √ E | NDC-L2-38
- ◆ Based upon the design of the T2K ND-280 ECAL (to be further optimized)
- ✦ Sampling electromagnetic calorimeter with Pb absorbers and alternating horizontal and vertical (XYXYXY....) $3.2m \times 2.5cm \times 1cm$ scintillator bars readout at both ends by \sim 1 mm diameter extruded WLS fibers and SiPM
	- Forward ECAL: 60 layers with 1.75 mm Pb plates $\Longrightarrow 20X_0$
	- Barrel ECAL: 18 layers with 3.5 mm Pb plates $\Longrightarrow 10X_0$
	- Backward ECAL: 18 layers with 3.5 mm Pb plates $\Longrightarrow 10X_0$

Forward ECAL *mass&21.7&tons*

Barrel ECAL Module *(16&Barrel,&2&Backward&ECAL) mass&4.9&tons*

SiPM reading a WLS fiber

Backup slides

Roberto Petti alla suomen valtaa kuningas valt

Simulation of a 10 STT MODULES

Total longitudinal length of 10 STT modules (double layers) 40 cm

STT READOUT

✦ Double readout at both ends of straws: 215,040 channels in STT

✦ Each of the 80 STT XXYY assemblies equipped with:

- \bullet 44 I/O Boards (11 per side) with 64 channels each;
- 44 Front End Boards (FEB) with 64 channels each (11 per side). Consider VMM2 chip (ASICS) developed for ATLAS upgrades, with fast ADC and TDC;
- Number of straw ends readout: 21 groups of 32 straws per double layer (XX or YY) \times 2 ends \times 2 modules = 2,688

← Back End electronics:

- 80 receiver modules Readout Merger Board (RMB) (one per XXYY assembly) mounted in racks;
- 5 crates (MicroBooNE), each holding 16 receiver modules, 1 controller, 1 XMIT, 1 trigger module;
- ✦ High Voltage: 160 channels, one for each XX (or YY) double layer module
- \blacklozenge Low Voltage: one per RMB (80 total) servicing each 48 FEB $+$ 80 distribution boards.

Straw Tube Chamber IO Board (304mm x 30mm): 3,520 total

Front End Board (175mm x 60mm): 3,520 total Back End Board (200mm x 300mm): 80 total

STT GAS SYSTEM

- \blacklozenge The active gas is $Xe(70\%)/CO_2(30\%)$ mixture for the STT modules with radiators and $Ar(70\%)/CO_2(30\%)$ for the STT modules with nuclear targets.
- \blacklozenge Total active gas volume 26.7 m³ and should be flushed with approximately one volume change/hour;
- ✦ Gas distribution is a closed recirculation system to minimize Xe losses;
- \triangle Exit gas from the straws is recovered, cleaned and recirculated;
- ✦ Gas tightness of straws [∼] ¹ mbar/min/bar to minimize Xe losses (standard ATLAS acceptance criteria);
- \blacklozenge To protect straws from moisture CO_2 is flushed around the straws throughtout the outer envelope of the STT (53.4 m^3);
- **← Forced flaw of** \sim 100 m³/hour.

TRIGGER AND EVENT RATES

- \blacklozenge The maximum drift time for a Xe/CO_2 gas mixture is 125 ns for a distance of 5mm (lower for Ar), as measured in testbeam.
- ✦ The STT can resolve individual beam pulses (resolution ∼ ns)
- ✦ Expect a rate of 1.5 events/spill (∼ 10 µs) for events originated within STT volume.
- ✦ Possible a self-triggering scheme in which hits are stored in pipelines (can use FE ADC to operate in digital domain) waiting a later decision

 \implies Avoid trigger based upon geometrical acceptance (problem in NOMAD).

- ✦ Depending upon the background rate, it should be possible to read and timestamp everything within one spill and to take a decision later in the cycle.
- ✦ In addition, calorimetric trigger (complementary)