THIN FILMS DEPOSITION OF Nb₃Sn ON COPPER

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OUTLINE

Motivation

- □ Sample preparation & analysis
- □ Critical temperature
- Microstructural properties of the films
- Substrate choice
- □ Summary

MOTIVATION

Proposed solutions to achieve desired characteristics and operational cost reduction for SRF application using A15 materials:

Replace expensive Nb bulk cavities with coated copper ones

- Copper cavities offer high thermal conductivity at low temperature, which should greatly help to increase the stability of the cavity against breakdown.
- ✓ Nb coated copper cavities are successfully used in CERN (LEP, LHC and HIE-ISOLDE machines).

Replace Nb thin films with superconductor with superior parameters (AI5 intermetallic compound)

WHY Nb₃Sn?

Advantages

High critical temperature

Tc	Nb ₃ Sn ~ 18.3 K
	Nb ~ 9.3 K

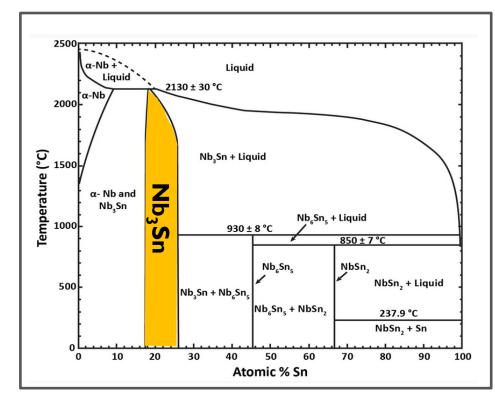
Low BCS resistance



Challenges

- Stoichiometry control (Sn At% 19-26 %)
- Requires high temperature treatment
- Limited range of annealing temperatures
- Substrate importance

WHY Nb₃Sn?



Binary phase diagram of the Nb-Sn system [1]

[1] J. Charlesworth, I. MacPhail, and P. Madsen, J. Mater. Sci. 5, 580 (1970).

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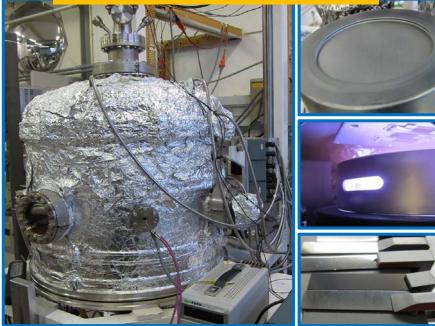


Challenges

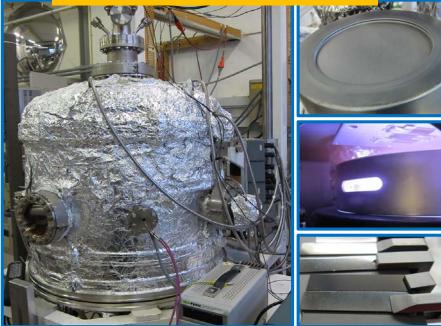
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Reacted After Coating

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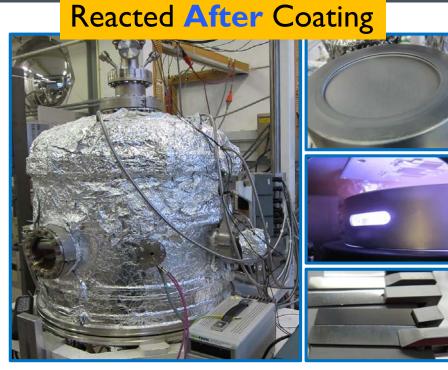


Reacted After Coating



Compulsory Annealing

Annealing temperatures	600 - 800°C	
Annealing time	24 h 72 h	



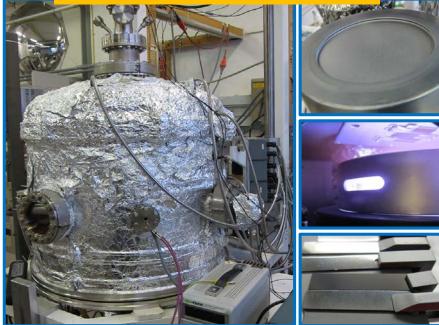
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Reacted **During** Coating

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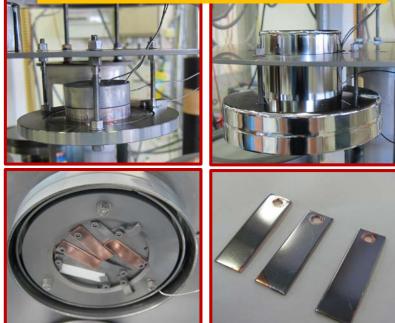
Reacted After Coating



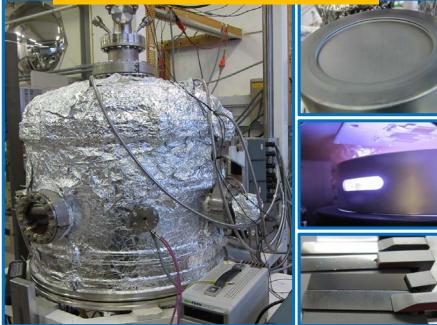
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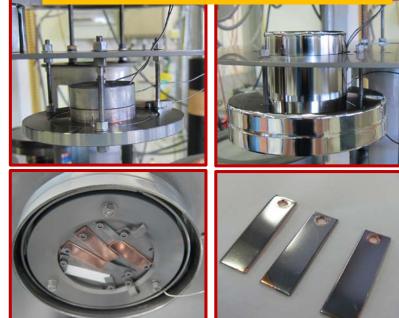
Reacted **During** Coating



Reacted After Coating



Reacted **During** Coating



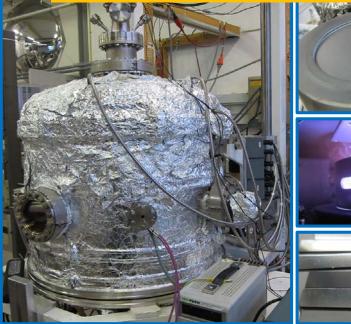
Alternative Annealing

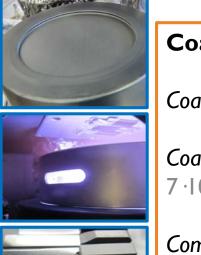
Coating temperatures	600 - 735°C	
Alternative Additional Annealing	24 h 72 h	

