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Magnetrons - High Power RF Sources

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Magnetron Collaboration

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 - Michael Read, R. Lawrence Ives, Thuc Bui
- Fermi National Accelerator Laboratory
 - Brian Chase, Ralph Pasquinelli, Ed Cullerton, Philip Varghese
Josh Einstein, John Reid
- Communications and Power Industries LLC
 - Chris Walker, Jeff Conant

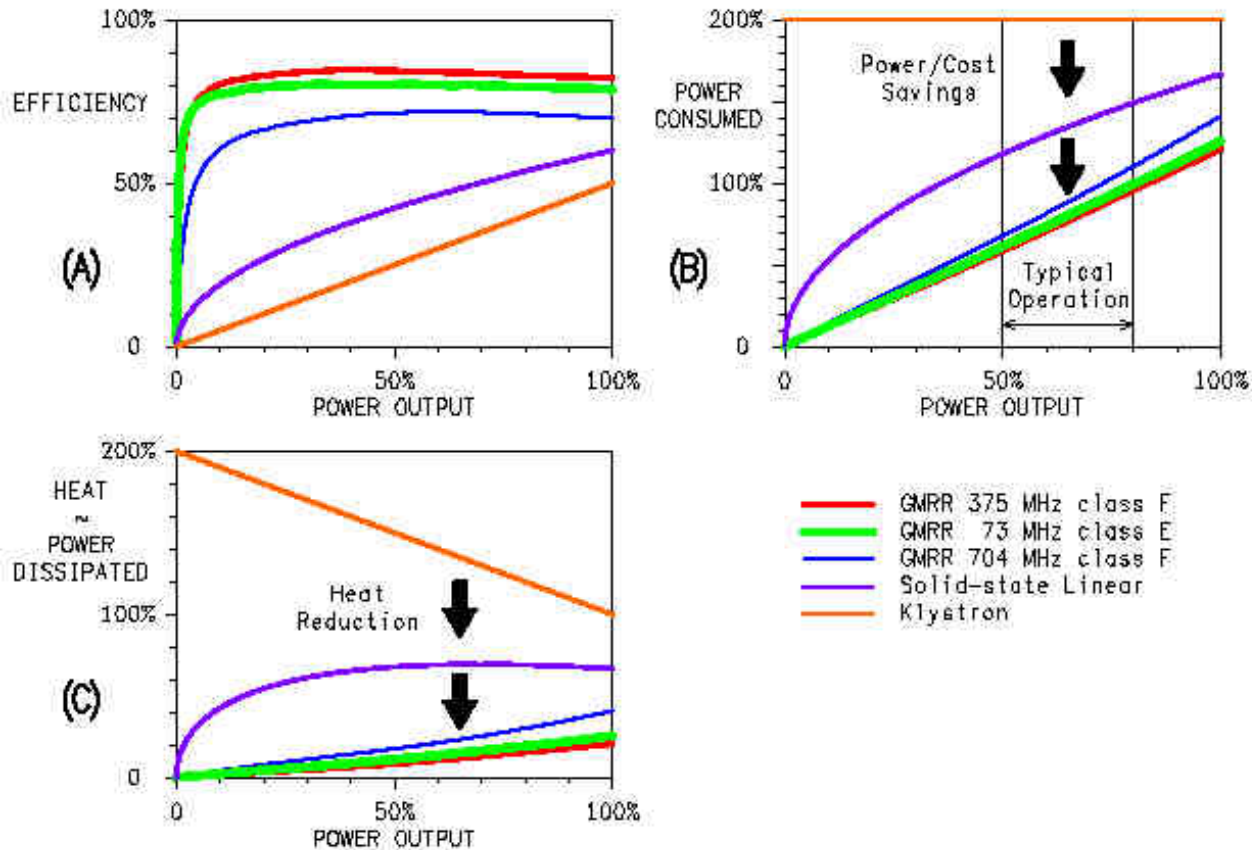
Outline

- Demands for high power, high efficiency RF
- Vector control schemes for magnetrons
- Experimental results
- Ongoing research

Take-a-ways from the Proton Driver High Efficiency Workshop at PSI

- **Proton Drivers:**
 - GeV-energy range
 - **MW-beam** power range
- Applications: neutrinos, muons, neutrons, Accelerator Driven Systems(ADS).
- **Types of accelerators for proton drivers:**
 - Cyclotrons and Fixed-Field Alternating Gradient accelerators (FFAG);
 - Rapid Cycle Synchrotrons (RCS);
 - High intensity pulsed linear accelerators;
 - **CW Superconducting RF linear accelerators.**
- **High RF efficiency is critical for high beam power application**

EFFICIENCY - IMPACT



- Cooler -> More reliable

- Lower operating cost
- Lower HVAC requirements



PROPRIETARY INFORMATION

4

The basics of magnetron operation

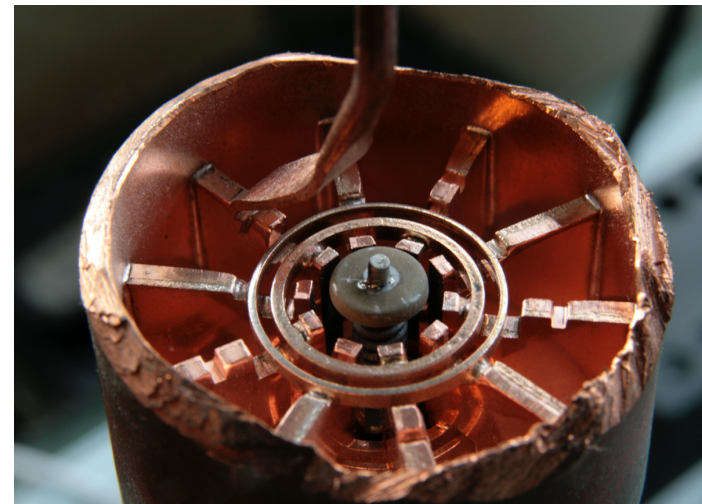
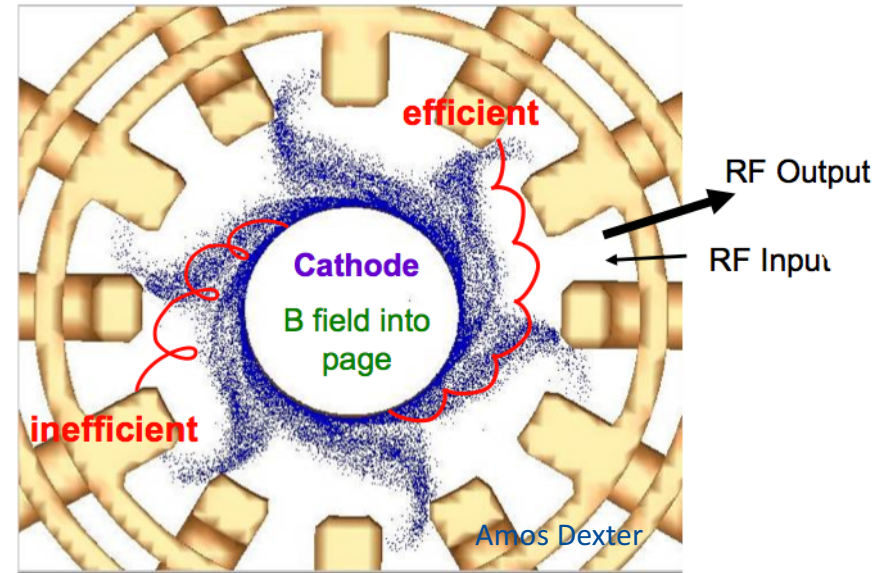
Cathode at negative potential accelerates electrons outward.
B field causes electrons to spiral
E field across gaps causes bunching into electron cloud spokes. Rotating spokes interact with cavities. RF power is coupled out and is constant amplitude.

