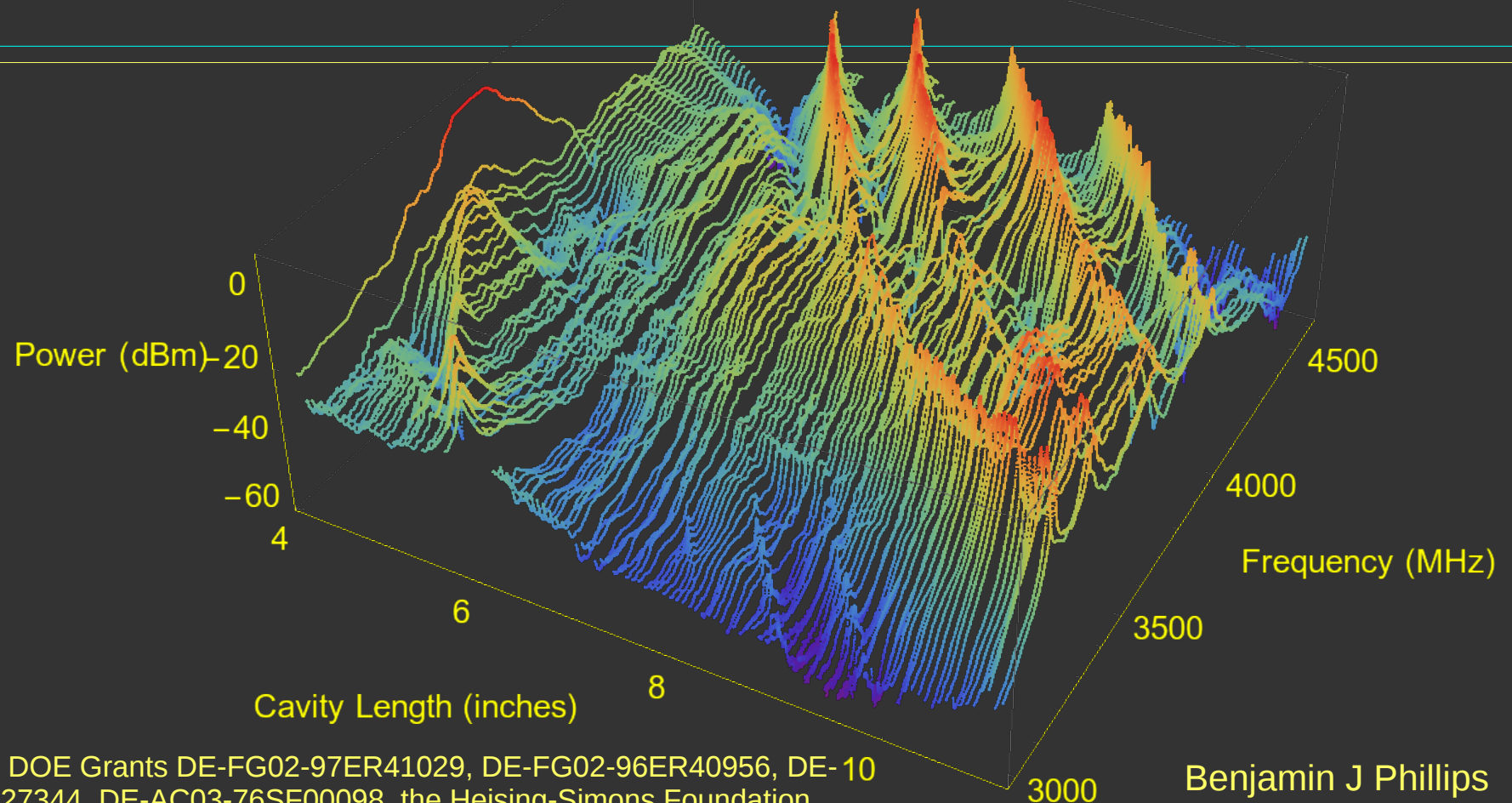


# The Electric Tiger Experiment

## a Proof-of-Concept for the Periodic Dielectric Loaded Resonator



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# Motivation

# Design Goals

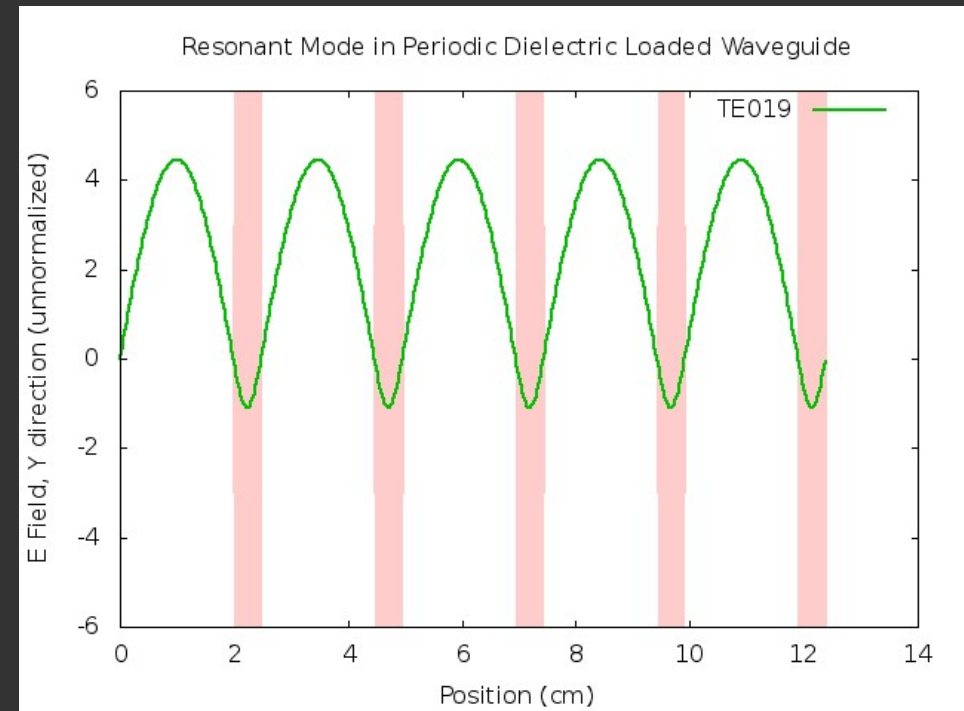
- Experiment to search high frequency regions ( 4 – 7 GHz )
- Rapid prototyping with on-hand materials
- Cavity is reasonably simple to tune (e.g. manageable mode crossings )
- Lay foundations for experiments that rely on dielectrics ( very high frequency searches )

# Motivation

- Makes use of dielectric media inside a resonant cavity
- Dielectric media compresses wavenumber – prevents form-factor integral from going to zero