Compulsory Annealing

Annealing temperatures	600 - 800°C	
Annealing time	24 h 72 h	

Reacted After Coating





Coating parameters:

Coating gas: Ar or Kr

Coating pressures: 7 ·10⁻⁴ mbar ... 5 ·10⁻² mbar

Composition: Sn 20 At% to 27 At%,

Reacted **During** Coating









Compulsory Annealing

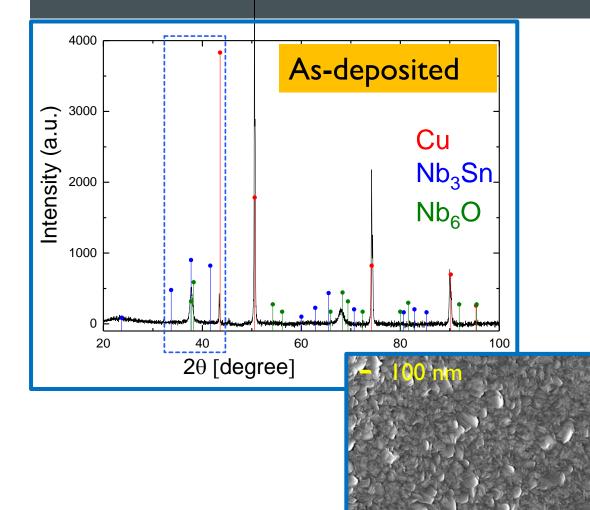
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Alternative Annealing

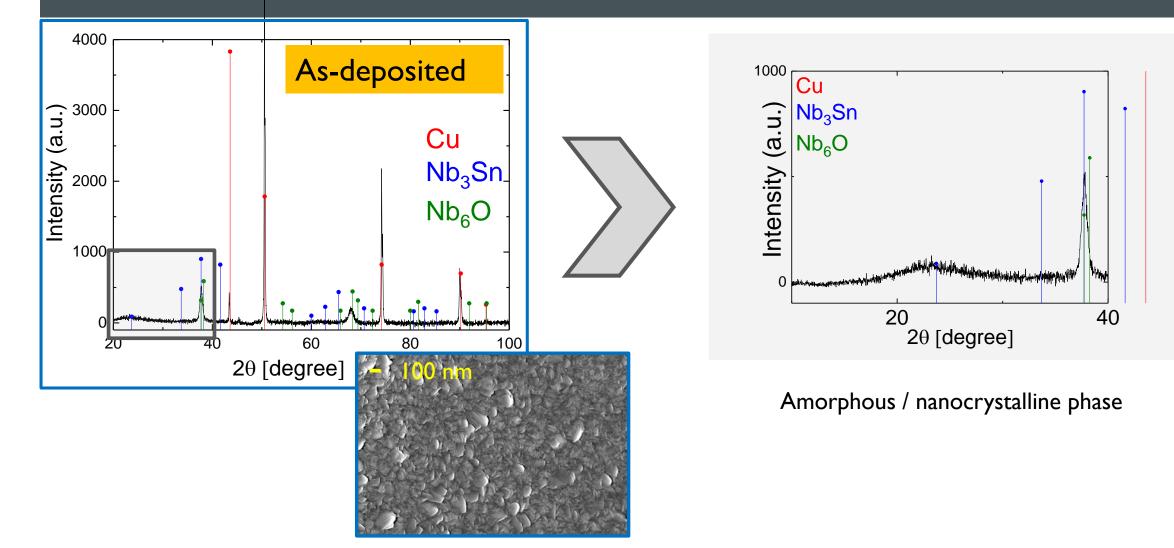
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AI5 phase formation. XRD analysis & Morphology

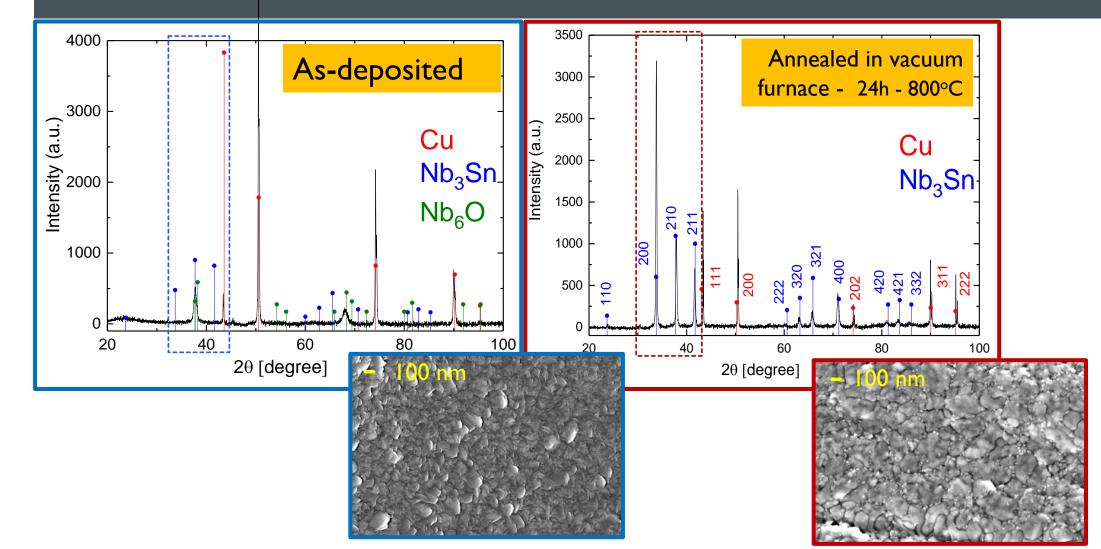
AI5 phase formation. XRD analysis & Morphology



