

Resonance Control of LB650MHz and HB650MHz SRF Cavities

*Yuriy Pischalnikov
in behalf of the Tuner Team*

December 7, 2017

*Technical Meeting
with Peter McIntosh and Alan Wheelhouse*

Outline

- **Status of Tuner Design for LB/HB650MHz and HB650MHz SRF Cavities**
Modification of Tuner design
 - (goal → Lower LFD → high tuner/dressed cavity stiffness)
- **FNAL's Resonance Control experience**
 - (LFD & microphonics compensation)
- **Reliability of the Piezo Tuner**

“ Some” specs for LB/HB650 MHz Tuner (*challenges*)

1. To design tuner that will work with 3 types of 650MHz cavities

a) $K_{cav.stiffness} \sim 20 \text{ kN/mm}$ (several (4?) cavities built for Project X) $\rightarrow F_{max} \sim 11 \text{ kN}$

b) $K_{cav.stiffness} \sim 4 \text{ kN/mm} \rightarrow F_{max} \sim 4-5 \text{ kN}$ (for newest LB/HB650)

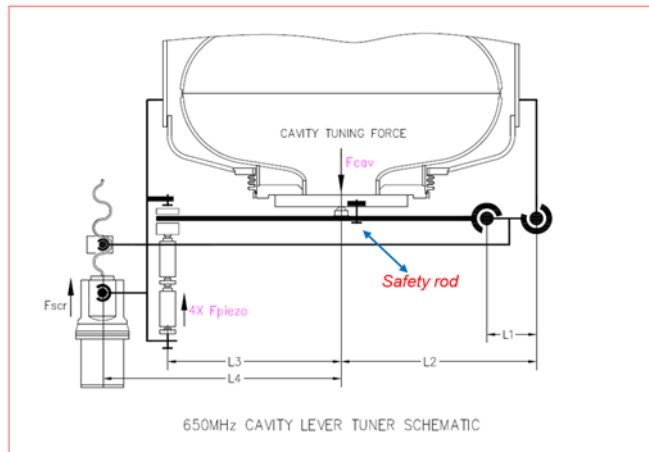
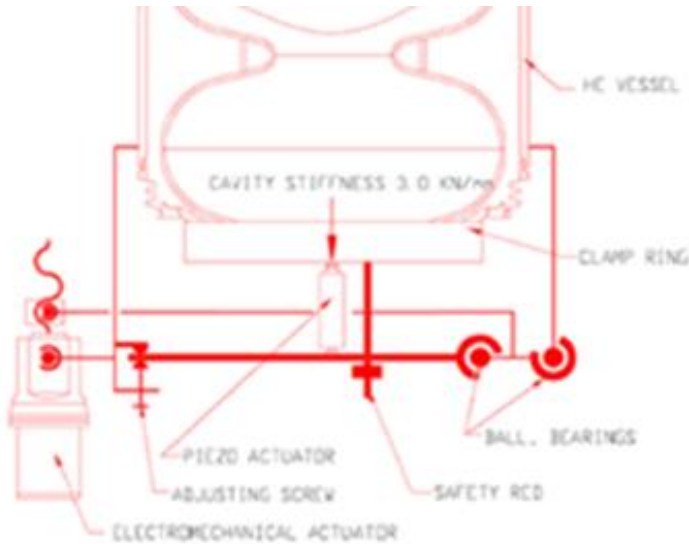
(Overloading piezo-capsules beyond specs !!!)

Decision to move piezo-capsules on the side of Tuner (decreased F_{max} on 50%)
...to keep the required piezo stroke in the specs double amount of the piezo-capsules (in serious)

2. To design tuner with $K_{tuner.stiffness} \sim 70 \text{ kN /mm}$

➤ To minimize K_{LFD}

Tuner specs for 650MHz cavities (0.9; 0.92; 0.61)

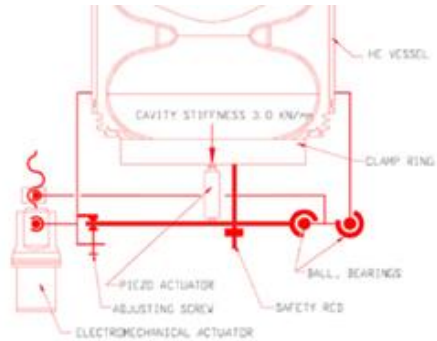
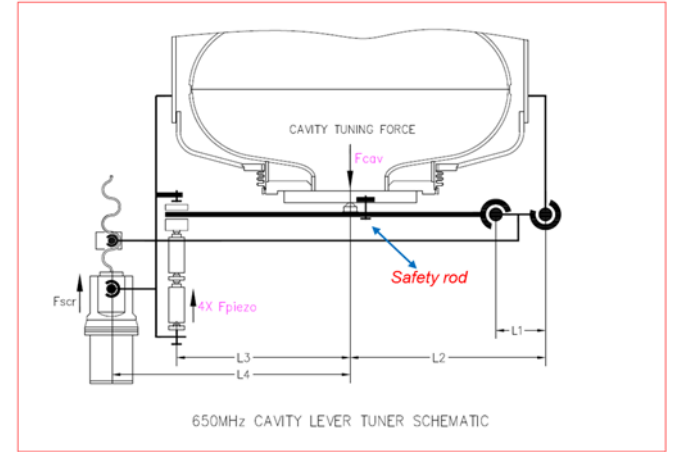
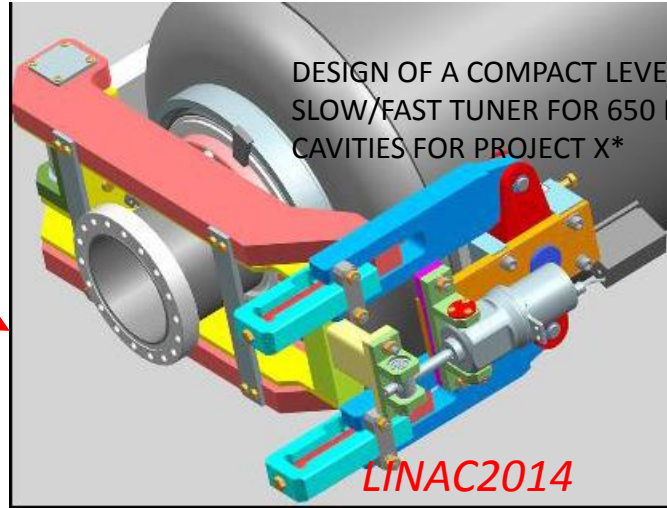
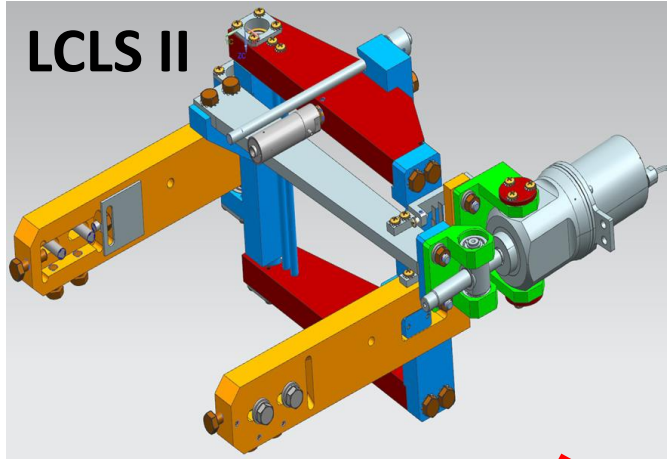


Requirements to built tuner “all size fit all” led to decision to move piezo-capsules to the side and install 4 piezo-capsules
Gain in 2 in forces and gain ½ in stoke

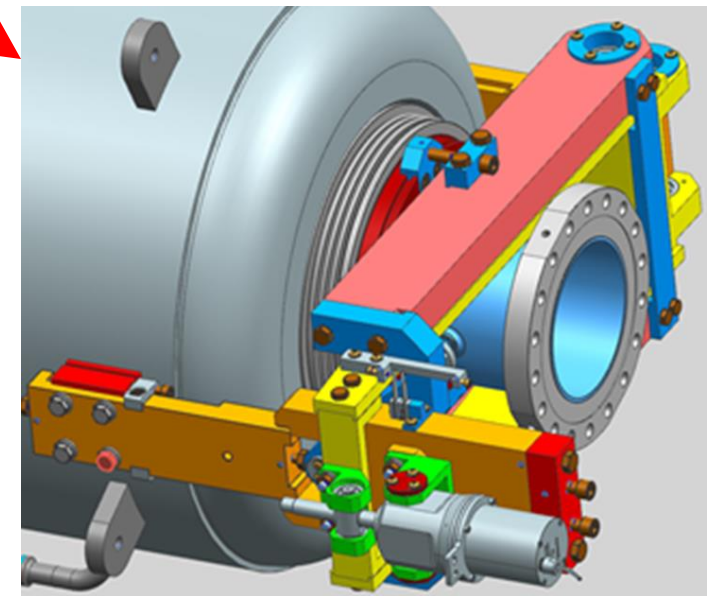
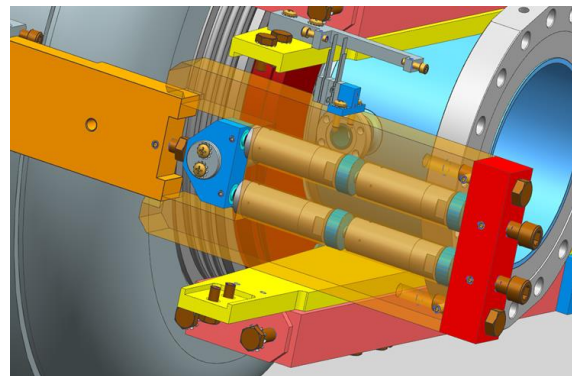
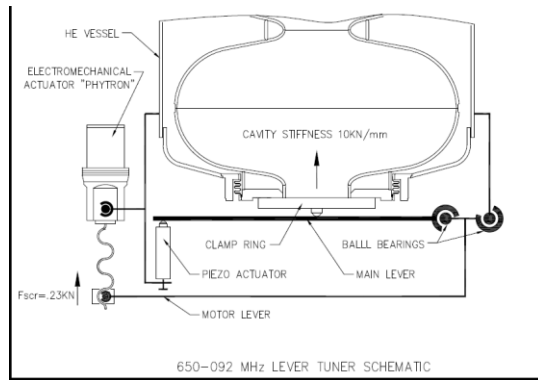
		<i>beta</i>	
	0.9	0.92	0.61
stiffness, (N/um)	20	3-4	3-4
cavity tuning sensitivity, [Hz/um]	180	160	240
bandwidth ($F_{1/2}$), [Hz]	29	29	29
Lorentz Force Detuning coefficient, [Hz/MV/m] ²	<1	<1	<1
Cavity sensitivy to pressure, dF/dp [Hz/mbar]	20	20	20
Tuner stiffness [N/um]	>40	>40	>40
required coarse tuning range, [kHz]	100(60)	200	200
coarse tuner resolution, [Hz/step]	1-2	1-2	1-2
fine tuner range, [Hz]	1200	1200	1200
fine tuner range, [um] at T=20K (20% from RT)	6.7	7.5	5
fine tuner range, [um] at T=300K	33.5	37.5	25
cavity resonance control reqs (peak), [Hz]	20	20	20
fine(piezo) tuner resolution, [Hz]	1	1	1
max. forces on the tuner system, kN	11(7)	5	3.3
max. forces on the each piezo-capsule, kN	6(3.5)	2.5	1.7

!

History of 650MHz Tuner design

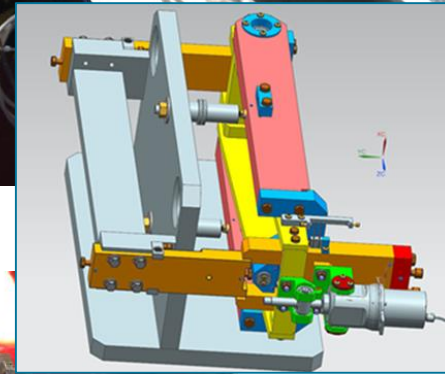
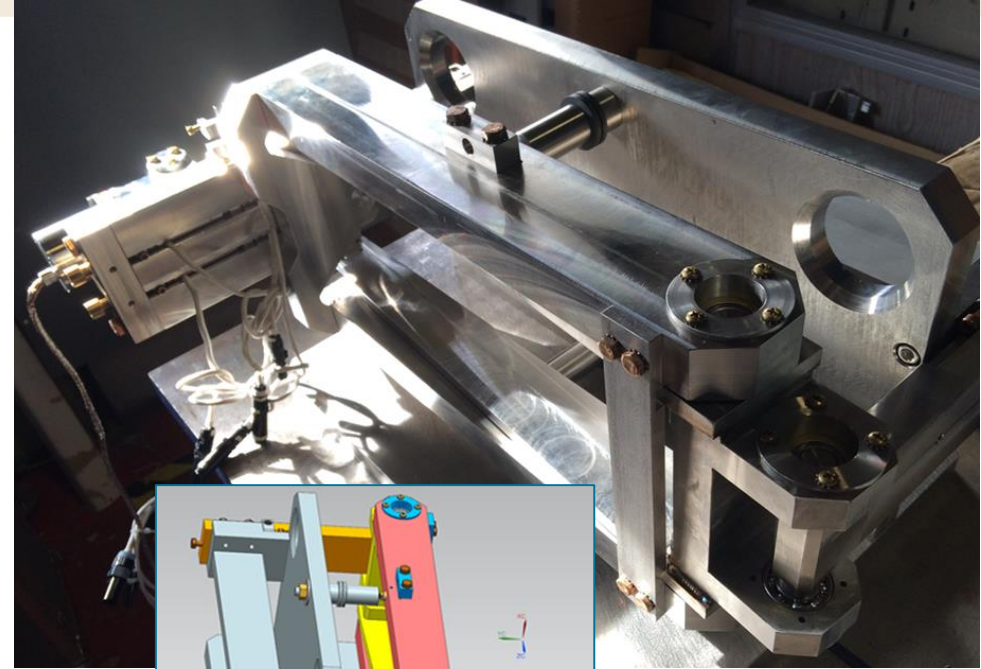
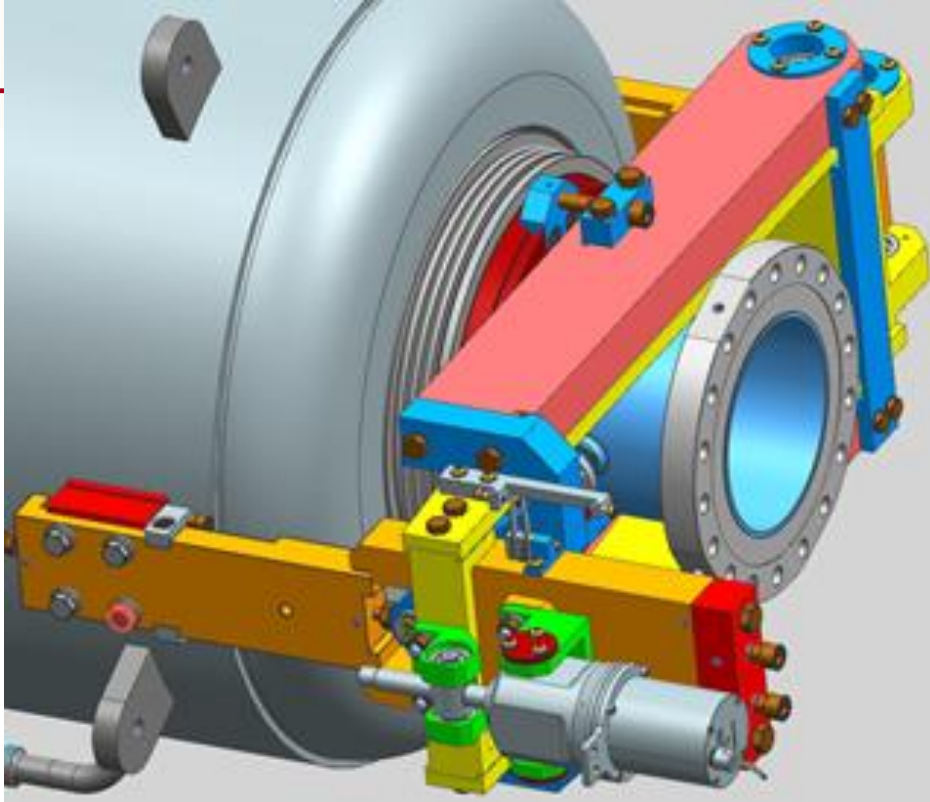


Tuner stiffness
(Ivan's simulations) $\sim 34\text{kN/mm}$

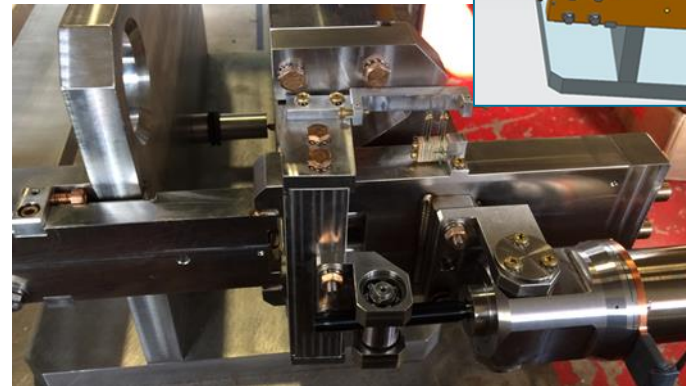


3D-model of the 650MHz tuner

*First prototype tuner assembled
on the of the cavity/He vessel mock-up.
Ready for tests.*



*Initial ANSYS simulations (before
prototype built) stated that
 $K_{tuner} \sim 65-70 \text{ kN/mm}$.
Later we found that model/simulation
was not correct... but only AFTER we
built & tested first prototype.*

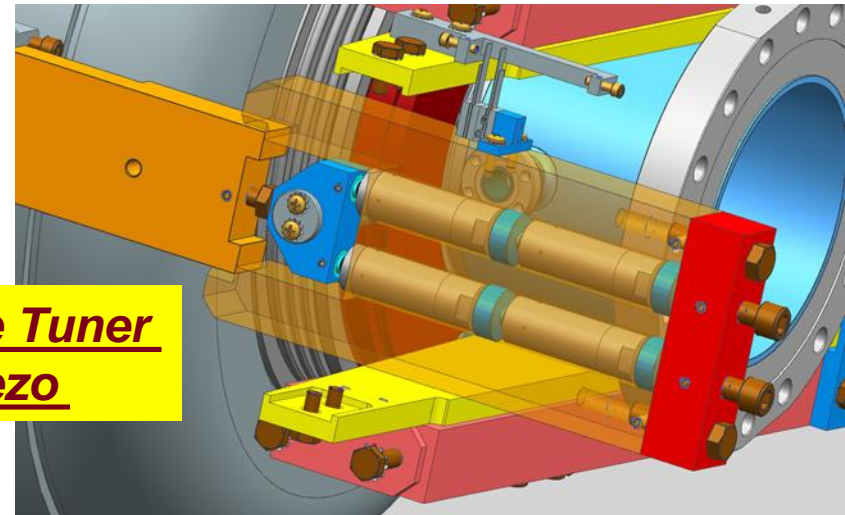


Measurements with Prototype TUNER, mounted on the “cavity’s mock-up” provided us with results that initiate TUNER MODIFICATION efforts.

1. Measured tuner stiffness is **~30kN/mm** (but not 70kN/mm as expected)
 - ❑ *Additional ANSYS expert became involved into development correct tuner model & detail simulations... NOW we have good correlation of simulations & tests results.*
2. Measured fast tuner response (stroke) was **TWO times smaller** than expected (we got at T=300K $\Delta X \sim 17\mu\text{m}$ instead of $\sim \Delta X \sim 36\mu\text{m}$). It will translate to $\Delta F \sim 700\text{-}800\text{Hz}$ (at T=20K)

Both deficiencies (stiffness & piezo stroke) contributed to “complex” fast tuner design.