Injection Locking:

RF maybe driven in on same port and cause the spokes to phase lock up to source providing low noise RF

Cross section of a cooker magnetron showing cathode and RF cavities

R. Adler, A study of locking phenomena in oscillators, Proc. IRE and Waves and Electrons, vol. 61, no. 10, pp. 351-357, June 1946.



Magnetrons excel at many RF source requirements

- Power: >100 kW CW and MW scale pulsed operation
 - average power capability increase with lower frequency
- Efficiency: High power devices $> 85\%$ at L-band
- Power supply voltage: typically < 25 kV
- Low cost: $\$0.50/\text{watt}$ at 100kW and 50 units
- Small size: 100 kW pulsed 1300 MHz tube is <1 foot high and does not require an oil tank
- They are easy to replace and rebuild and can be designed for a reasonably long life and low noise when injection locked
- **However, they are basically a constant power device, not a linear amplifier like a klystron**

Industrial CW Magnetrons

Table 1. Characteristics of CW Industrial Heating Magnetrons from Domestic Manufacturers

Manufacturer	Type	Frequency (MHz)	Power (kW)	Effic (%)	Voltage (kV)	Current (A)
California Tube Labs	CWM-300L	915	300	90	32	10
California Tube Labs	CWM-100L	896, 915	100	88	19.5	5.8
Burle Technologies	S94608E	896, 915	90	85	21	6.5
CPI Beverly	915MHz-75	915	100	85	20	6.0
California Tube Labs	CWM-15s	2450	15	72	12.6	1.7
California Tube Labs	prototype	2450	30			

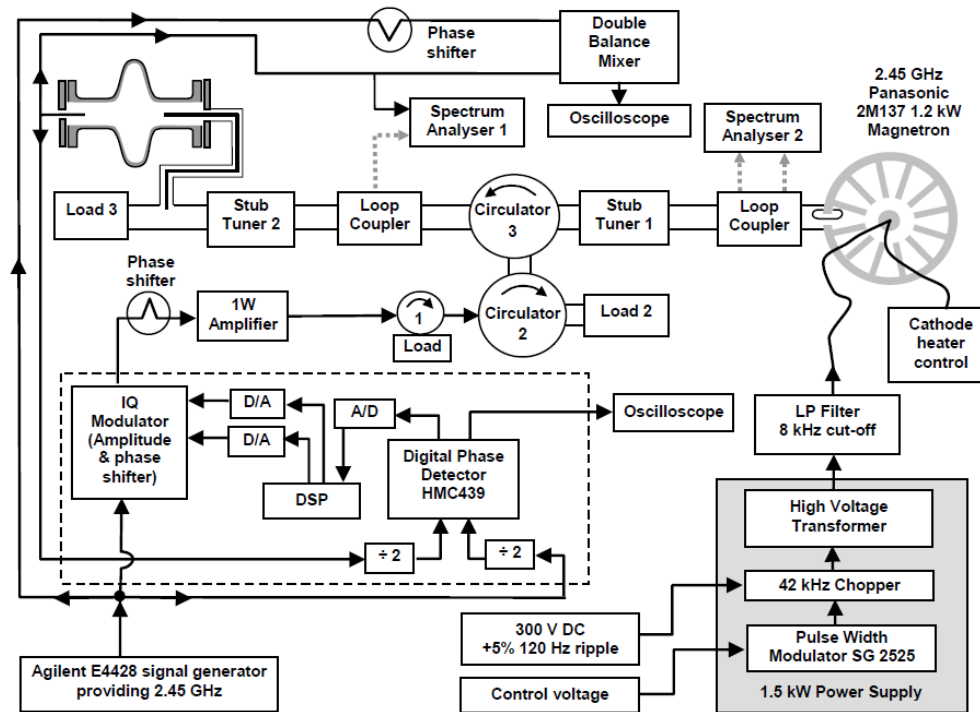
- High power CW magnetrons used for industrial heating are catalog items
- > 85% efficiency typical
- 100 kW L-band - 18" length, 5" diameter

Phase control loop around SRF cavity

Lancaster: Amos Dexter, Graeme Burt and Chris Lingwood

Demonstration of CW 2.45 GHz magnetron driving a specially manufactured superconducting cavity in a VTF at Jlab.

Control of phase in the presence of microphonics was successful.