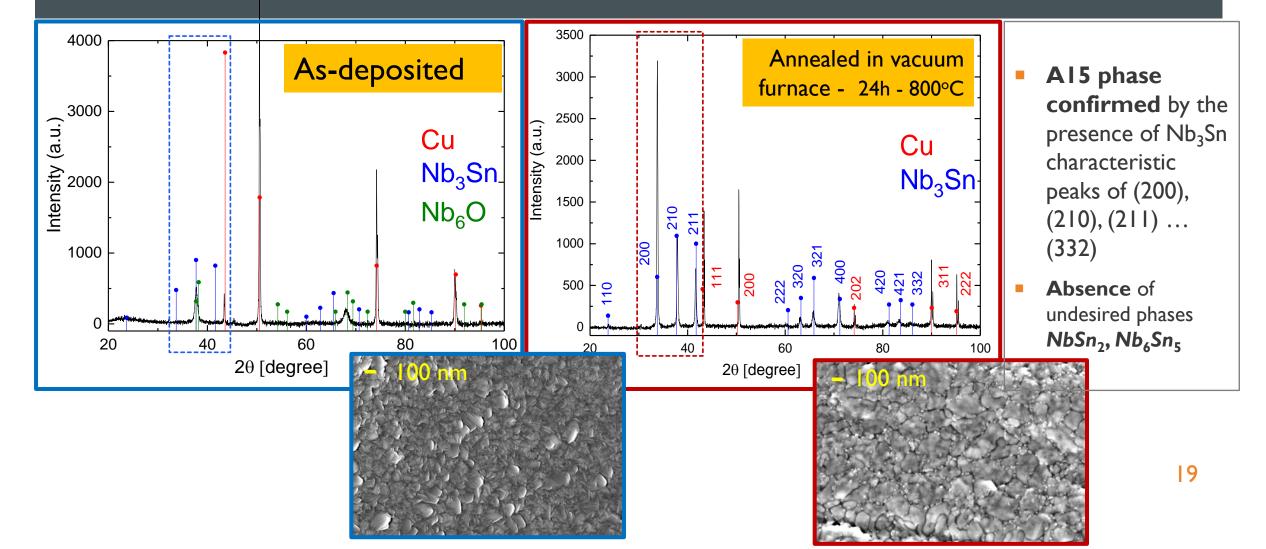
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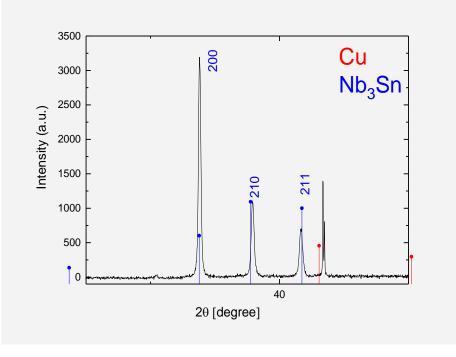


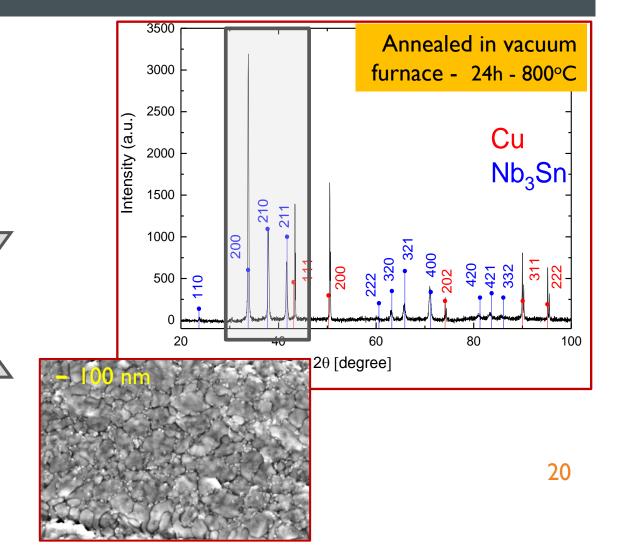
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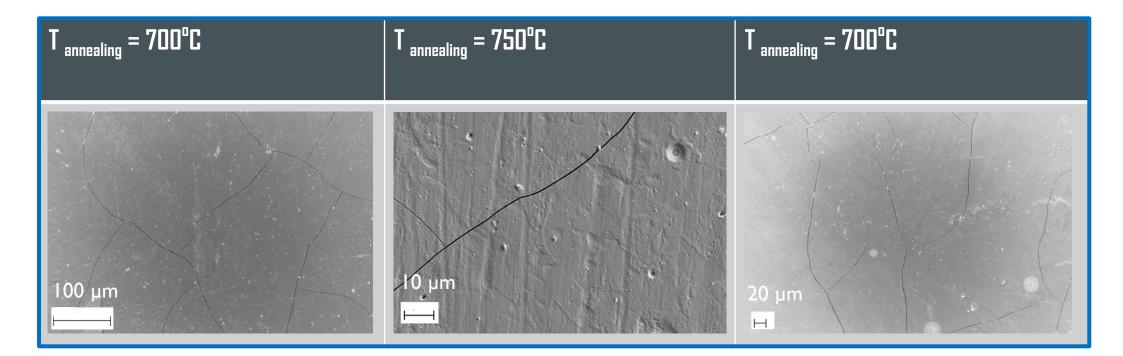
AI5 phase formation. XRD analysis & Morphology

Texturation - Preferred orientation of (200)