The Fast/Fine Tuner with 4 piezo

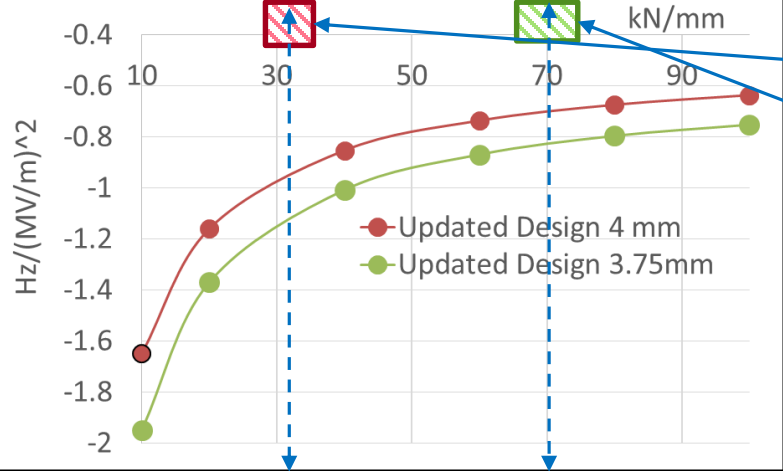


LFD_{static} vs. Tuner Stiffness

Estimated cavity detuning by LF (static)

HB 650MHz

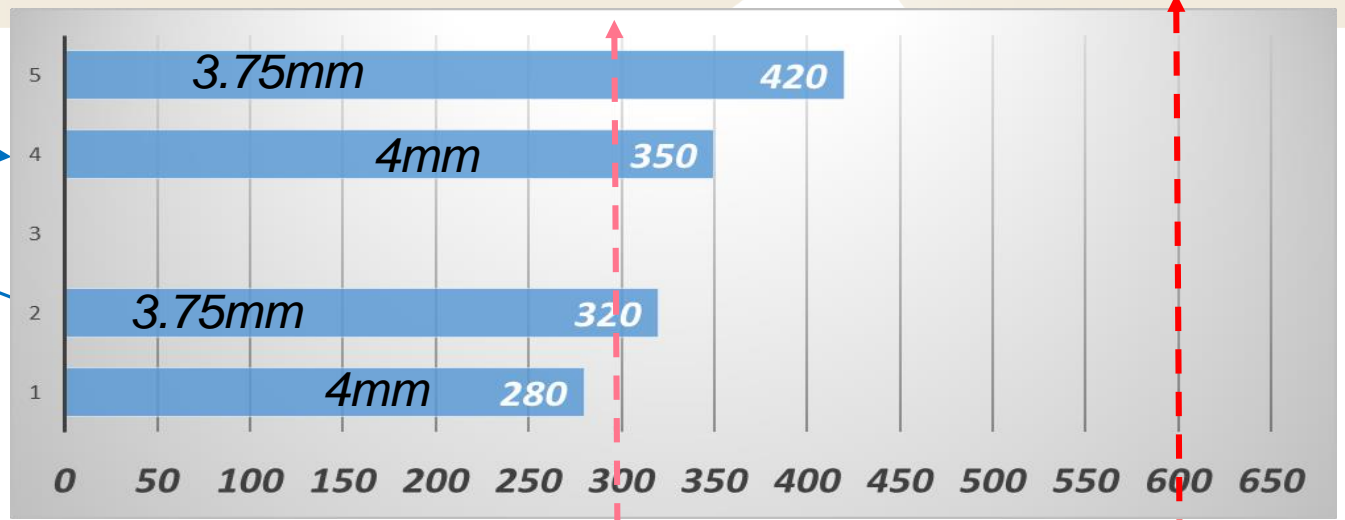
LFD vs. Tuner Stiffness



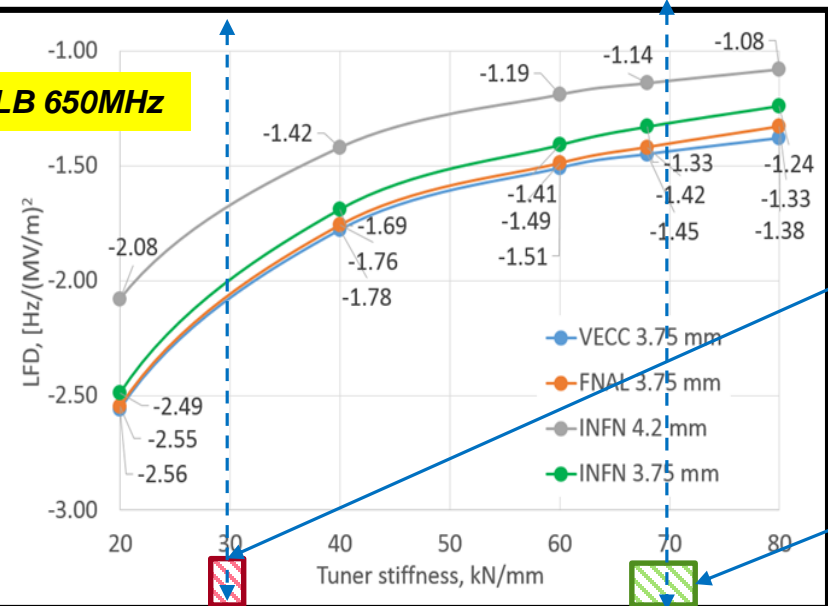
30kN/mm

70kN/mm

18.8 MV/m



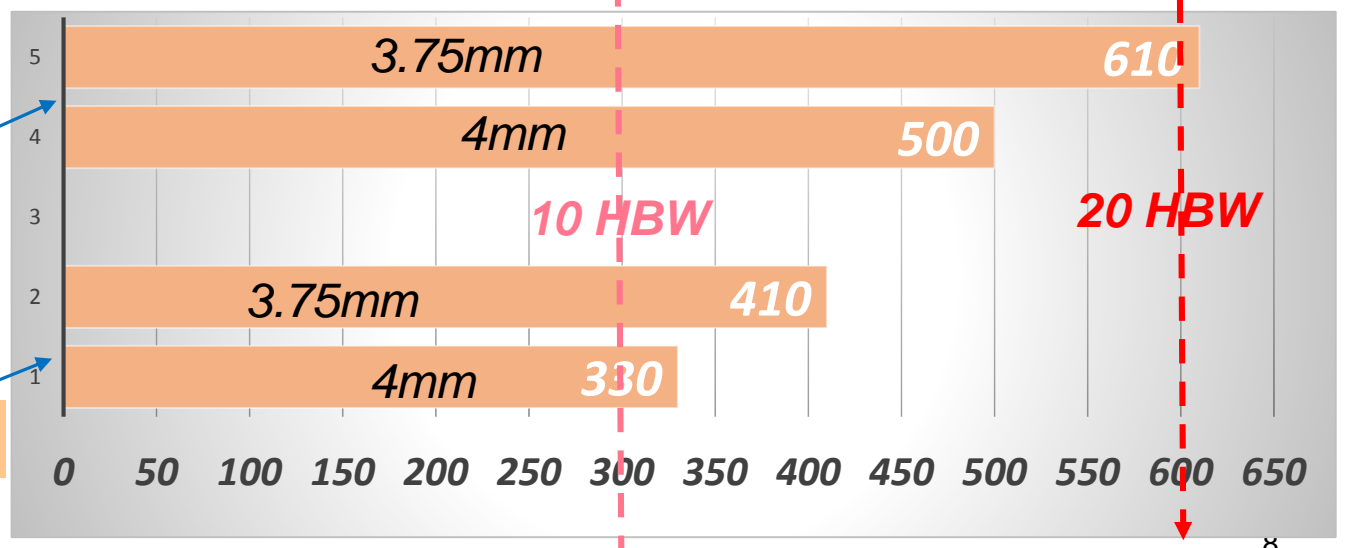
LB 650MHz



30kN/mm

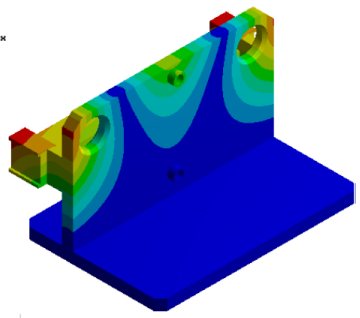
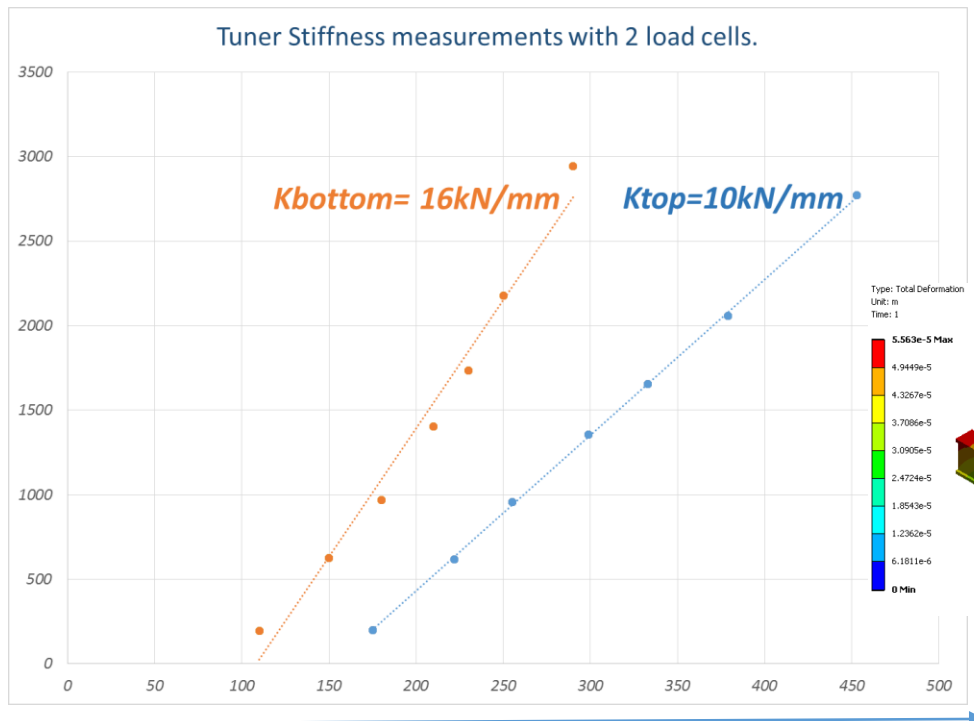
16.9 MV/m

70kN/mm



Measurements of Stiffness of the Tuner, mounted on the test stand

Forces on the Tuner, N

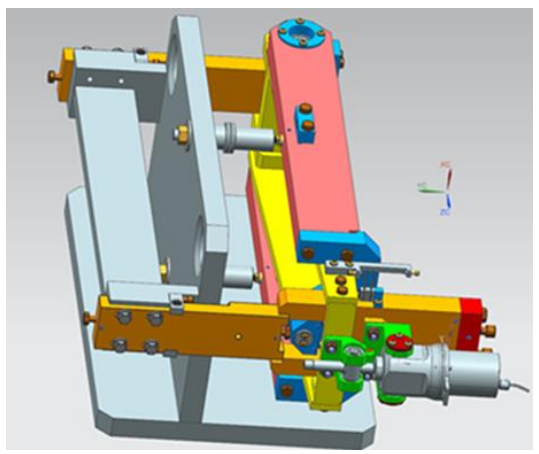
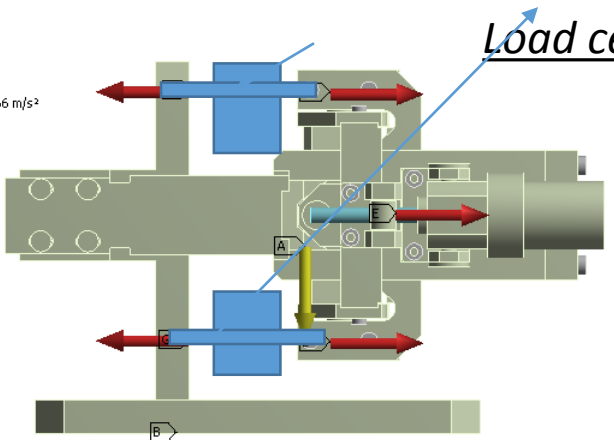


	Meas	Simul
K_{top}	10	12
K_{bottom}	16	20
K_{tuner}	26	32

Good agreement between simulations and measurements 26kN/mm .VS. 32kN/mm. We contributed the slightly higher simulation K_{tuner} to the fact that simulations do not take in account bearing and fasteners..

dX , Displacement of main lever, um

- Static Structural
- Time: 1. s
- A** Standard Earth Gravity: 9.8066 m/s²
- B** Fixed Support
- C** Force: 2500. N
- D** Force 2: 2500. N
- E** Joint - Displacement: 0. m
- F** Force 3: 2500. N
- G** Force 4: 2500. N



Prototype Tuner Stiffness

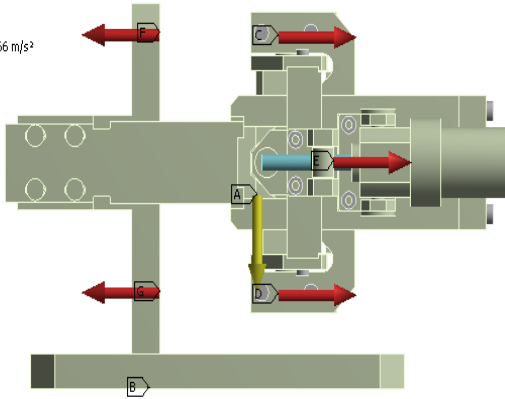
~30kN/mm

**Tuner Model... ANSYS Simulation provided results that are close to measurements results..
Simulation tools used to optimize (increase) tuner/dressed cavity system stiffness.**

GRAVITY+FORCE

Static Structural
Time: 1. s

- A Standard Earth Gravity: 9.8066 m/s²
- B Fixed Support
- C Force: 2500. N
- D Force 2: 2500. N
- E Joint - Displacement: 0. m
- F Force 3: 2500. N
- G Force 4: 2500. N



TEST STAND

$$\frac{2500}{\left(\frac{2.0791e-004 + 1.9982e-004}{2}\right)} = 1.226 \times 10^7$$

12kN/mm

$$\frac{2500}{\left(\frac{2.0791e-004 + 1.9982e-004}{2}\right)} + \frac{2500}{\left(\frac{1.2506e-004 + 1.2115e-004}{2}\right)} = 3.257 \times 10^7$$

32kN/mm

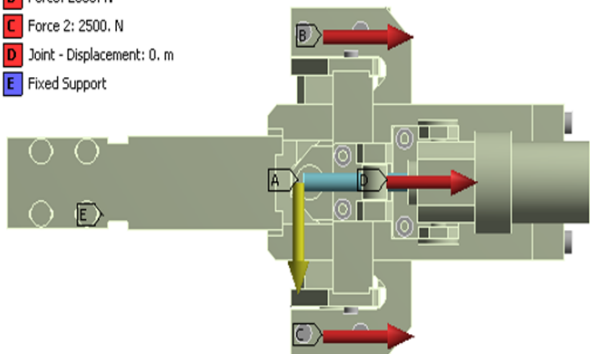
$$\frac{2500}{\left(\frac{1.2506e-004 + 1.2115e-004}{2}\right)} = 2.031 \times 10^7$$

20kN/mm

Sergey Cheban is leading ANSYS Simulations efforts

GRAVITY+FORCE

- A Standard Earth Gravity: 9.8066 m/s²
- B Force: 2500. N
- C Force 2: 2500. N
- D Joint - Displacement: 0. m
- E Fixed Support



NO TEST STAND

TUNER MOUNTED ON ABSOLUTE STIFF BLOCK

$$\frac{2500}{\left(\frac{1.2909e-004 + 1.2413e-004}{2}\right)} = 1.975 \times 10^7$$

20kN/mm

$$\frac{2500}{\left(\frac{1.2909e-004 + 1.2413e-004}{2}\right)} + \frac{2500}{\left(\frac{1.0926e-004 + 1.0586e-004}{2}\right)} = 4.299 \times 10^7$$

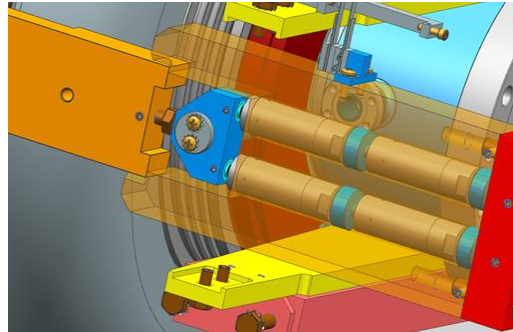
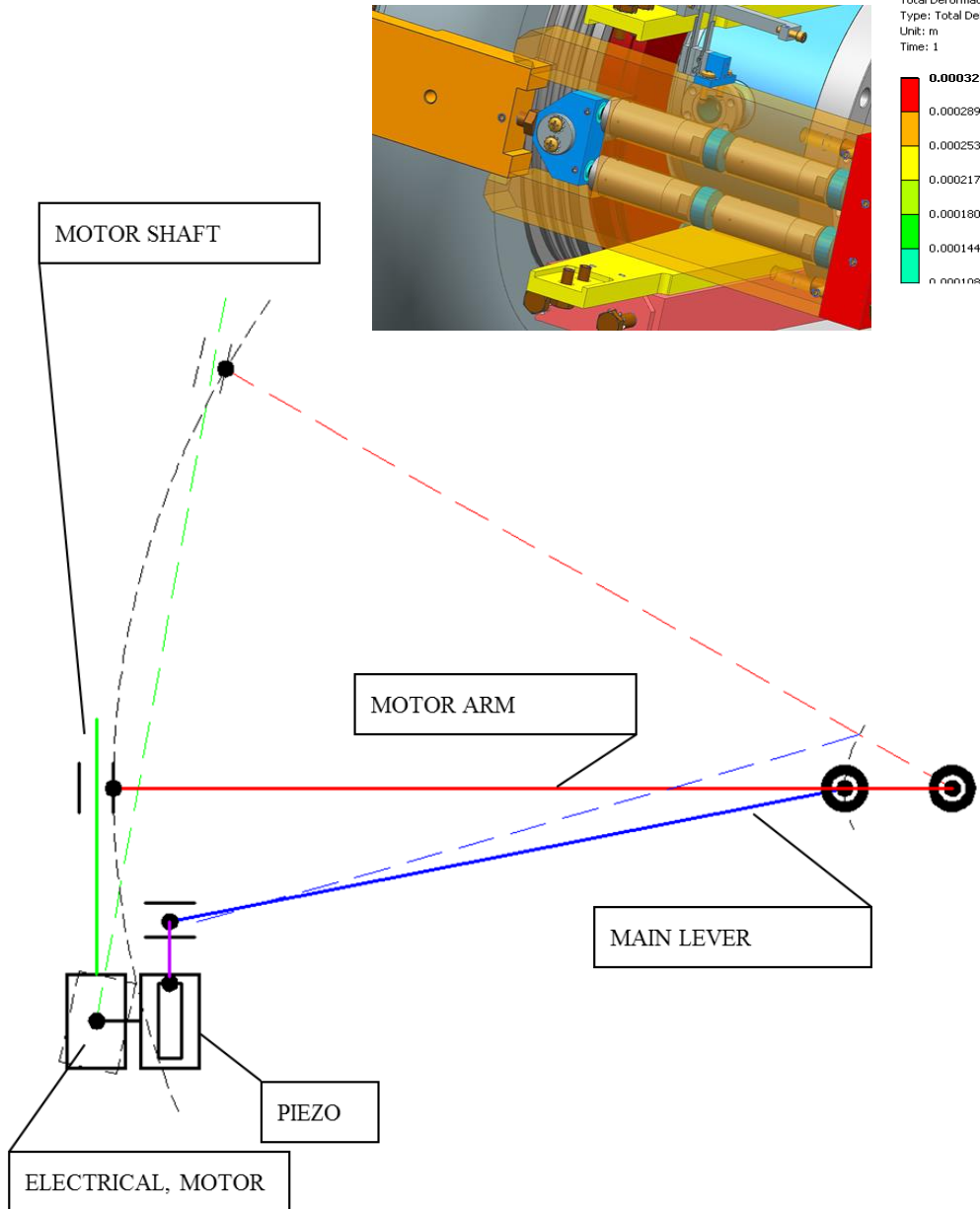
43kN/mm

$$\frac{2500}{\left(\frac{1.0926e-004 + 1.0586e-004}{2}\right)} = 2.324 \times 10^7$$

23kN/mm

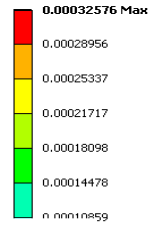
What part of the prototype Tuner contributed more into system stiffness ?