# The P.D.L.R. Design

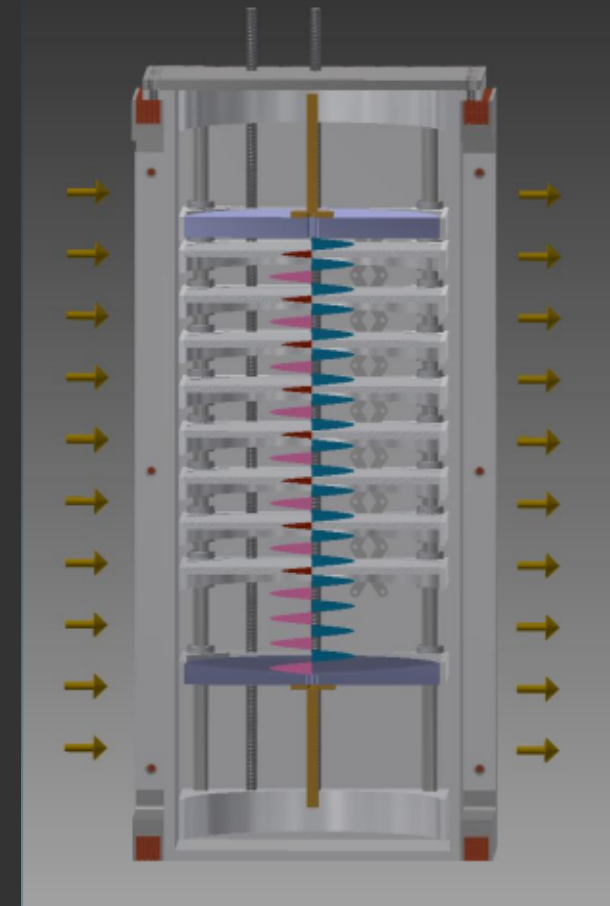
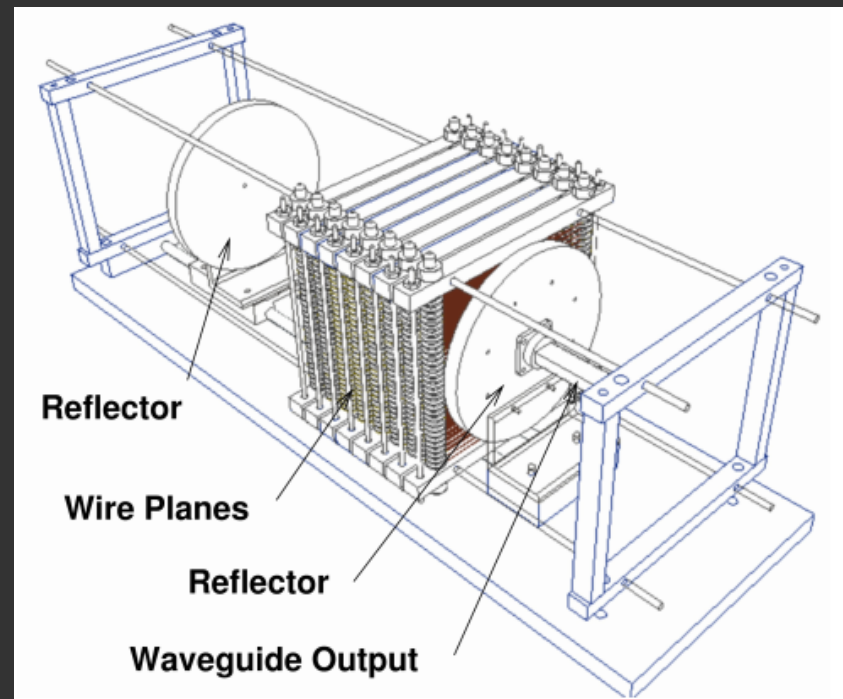
$$F \propto \frac{\left( \int_V E \cdot B dV \right)^2}{\int_V E^2 dV \int_V B^2 dV}$$



# Motivation

# Laying Foundations

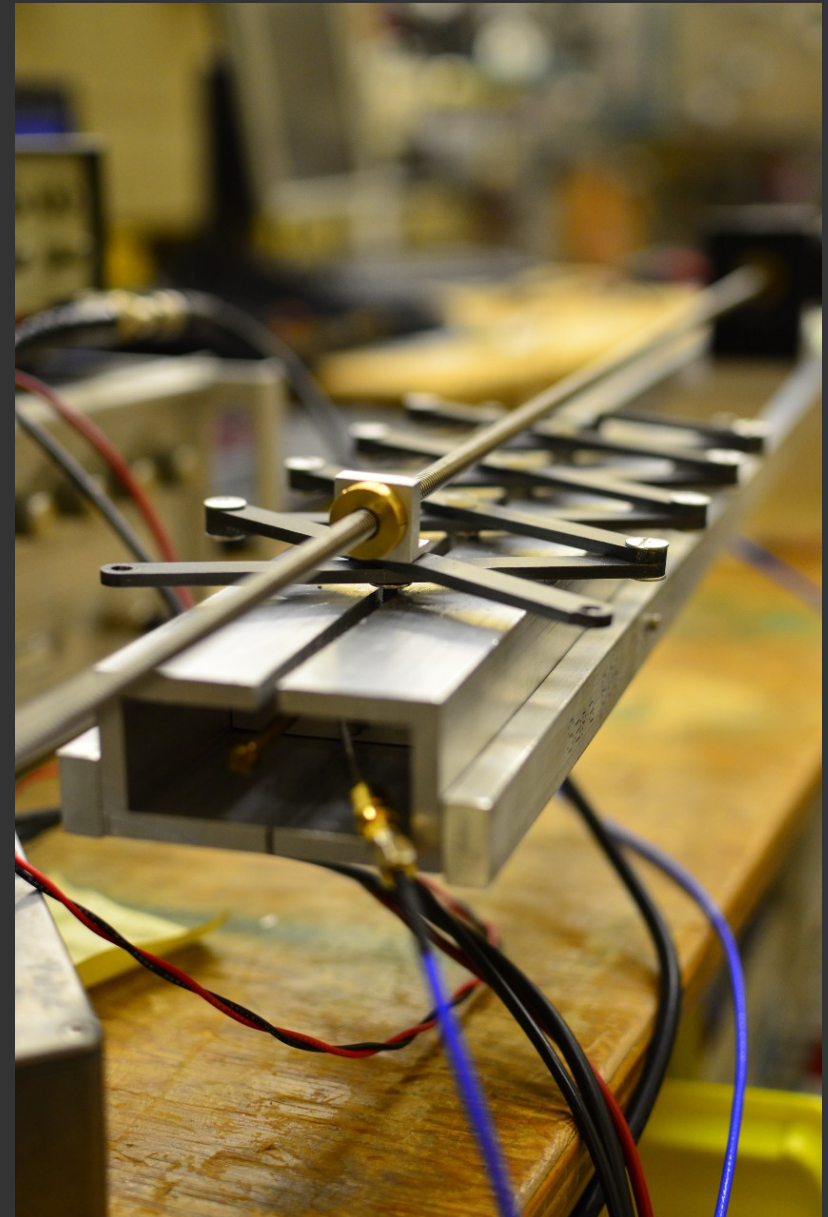
- Resonant cavities that use dielectrics are difficult to tune – dielectrics have to be moved in unison
- Tuning procedures developed by Electric Tiger can be used by these types of experiments ( e.g. Orpheus )