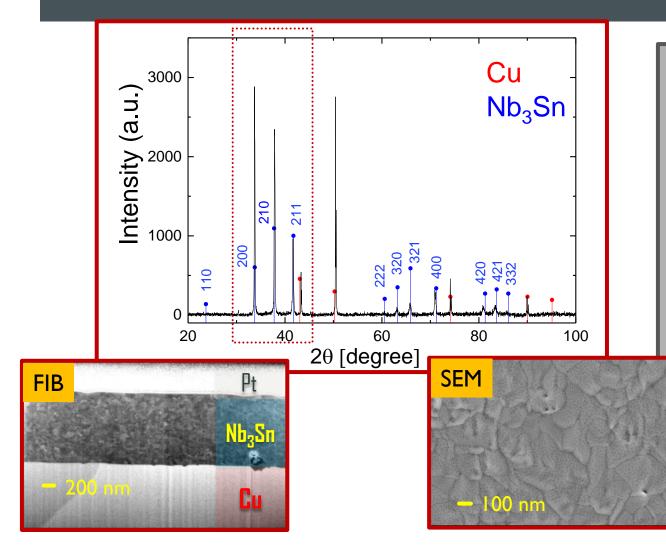


CRACKING OF THE FILMS AFTER ANNEALING

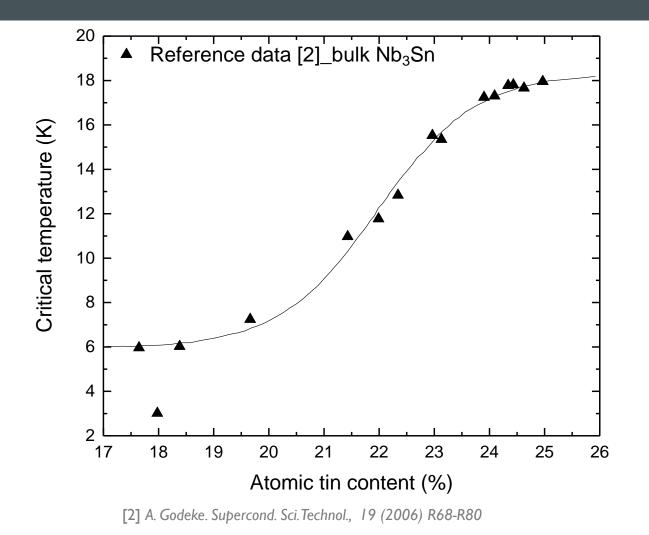


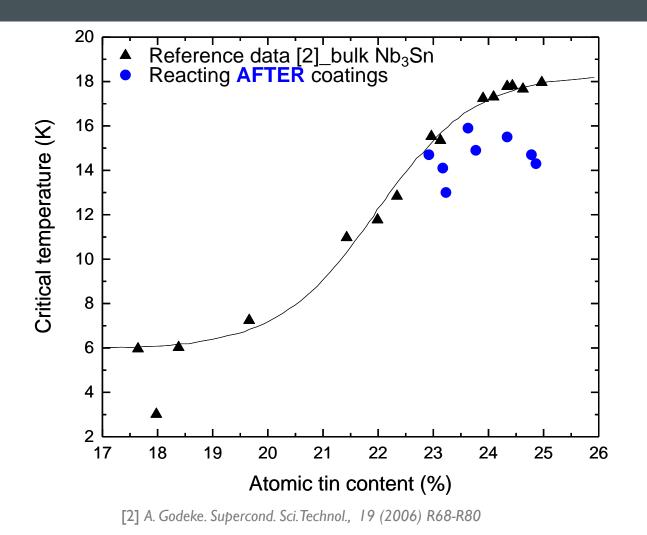
Without solving "cracking" problem not RF compatible

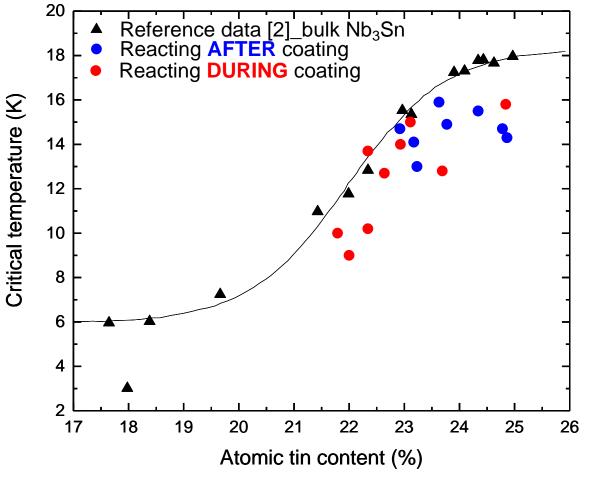
FILMS REACTED DURING COATINGS



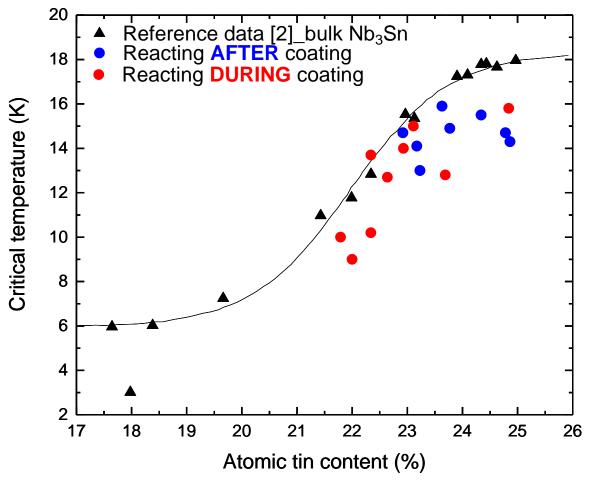
- Characteristics peaks after the coating of (200), (210), (211) ...
 (332) Confirmation of the superconducting A15 phase
- Absence of undesired phases
 NbSn₂, Nb₆Sn₅
- Dense, crack-free morphology