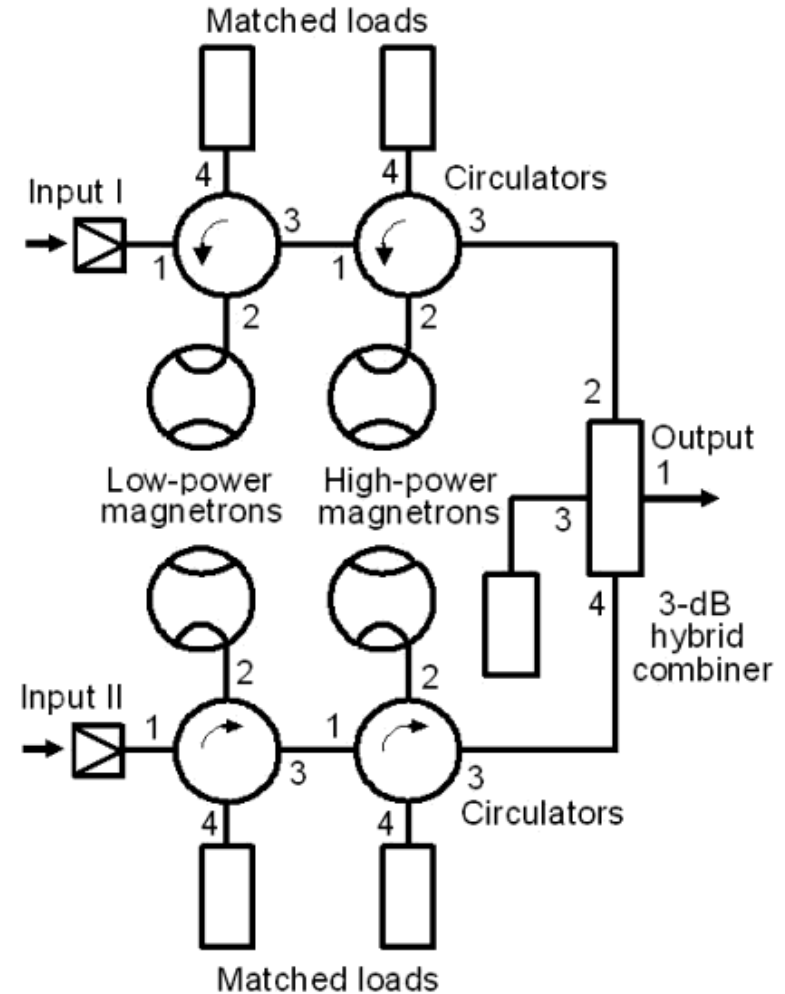
H. Wang *et al.*, "USE OF AN INJECTION LOCKED MAGNETRON TO DRIVE A SUPERCONDUCTING RF CAVITY," in *Proceedings of IPAC'10*, Kyoto, Japan, THPEB067.

Cascaded magnetrons and out-phasing AM control

Concept: cascade injection locked magnetrons to increase gain, combine two pairs to get amplitude control by outphasing in pulsed mode operation

Outcome: Proof of concept for cascade stage and the realization that we needed CW power supplies to make real progress. Strong belief that this scheme would work but it does have its complexities.

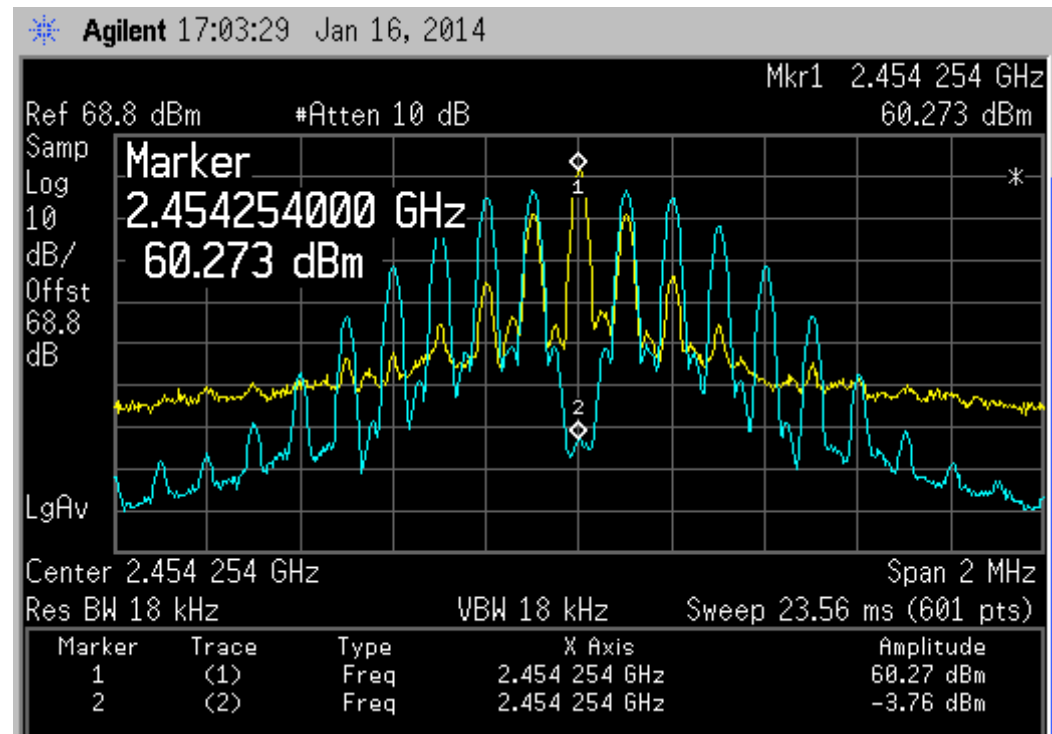
Grigory Kazakevich, et al. Muons Inc.
Yakovlev, Pasquinelli, Chase, et al. Fermilab