# Implementation

## Construction of Cavity

- Rectangular waveguide with one stationary antenna, one movable
- Dielectric media is provided by three nylon blocks
- Tuning is provided by scissor-jack and stepper motor driving auger screw
- Cavity length is measured by string potentiometer
- Cavity design limits mode Quality Factor





# Implementation

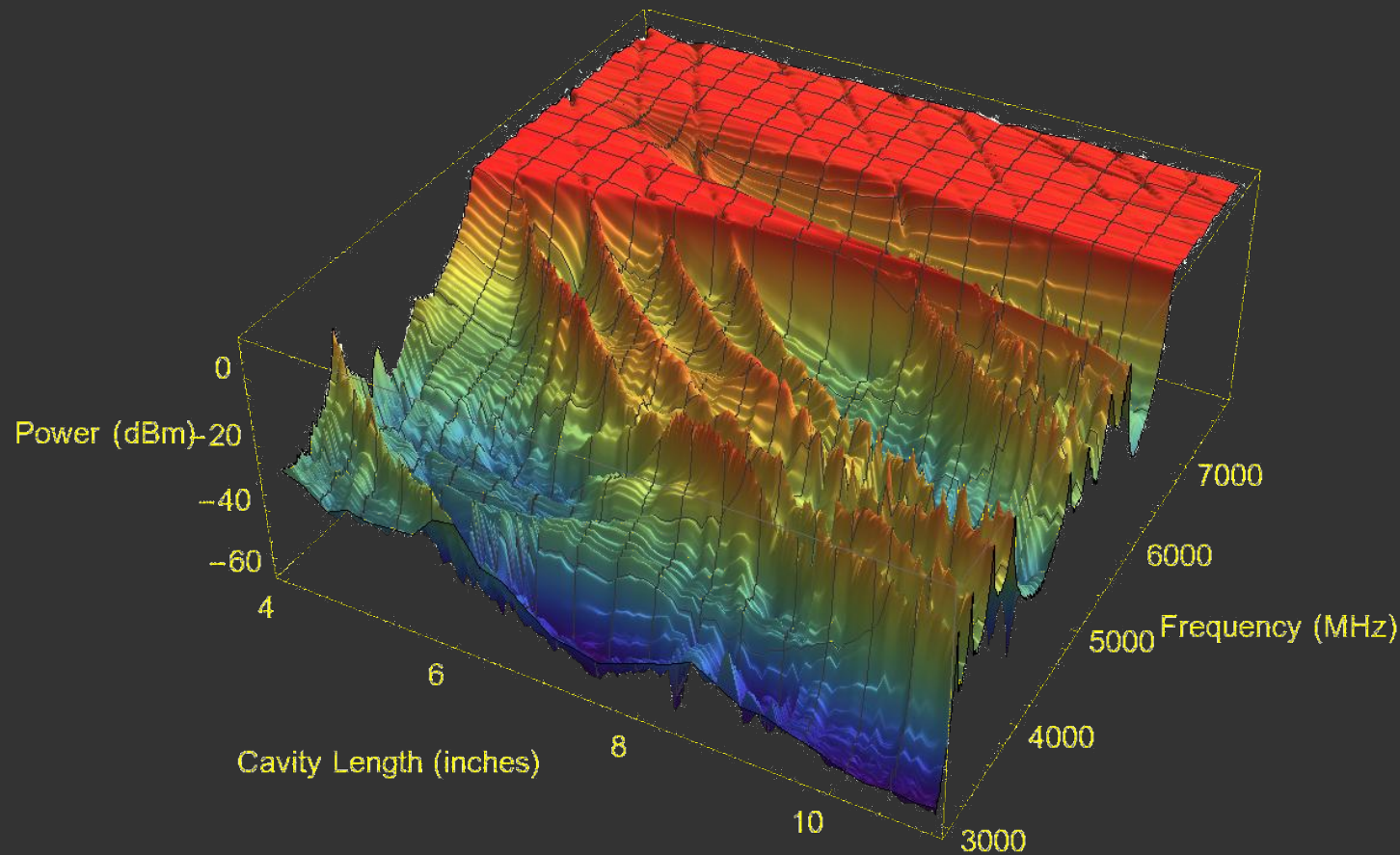
## Magnetic Field

- Rectangular cavity geometry permits use of constant z-axis magnetic field
- Magnetic field provided by 1.54 Tesla DC Magnet



# Implementation

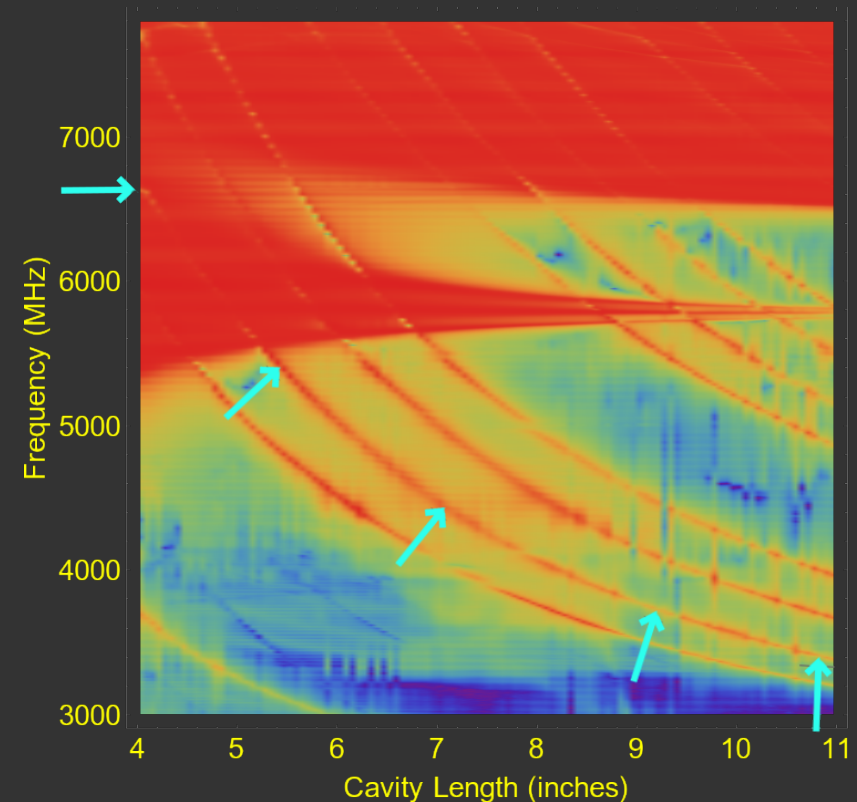
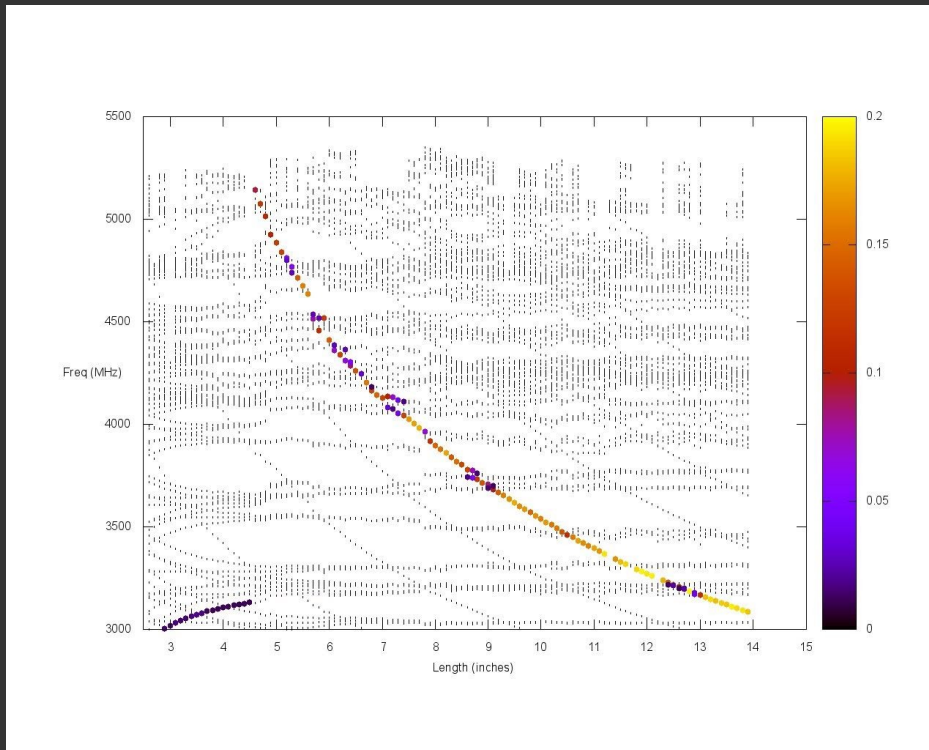
## Cavity Structure (Transmission)