^[2] A. Godeke. Supercond. Sci. Technol., 19 (2006) R68-R80

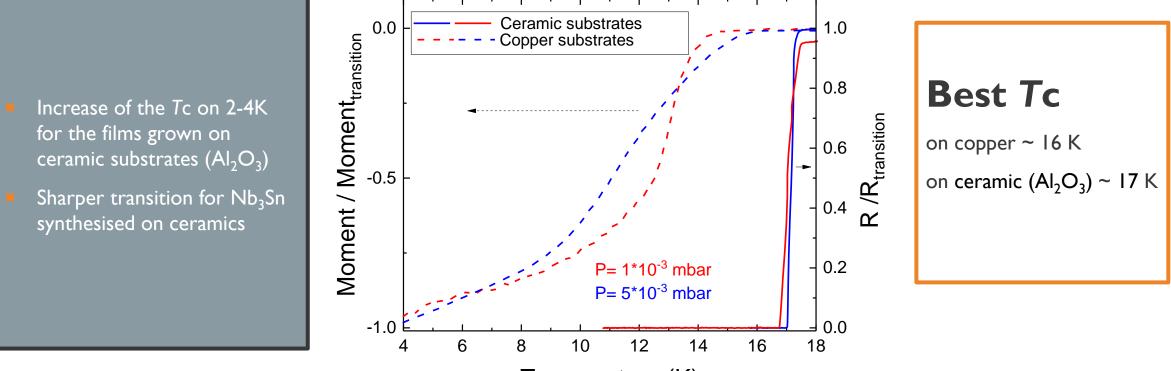




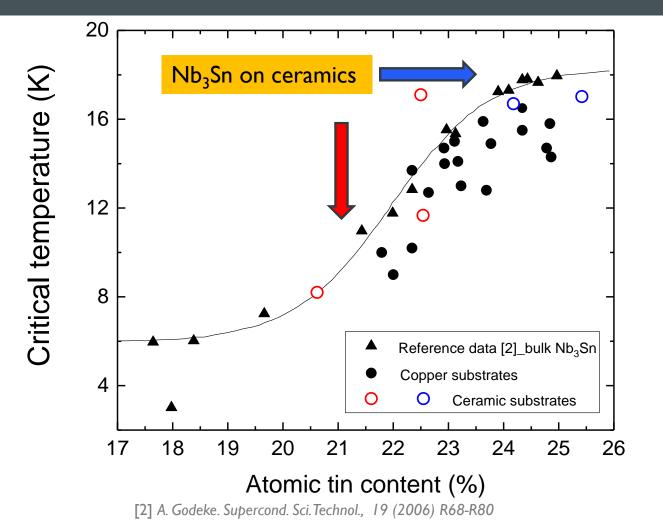
Composition

- Films of Nb₃Sn on copper substrate
- Reacting AFTER /DURING coating
- High temperature treatment duratior
- Additional Annealing

IMPACT OF THE SUBSTRATE CHOICE ON $T_{\rm C}$ TRANSITION



Temperature (K)



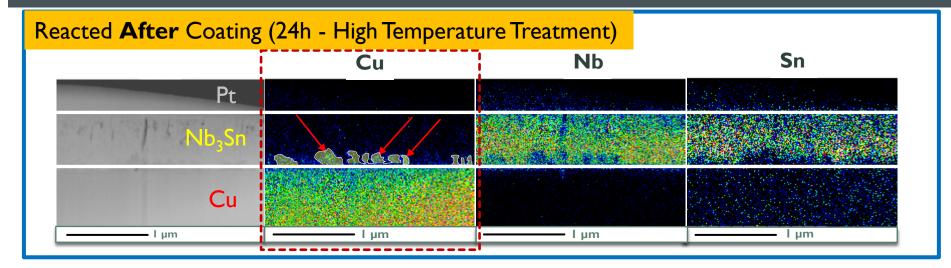
How to increase T_c ?

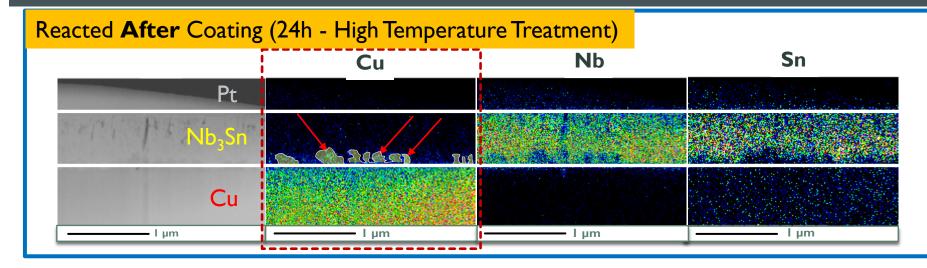
Composition

- Substrate choice
- Reacting AFTER /DURING coating
- High temperature treatment duration
- Additional Annealing

eacted After Coating	(24h High Temperatu	re Treatment)	
	Cu	Nb	Sn
Pt			
Nb ₃ Sn	Sanding the Second Second		
Cu			
I μm	I μm	I μm	I μm

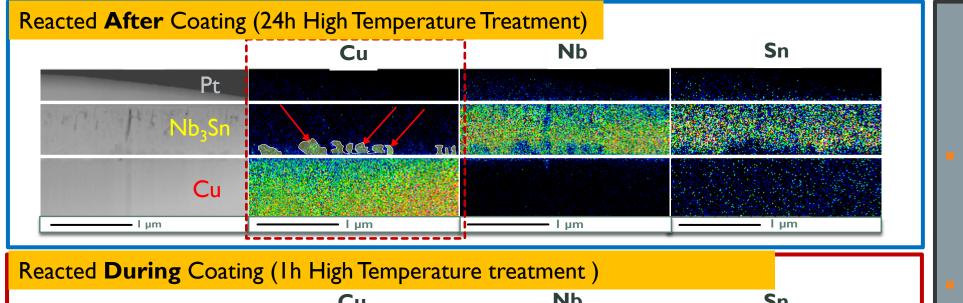
Reacted After Coating (24h High Temperature Treatment)				
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Pt		a and the second second		
Nb ₃ Sn				
Cu				
I μm	Ι μm	I μm	I μm	

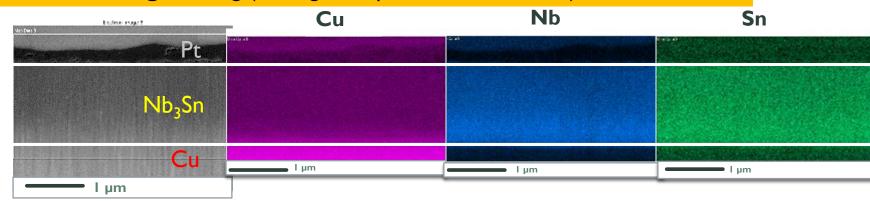




Nb and Sn distribution are **homogenous**

High temperature treatment causes copper interdiffusion





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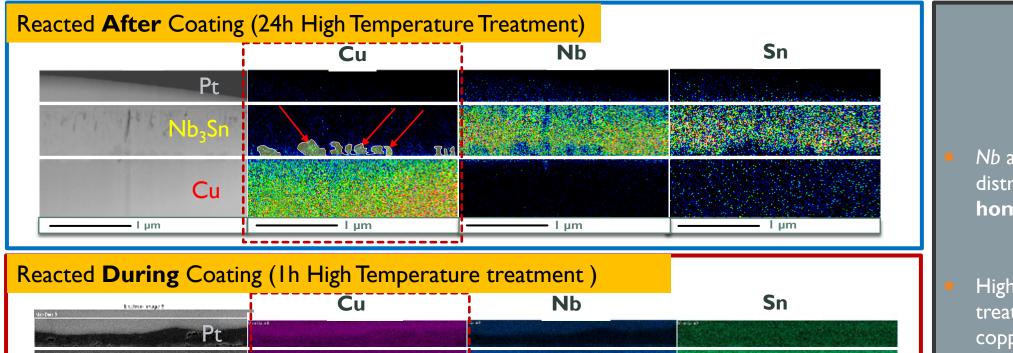
High temperature treatment causes copper interdiffusion