Fast/Piezo Tuner interface

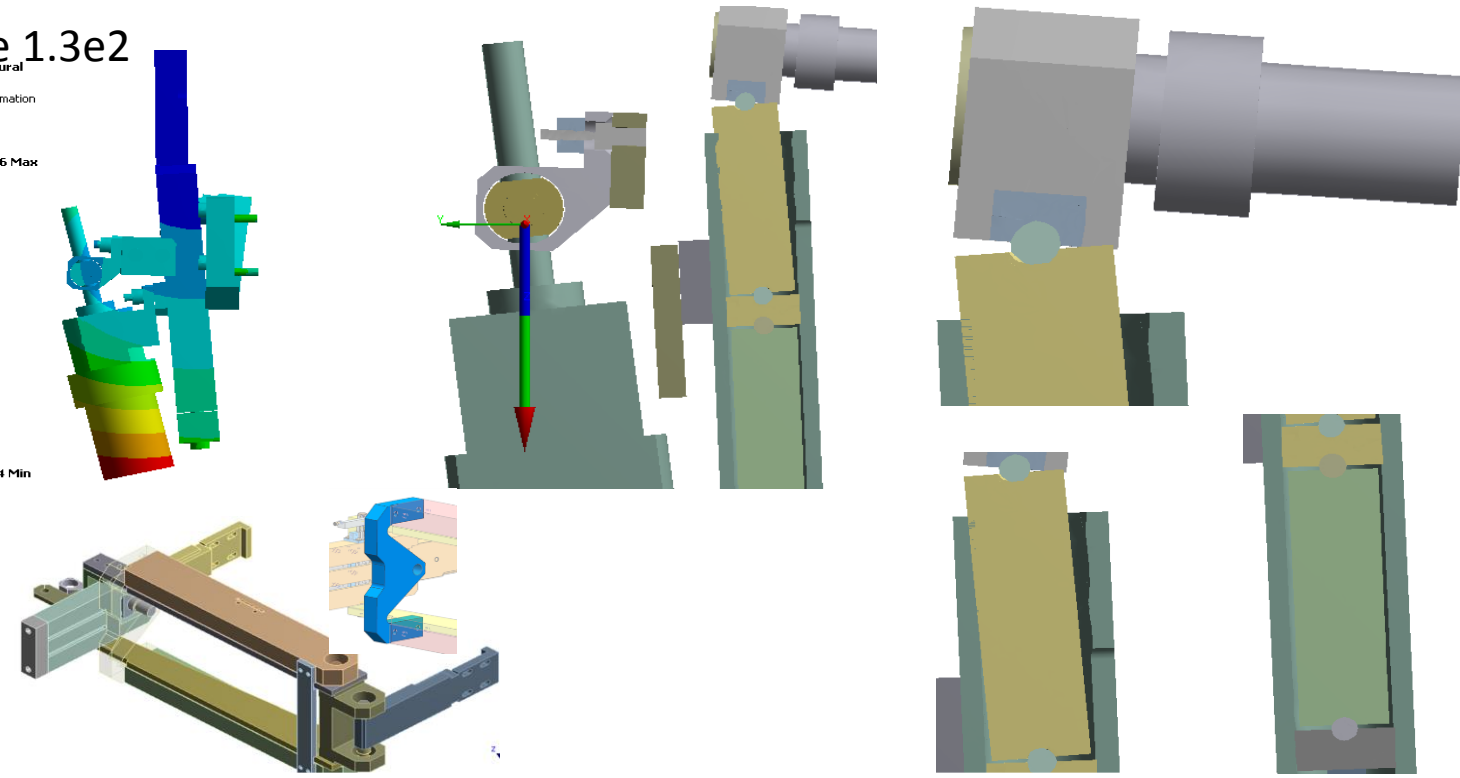


Scale 1.3e2

C: Static Structural
Total Deformation
Type: Total Deformation
Unit: m
Time: 1



24 Min



PIEZO

New (modified) Tuner Design

Decision to follow as close as possible to LCLS II Tuner Design...

- *two piezo-capsule located close to cavity's He Vessel/bellow interface ring*

- *piezos still need to be replaceable through designated port*

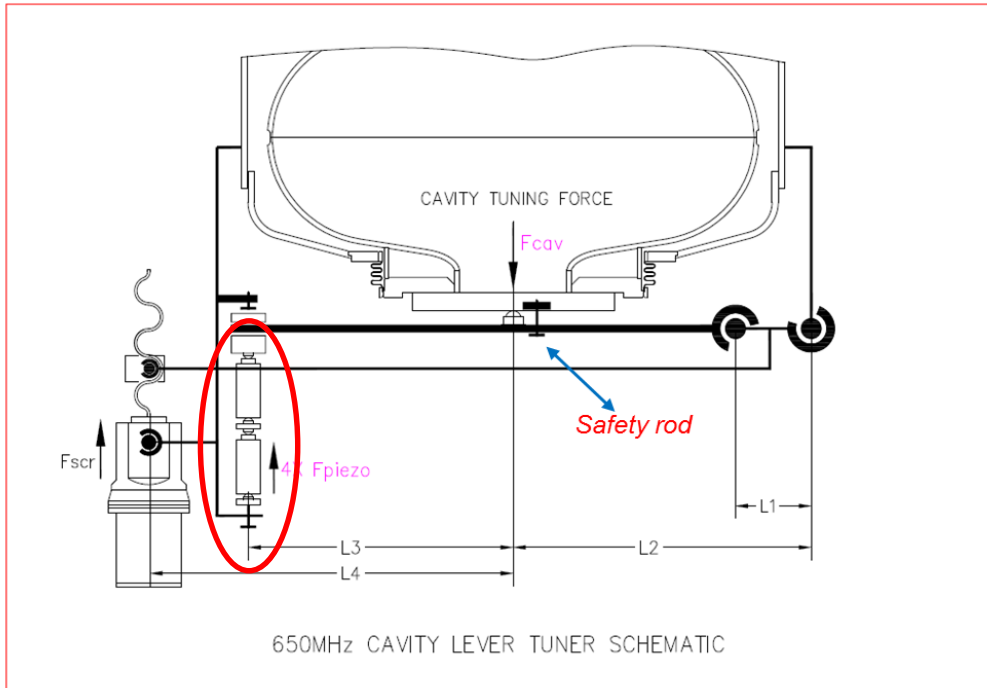
- *optimization (maximization) of the $K_{\text{Tuner Stiffness}}$*

- *Updated ANSYS tuner model "trustful" tool to design new tuner... (from the point of view stiffness optimization)*

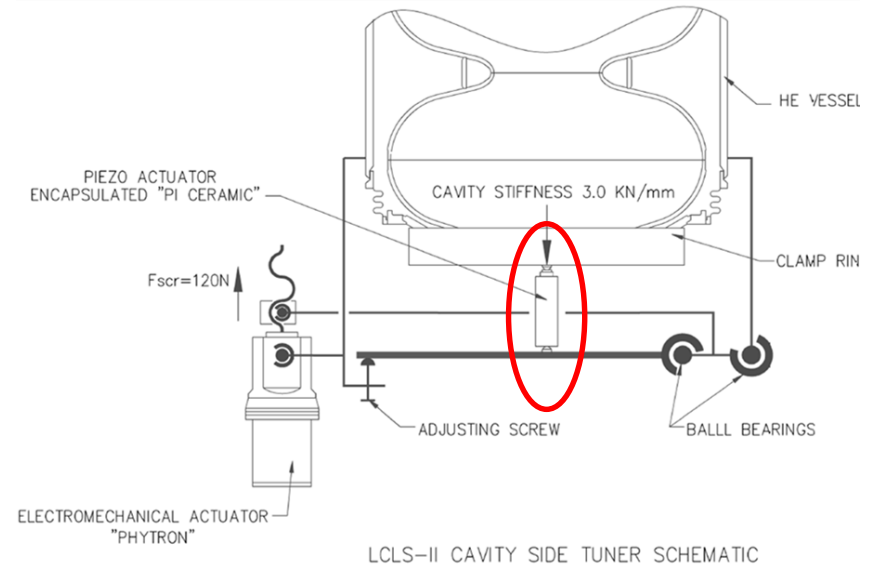
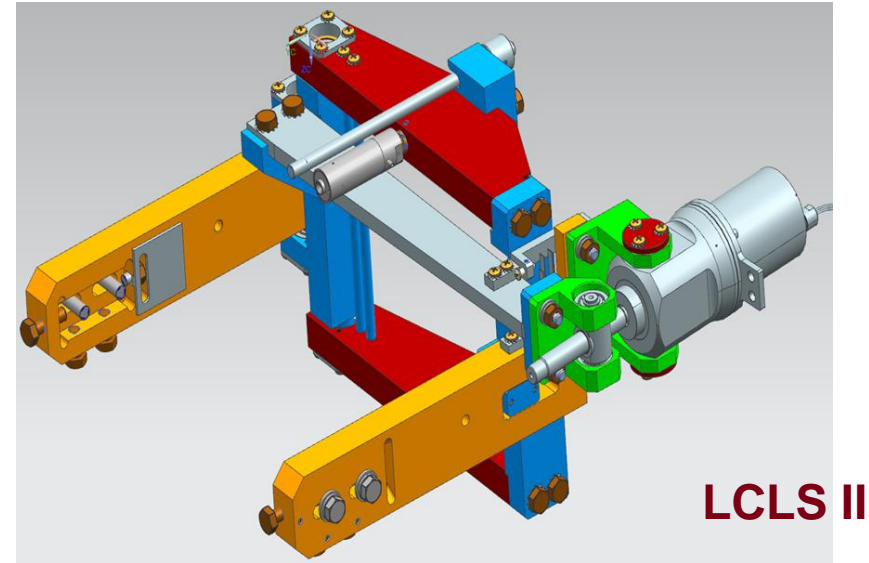
** New tuner can be used for cavity with $K \sim 20 \text{ kN/mm}$ with some limitations (shorter slow tuner range $\Delta F \sim 50 \text{ kHz}$)- to avoid piezo's overloading*

Kinematics of the LCLS II & 650MHz prototype Tuner

650MHz prototype Tuner



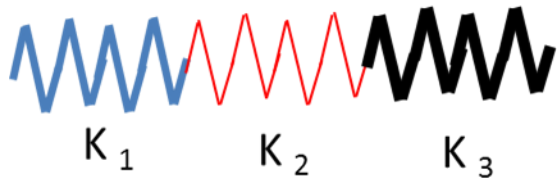
Piezo Location



Tuner Stiffness... How stiff system we can build?

1. Important to understand that we need to talk about stiffness of the system: “tuner-dressed cavity” that include not only “TUNER AS MECHANICAL FRAME” but also He Vessel & Tuner-to-cavity transition ring, etc...

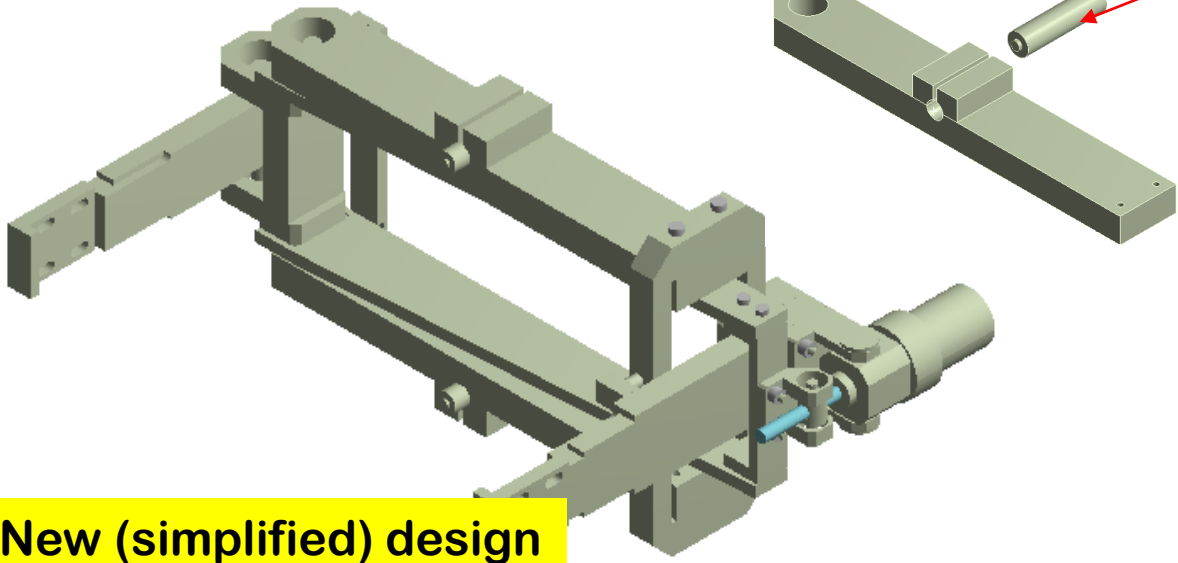
$$\frac{1}{X_1} + \frac{1}{X_2} + \frac{1}{X_3} = \frac{1}{X}$$



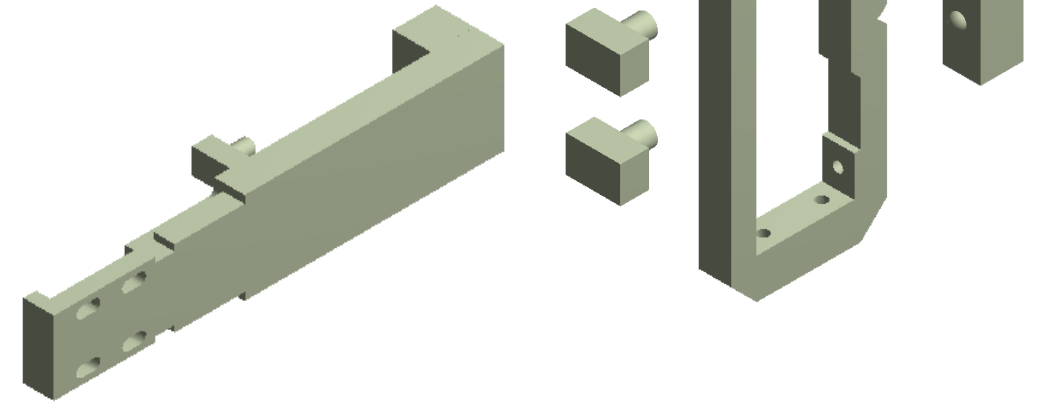
$X_1=100\text{kN/mm}$; $X_2=200\text{kN/mm}$; $X_3=300\text{kN/mm}$ → **$X=55\text{kN/mm}$**

$X_1=150\text{kN/mm}$; $X_2=200\text{kN/mm}$; $X_3=300\text{kN/mm}$ → **$X=66\text{kN/mm}$**

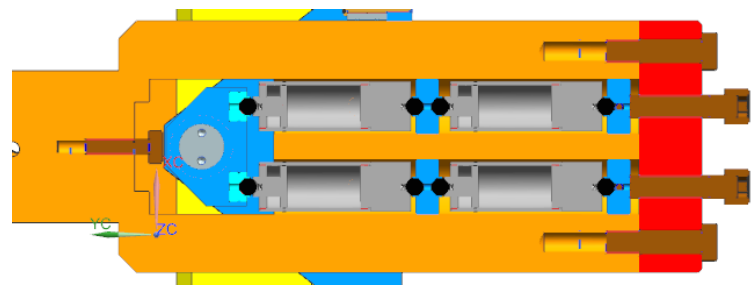
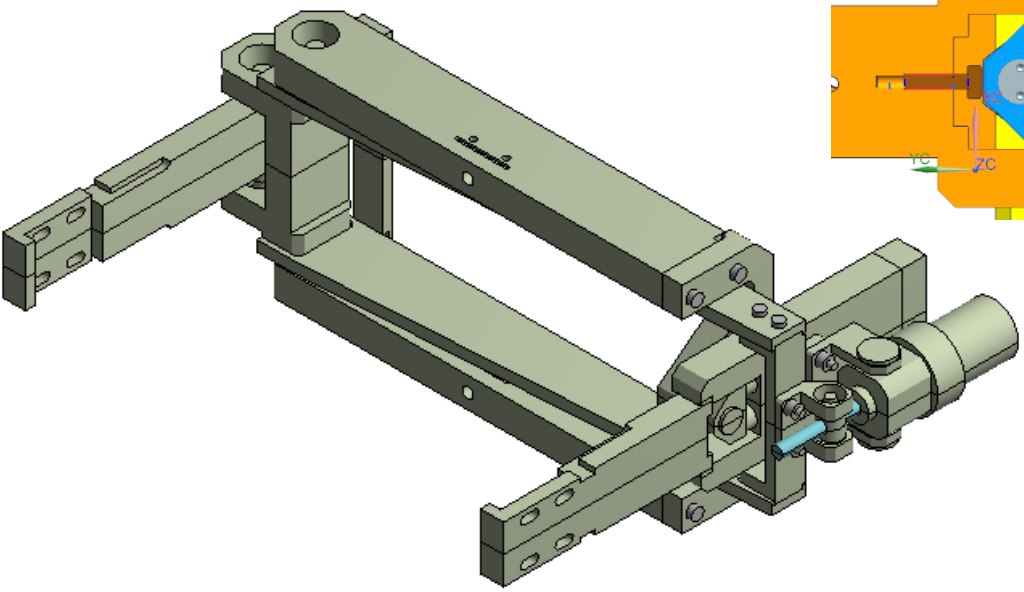
Sergey Cheban design



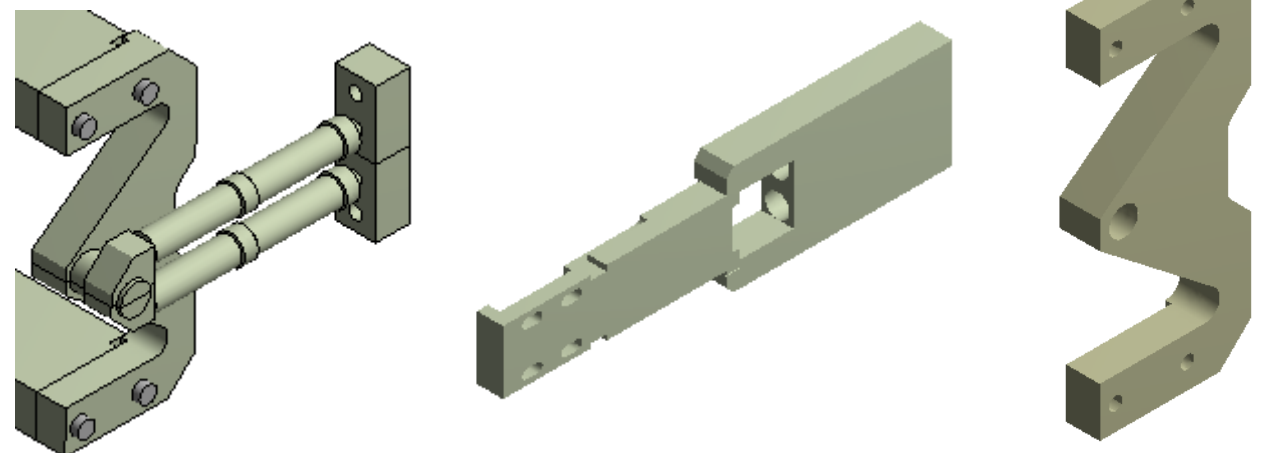
Piezo (1 top & 1 bottom) moved on the main lever arms to transfer stroke directly to cavity transition ring



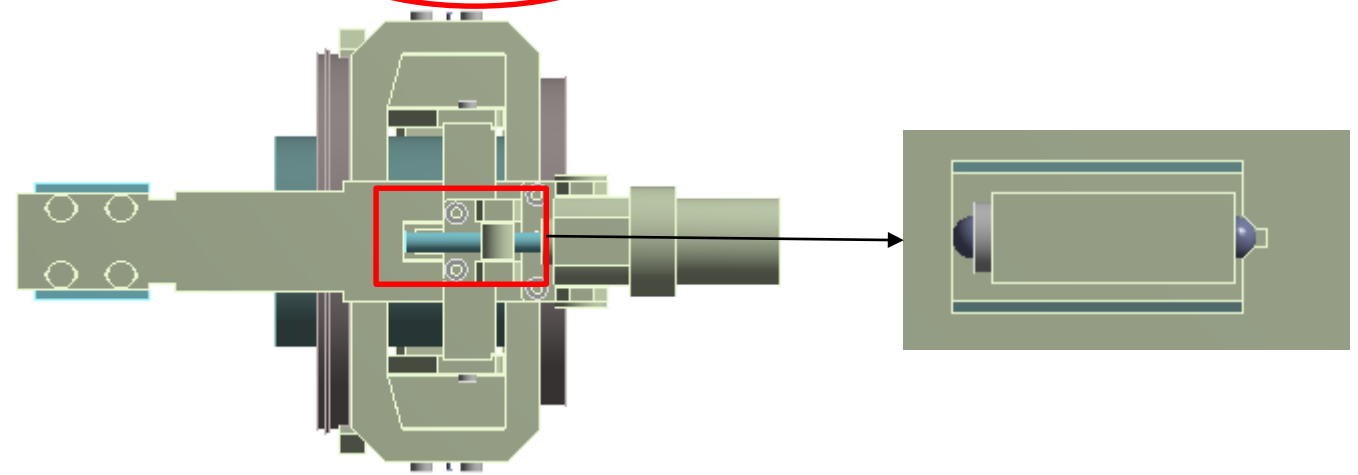
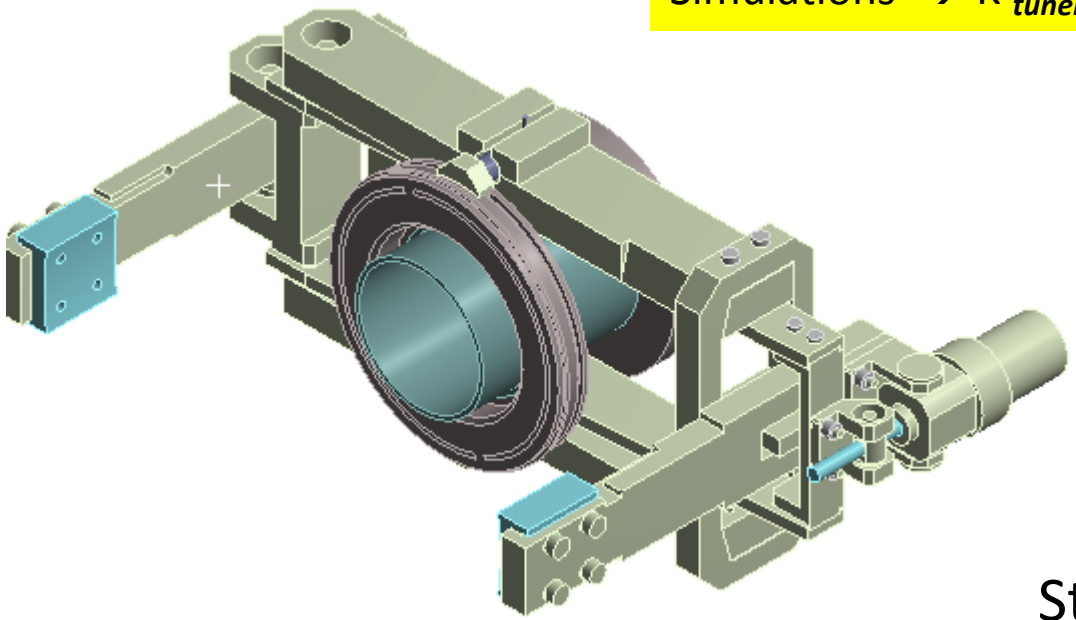
New (simplified) design