- Cavity has a non-trivial amount of static structure
- Modes are broad and amplitude is not always significantly higher than static structure

# Implementation

# Cavity Structure (Transmission)

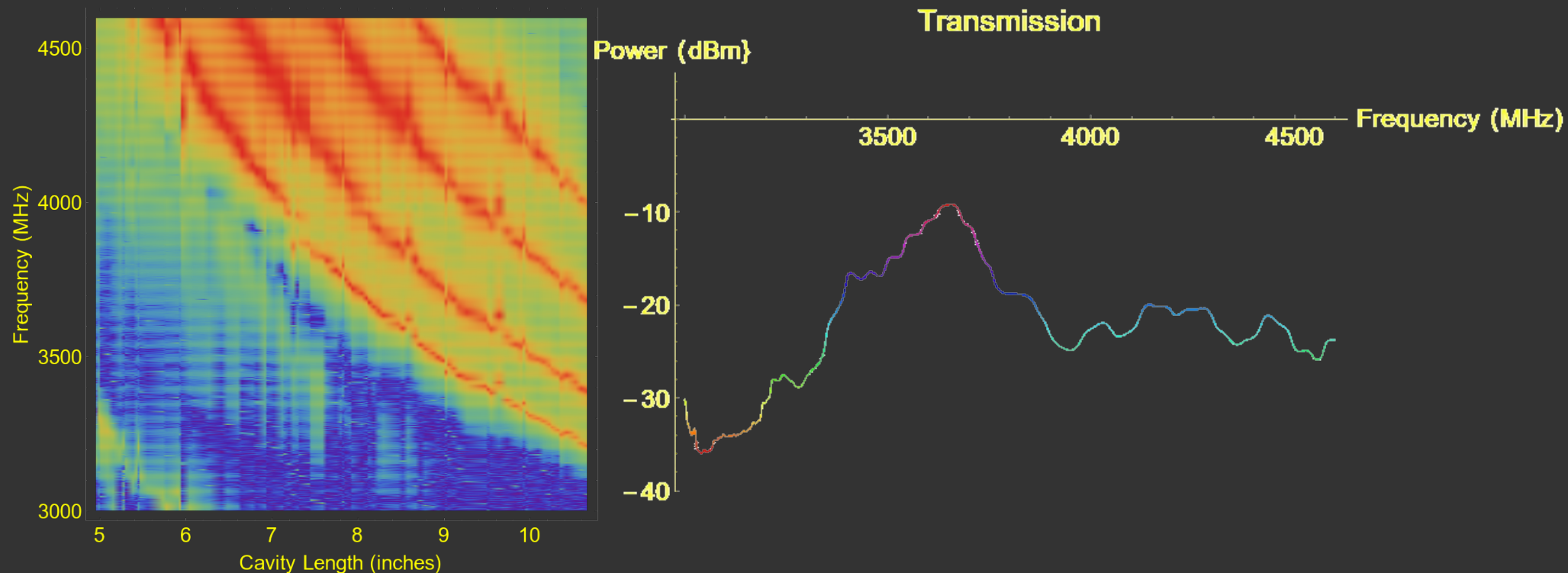


- Simulations of cavity determines mode that couples best with axion field
- Mode moves over a wide frequency range,  $\sim 3.5 - 6.5$  GHz, including regions currently blocked by RF components