Ιμm

Nb₃Sn

I μm

Cu

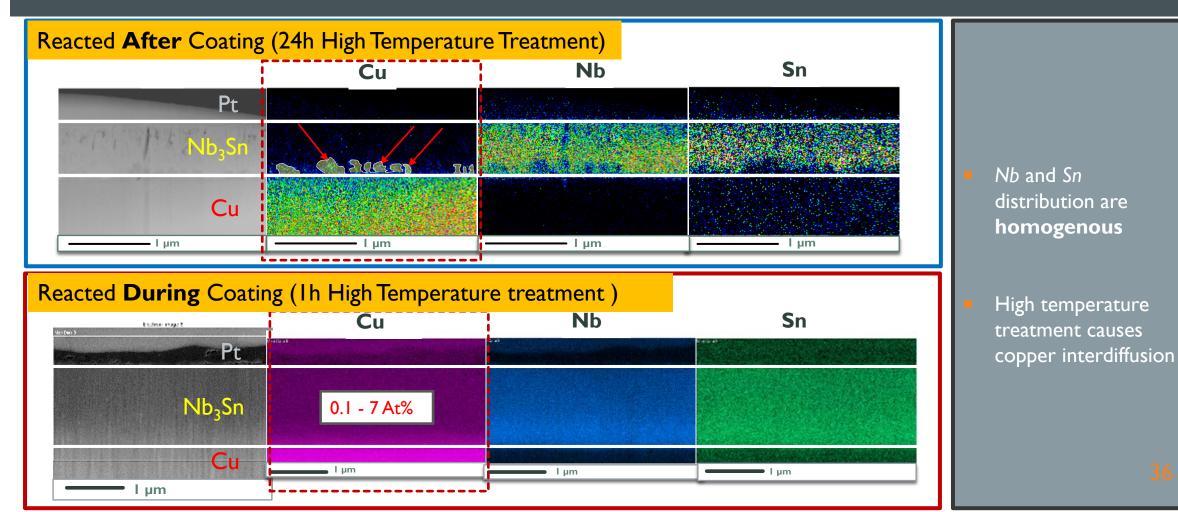


▶ Iµm

l µm

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High temperature treatment causes copper interdiffusion

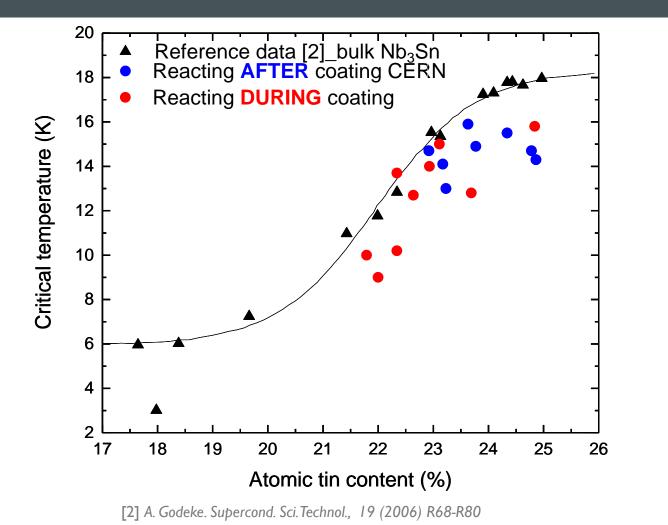


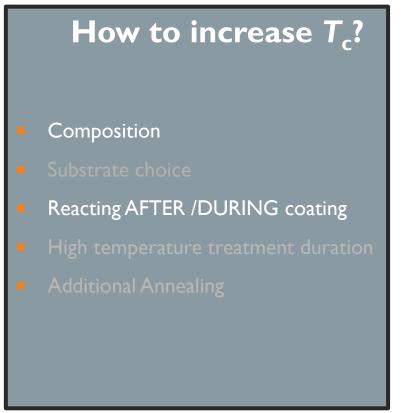
SOLUTION: INTERMEDIATE LAYER

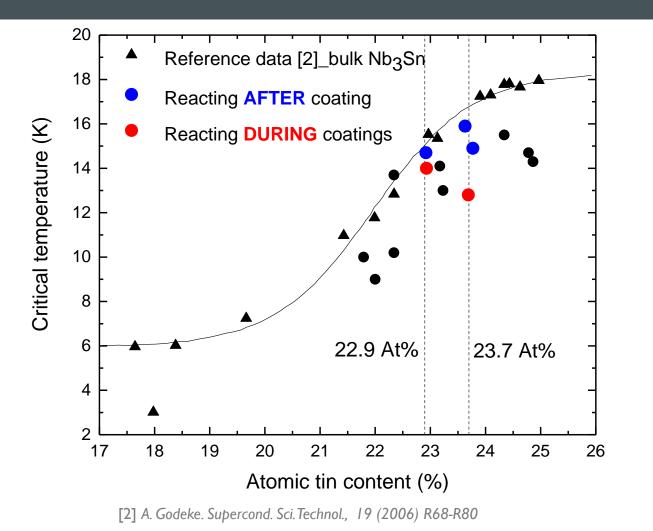
- Works as "buffer" layer to reduce residual stresses in the films (to solve cracking problem for the films reacted AFTER the coating)
- Decrease lattice mismatch, i.e. improving crystalline lattice order (to avoid T_c depression) [3]
- Diffusion barrier layer (to prevent copper interdiffusion into Nb₃Sn layer)

