Towards TPC Signal Formation, Simulation in Single Phase LArTPC

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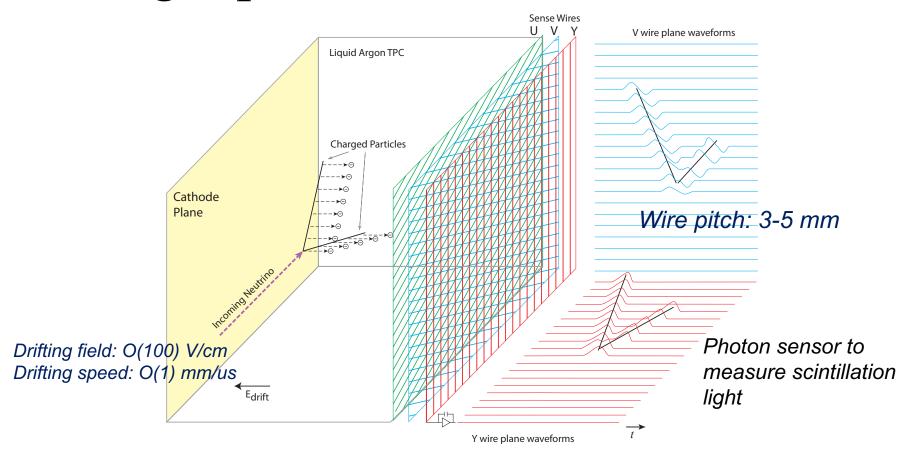
APA consortium meeting Sep. 18, 2017

Outline

MicroBooNE detector context and experience.

- LArTPC introduction
- Signal formation (wire readout)
- Signal simulation (time & wire dimension)
- Noise simulation (analytic method)
- Summary

Single phase LArTPC



- ✓ Wire readout instead of pixel readout
- ✓ Three wire planes in general design sense the induced current signal.

Signal Formation

Definition: from ionization electrons to ADC waveforms

LAr

At production

- ✓ Ionization
- ✓ Recombination (signal loss)

In drifting

- ✓ Diffusion (signal shape change)
- ✓ Attachment/absorption (signal loss)

Wire induced current (field response)

Long-range effect

- √ Time dimension
- ✓ Wire dimension

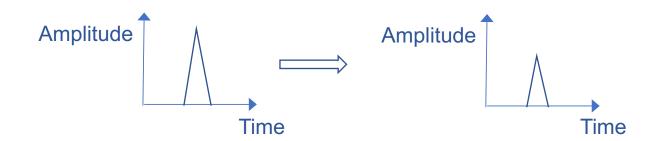
Electronics

Cold electronics

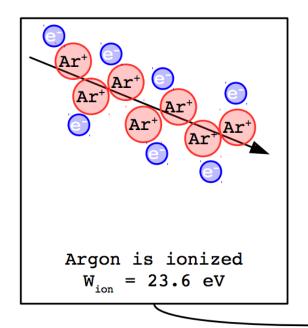
- ✓ Preamplifier
- ✓ RC filter
- ✓ ADC

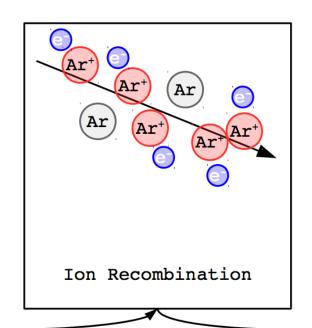
In uBoone, only cold preamp In future design, all in cold

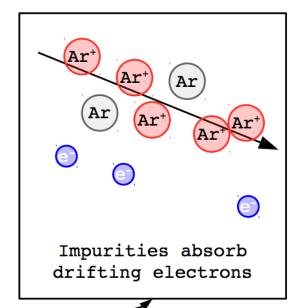
Signal formation – signal loss in LAr



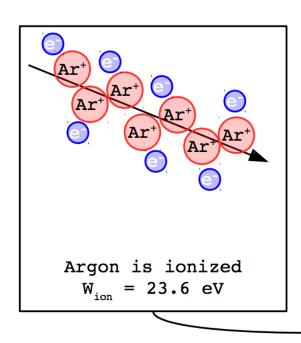
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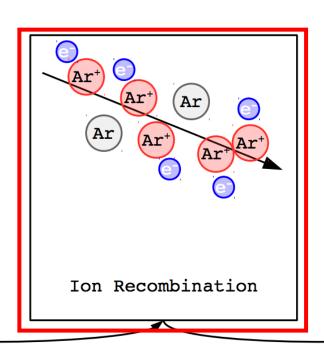