# Implementation

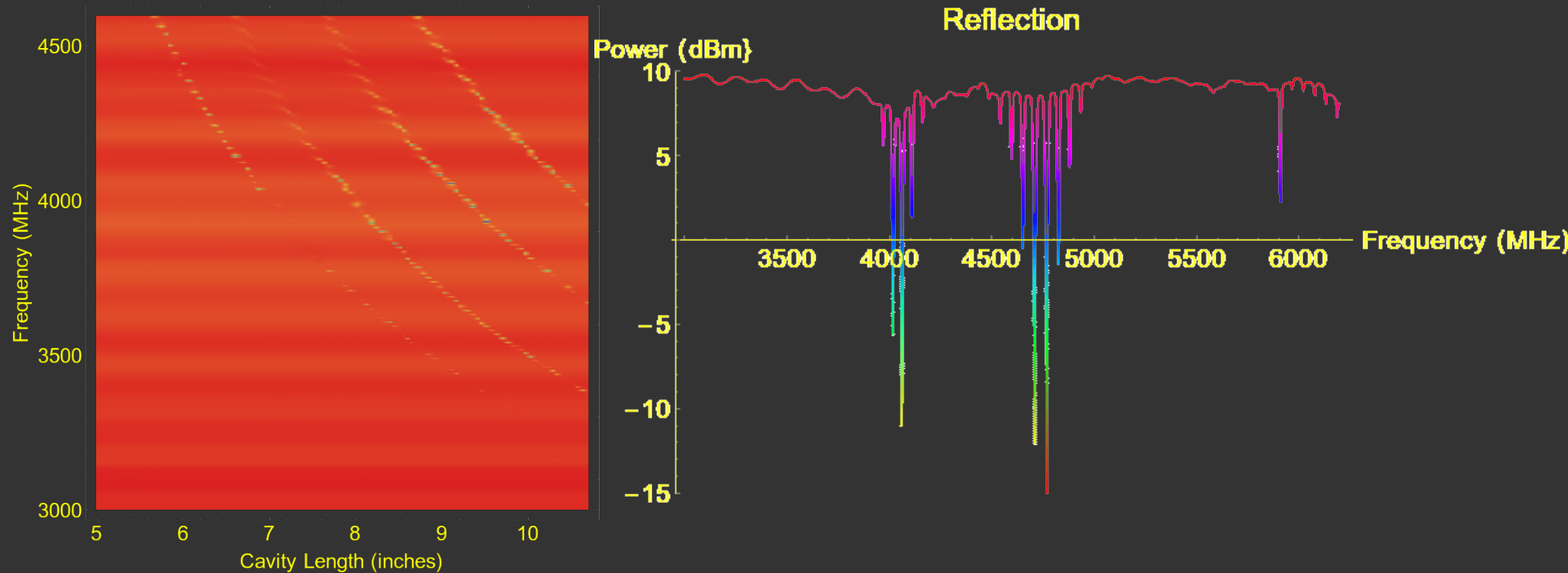
# Transmission



- Static structure in transmission measurements makes modes difficult to follow
- Q's of  $\sim 250$
- Traditional approaches (e.g. Lorentzian fitting) are unsuitable

# Implementation

# Reflection

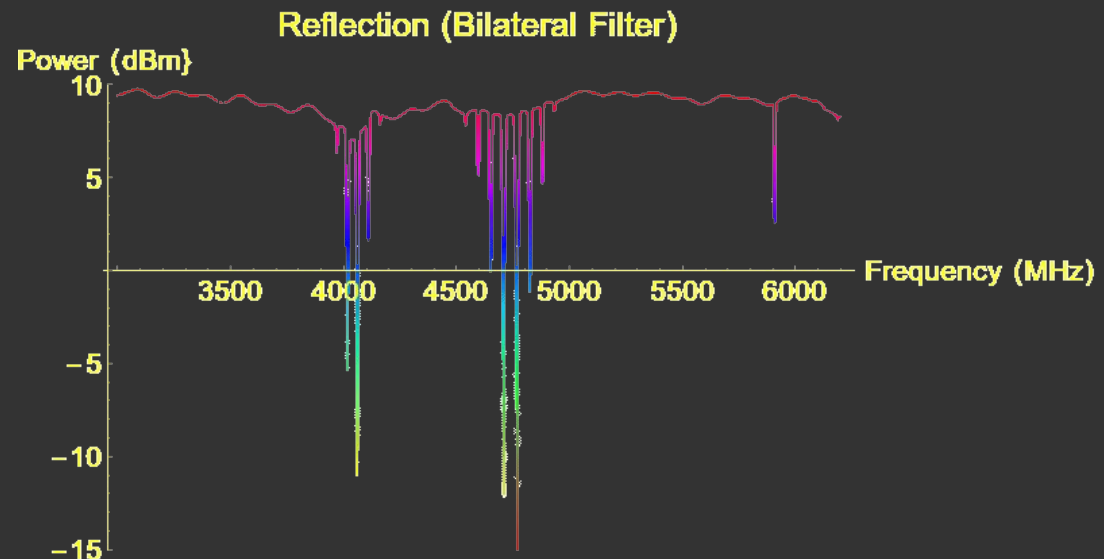


- Reflection modes show much less static structure
- Strategy: Identify and follow modes in reflection, switch to transmission to take data

# Implementation

# Filtering

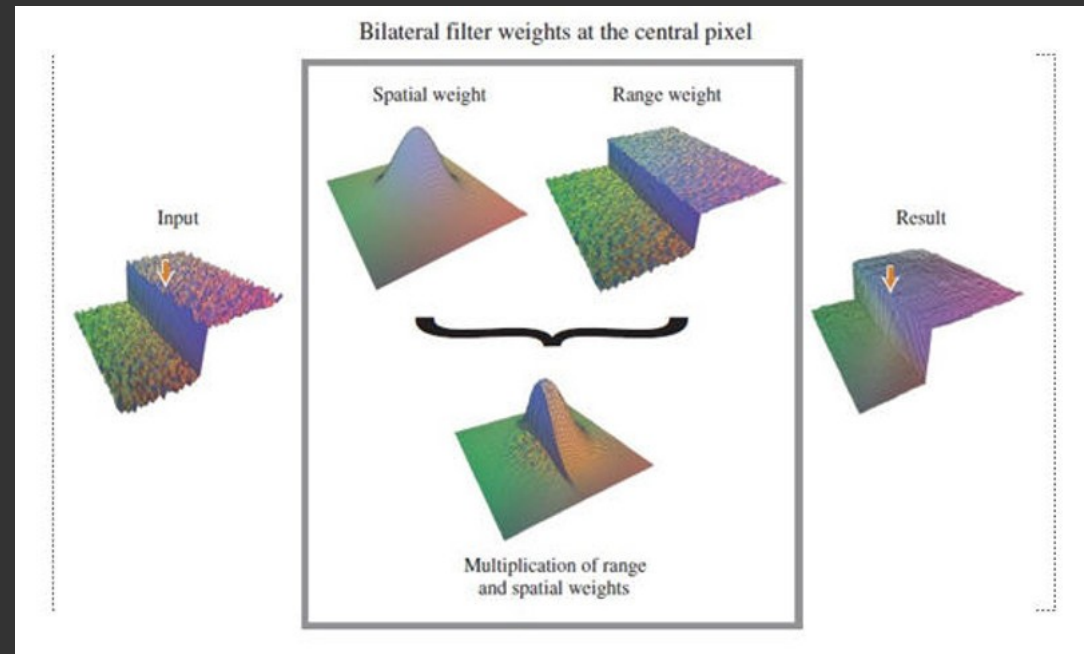
- Even in reflection, traditional mode-tracking techniques are not appropriate
- Simple band-pass filters either suppress actual peaks, or amplify static structure
- Solution: Use non-linear filters – suppress noise while preserving peaks



# Implementation

## Non-Linear Filters

- Mode Identification scheme only needs heuristic idea of what a peak is
- Criteria is  $\sim f'[n] < 0$  &  $f'[n+1] > 0$
- Since we only need a loose idea of what a peak is, namely that it is 'sharp', we can use filters that do not linearly modify signal power
- Use bilateral filter, a specific example of a non-linear convolution