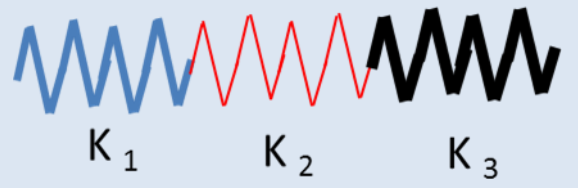
Prototype Tuner design



Simulations $\rightarrow K_{\text{tuner-dressed cavity system}} = 42\text{kN/mm}$



Stiffness of the **Tuner frame** $K_{\text{tuner}} \sim 140\text{kN/mm}$
without "piezo" and transition ring

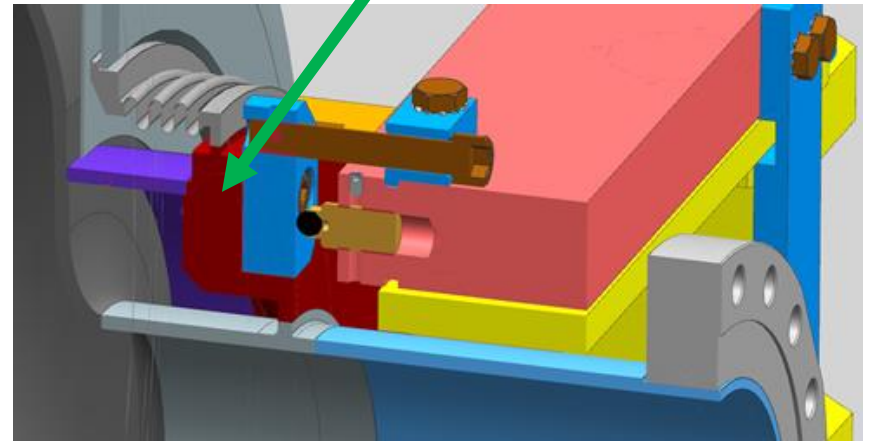


$$k_1 := 100 \quad k_2 := 200 \quad k_3 := 300$$

$$\left(\frac{1}{k_1} + \frac{1}{k_2} + \frac{1}{k_3}\right)^{-1} = 54.545$$

$$k_1 := 150 \quad k_2 := 200 \quad k_3 := 300$$

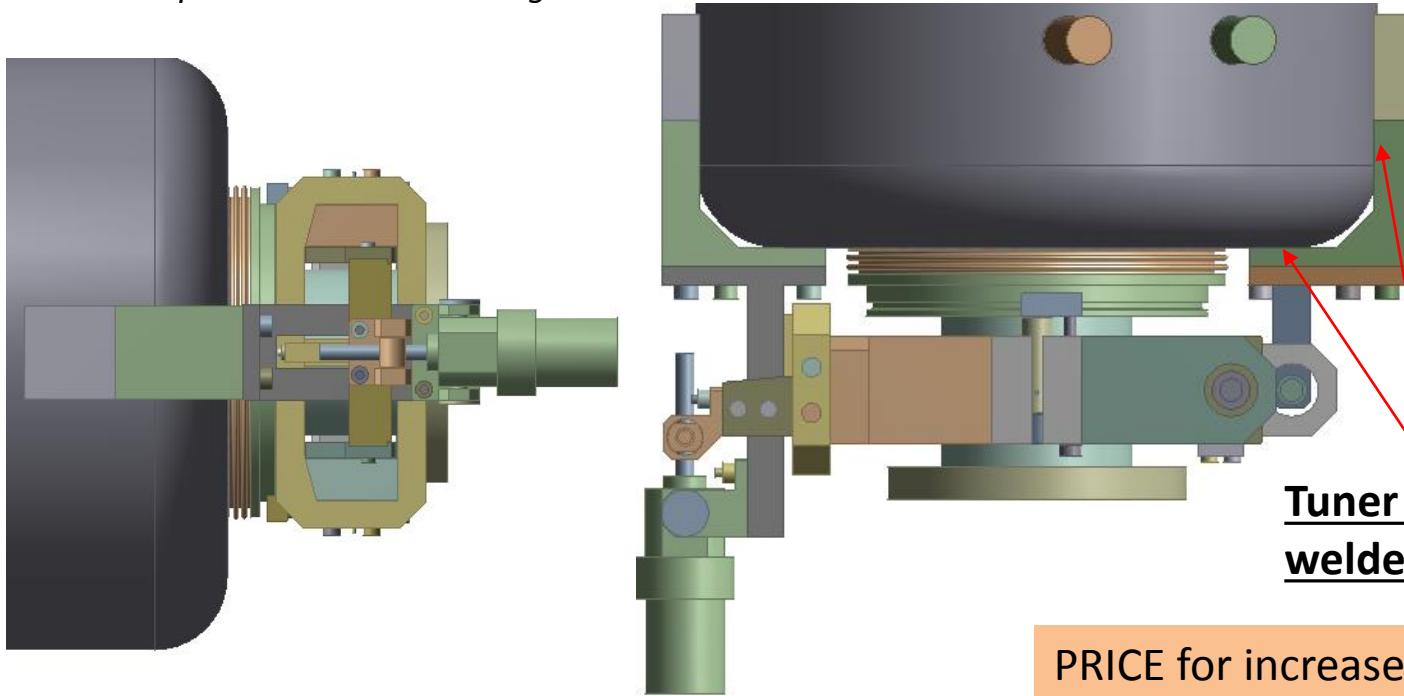
$$\left(\frac{1}{k_1} + \frac{1}{k_2} + \frac{1}{k_3}\right)^{-1} = 66.667$$



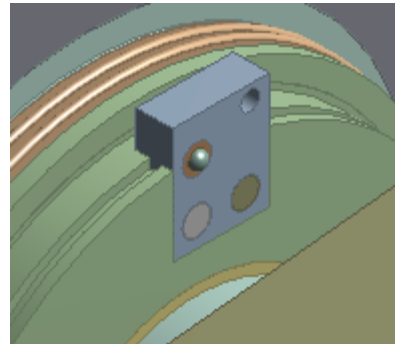
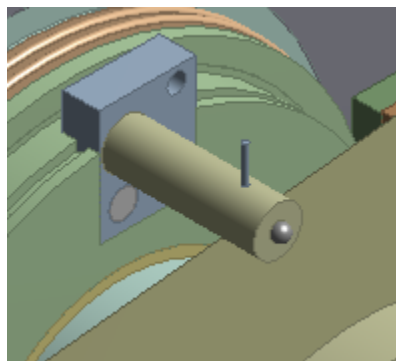
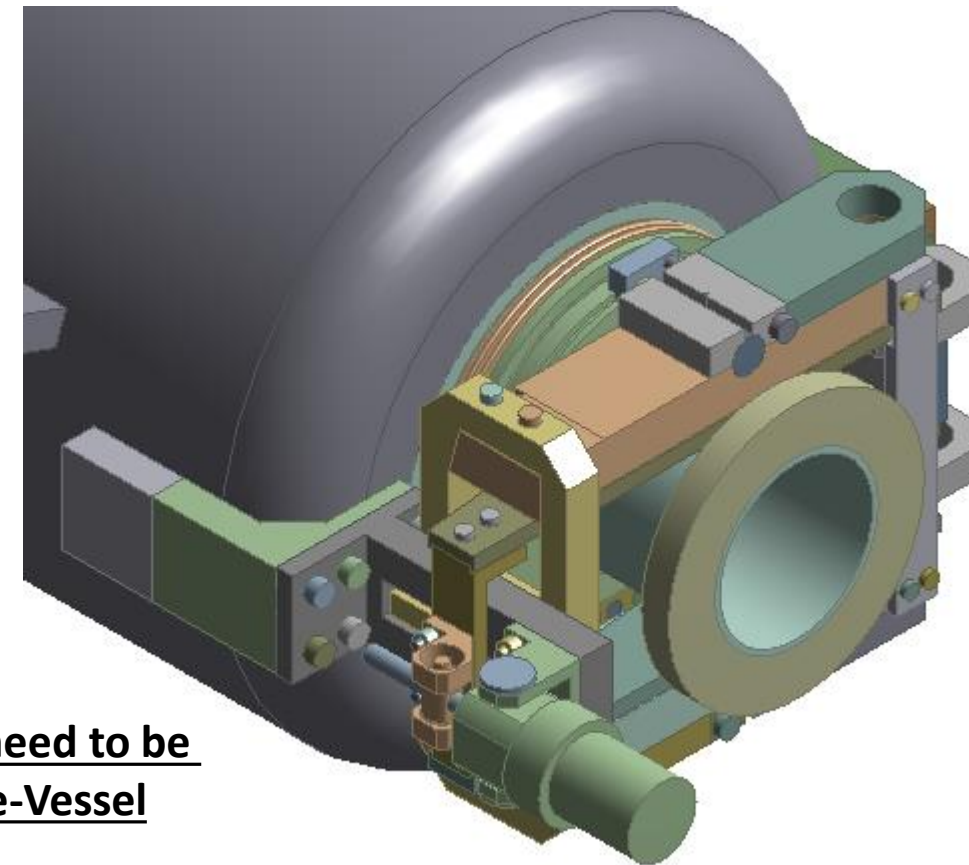
Latest upgraded version of the tuner with highest stiffness so far...

Simulations $\rightarrow K_{\text{tuner-dressed cavity system}} = 55 \text{ kN/mm}$

Stiffness of the Tuner frame $K_{\text{tuner}} \sim 600 \text{ kN/mm}$
without piezo and transition ring



Tuner arms need to be welded to He-Vessel



PRICE for increase of Tuner frame stiffness in **3-4 times**:
(but increase of $K_{\text{tuner-cavity}}$ stiffness from 42 to 55kN/mm)

Significant modifications/ of the He Vessel /Tuner interface...

- (a) arms must be welded to He vessel at several places..
- (b) more complex adjustment of the tuner to cavities with different length
- (c) endcap magnetic shielding (?)
- (d) etc...

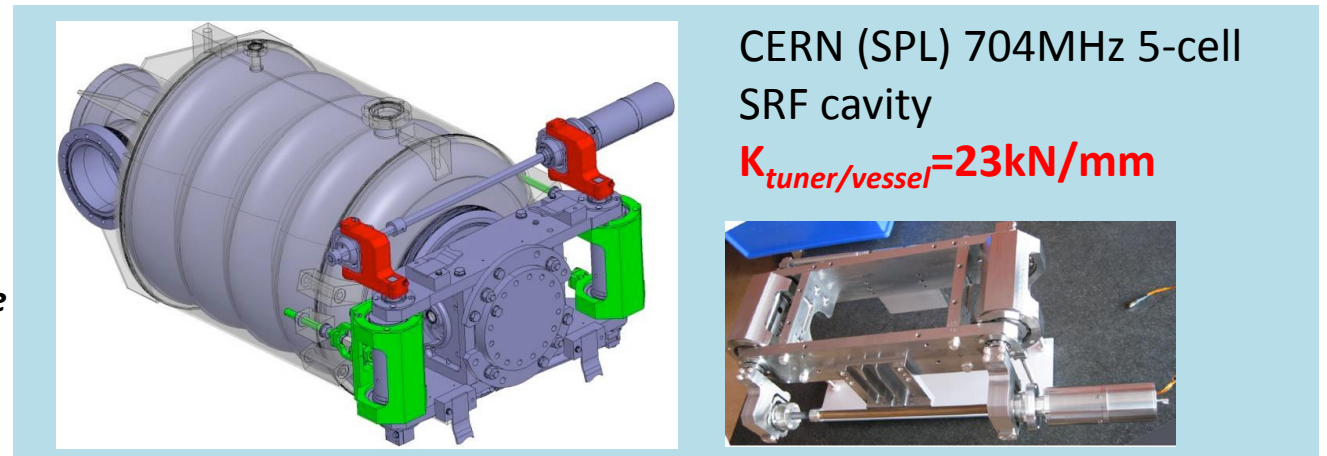
Summary

of Tuner/Dressed cavity system stiffness studies

- Possible to design Tuner frame with stiffness several 100's of kN/mm
- But it is close to impossible (without significant re-design of whole concept of dressed cavity & new piezo-capsule) to have stiffness of the tuner/dressed cavity system above 50kN/mm
- We need to review parameters of the cavities (particularly LFD) with assumption that stiffness will be $\sim 40\text{kN/mm}$

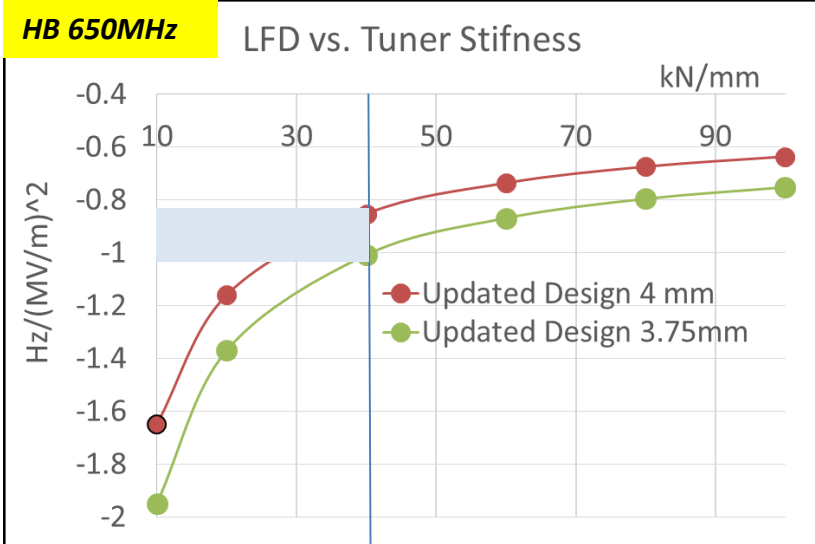


Examples of the large size cavities with tuner



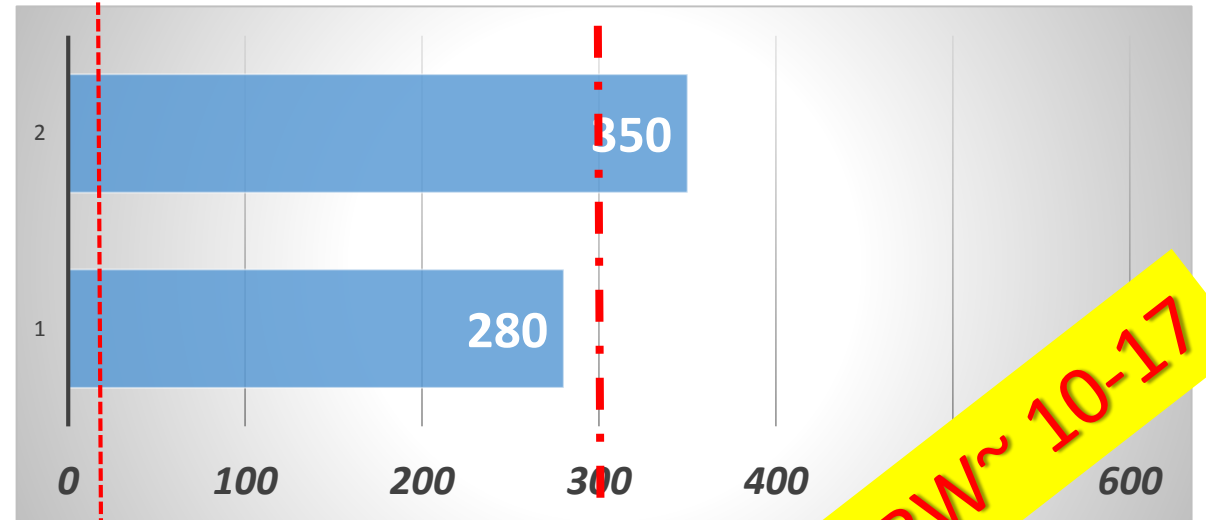
Lorentz Force Detuning (static)

values of expected (with 40kN/m)



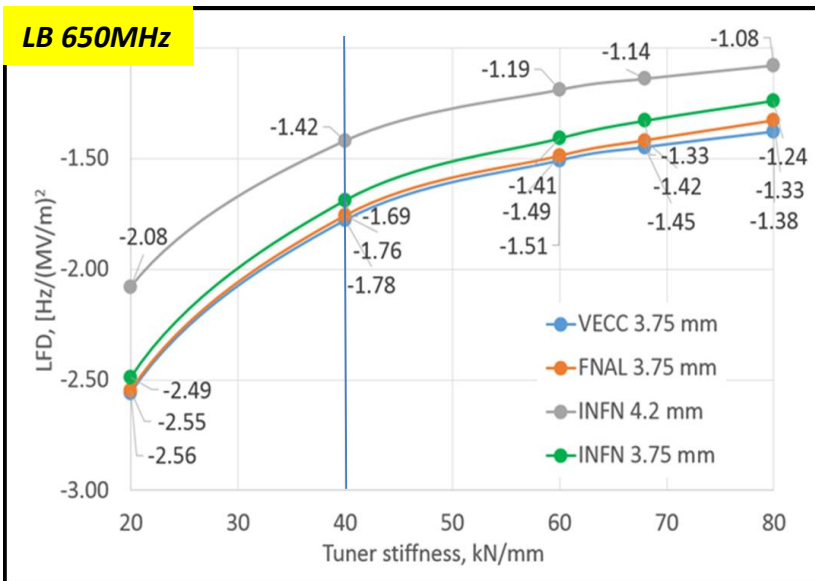
$$E_{ac} = 18.8 \text{ MV/m}$$

$$K_{LFD-Static} = 0.8-1.0$$



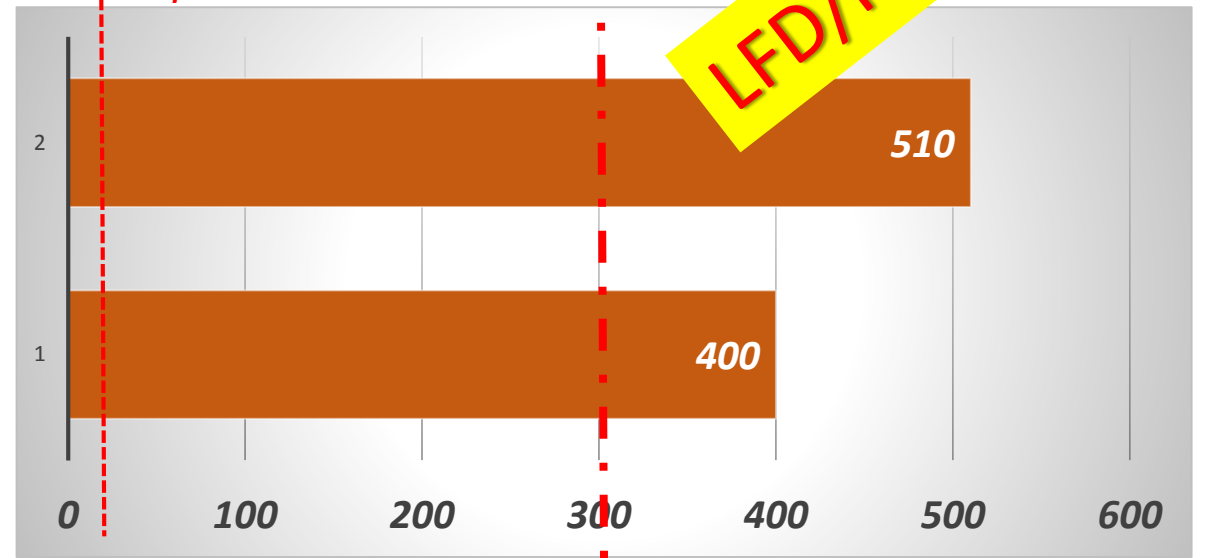
$\Delta f \sim 20\text{Hz}$
control reqs