Amplitude control by fast phase modulation technique

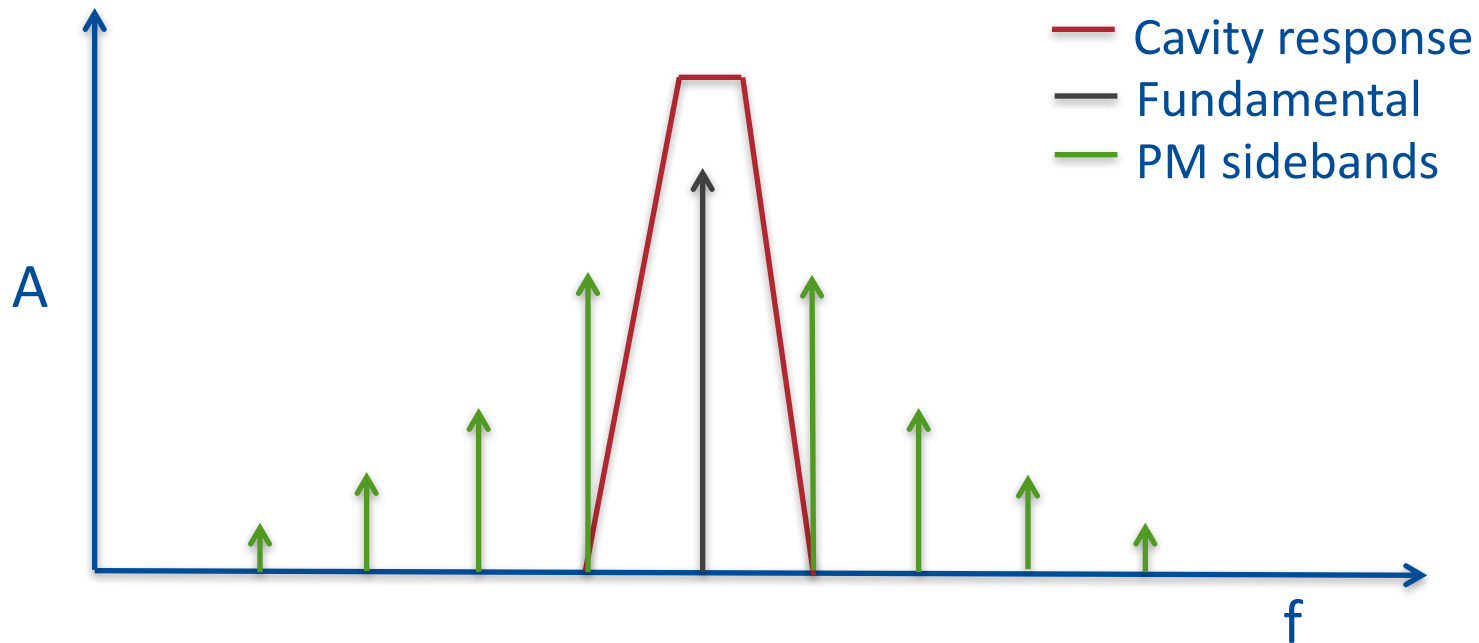
Magnetrons are constant output power devices. However, the power in the carrier destined for the cavity can be reduced by fast phase modulation, moving power from the carrier into discrete Bessel sidebands that are outside the cavity bandwidth. These sidebands will be reflected from the cavity and back to the circulator load

Increasing the modulation depth (137 degrees) suppresses the carrier over a measured 64 dB dynamic range in lab



Rejection of PM sidebands by Narrowband Cavity

While output power is constant, sinusoidal phase modulation creates discrete sidebands at multiples of the modulation frequency while the power shifted from carrier to sidebands is determined by modulation depth



Phase Modulation Equations

$$A \cos(\omega_C t + b \sin \omega_M t) = A J_0(\beta) \cos \omega_C t +$$

$$\sum_{k=1}^{\infty} J_{2k}(\beta) [\sin(\omega_C + 2k\omega_M)t + \sin(\omega_C - 2k\omega_M)t] +$$

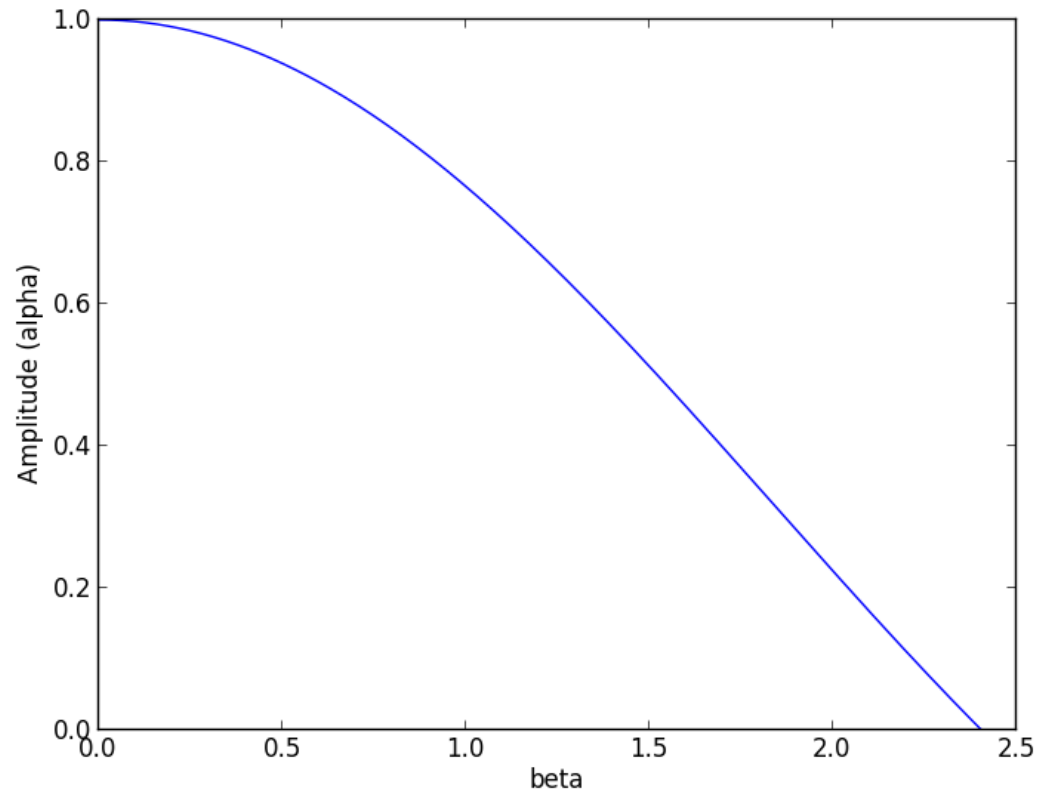
$$\sum_{k=0}^{\infty} J_{2k+1}(\beta) [\cos(\omega_C + (2k+1)\omega_M)t - \cos(\omega_C - (2k+1)\omega_M)t]$$

$$J_0(\beta) = 1 - \frac{\beta^2}{2^2} + \frac{\beta^4}{2^2 \cdot 4^2} - \frac{\beta^6}{2^2 \cdot 4^2 \cdot 6^2} + \dots$$

Used for generation of amplitude-to-phase LUT. Generates a lookup table such that the region before the first null in the Bessel is covered by the controller. Allows for linearization corrections by just adding a scaling table.