$$f * g(n) \equiv \sum_{k=-M}^M f(k)g(f(n) - f(k))h(n - k)$$

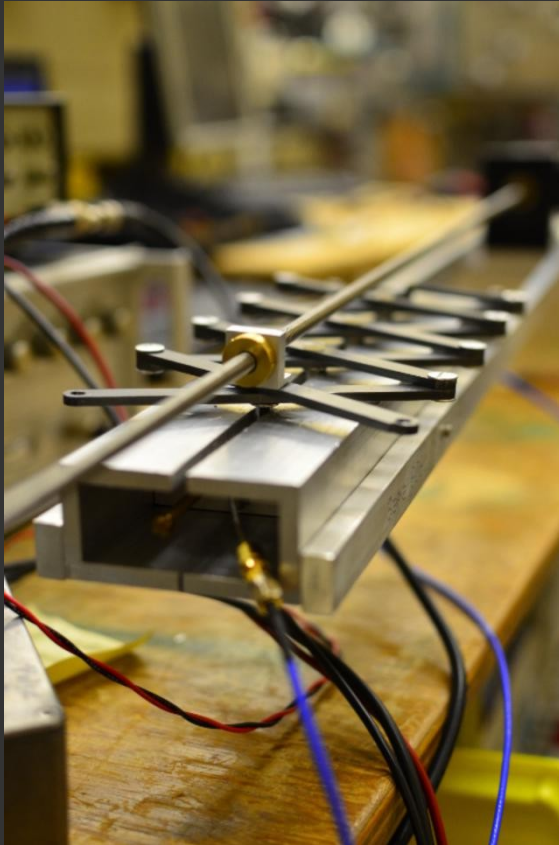
Let  $G_{\sigma_s}$  and  $G_{\sigma_r}$  be Gaussians with  $\sigma_s$  and  $\sigma_r$  respectively

$$BL(n) = \sum_{k=-M}^M f(k)G_{\sigma_r}(f(n) - f(k))G_{\sigma_s}(n - k)$$



# Implementation

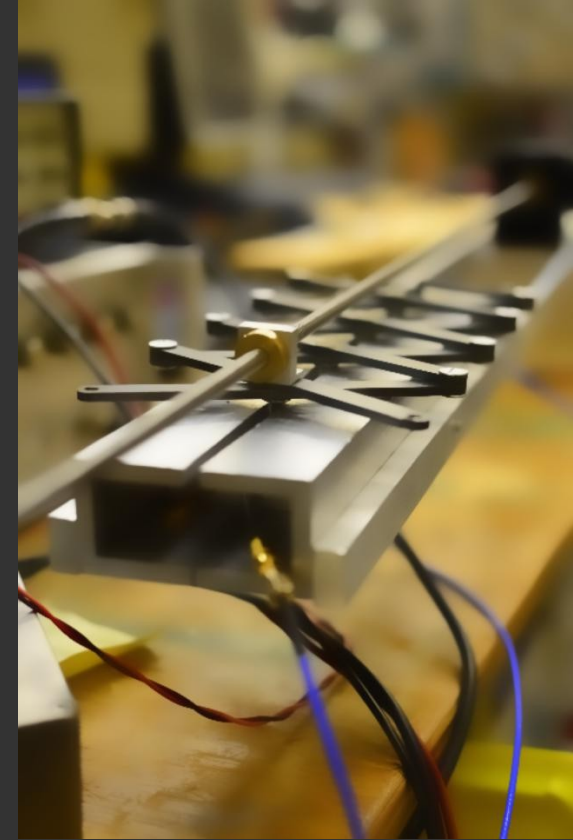
## Non-Linear Filters



Original



Gaussian Blur



Bilateral Filter

- Effects of Bilateral filter are more obvious when looking at 2D figures
- Low-pass filters ( Gaussian Blurs ) suppress noise, but erase features
- Bilateral filter suppresses noise while preserving edges

# Implementation

# Thoughts on Mode Maps

- Why not rely on the mode map alone?
- Electric Tiger has a high degree of mechanical slop
- Modes tend to vanished at certain cavity positions
- Goal is to divorce mode tracking procedure from mode map
- Current mode tracking procedure uses mode map – real peaks can be ~ 175 MHz away from mode map

```
bephillips2@LULU: ~/Qt-Projects/build-modetrack-Desktop-Release
Match for peak: 3, Using real value of: 4310.7231920199501MHz
Data set: 71
Smallest frequency seperation: 64.2578 at Peak: 2
Smallest frequency seperation: 20.3675 at Peak: 2
Smallest frequency seperation: 165.19 at Peak: 3
Smallest frequency seperation: 221.051 at Peak: 3
Smallest frequency seperation: 278.906 at Peak: 3
Smallest frequency seperation: 338.757 at Peak: 3
Smallest frequency seperation: 1424.04 at Peak: 3
Identified peak was too far from any estimated value.
Match for peak: 2, Using real value of: 4063.3416458852871MHz
Match for peak: 3, Using real value of: 4655.8603491271824MHz
Data set: 35
Smallest frequency seperation: 89.4525 at Peak: 0
Smallest frequency seperation: 47.5572 at Peak: 0
Smallest frequency seperation: 62.1685 at Peak: 0
Smallest frequency seperation: 82.1186 at Peak: 0
Smallest frequency seperation: 91.3349 at Peak: 1
Smallest frequency seperation: 149.19 at Peak: 1
Smallest frequency seperation: 203.056 at Peak: 1
Smallest frequency seperation: 256.549 at Peak: 2
Smallest frequency seperation: 194.703 at Peak: 2
Match for peak: 0, Using real value of: 4063.3416458852871MHz
Match for peak: 1, Using real value of: 4600MHz
```

- Initial data run performed at room temperature
- Exclusion limits set in 4-4.2 GHz Range using rudimentary equipment
- Sensitivities of  $\sim 10^{-9}$
- Mode tracking scheme was able to follow modes throughout tunable range
- Experiment ran autonomously for  $\sim 8$  days