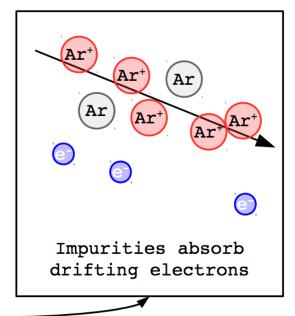


Signal formation – signal loss in LAr





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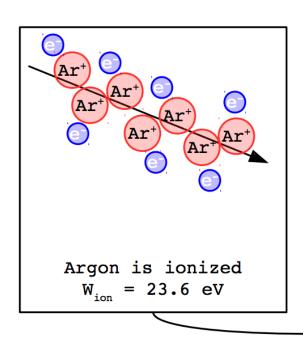


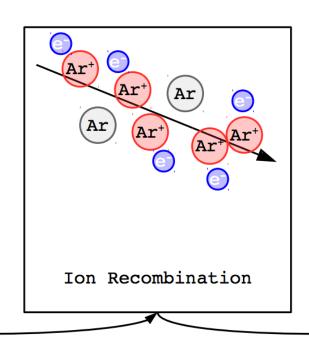
$$R = \frac{dQ/dx}{dE/dx}$$

$$R \cong 60\% \text{ @87K, 273V/cm}$$

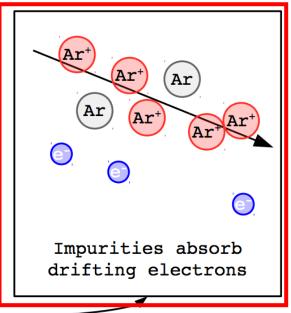
$$R \cong 70\% \text{ @87K, 500V/cm}$$

Signal formation – signal loss in LAr





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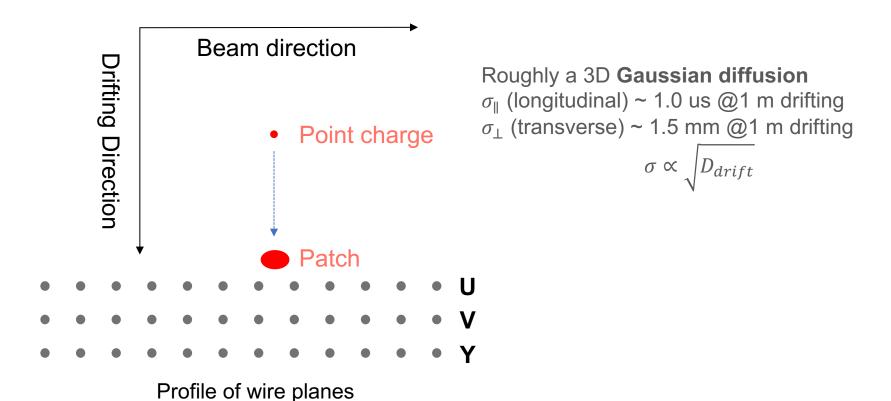


 $L=e^{-t_{drift}/\tau}$, τ is defined as electron lifetime, τ > 18.5 ms (normal MicroBooNE operation, O_2 equivalent contamination < 16 ppt)

Maximum signal loss <12% at MicroBooNE (2.3 ms drift from anode to cathode).

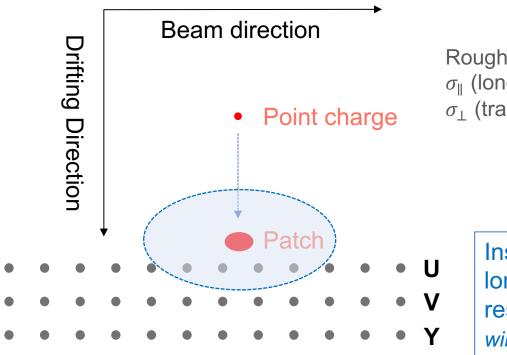
Signal formation – diffusion in LAr

- Signal shape change
 - Longitudinal (time dimension)
 - Transverse (wire dimension)



Signal formation – diffusion in LAr

- Signal shape change
 - Longitudinal (time dimension)
 - Transverse (wire dimension)



Roughly a 3D **Gaussian diffusion** σ_{\parallel} (longitudinal) ~ 1.0 us @1 m drifting σ_{\perp} (transverse) ~ 1.5 mm @1 m drifting $\sigma \propto \sqrt{D_{drift}}$

Insignificant in comparison with long-range wire induction field response (signal expansion in time & wire dimensions)

Profile of wire planes

Field response

- Wire readout induced current signal
 - All three wire planes (induced signal ceased at collection)