$$J_0(\beta) - \alpha = 0$$

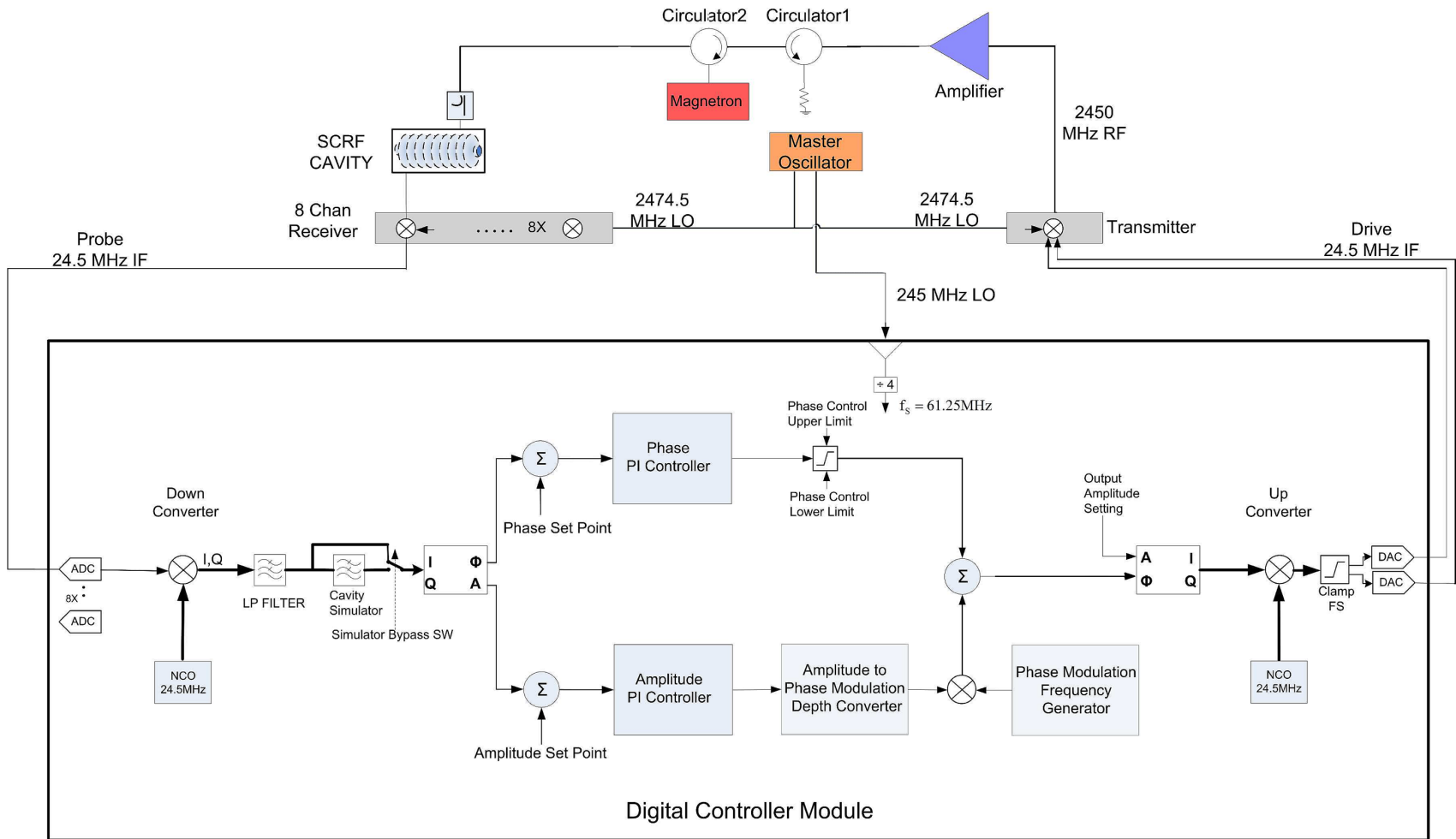
Bessel of the first kind, Region before first null



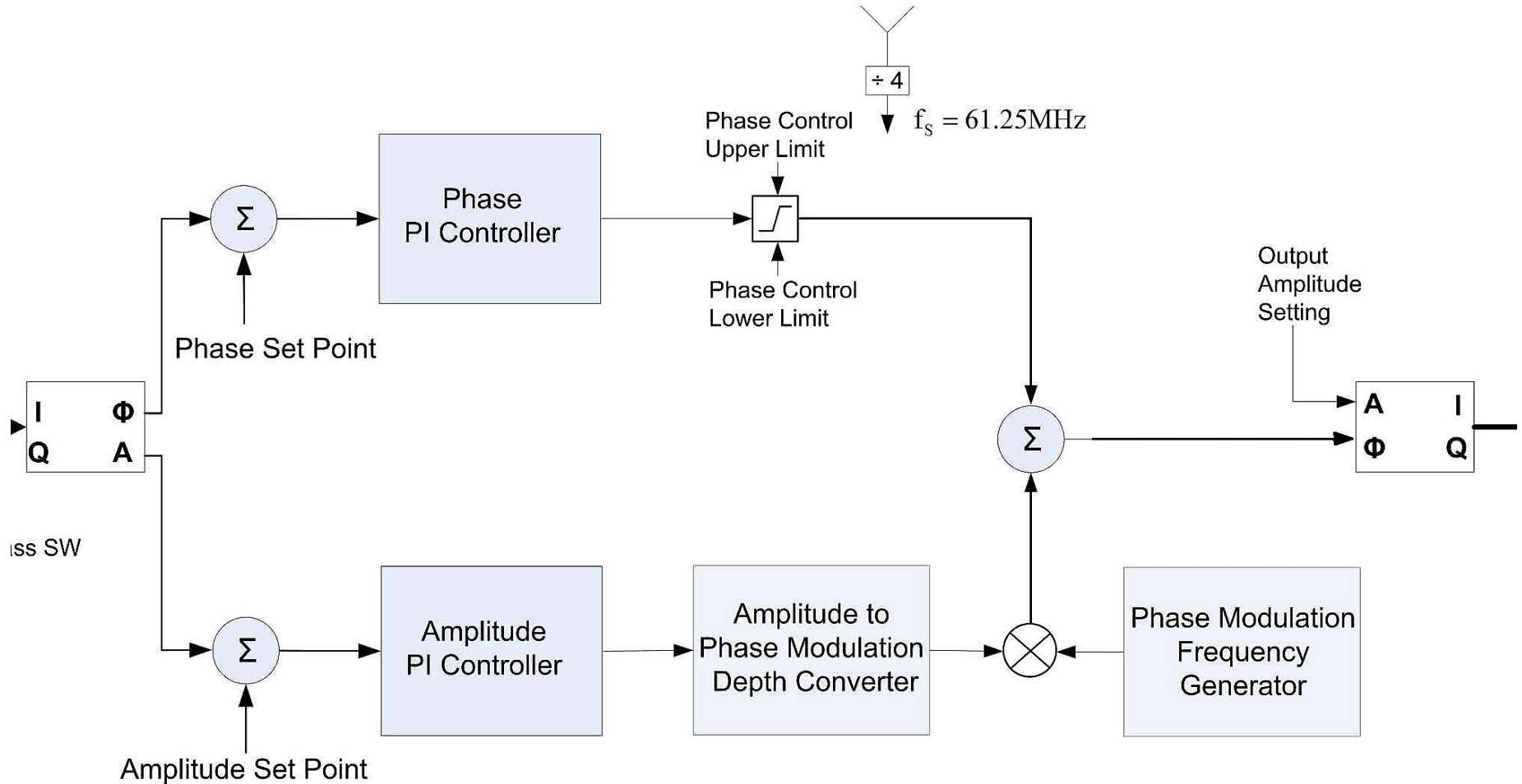
Inverse function in look up table drives phase modulation depth to linearize cavity drive