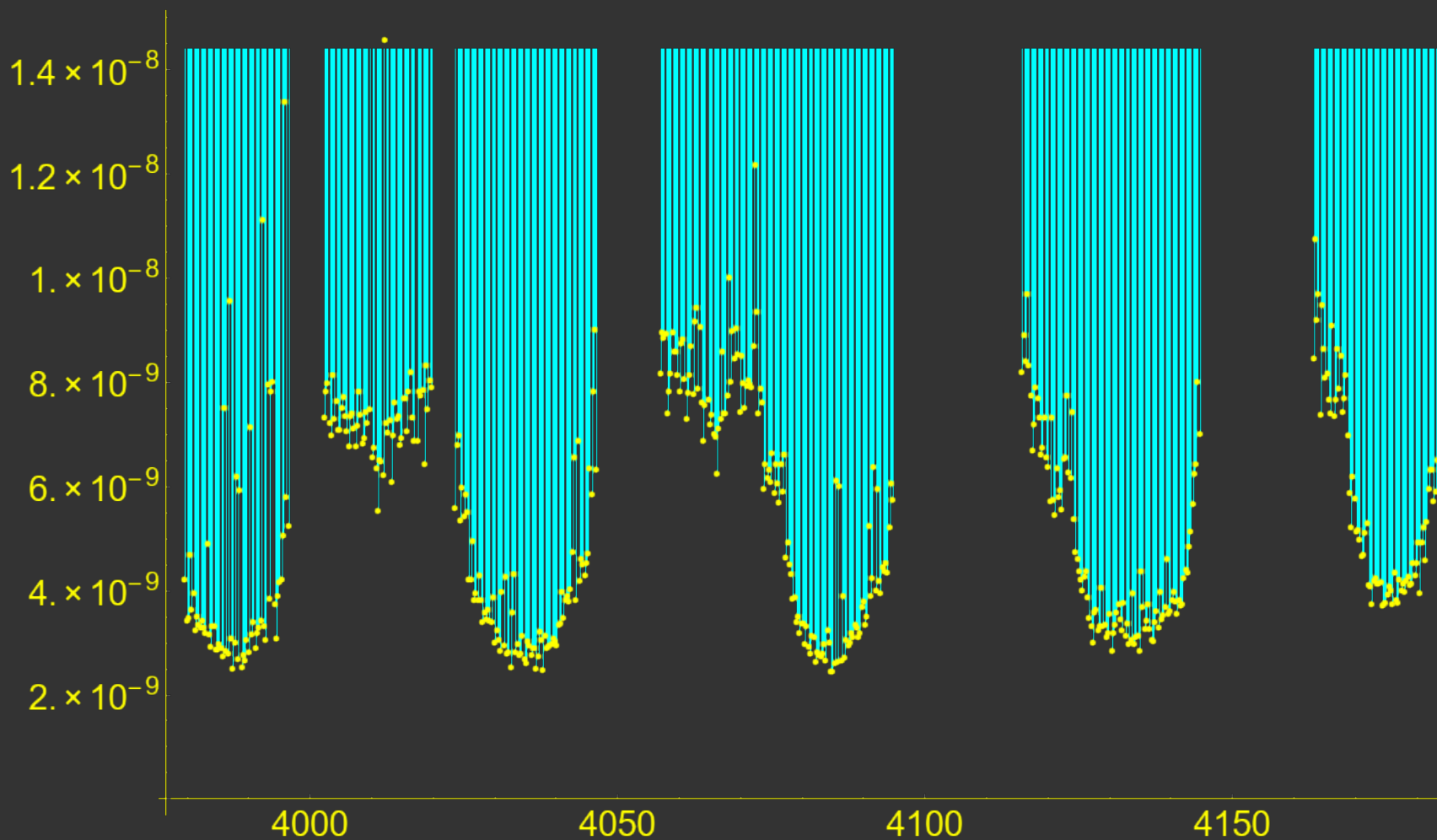
# Data Collection

# Preliminary Results

90% Exclusion Limit

$g_{a,\gamma\gamma}$  ( $\text{GeV}^{-1}$ )

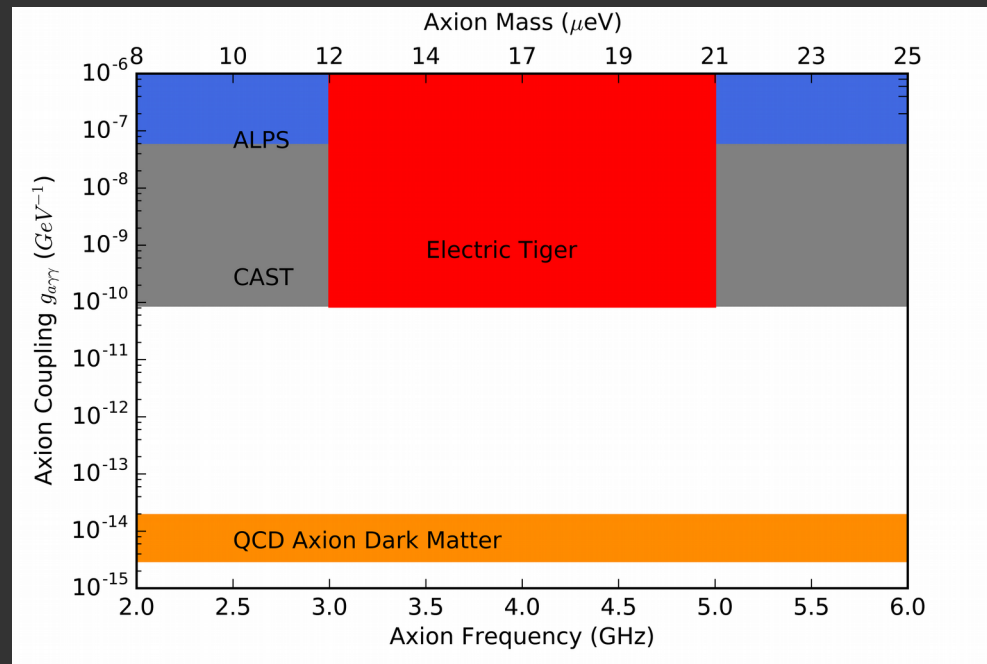
Frequency (MHz)





# Data Collection

# Next Steps



Projected Sensitivity for 8 week integration time

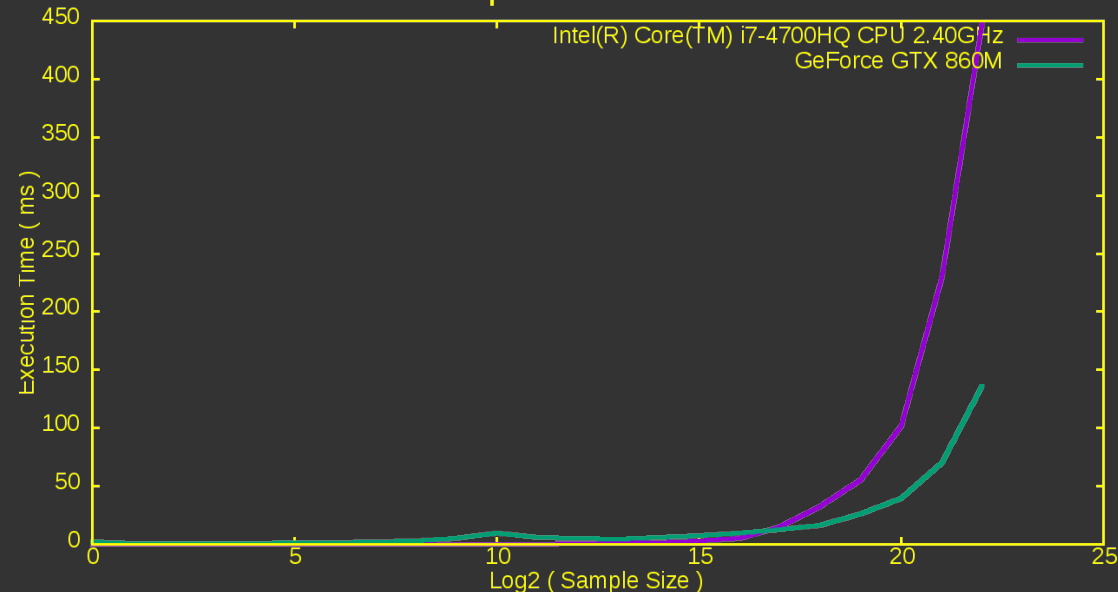
- Initial data run made use of Signal Analyzer – collected  $\sim 10^5$  points per spectra, averaged  $\sim 10^4$  signals
- Next data run will make use of digitizer –  $10^8$  points per spectra, virtually unlimited number of averages
- Longer integration times
- Cryogenic temperatures