Weighting Field of a U Wire

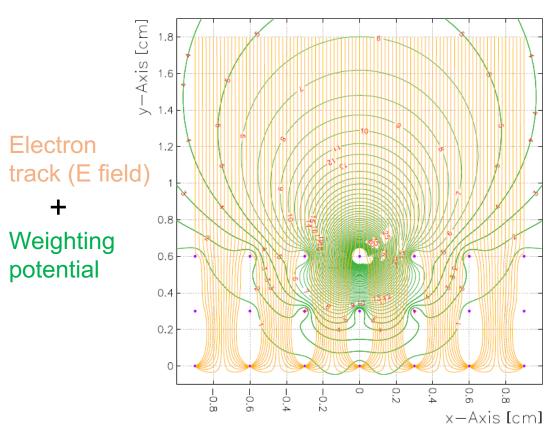
Shockley-Ramo theorem

$$i = -q \cdot \vec{E}_w \cdot \vec{v}_q$$

$$\int idt = q \cdot (V_w^{end} - V_w^{start})$$

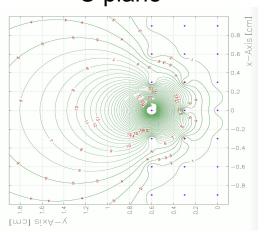
 E_w/V_w : weighting electric field/potential

- placing the target wire to the unity potential, and the rest to zero
- Long range effect

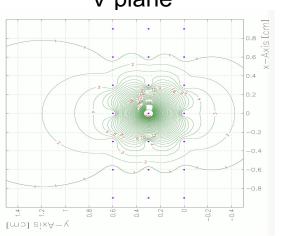


Field response -- 2D Garfield calculation

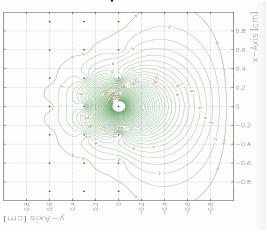
Weighting potential U plane



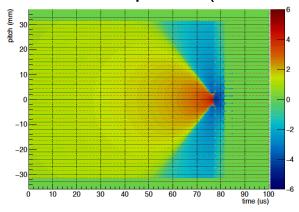
V plane

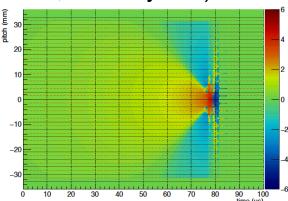


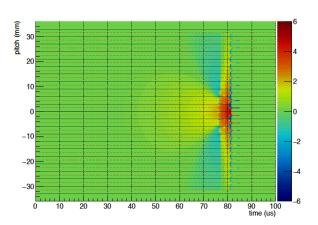
Y plane



Field response (Plot in log scale, arbitrary unit)