LLRF controller for 2.45 GHz SRF cavity driven by 1.2 kW Magnetron using Fast Phase Modulation

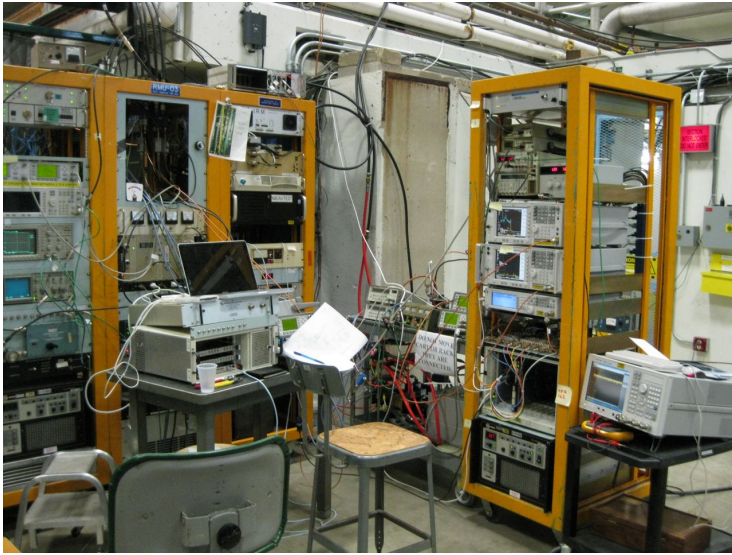
Magnetron Amplitude and Phase Control System



Controller architecture



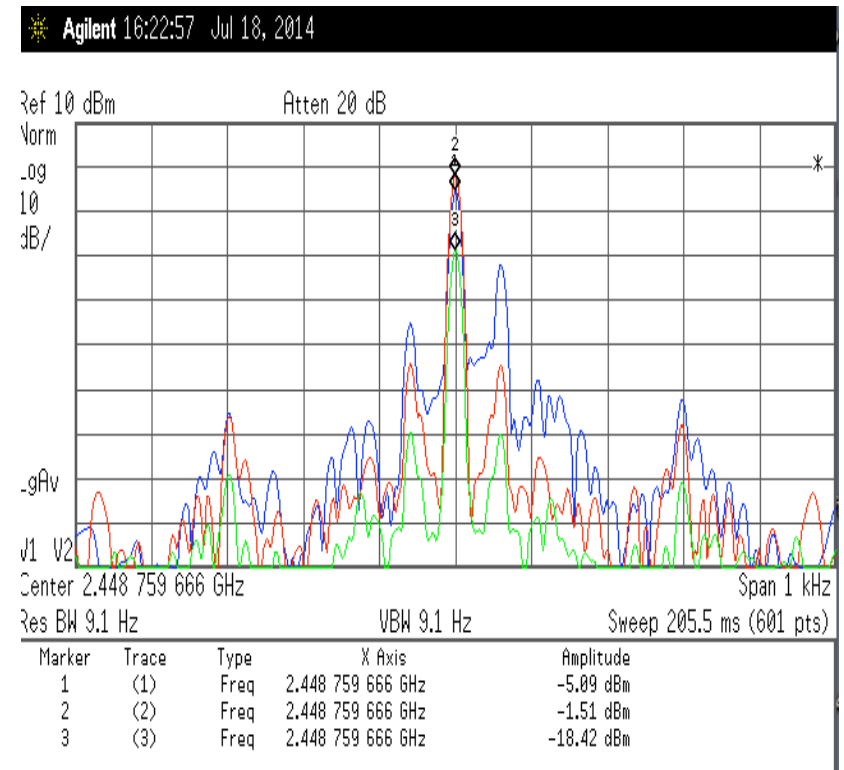
Injection Locked 2.45 GHz magnetron driving SRF cavity



Commercially procured 2.45 GHz 1.2 kW magnetron
Loaned SRF cavity from JLab
Testing took place over one week period in July 2014.
Published in JINST

A0 VTS 2.4 GHz Magnetron - Cavity test results

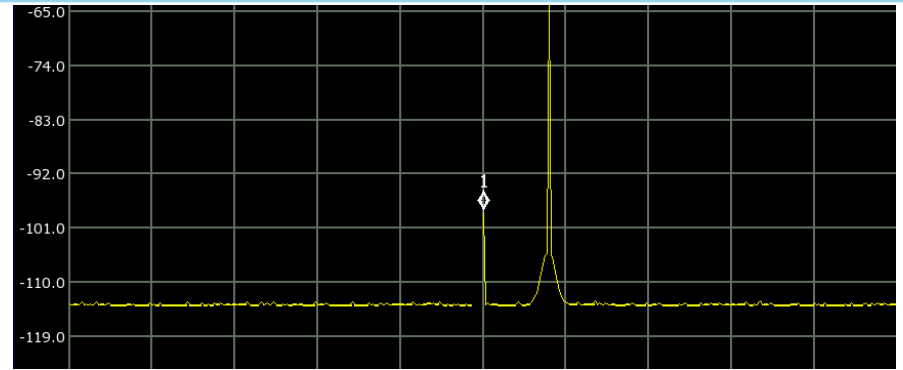
- Amplitude control shown linear over 30 dB range
- Moderate feedback performance demonstrated
- 0.3% r.m.s, and phase stability of 0.26 degrees r.m.s.
- Tests limited by extreme cavity microphonics and very limited time with the test cave