10 HBW

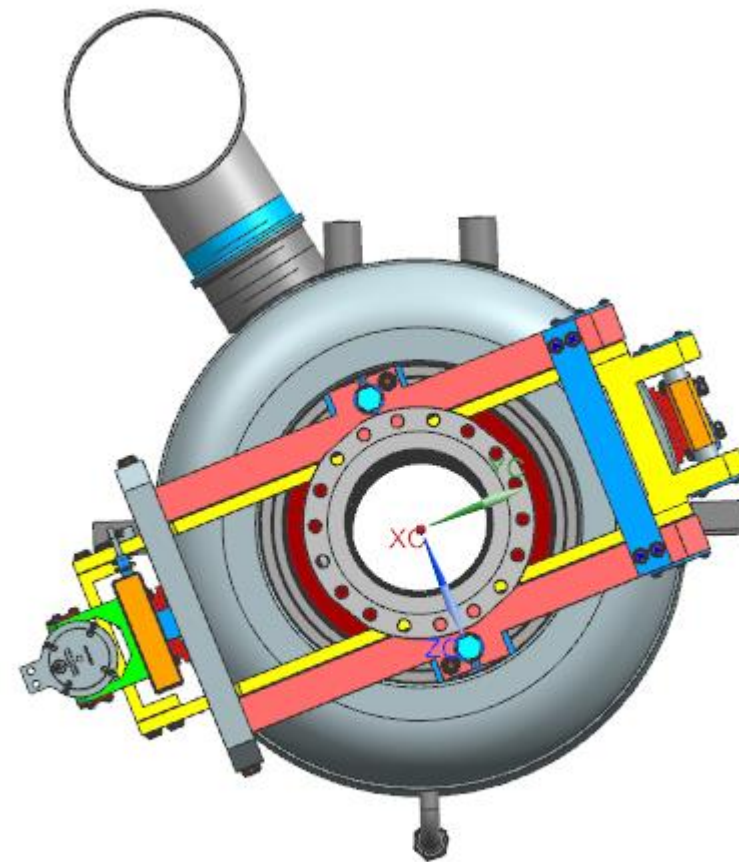
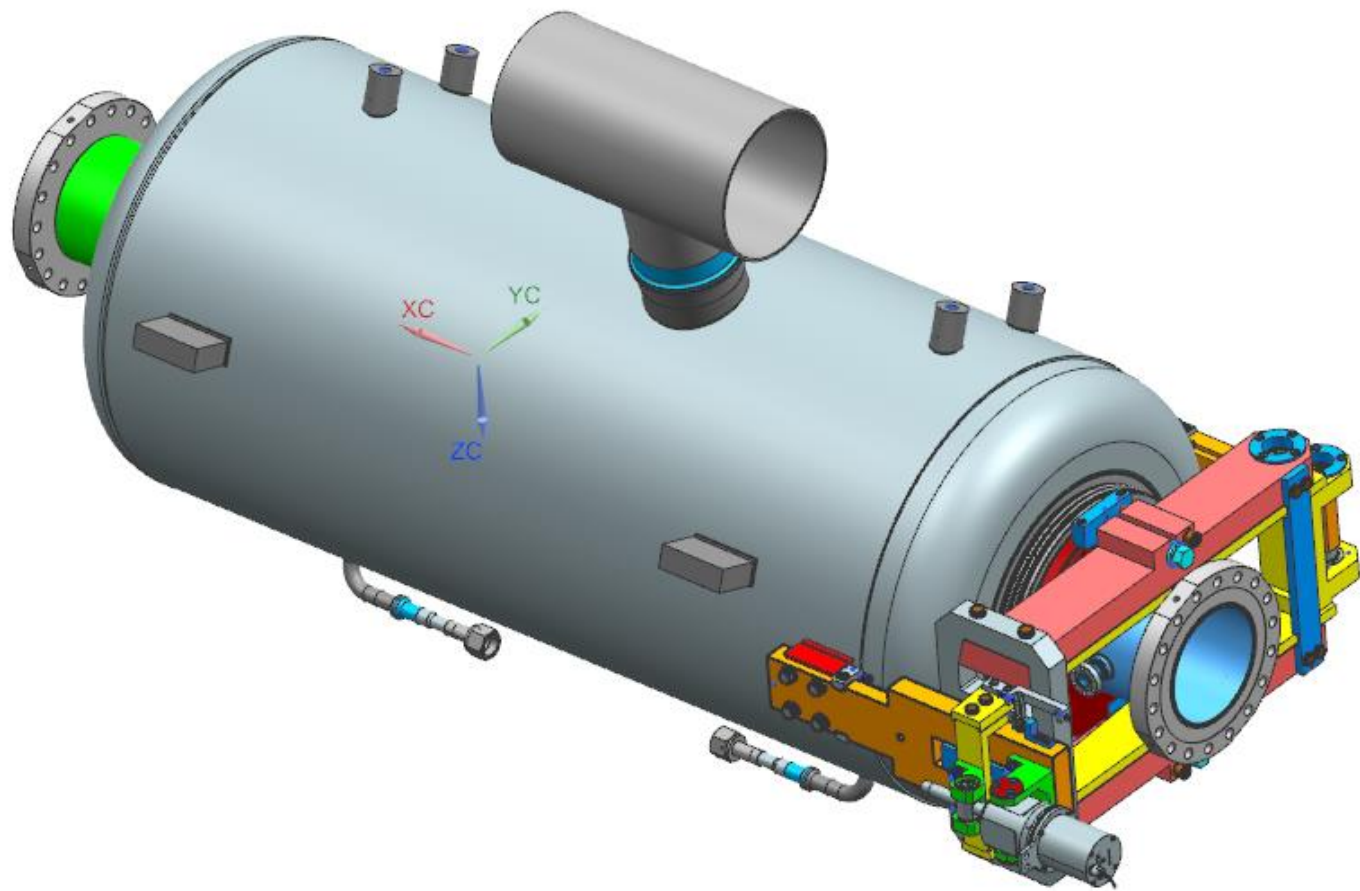


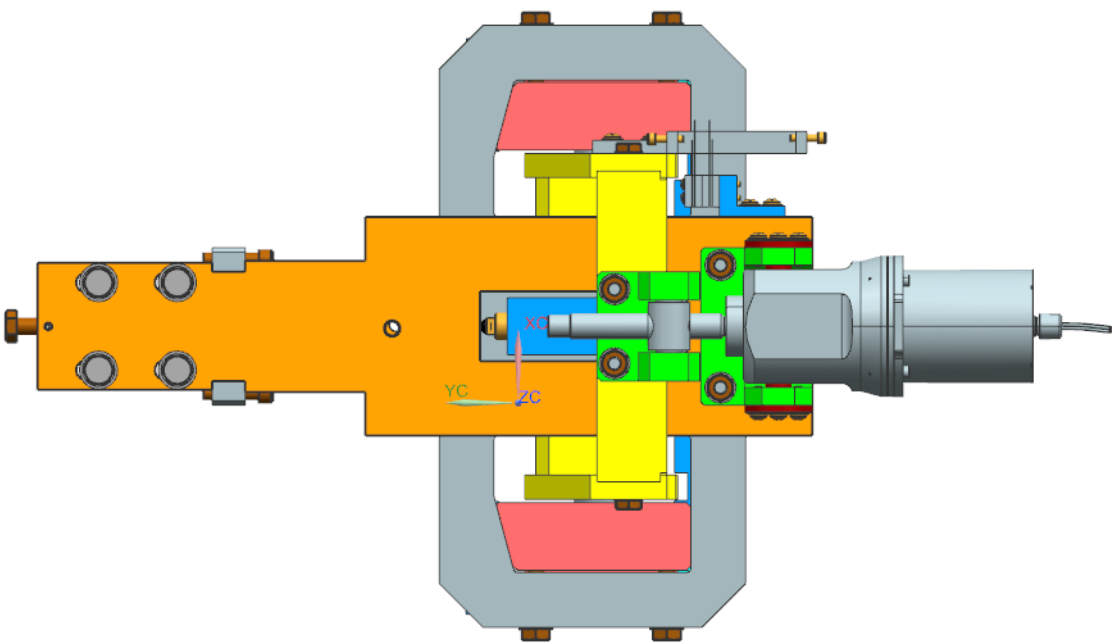
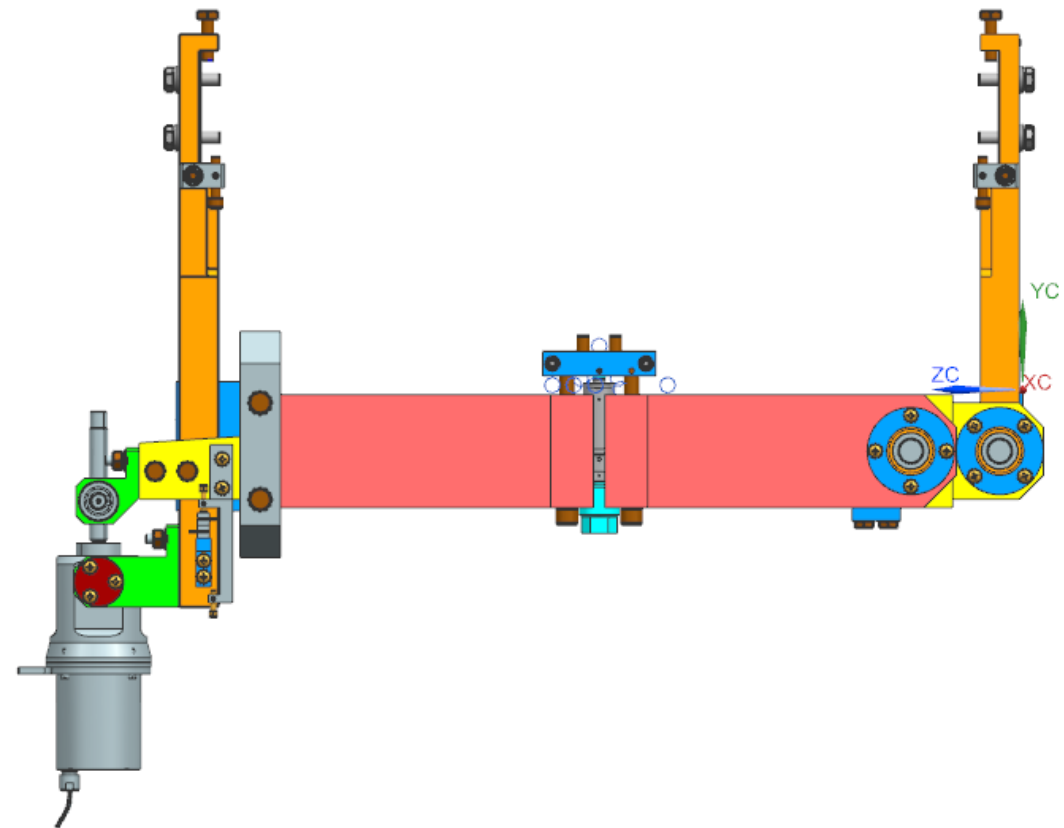
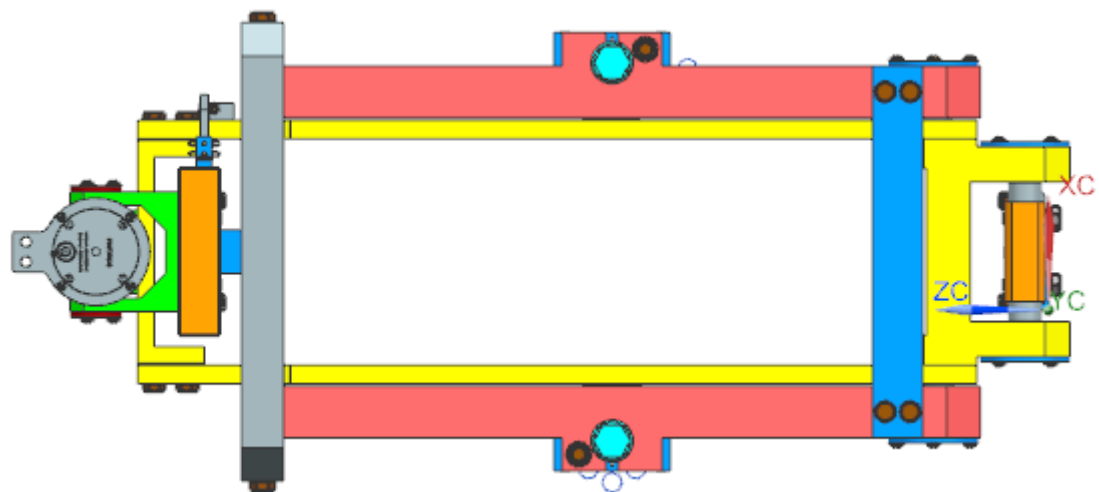
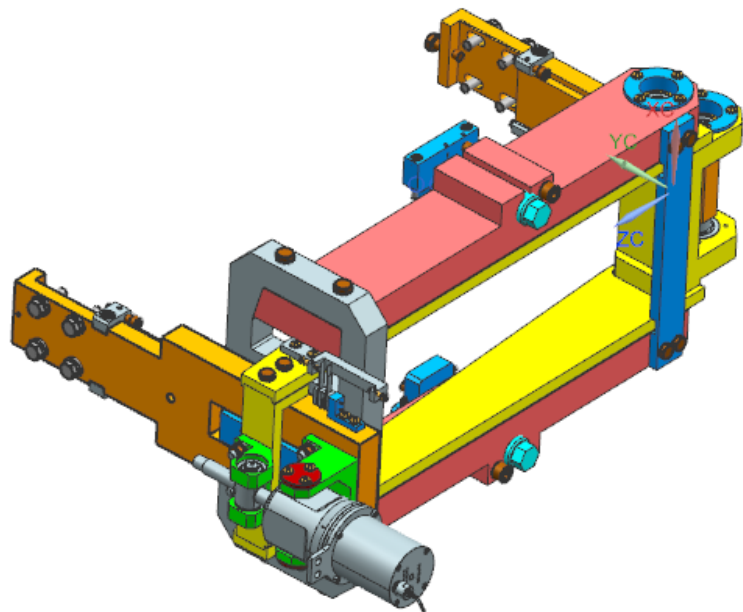
$$E_{ac} = 16.9 \text{ MV/m}$$

$$K_{LFD-Static} = 1.4-1.8$$

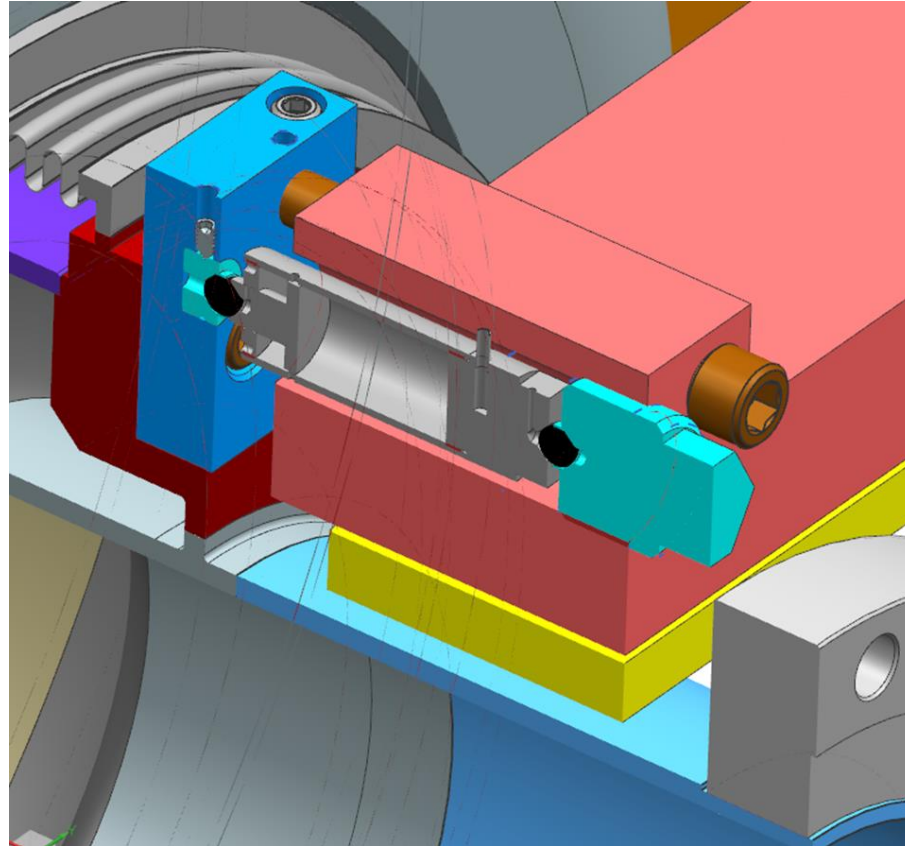
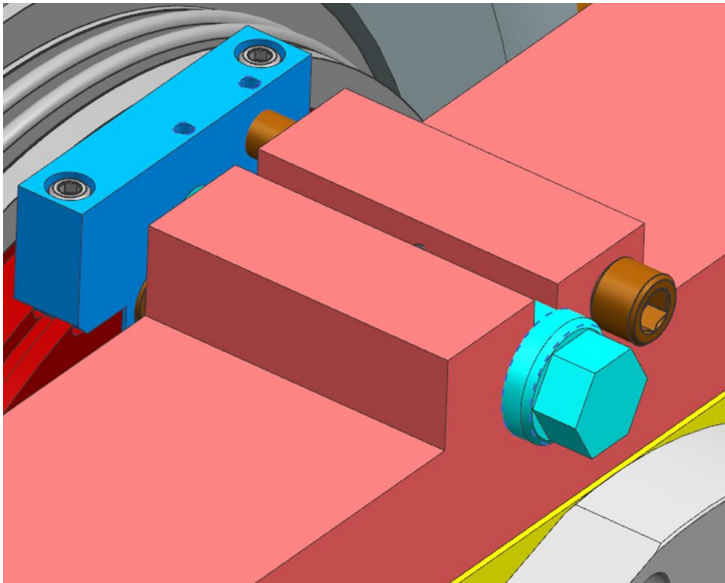
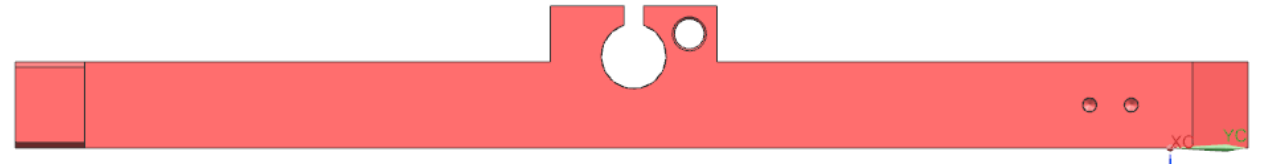
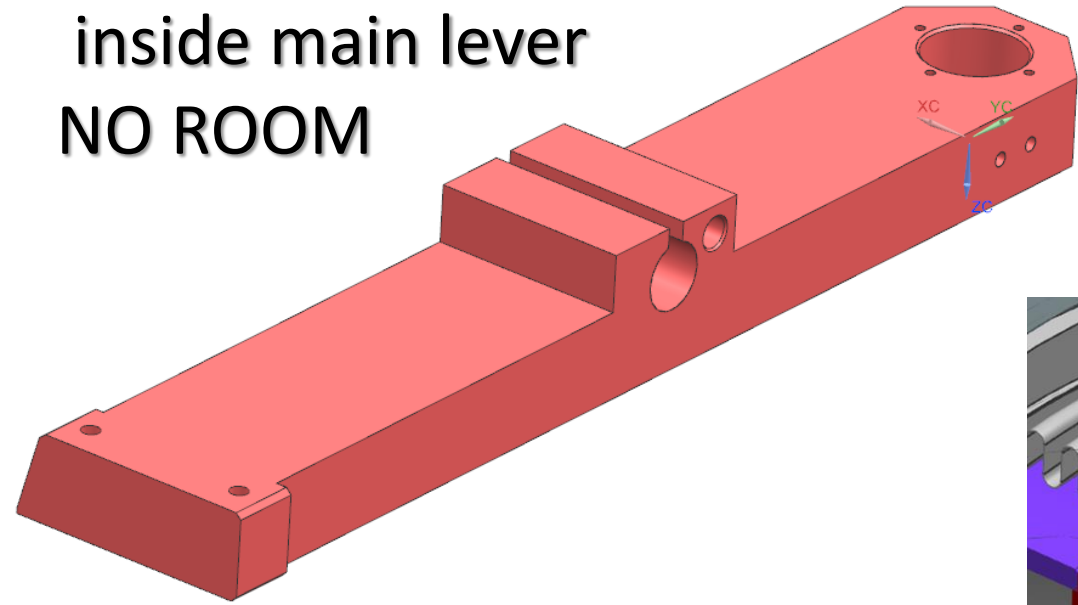