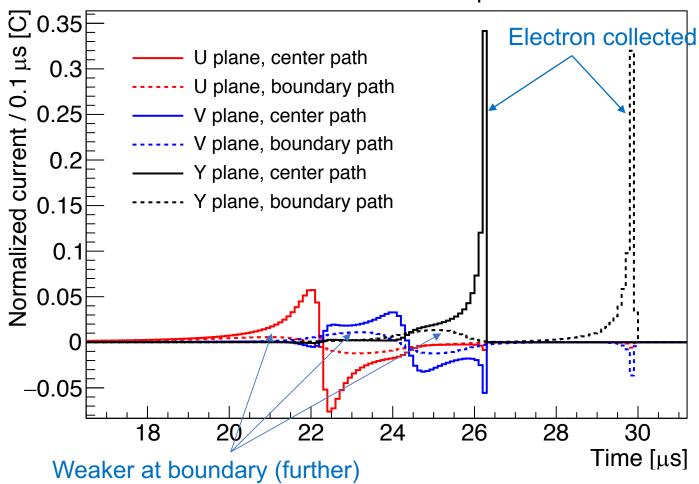






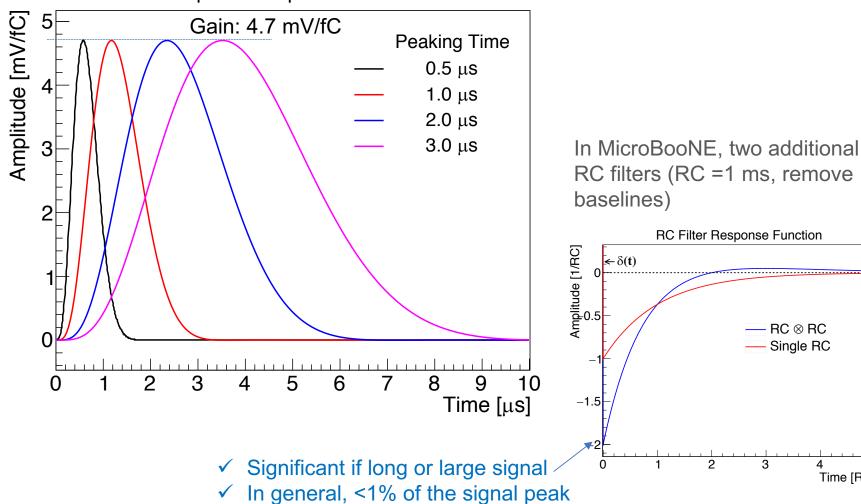
Field response shape

Central Wire Field Response



Electronics responses



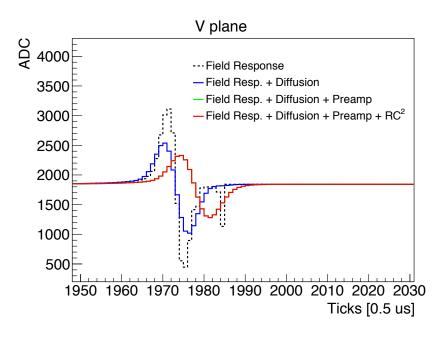


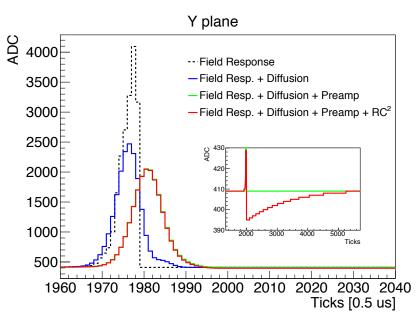
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Time [RC]

 $\mathsf{RC} \otimes \mathsf{RC}$ Single RC

Overall response





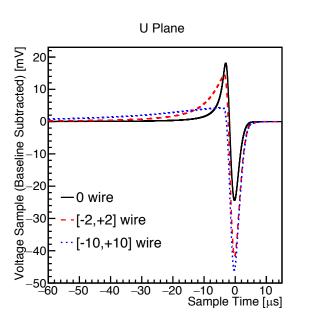
- ✓ Effects/Responses changing the signal shape (from a point source of charge)
- ✓ In time dimension

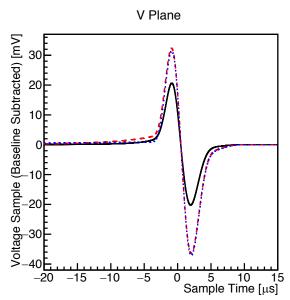
Do not forget about signal shape changes/smearing in wire dimension

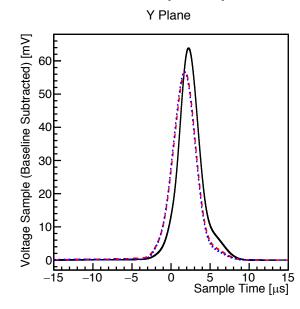
- Diffusion
- Field response

Responses over wires

Field response + Pre-amp response



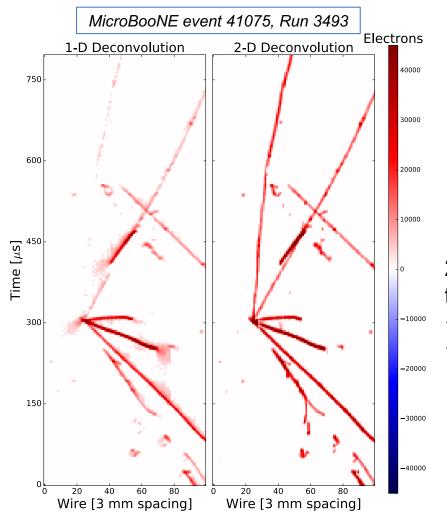




- ✓ Significant contribution from adjacent wires
 - √ [-10, 10] (21) wires for U plane
 - ✓ [-2, 2] (5) wires for V, Y planes (shield by U plane)
- ✓ Equivalent to an isochronous track (parallel to wire plane) and perpendicular to wire orientation (along wire pitch direction)

2D signal formation validation

Largely by 2D (time + wire dimension) field response



Reconstructed charge after signal processing (kernel -- deconvolution)