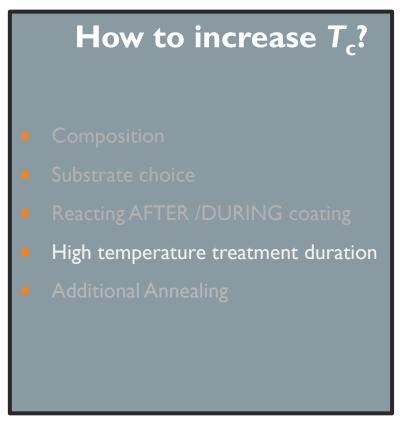
Possible candidates – Nb, Ta, Al_2O_3

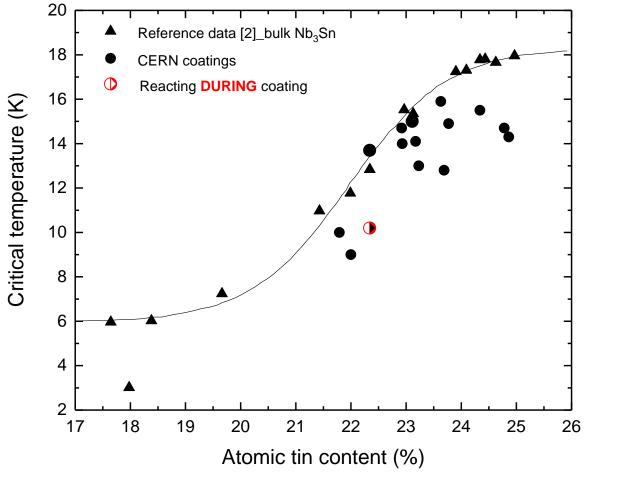
[3] Hein. The AI5 story. The Science and Technology of Superconductivity pp 333-372

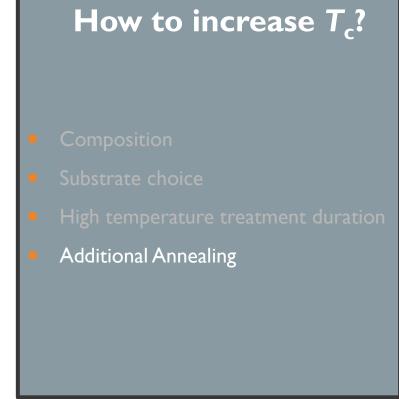


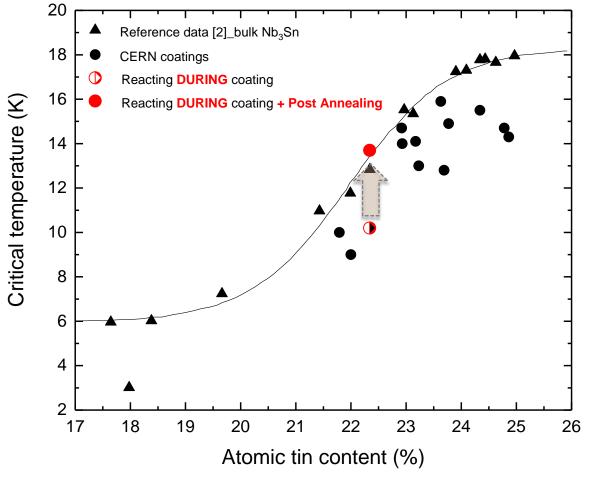


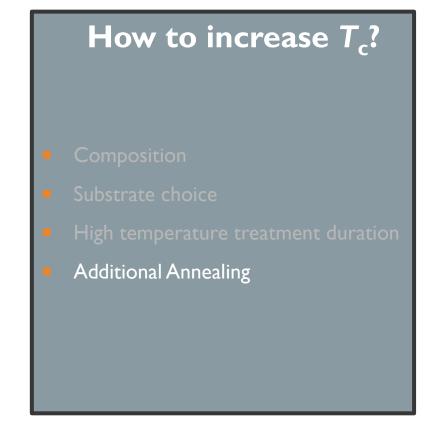


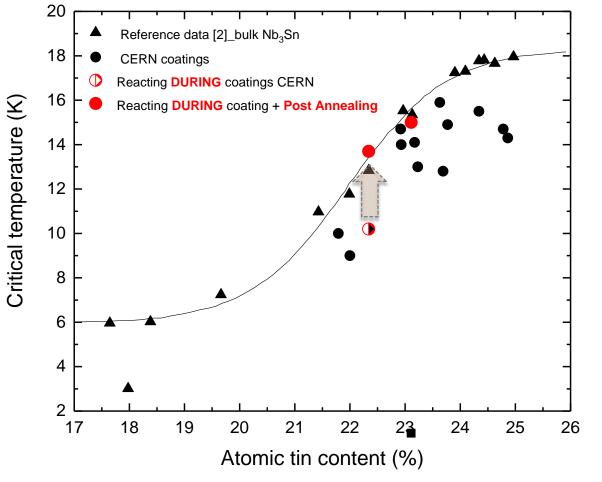


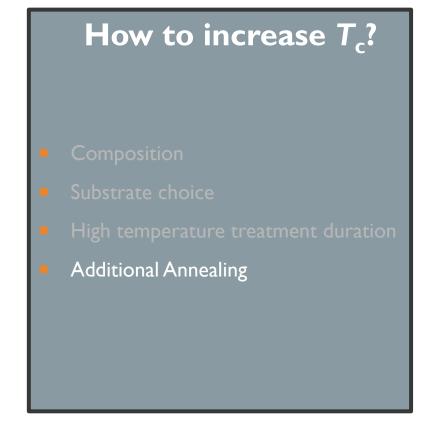






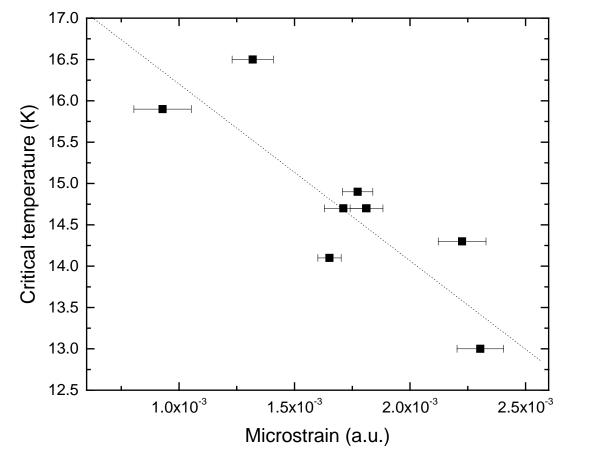






[2] A. Godeke. Supercond. Sci. Technol., 19 (2006) R68-R80

MICROSTRUCTURAL PROPERTIES



- Calculated values from broadening of the diffraction lines using Rietveld analysis [4].
- Only samples reacted AFTER the coating were taken into consideration.
- Uniform residual stress is released but impact of microstrain remains important.
- Dependence of critical temperature on microstrain in the films is established.