New Tuner for LB/HB650MHz

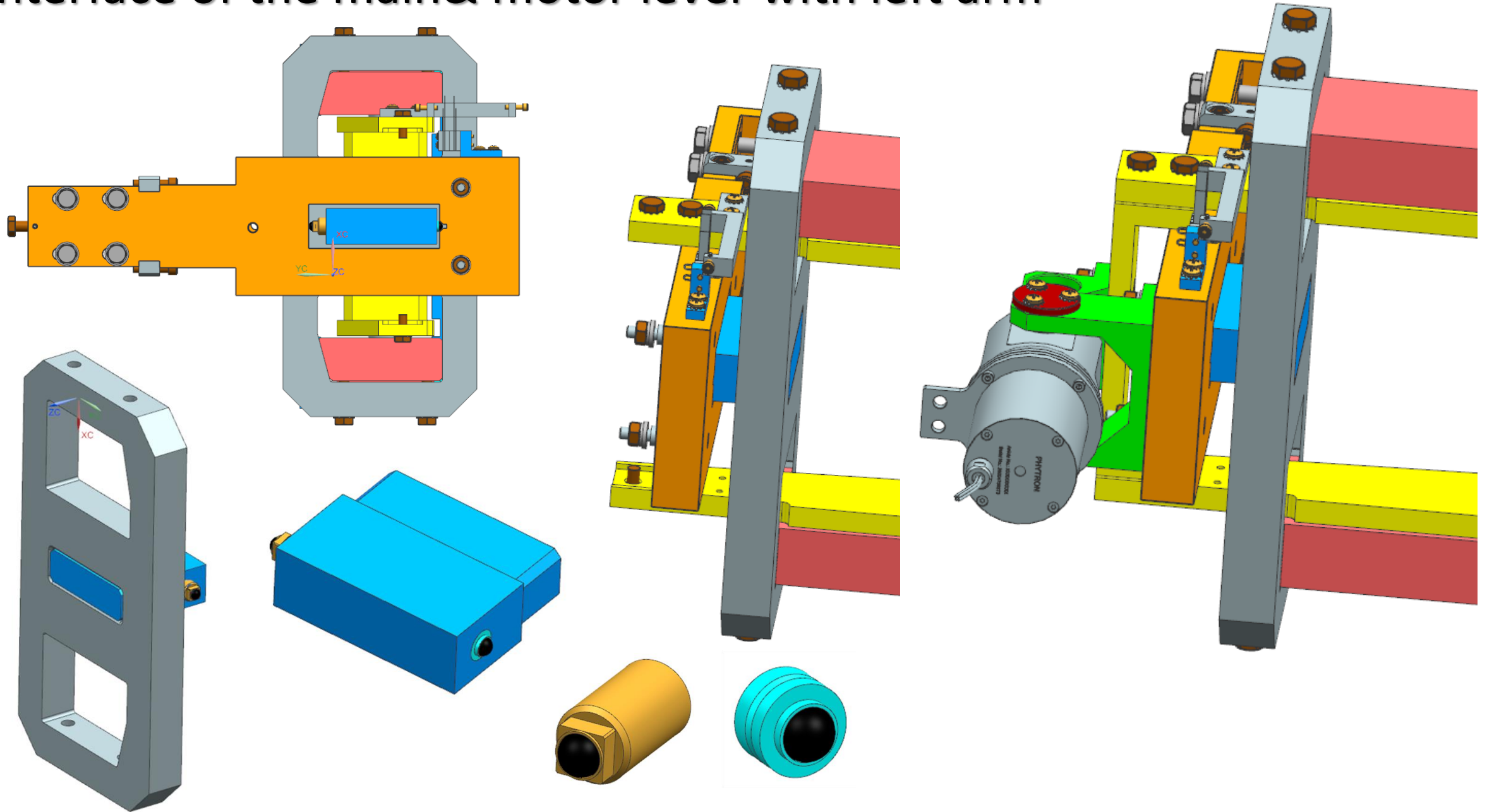


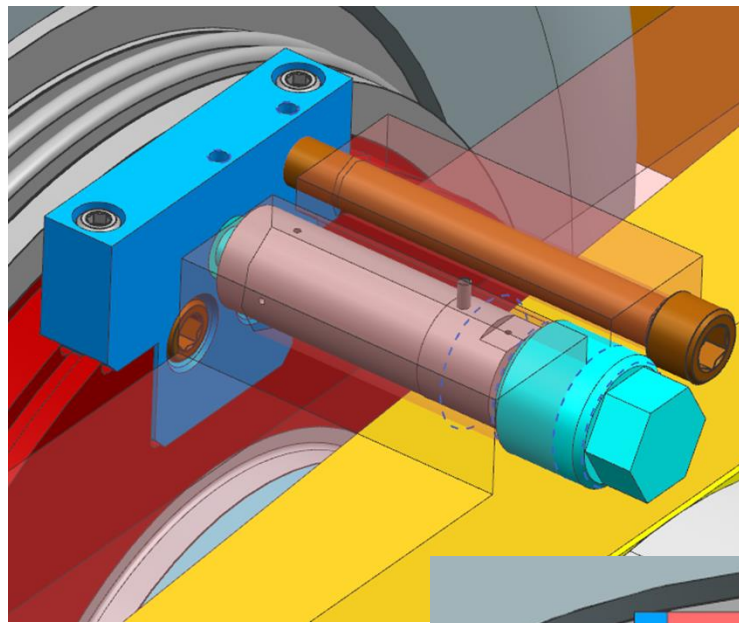
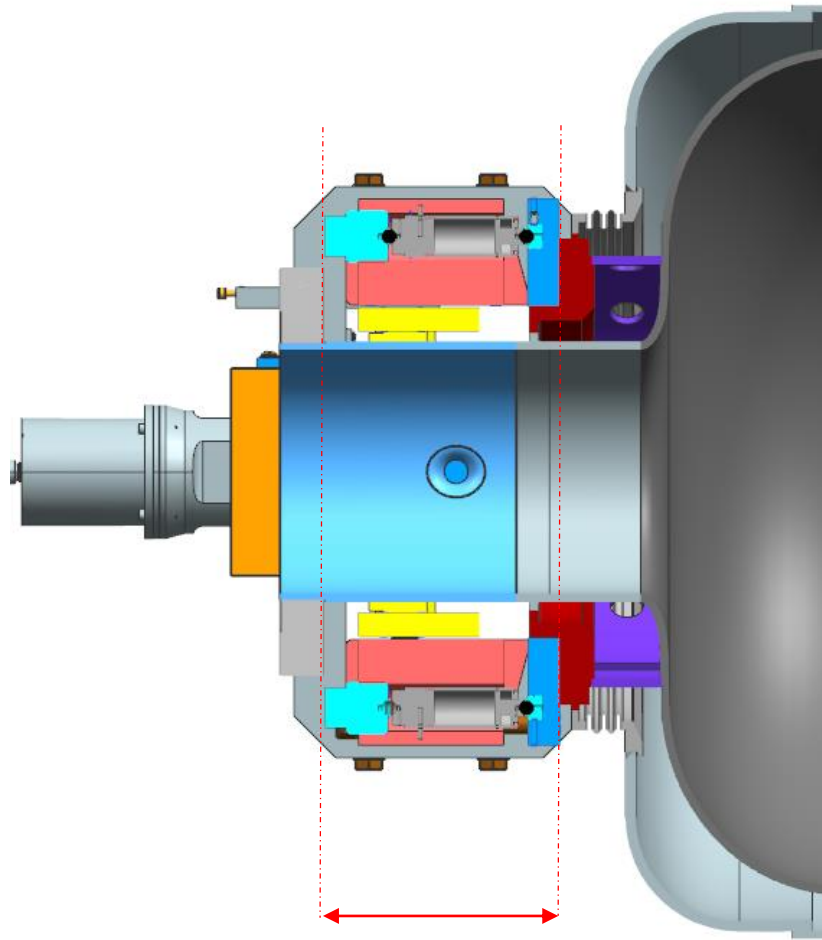


Housing of the piezo-capsule
inside main lever
NO ROOM

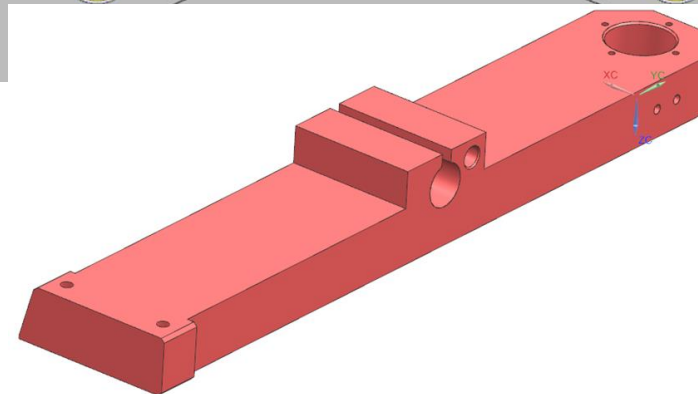
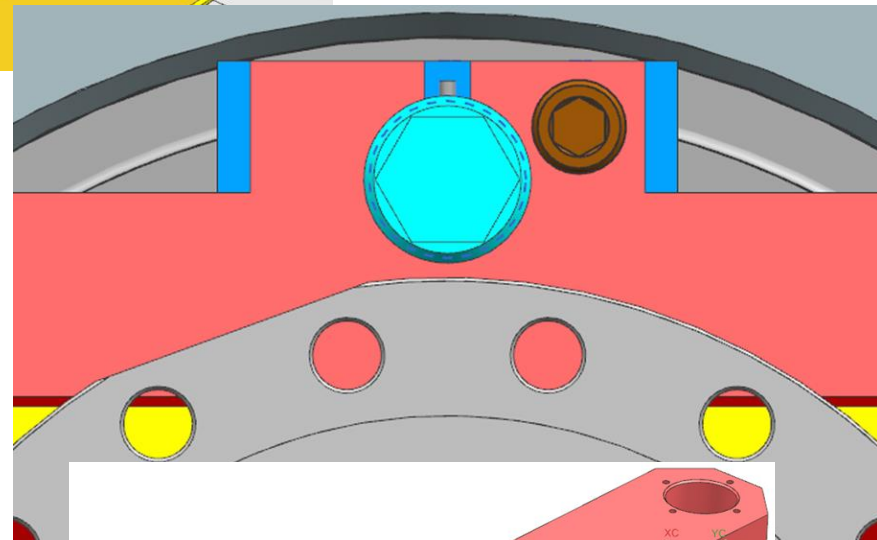


Interface of the main& motor lever with left arm



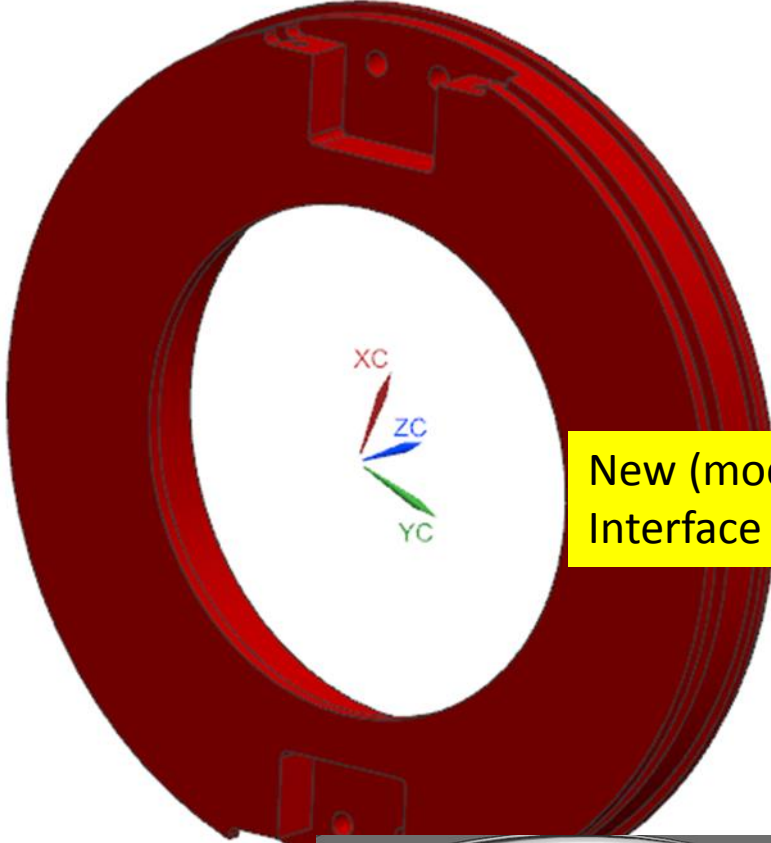


Cavity/tuner interface
piezo –to – NbTi ring

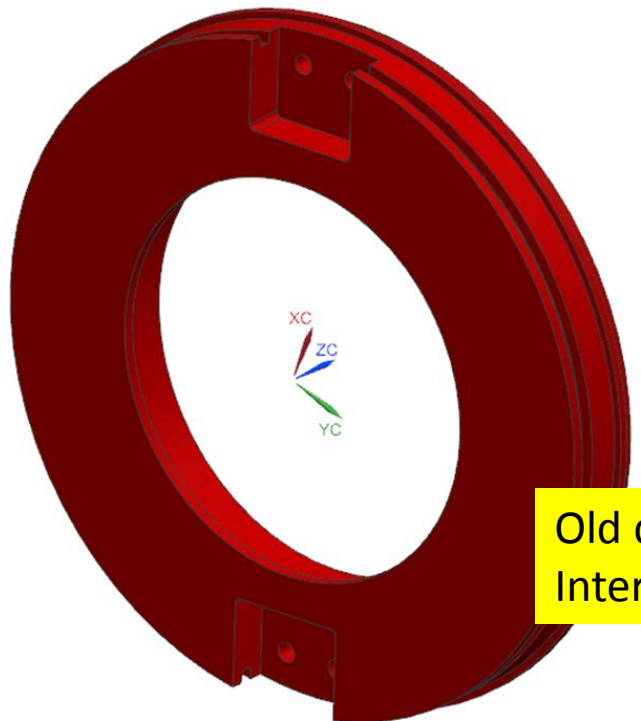
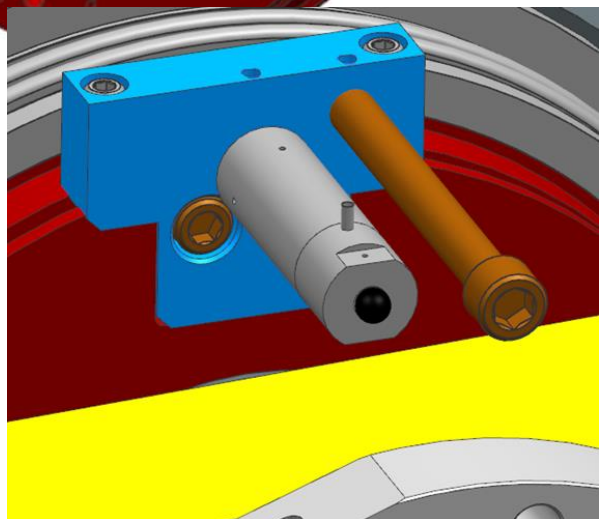
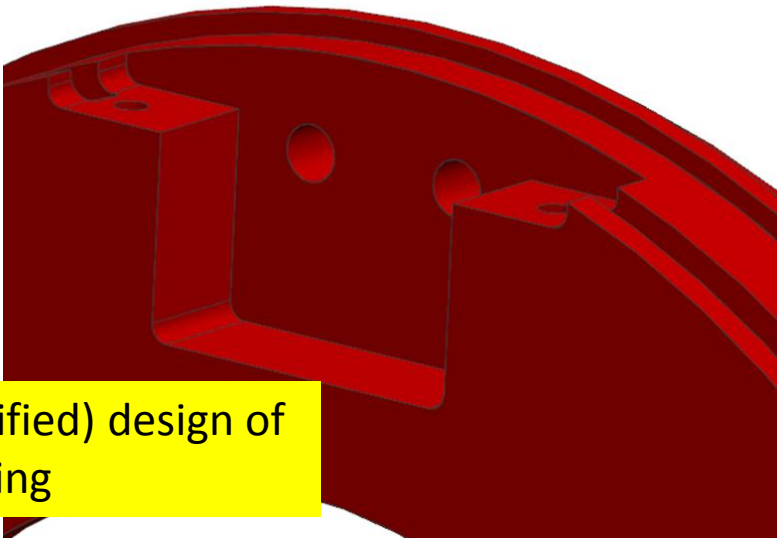


Why we “put ourselves into difficult position”
By making short beam-pipe →
limiting available space for tuner ???

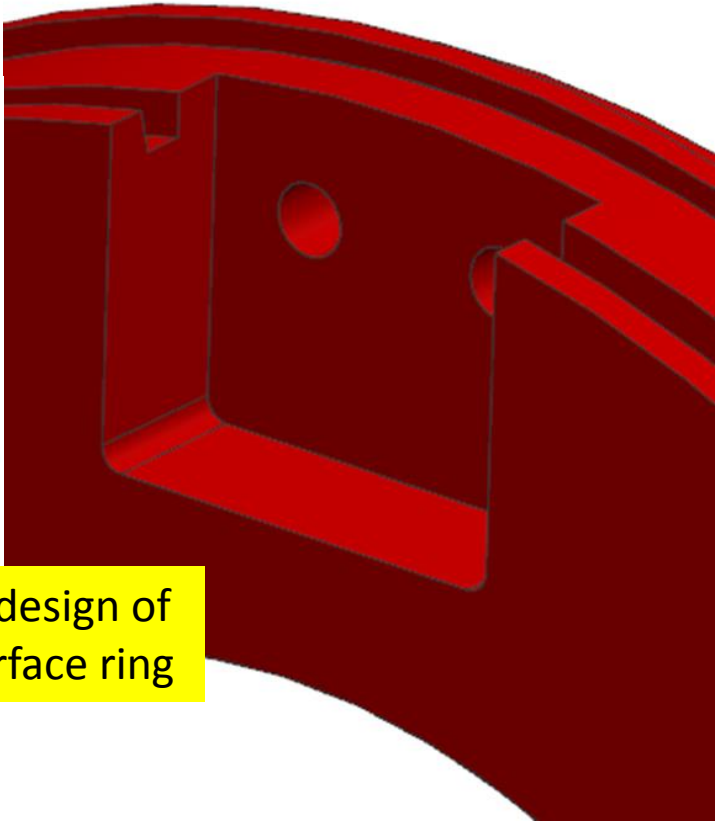
Cavity/tuner interface
piezo –to – NbTi ring



New (modified) design of
Interface ring



Old design of
Interface ring



Fast Tuner Piezo Stroke....

- Based on
 - the similarity of the LCLS II & 650MHz tuner design
 - On the stiffness of the 650MHz cavity $\sim 4\text{kN/mm}$
 - On the $\Delta F/\Delta L$ of the 650MHz $\sim 200\text{kHz/mm}$
 - On the LCLS II tests of piezo tuner

We are expecting that fast tuner tuning range

at $T=2\text{K}$ for $V_{\text{piezo}}=100\text{V}$ will be $\Delta F \sim 2\text{kHz}$

Questions for Discussion

- What reasons are preventing us from making cavity's Nb beam pipe longer?
 - It will simplify tuner installation/replacement piezo-capsules
 - It will be not close options to make piezo-ceramics actuator longer... increase lifetime of piezo
- We need slightly change design (dimensions of the notch to mount bracket for piezo push point & safety rod)
 - It will increase stiffness of the overall system
 - It is important for translation from piezo to cavity stroke in the range of 10's of nanometers

Overall status of LB/HB650 Tuner

- ~~• Model is ready~~
- ~~• Will be reviewed by TD/SRF engineers~~
- Drawings will be ready in 2-3 weeks **(STARTED)**
- Procurement & machining can be done in the scale of couple month
- Previous tuner production cost ~\$17k
- New tuner tests (stiffness & piezo stroke) assembled on the “cavity mock-up” stand can be done during 2-3 weeks
- Warm Tuner design verification program will significantly benefit if tuner can be assembled and tested on the dressed cavity

What Lorenz force detune could we tolerate (compensate...)?