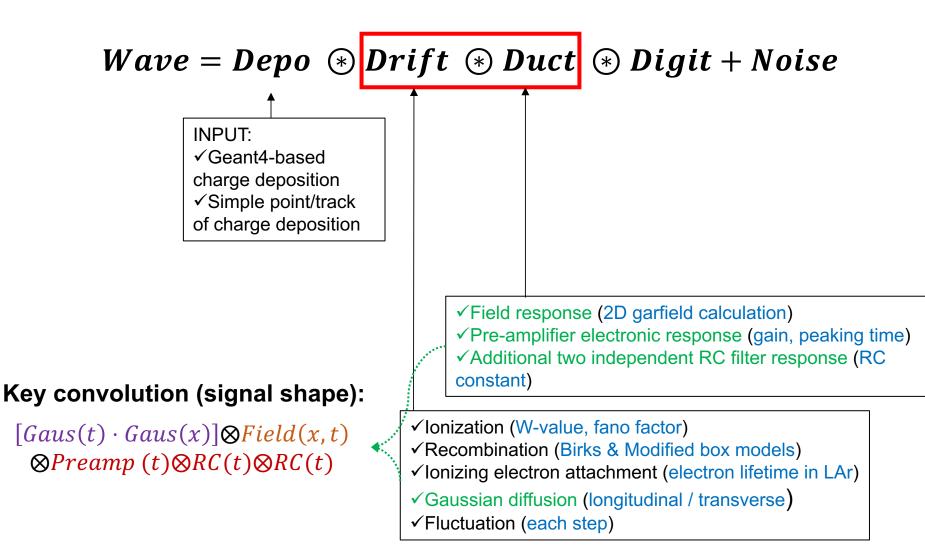
2D decon has much better performance than 1D decon

- ✓ Significantly improved for large angle track
- ✓ Intense charge density along the track

TPC signal simulation

Consist with abovementioned 2D signal formation

Overview of full TPC simulation



Interpolation of field response

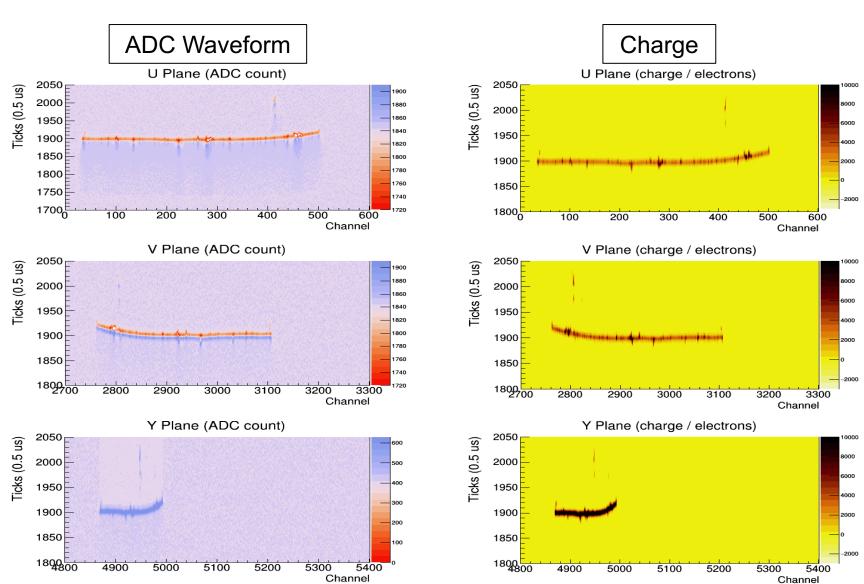
Input (126 paths): $Diffusion[Gaus(t) \cdot Gaus(x)]$ $0 \pm 10 \text{ wires (63 mm)}$ Fine-grained calculation (per 0.3 mm) $\bigotimes Field(x,t)$ \otimes Preamp $(t)\otimes$ RC $(t)\otimes$ RC(t)Linear interpolation performed A large angle (to wire plane) track Average Linear 1000 1000 Naveform (a.u.) Waveform (a.u.) 500 500 -500 -500 -1000-1000-1500-1500-50-2000 -2000800 1000 1200 1400 1000 1200 1400 -2500L -25001000 1500 2000 500 500 1000 1500 2000 **Ticks**