# “Side Effects”

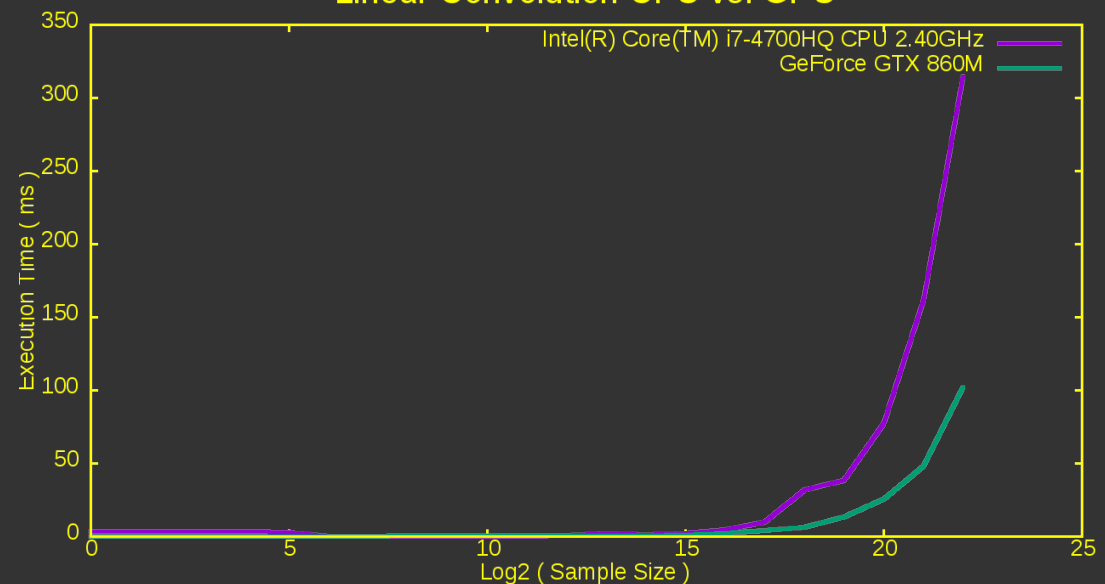
- Wide band-widths and fast digitization rates require very fast data processing
- Use GPU for signal processing operations to keep up with data stream
- GPU - accelerated methods are completely general and can be used by other experiments

# High Performance Signal Processing

Power Spectrum CPU vs. GPU



Linear Convolution CPU vs. GPU



# “Side Effects”

- Analysis procedure developed by Electric Tiger is generic
- Applicable to wide variety of resonate cavity searches
- May be incorporated into ADMX analysis in the near future

# Analysis Procedures

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## Algorithm 7 Construction of the Grand Spectrum

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**Input:**  $\mathcal{S}$

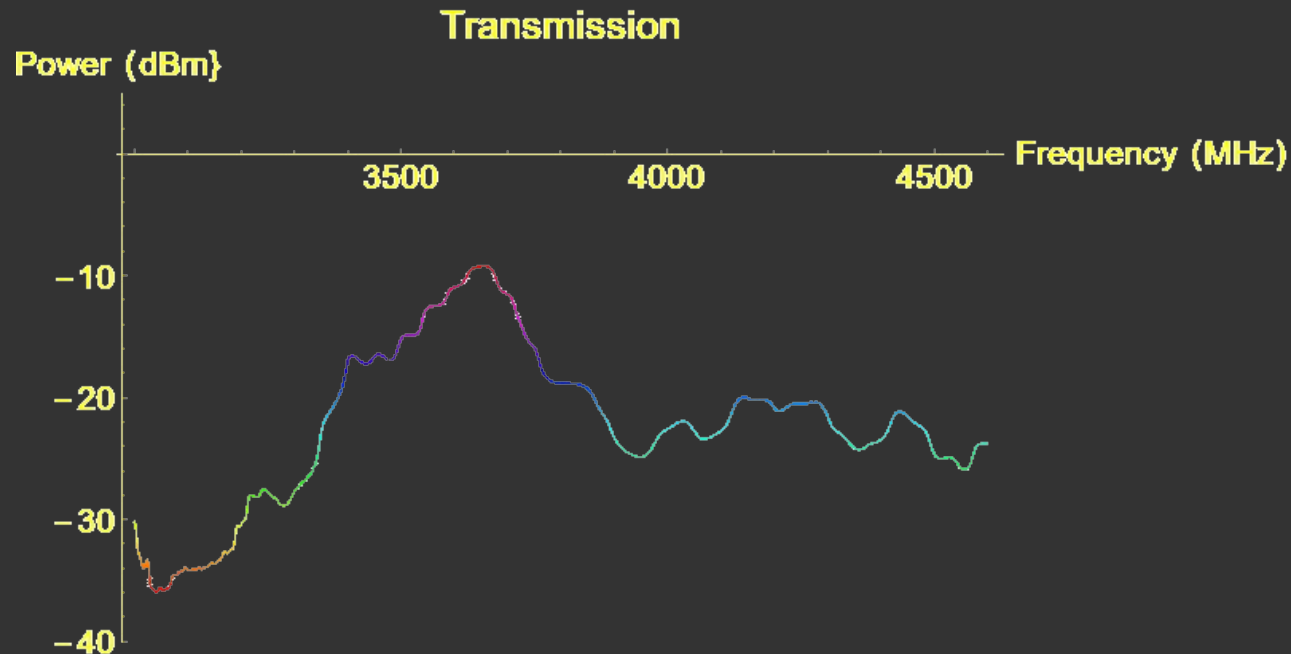
```
1: Let  $k = \lfloor (f_{max} - f_{min})/bw \rfloor$ 
2: Let  $GS = 0_{2,k}$ 
3: for each  $k$  do
4:   Let  $f_{center} \leftarrow$  center frequency of bin  $k$ 
5:   for each  $s \in \mathcal{S}$  do
6:     if  $f_{center} \in \Omega_s$  then
7:        $j \leftarrow$  bin at  $\omega_s^{-1}(f_{center})$ 
8:       if  $GS_{1,k} \neq 0$  then
9:         Let  $\tau_0 \leftarrow \frac{1}{\delta_{GC}(k)^2}$ 
10:        Let  $\tau_1 \leftarrow \frac{1}{\delta_{S_i}(j)^2}$ 
11:         $GS_{1,k} \leftarrow \frac{\tau_0 * GC(k) + \tau_1 * S_i(j)}{\tau_0 + \tau_1}$ 
12:         $GS_{2,k} \leftarrow \sqrt{\frac{1}{\tau_0 + \tau_1}}$ 
13:       else  $GS_{1,k} = 0$ 
14:          $GS_{1,k} \leftarrow s_{1,k}$ 
15:          $GS_{2,k} \leftarrow s_{2,k}$ 
16:       end if
17:     else  $f_{center} \notin \Omega_s$ 
18:       continue
19:     end if
20:   end for
21: end for
```

**Output:** GS

---

# Conclusion

## The two roles of Electric Tiger



- Platform to address concerns raised by other searches
- Electric Tiger is validation of the P.D.L.R. Design – will search in unexplored axion-like particle parameter space