1. In all previous slides references were to simulated average STATIC detuning
2. Even if we assume that STATIS=Dynamic we also need to take into account that distribution of detuning from cavity-to-cavity is quite WIDE ($\sigma \sim 30\%$)... and tuner/algorithms must be able to deal with highest possible detuning (not just average)...
3. Dynamic (RF-pulse mode) LFD detuning is function of
 1. RF-pulse length (fill-time; flat-top & decay)
 2. RF-pulse repetition rate....
 3. And of course, mechanical resonances (frequency & Q) of the cavity/He vessel/tuner/piping structure

Strategy and Status of the R&D – Resonance Control

PIP II LB/HB 650MHz cavities will experience LARGE LFD.

Operation with rep. rate 20Hz will add significant microphonics (residual vibration from previous pulse).

Cavities Resonance Control for narrow bandwidth cavities with ratio

LFD/HBW ~20 is extremely challenging:

- Large Lorentz Force Detuning
- Significant residual vibration/ excessive microphonics

Pulsed SRF accelerators, existing and projects	Cavities Half-bandwidth, Hz	LFD, Hz	LFD/HBW
<i>SNS (LB/HB)</i>	550/500	300/100	0.55/02
<i>ESS(HB)</i>	500	400	0.8
<i>FLASH/XFEL</i>	185/141	550	3/4
<i>PIP II (LB/HB)</i>	29/29	300/500	10/17
<i>MaRIE</i>	50	1000	20

Lorentz Force Detune is an issue!

FNAL's Resonance Control experience
Developed at FNAL Feed-Forward
Adaptive LS Lorentz Force Detuning Algorithm
(RF-pulse mode)

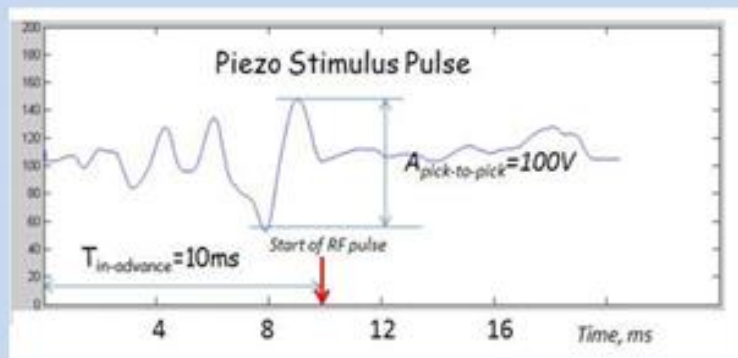
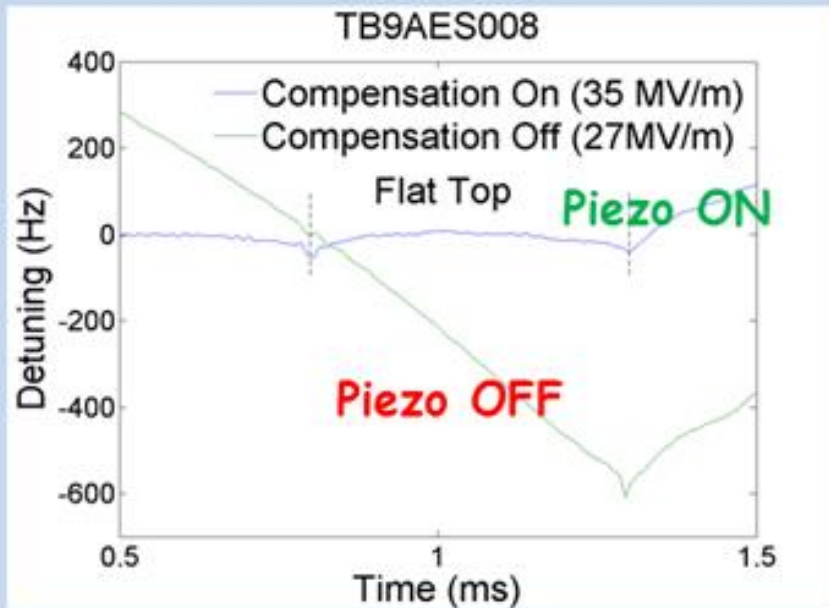
(1) 1.3 GHz (ILC & Project X)

(2) SSR1(HINS and PIP II)

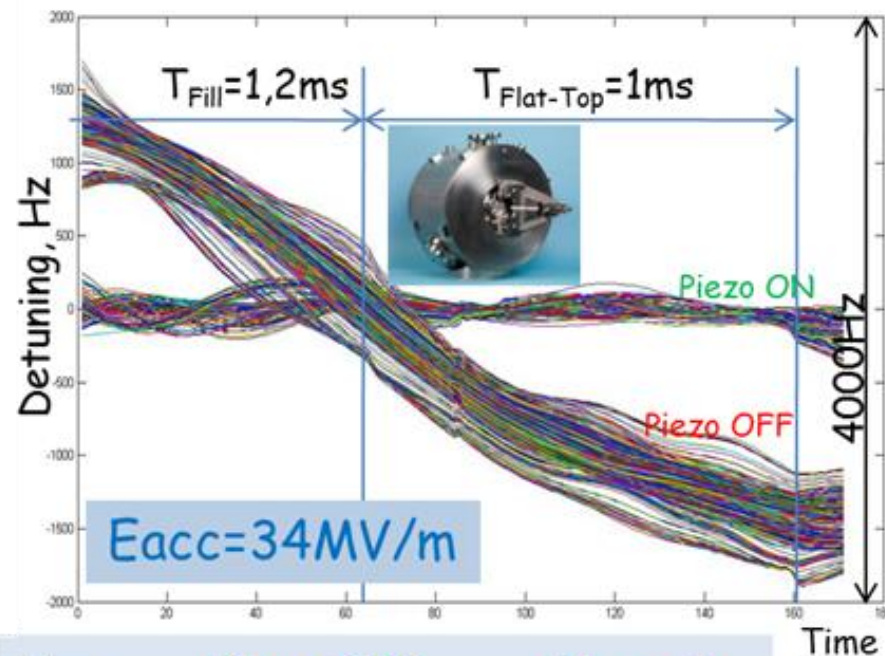
1.3GHz for ILC/XFEL pulse operation



LFD during 1,3ms RF-pulse (Fill+FlatTop) ~2300Hz
 After LS LFD compensation -- to less than 20Hz during 1,3ms pulse



325MHz SSR1 cavity



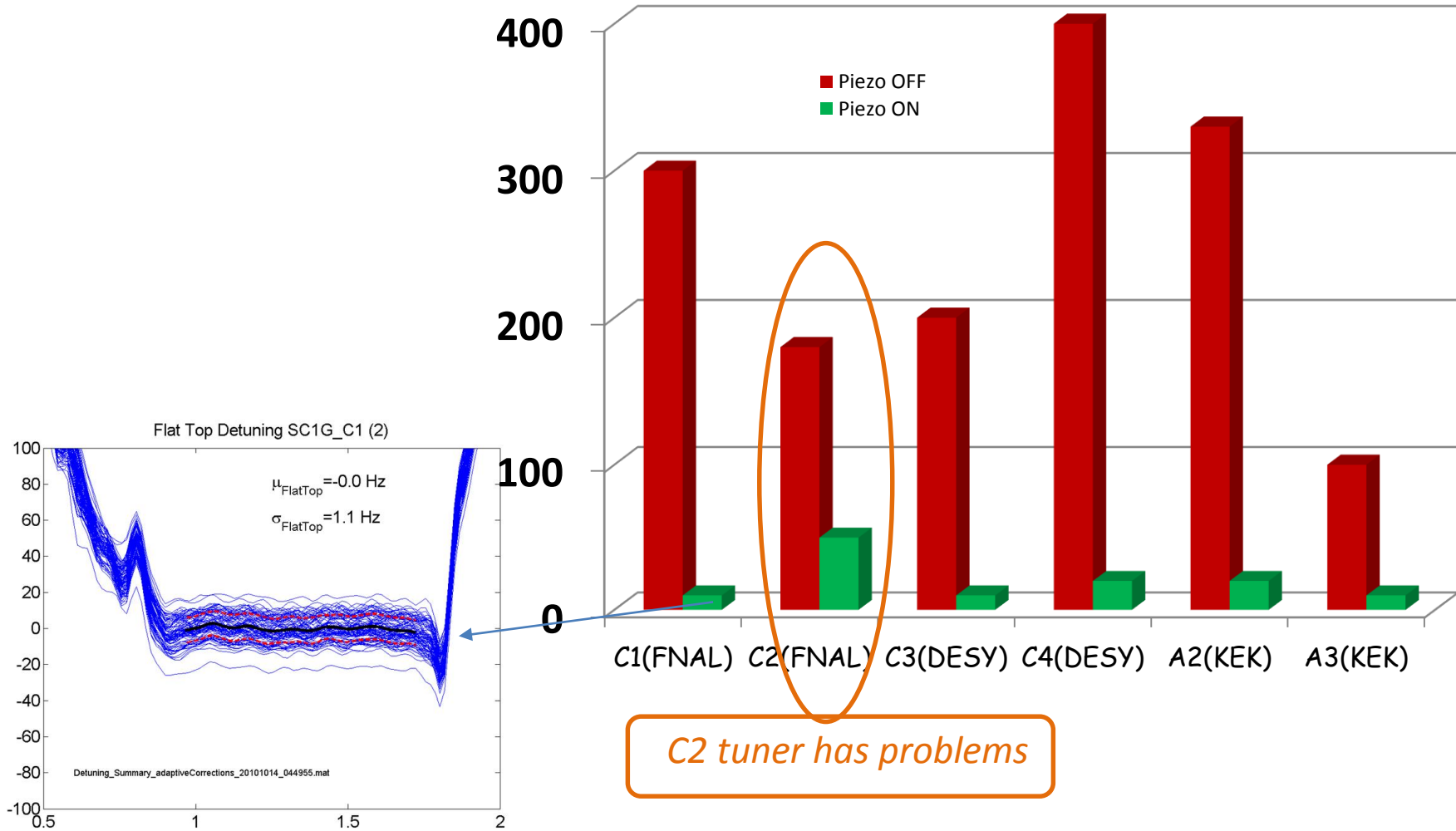
E_{acc}	Piezo OFF	Piezo On
34MV/m	3500Hz	75Hz

$\Delta F = -kE_{acc}^2$ $K \sim 1,2 \text{ Hz}/(\text{MV}/\text{m})^2$

S1Global

Lorentz Force Detuning (Hz)

(during 1ms Flat-Top)
before and after Compensation

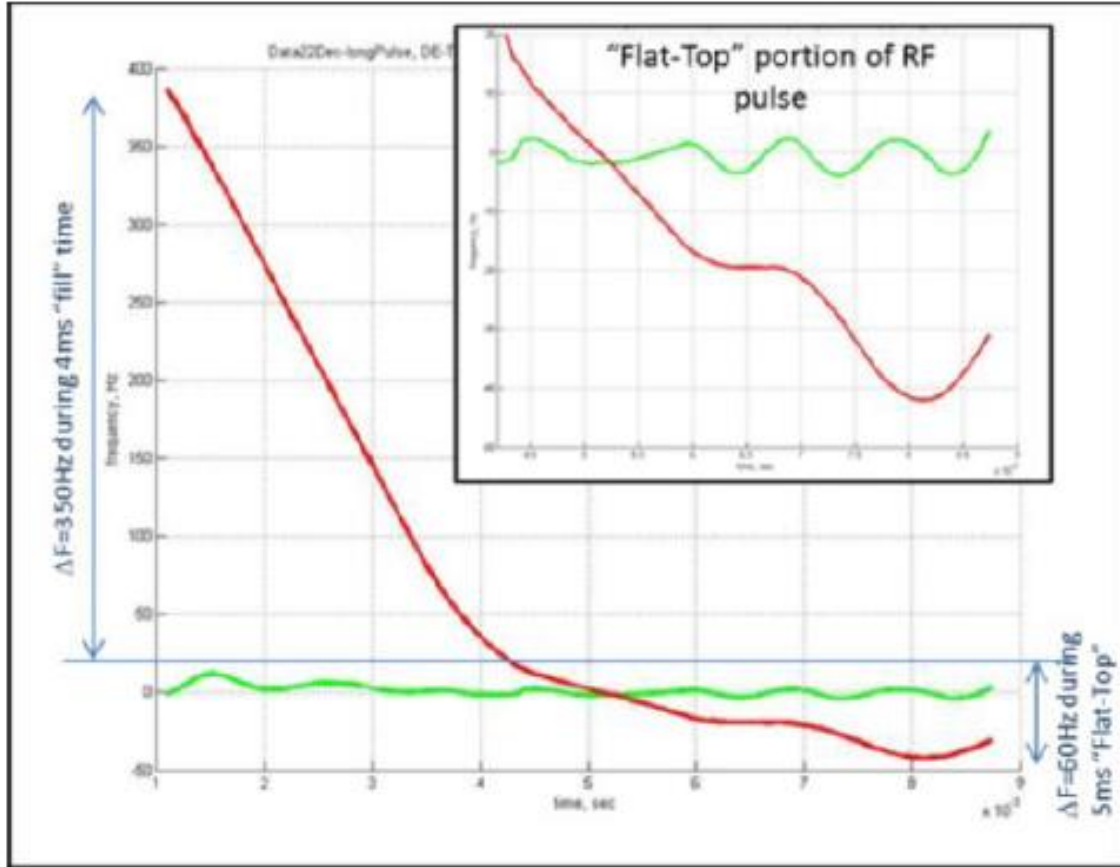


	Eacc	Piezo OFF	Piezo ON
C1(FNAL)	27	300	10
C2(FNAL)	22	180	50
C3(DESY)	18	200	10
C4(DESY)	25	400	20
A2(KEK)	39	330	20
A3(KEK)	31	100	10

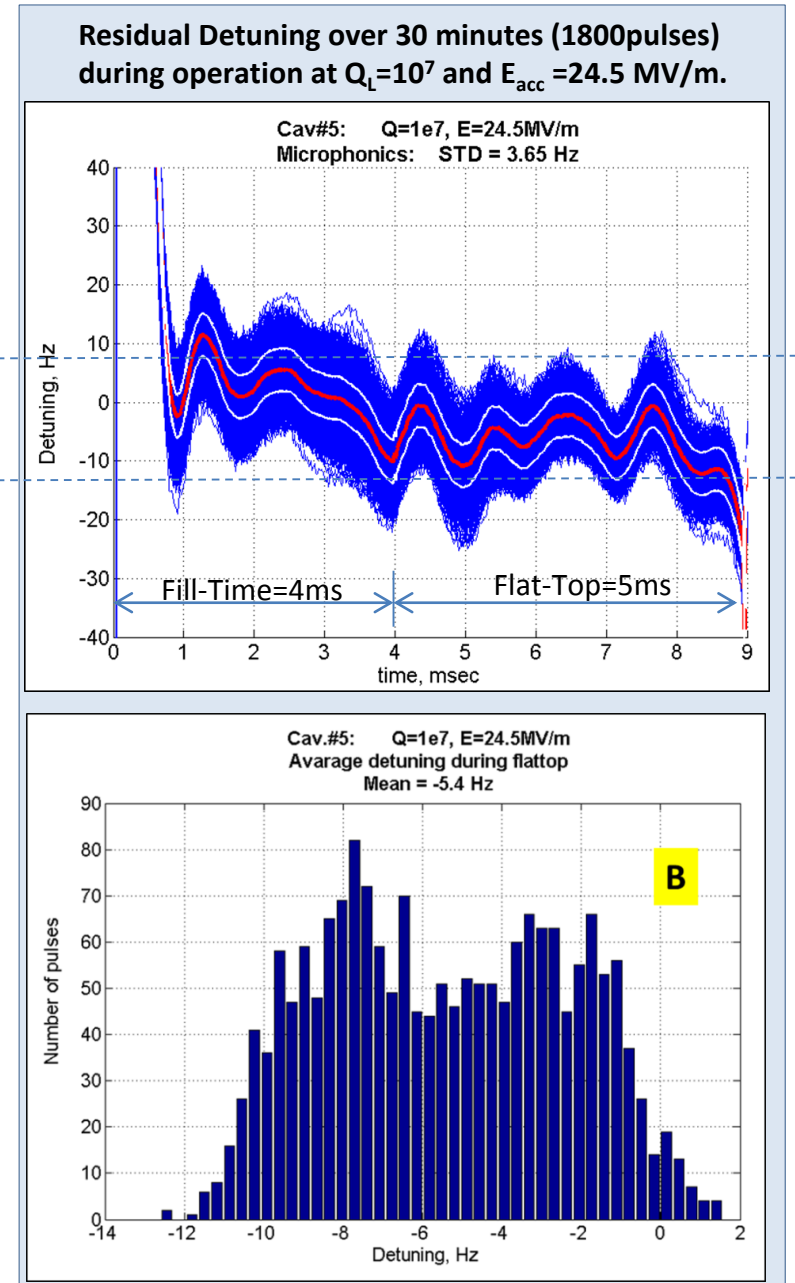
Level of detuning is close to what we are expecting with 650MHz PIP II cavities

BUT
HBW for ILC is 200Hz or 7 times large than 650MHz...

1.3GHz Long Pulse (4ms-fill&5ms flat-top)



“Slow “-4ms- fill time of the cavity do not exited
 “strong” 200Hz (5ms-period) main cavity resonance vibrations
 Cavity “push” by LF on $dF\sim 350\text{Hz}$

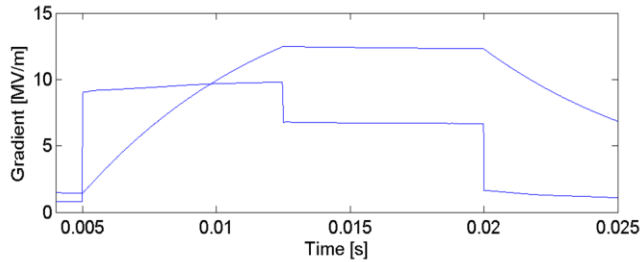


SSR1 at STC

PIP II operating conditions test

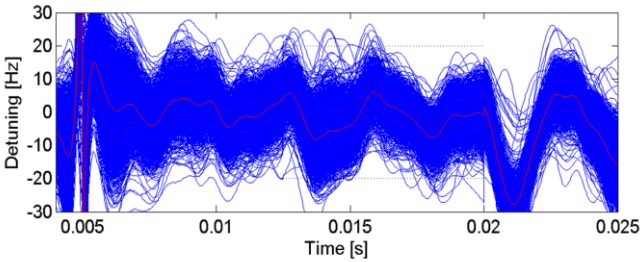
- PIP-II nominal operating conditions

- 12.5 MV/m
- 20 Hz repetition rate
- 15% duty cycle
- 0.5ms flattop

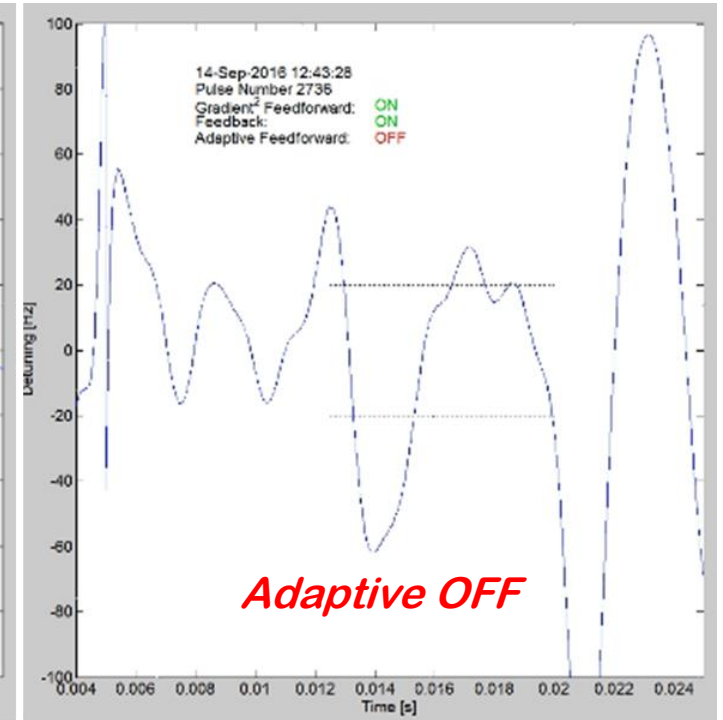
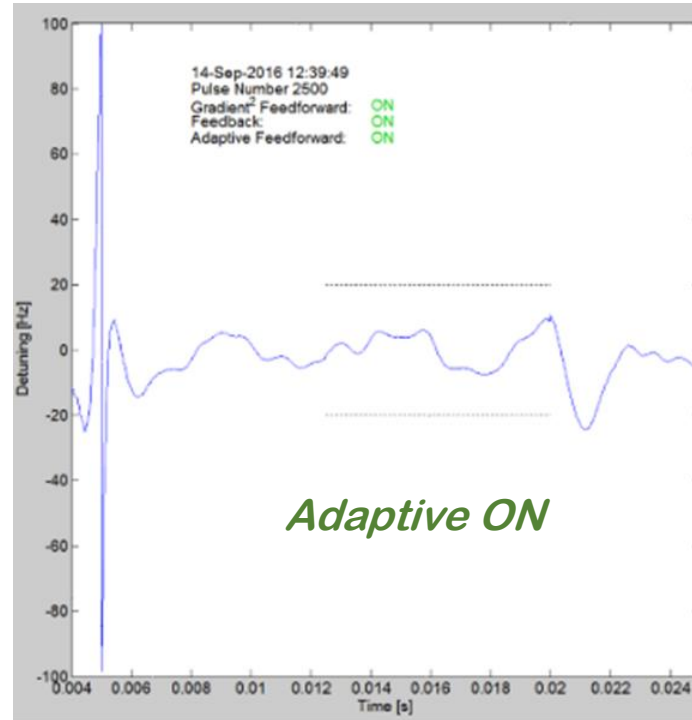
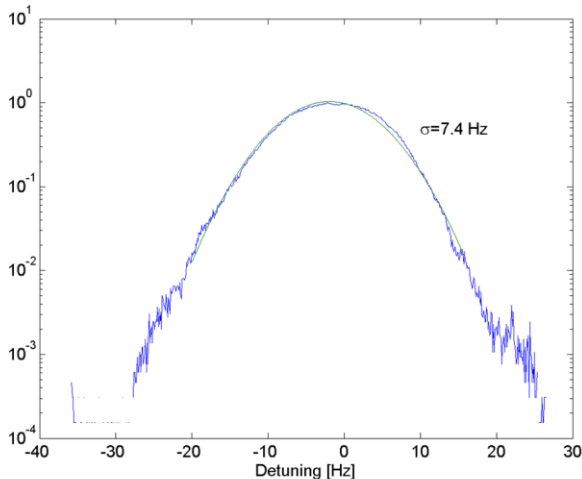


- STC operating condition

- >12.5 MV/m
- 25 Hz repetition rate
- 7.5 ms fill
- 7.5 ms flattop



~7.4 Hz RMS detuning on the flattop. Specification is a peak detuning of 20 Hz, so a further improvement in RMS of ~2 is needed.