Non-proper bipolar cancellation at boundary of 0.3 mm sub-pitch

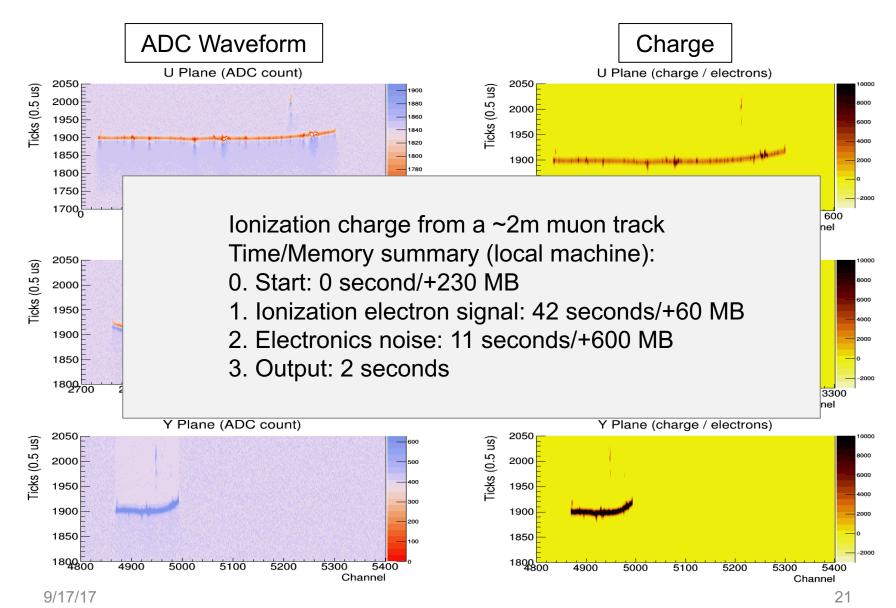
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Ticks

A simulation of 5-GeV muon



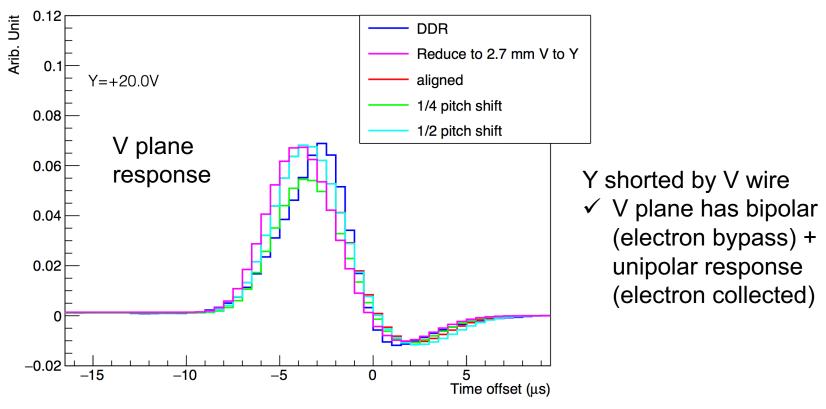
A simulation of 5-GeV muon



Shorted wire region

 Some special field response, e.g. shorted wire region of MicroBooNE detector, stays tuned by data-driven result.

DDR Vs. Garfield V plane Y-short Comparison



Noise simulation

- Inevitable in the electronics
- Critical to the signal processing (ADC waveforms to ionization charge)

Pre-amplifier inherent noise

					41 Mi D NE Linuid Anno - TDO!
noise type	also called	normalization	Time Domain pulse	s domain	the MicroBooNE Liquid Argon TPC", JINST 12 (2017) P08003 Thermal
Thermal 1	series white	$\sqrt{2k_BT_{temp}R_S} \times C_{\text{det}}$	$\times G \cdot \delta(t - t_j)$	$\times G \cdot e^{-st_j}$	fluctuation in the input transistor
Thermal 2	parallel white	$\sqrt{2k_{B}T_{temp}/R_{F}}$	$\times G \cdot u(t-t_j)$	$\times \frac{G}{S} \cdot e^{-st_j}$	Transistor bias current and resistors providing the bias voltage
Shot noise	parallel white	$\sqrt{qI_{leakage}}$	$\times G \cdot u(t-t_j)$	$\times \frac{G}{S} \cdot e^{-st_j}$	
Flicker noise (1/f or pink)	series 1/f	$C_{ m det} \sqrt{2\pi a_{\scriptscriptstyle F}}$	$\times \frac{G}{\sqrt{\pi \cdot (t - t_j)}}$	$\times \frac{G}{\sqrt{s}} e^{-st_j} \blacktriangleleft$	Charge trapping and de- trapping in the input
Man made noise	Various couplings	Usually has discrete frequency spectrum. Ignored here, could be modeled.			transistor

"Noise Characterization and Filtering in

- \diamond Noise occurring time t_i is uniformly distributed (origin of the fluctuations)
- In frequency domain, given a ω_0 , the stochastic effect just in phase term $e^{-i\omega_0 t_j}$ (delta function at t_i in time domain)

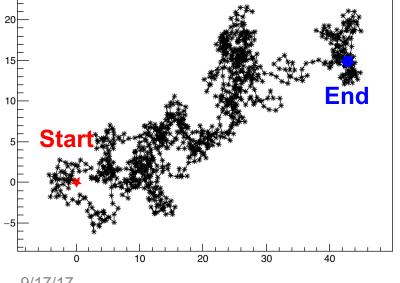
Noise -- Random Walk

Noise in frequency domain:

$$F(\omega) \propto \sum_{i=1}^{N} q_i(\omega) \cdot e^{-i\omega t_i} = \sum_{i=1}^{N} L(\omega) \cdot e^{-i\cdot\alpha}$$