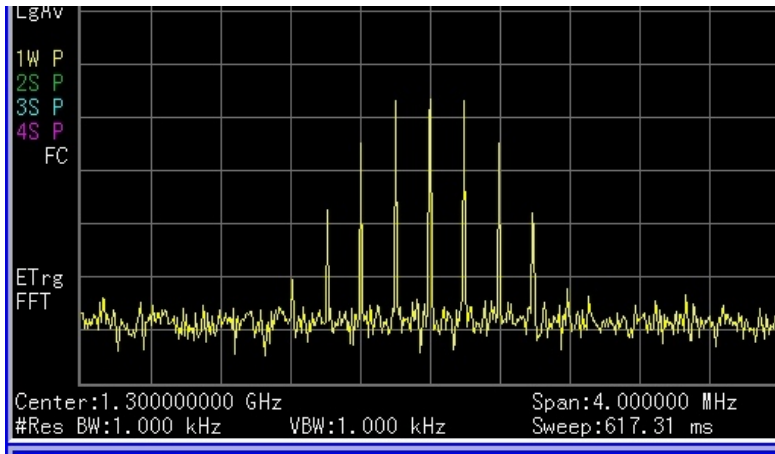
Cavity at 4 K, LLRF drive. Blue loops open, Red loops closed and maximum output, Green loops closed and amplitude reduced by 17 dB shows the PM modulation is effective for amplitude control.

Phase Modulation Tests on 1300 MHz 9-cell Cavity

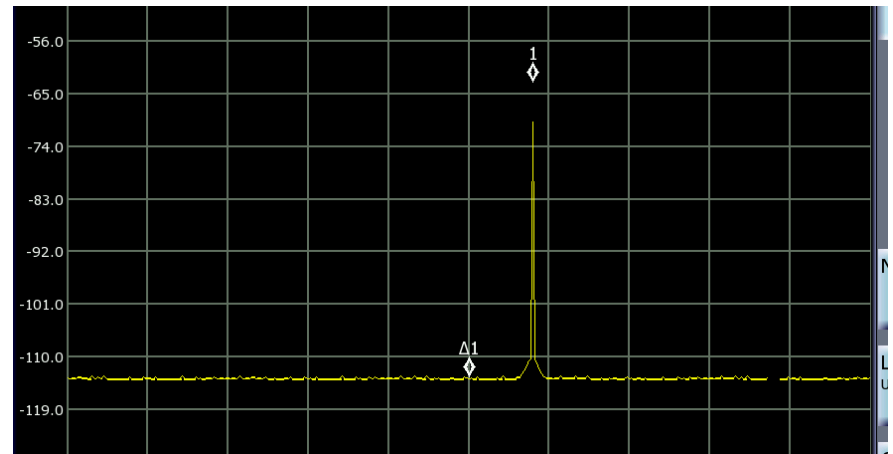
- 9 cell cavity is driven by a phase modulated source through a 4kW solid state amplifier



8/9 pi mode driven by carefully tuned 2nd sideband



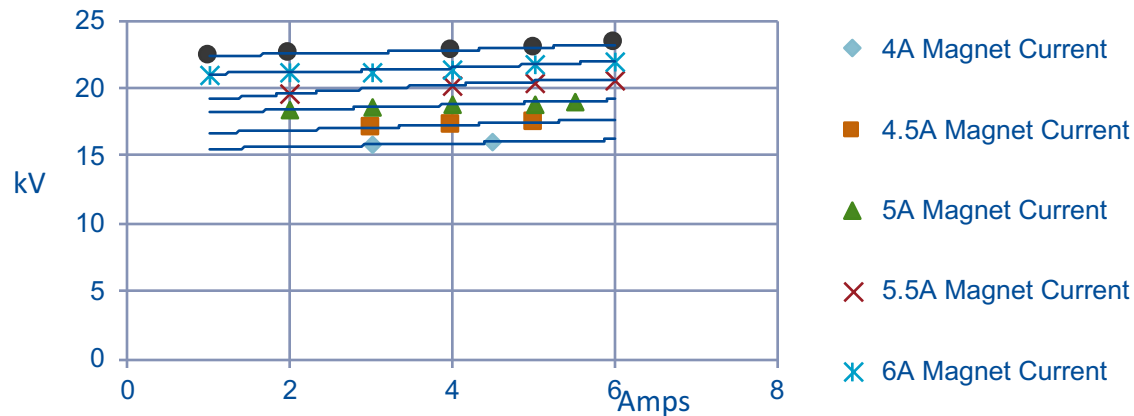
Forward power from SSA



8/9 pi mode is easily not excited by sidebands

CCR / CPI - 100 kW Pulsed, 10 kW Ave. 1.3 GHz Magnetron

Calabazas Creek Research Inc
Phase II SBIR grant to develop a 1.3 GHz, 100 kW
peak power, 10 kW average power magnetron
station in partnership with Fermilab and
Communications and Power Industries LLC, utilizing
a full vector control scheme developed by Fermilab.