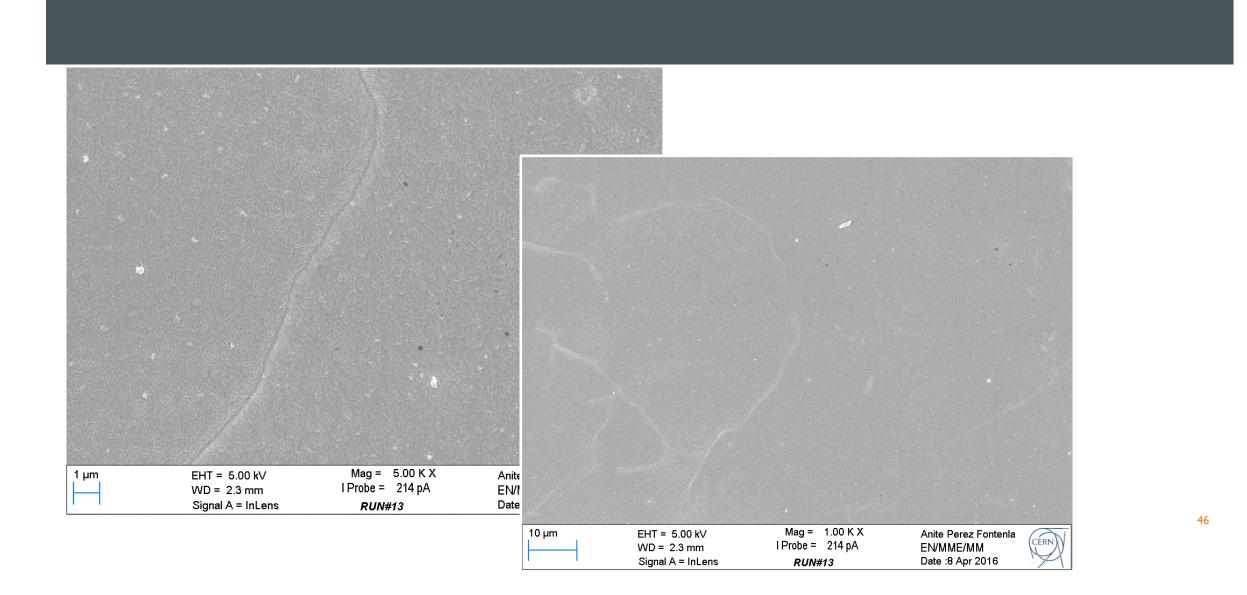
[4] L. Lutterotti, S. Matthies and H. -R. Wenk, MAUD (Material Analysis Using Diffraction): a user friendly Java program for Rietveld Texture Analysis and more, Proceeding of the Twelfth International Conference on Textures of Materials (ICOTOM-12), Vol. 1, 1599, 1999.

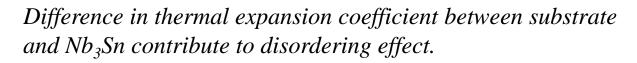
SUMMARY

- We are able to produce high quality films (good composition, crack-free surface, Tc on ceramic ~ 17.2 K and on copper ~ 16 K)
- Impact of the copper substrate, i.e. increasing in disorder degree and copper interdiffusion after annealing, can be minimised by using intermediate layer.
- The recipes for the synthesis applicable for RF applications using both producing routes (reacting AFTER and DURING coating) will be produced.
- Coating of the QPR sample in order to test RF properties of the film is planned for the beginning of the next year.



Thank you for your attention!





Element	α (x Ι0 ⁻⁶) Κ ⁻¹
Cu	16.8
Та	7.64
Nb	7.02
Nb ₃ Sn	6.3

In BCS theory:

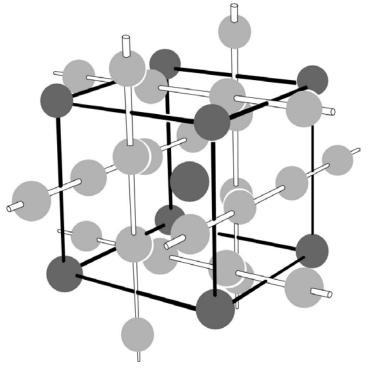
 $T_c \simeq \theta_D e^{-(1/N(0) \cdot V^*)}$

 $\theta_{\rm D}$ – Debye temperature N(0) – density of state at the Fermi surface V^* - interaction between electron and lattice vibration

From this expression one sees that a large N(0), implies a large T_c . The BCS interaction parameter, V^* , is approximately a constant. [5]

[5] SUPERCONDUCTING INTERMETALLIC COMPOUNDS - THE AIS STORY. Robert A. Hein. U. S. Naval Research Laboratory Washington, D. C. 20390

W. D. Gregory et al. (eds.), The Science and Technology of Superconductivity Plenum Press, New York 1973



 $\downarrow d \Rightarrow \uparrow N(0)$

d – interatomic distance between *Nb* atoms

$\uparrow N(0) \Rightarrow \uparrow T_{\rm c}$

"A15 phases." <u>McGraw-Hill Concise Encyclopedia of</u> <u>Physics</u>. 2002. The McGraw-Hill Companies, Inc. 3 Nov. 2017 https://encyclopedia2.thefreedictionary.com/A15+phases