Without the adaptive compensation on, the detuning was almost an order worse. Without the other two compensation methods, the cavity rapidly fell off resonance.

Significant progress has been made toward PIP-II specification of detuning.

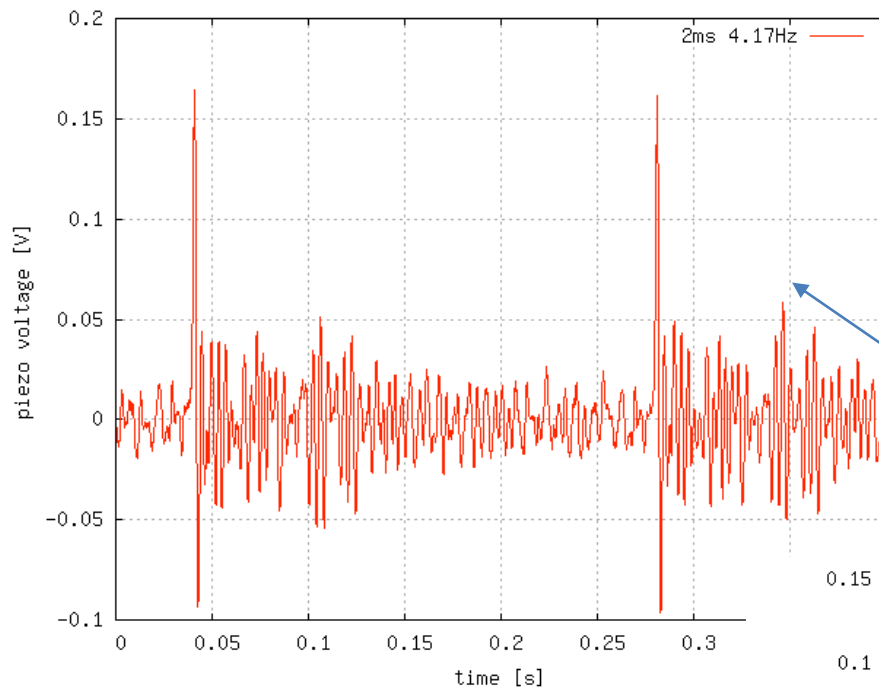
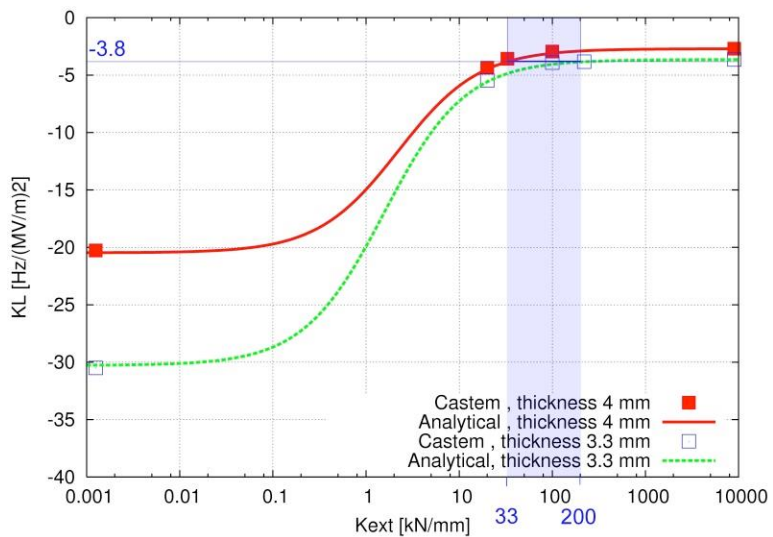
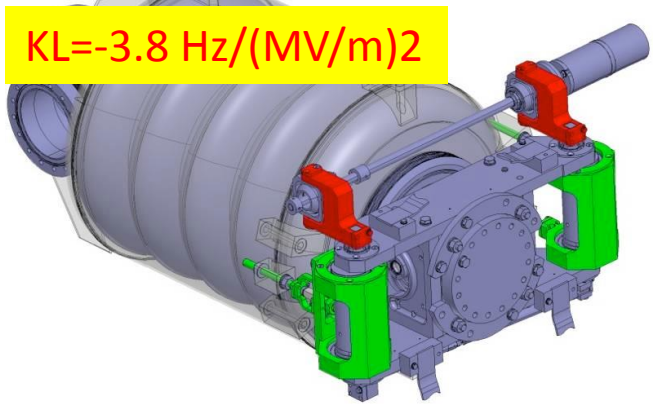
Plan for incoming test at STC:

- Improvements in feed back (automation of filter bank coefficients) should improve performance.
- May be possible to automatically extract optimal coefficients from delay scan data
- Further firmware improvements should allow more detailed studies of pulse structure.

Summary of Pulsed Cavities Resonance Control

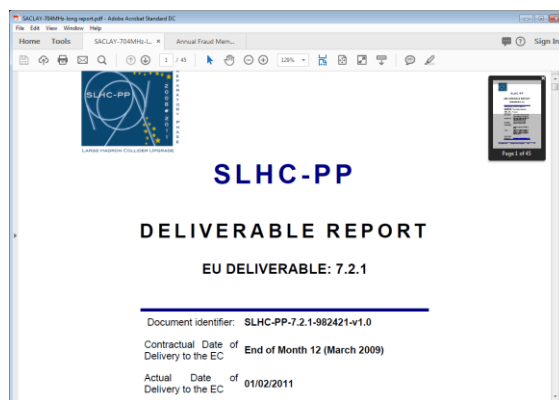
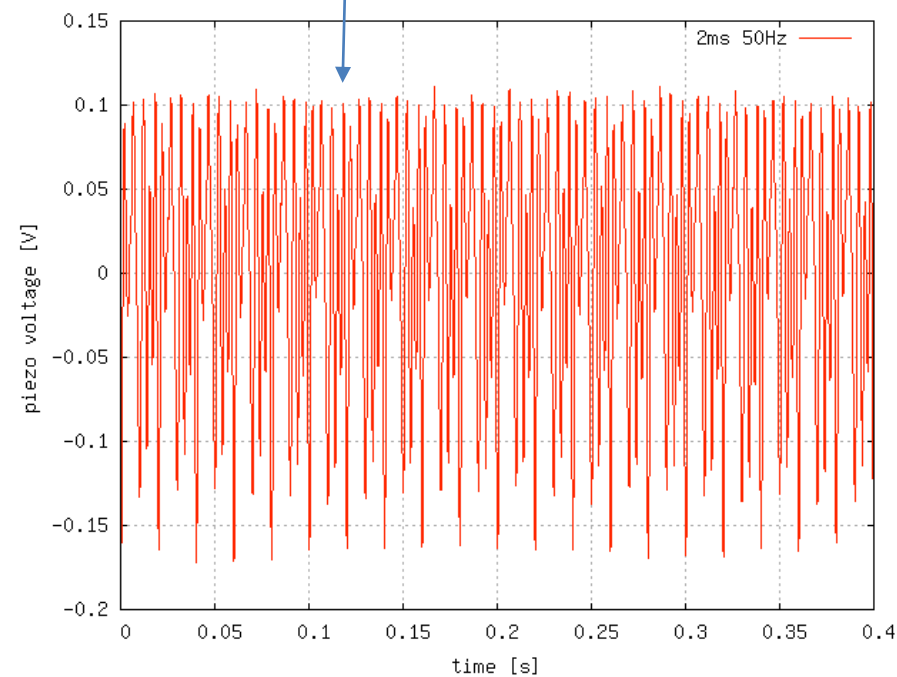
- FNAL accumulated significant experience of the Pulsed operations of the SRF cavities
 - (Developed at FNAL Feed-Forward Adaptive LS LFD Algorithm applied in all studies)
- So far we successfully worked in the range LFD/HBW ~3-5 ... for LB/HB650MHz we need to move in the range of **10-12...**
- **WE (AS A PIP II TEAM) MUST DEVOTE SIGNIFICANT AMOUNT OF “COLD CAVITY R&D TIME” FOR RESONANCE CONTROL. OTHERWISE (I am sure you could answer yourself what will be otherwise...)**
 - We need cold LB/HB650 cavities installed at HTS(2?) and available for reasonable amount of the time for RCG study... not cavity = no progress

Brief summary of CERN/SACLAY test of 5 cell 704MHz cavity in pulsed operation (SLHC-PP)



Piezo-as a sensor

2ms RF pulse with repetition rate 4Hz & 50Hz



FAST/Piezo TUNER

- So far there are NO any working machine that relay on the piezo control
- Many group around world building tuner's system that included fast/piezo tuner... but they doing this just fashionable ... if you talk with them in private discussion they will tell you that piezo is not reliable...
- LCLS II will be first machine that MUST have working 24/7 piezo tuner - FNAL worked with PI engineers to develop custom piezo-capsule for LCLS II tuner...
- So far we do not have any other options at this moment as to adopt LCLS II piezo-capsule to PIP II tuners (SSR1 & LB/HB650)
- This technical decision is far from optimal (see next Table)...
- **If we want reliable PIEZO-TUNER we need to develop Piezo-ceramic actuator that will satisfy PIP II project requirements**

*Requirements to the piezo for operation in XFEL/ PIP II and
LCLS II
Impact on the longevity of the piezo*

	XFEL/PIP II	LCLS II	FNAL-test-stand (2month)
Operation	10/20 pulses/sec	CW	CW
stimulus pulse, Hz	200 <i>(2 sinewave per pulse)</i>	40	5000
Vpp, V	120	2	2
piezo stroke,[um]	5	0.2	0.2
number pulses for 20 years	1E+10	2E+10	2E+10
total stroke of piezo for 20years, [km]	60/120	5	5
Piezo-stack motion speed (rms) (mm/s)	4.5	0.02	2.2
Piezo-stack motion acceleration (rms)(g)	0.6	0.0004	7
Heat dissipation, [mW]	90/200	0.05	6
Piezo ΔT raised	20K/ ~40K	0.1K	2K

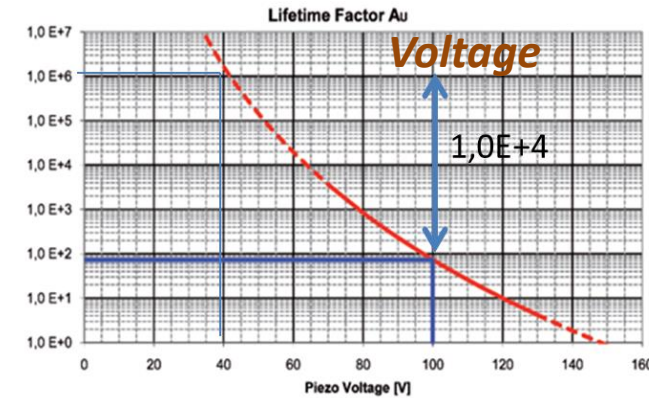
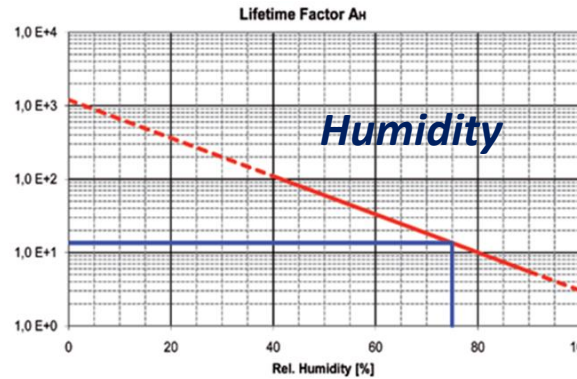
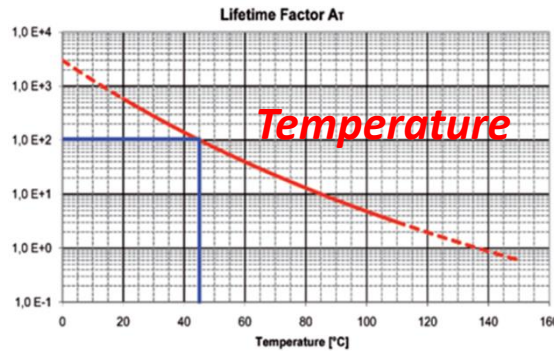
$P_{av} = \pi C U^2 f * D$, where D is dissipation Factor (~5-20%)

**estimated
measured**

**Operational voltage for PIP II piezo will be 60 times higher than that for LCLS II.
Power dissipation inside piezo-ceramic actuator for PIP II is 4000 large than for LCLS II
Overheating of PIEZO is major problem.**

Piezo Tuner Lifetime (1)

In contrast with electromechanical devices , cold vacuum is an almost ideal environment for piezo actuators.



.....cold vacuum is an almost ideal environment for piezo actuators... except the problems to heat transfer from piezo inside insulated vacuum...

Piezomechaniks $\Delta T \sim 70$ Degree

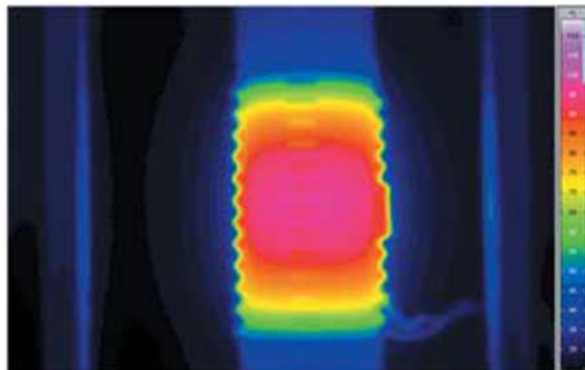


Fig. 5.1: Thermal image of a dynamically cycled high voltage actuator, clamped at its end faces. Environment: ambient air convection. Notice the cooling effect at the end-faces due to the clamping mechanics



In case of nonuniform current distribution at piezo structure the positive thermal feedback may happen! $\uparrow T \uparrow Z \downarrow (C \uparrow, R \downarrow) \uparrow T \dots$



LLRF13 Lake Ta
M.Grecki, DESY

With decrease voltage lifetime increase exponentially

Decreasing operational voltage from 100V to 40V will increase lifetime in **10,000 time.**

Do not design piezo-tuner with assumption to run NEAR V_{max} .

Selected longer piezo/ to operate at lower possible Voltage

High reliability of tuner components (piezo-actuator) Accelerated Piezo Lifetime test at FNAL

Designated facility at FNAL to test piezo at the CM environment (insulated vacuum and LHe)

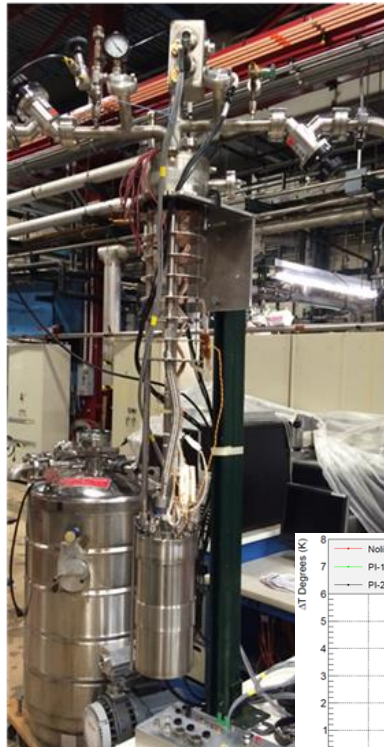


Insert into LHe dewar with cryo/vacuum and electrical connections

Capsules (up to 5) with Piezo-stacks Mounted on the copper block



- RTD (Cernox) –to mount on Piezos
- Geophones (to monitor piezo stroke)



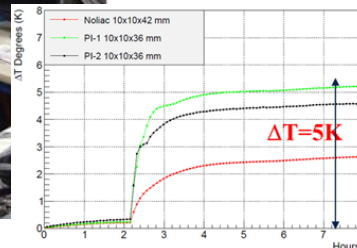
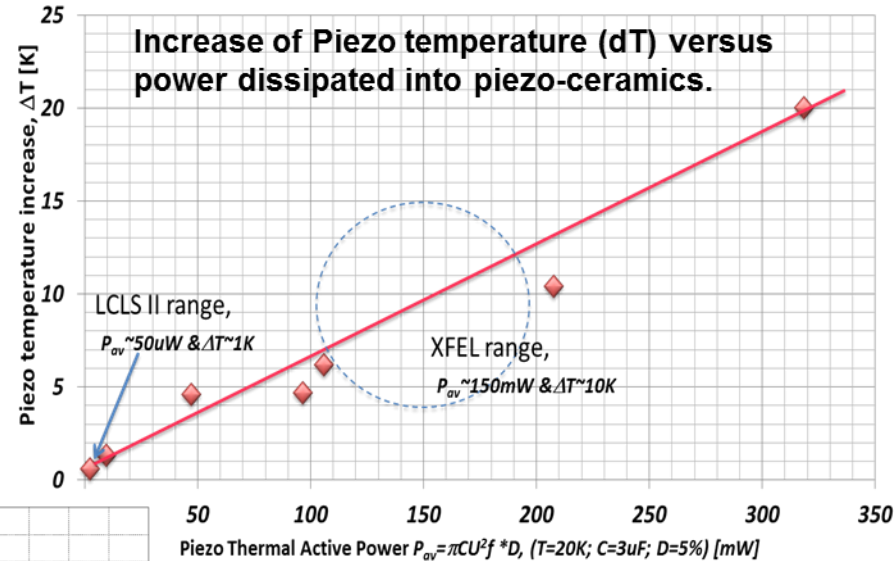
Accelerated piezo-stack lifetime test

$2 \cdot 10^{10}$ pulses ($V_{pp} = 2V$ & $F = 40Hz$)

20years \rightarrow 2 month (40Hz \rightarrow 5kHz)

LCLS II --- $P_{av} \sim 50\mu W$ (40Hz, 2V)

During ALT at 5kHz $P_{av} \sim 6mW$ ($\Delta T \sim 2K$)



LCLS II Tuner piezo-stacks run for $2.5 \cdot 10^{10}$ pulses (or 125% of LCLS II expected lifetime) without any degradation or overheating

Summary

1. We must expect that tuner/dressed cavity/He vessel system will have stiffness ~40kN/mm.
 - ❖ Expected value of LFD/HBW will be in the range of 12-15...
2. FNAL Active Resonance Control Experience (*for range of LFD/HBW~5*) provide cautious optimism for compensation LFD/microphonics for LB/HB650MHz cavities.
3. Significant R&D time with “cold dressed LB/HB650MHz cavities” required.
4. To have RELABLE fast/piezo tuner we need to collaborate with piezo-ceramic company (PI ?) to develop PIP II specific piezo-actuator