Sign of q_i (Bernoulli variable)

- unnecessary to be 50% + (-)
- absorbed into phase term



 α is uniformly distributed in [0, 2π)

o N needs to be large enough

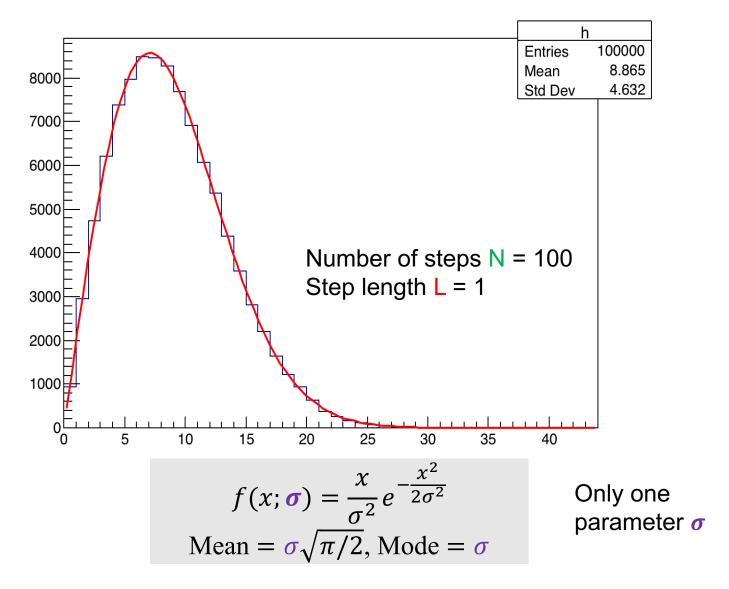
 $F(\omega)$ follows a random walk in the complex plane with the step length $L(\omega)$

How to describe vector 'End – Start'?

Amplitude: Rayleigh distribution

Phase: uniform

Rayleigh distribution

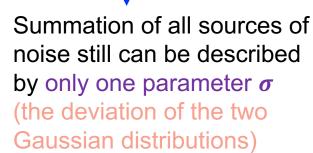


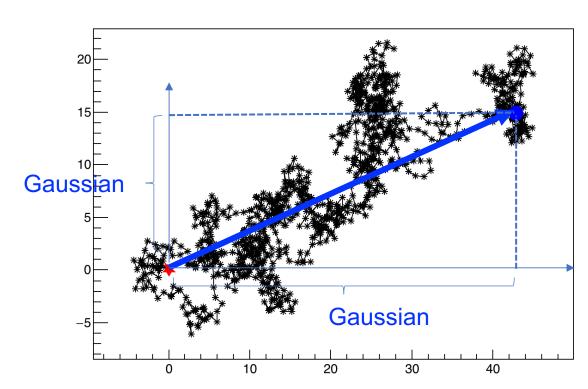
A simpler view

Random Walk (Rayleigh distribution + uniform phase):

Two independent Gaussian distributions with same deviation (the only parameter σ in Rayleigh distribution)

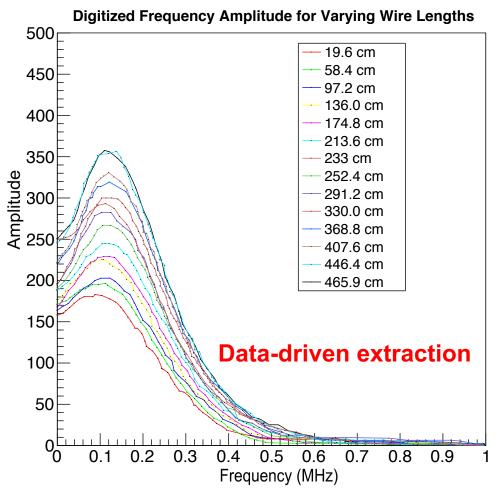
Additivity property of Gaussian distribution



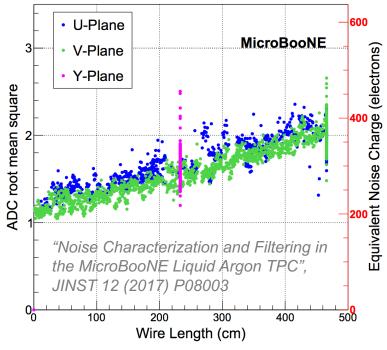


Only the mean amplitude of $F(\omega) = \sqrt{\pi/2} \cdot \sigma$ is needed

Mean frequency amplitude



Wire Noise Level in MicroBooNE



Summary

- The single phase LArTPC signal formation has been presented.
- 2D (time & wire) response is demonstrated.
- A corresponding/consistent signal simulation is introduced.
- A new analytic method of noise simulation is introduced.

Two MicroBooNE papers

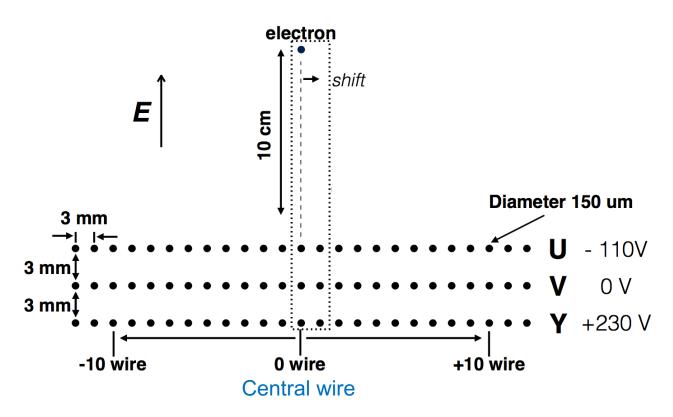
- Ionization signal analysis and processing in single phase LArTPCs
 - Paper 1: signal formation, simulation, extraction (signal processing)

Starting review.

- B. Russell will give a talk about the signal processing.
- Paper 2: data/MC comparison and performance in MicroBooNE

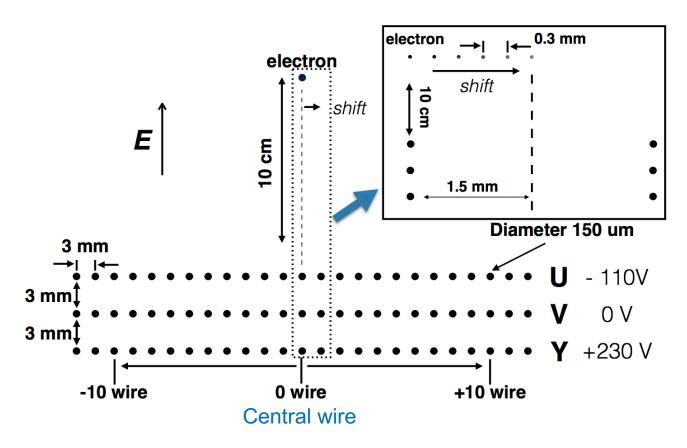
Be ready soon.

Field response -- 2D Garfield calculation



- ✓ A 2D configuration for MicroBooNE
- ✓ Average crosscut (ignore the dependency, residual 3D effect) along wire orientation

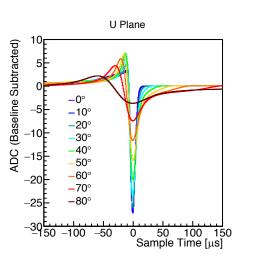
Field response -- 2D Garfield calculation

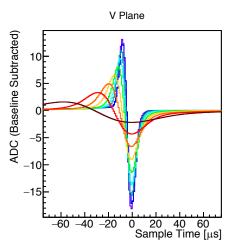


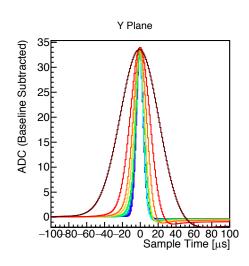
- ✓ 6 drifting paths (per 0.3 mm) for half wire pitch, the other half symmetrical.
- \checkmark 0 ± 10 wires
- √ 126 field responses are calculated

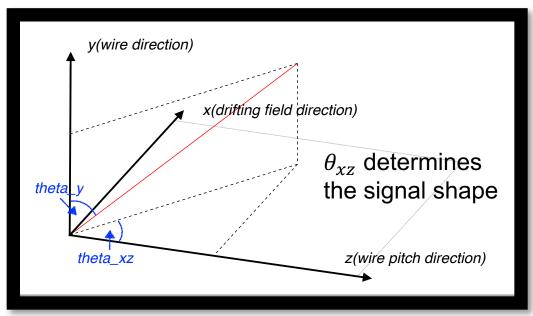
Topology-dependent event

Varying θ_{xz} given $\theta_y = 90^\circ$ (perpendicular to wire orientation)









Topology-dependent event

Varying θ_y given $\theta_{xz} = 0^\circ$ (isochronous)