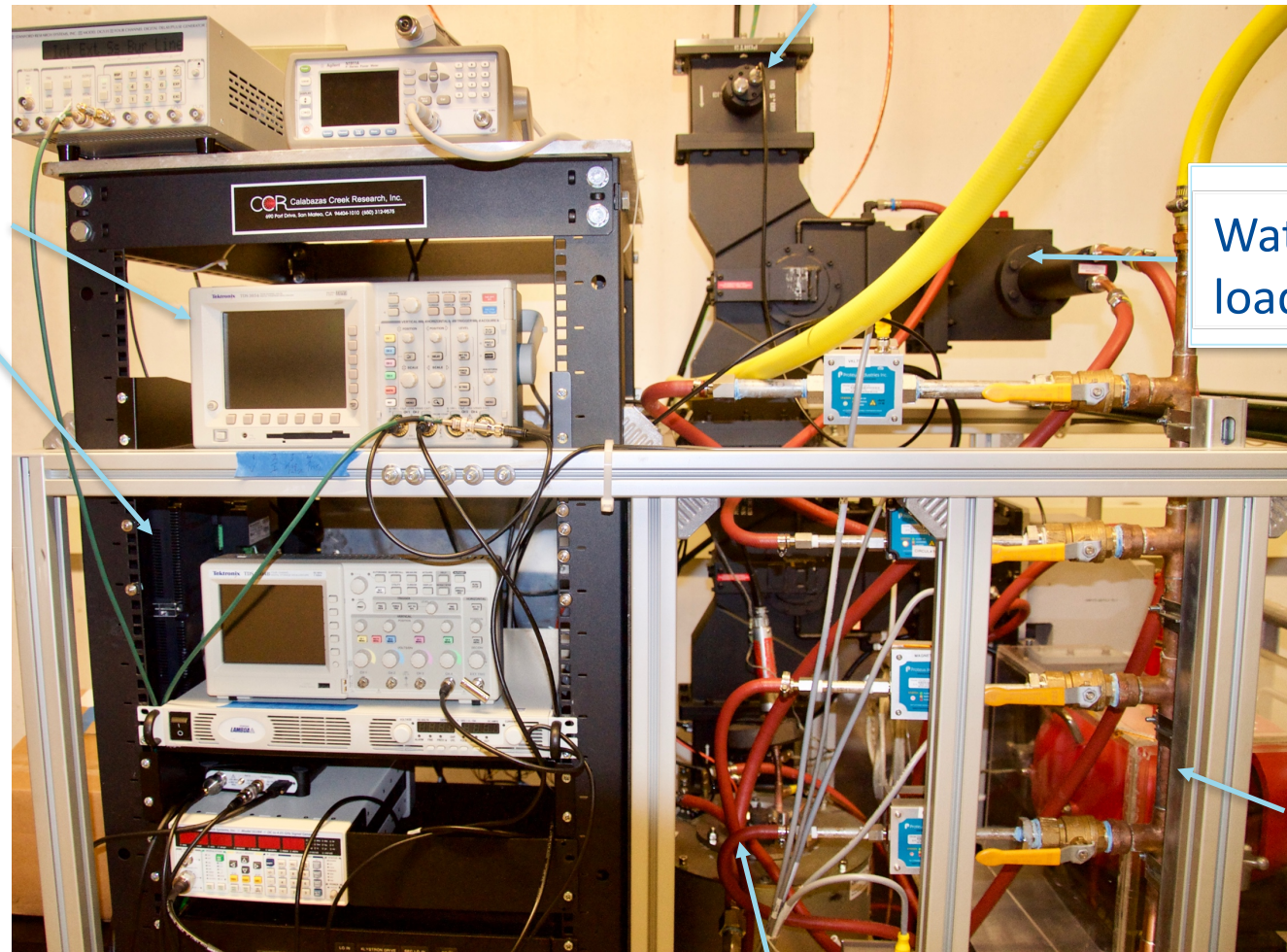
V-I Characteristics of Magnetron at
Varying Electromagnet Current
Values from initial short pulse tests.



tube~12" tall

CCR 1.3 GHz 100 kW magnetron testing at HTS Fermilab

Isolator with shorting plate



Diagnostics and control

Water cooled load

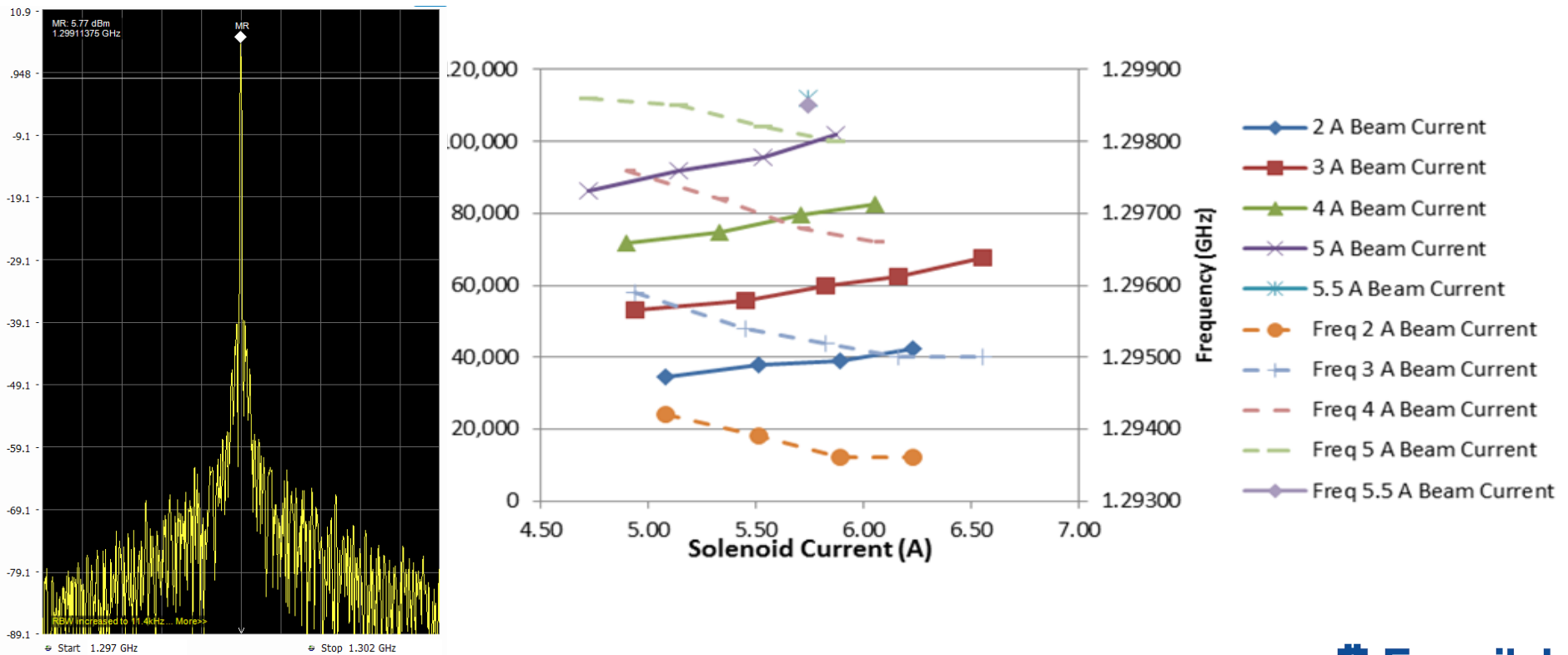
High voltage modulator not shown

Klystron

100 kW Magnetron

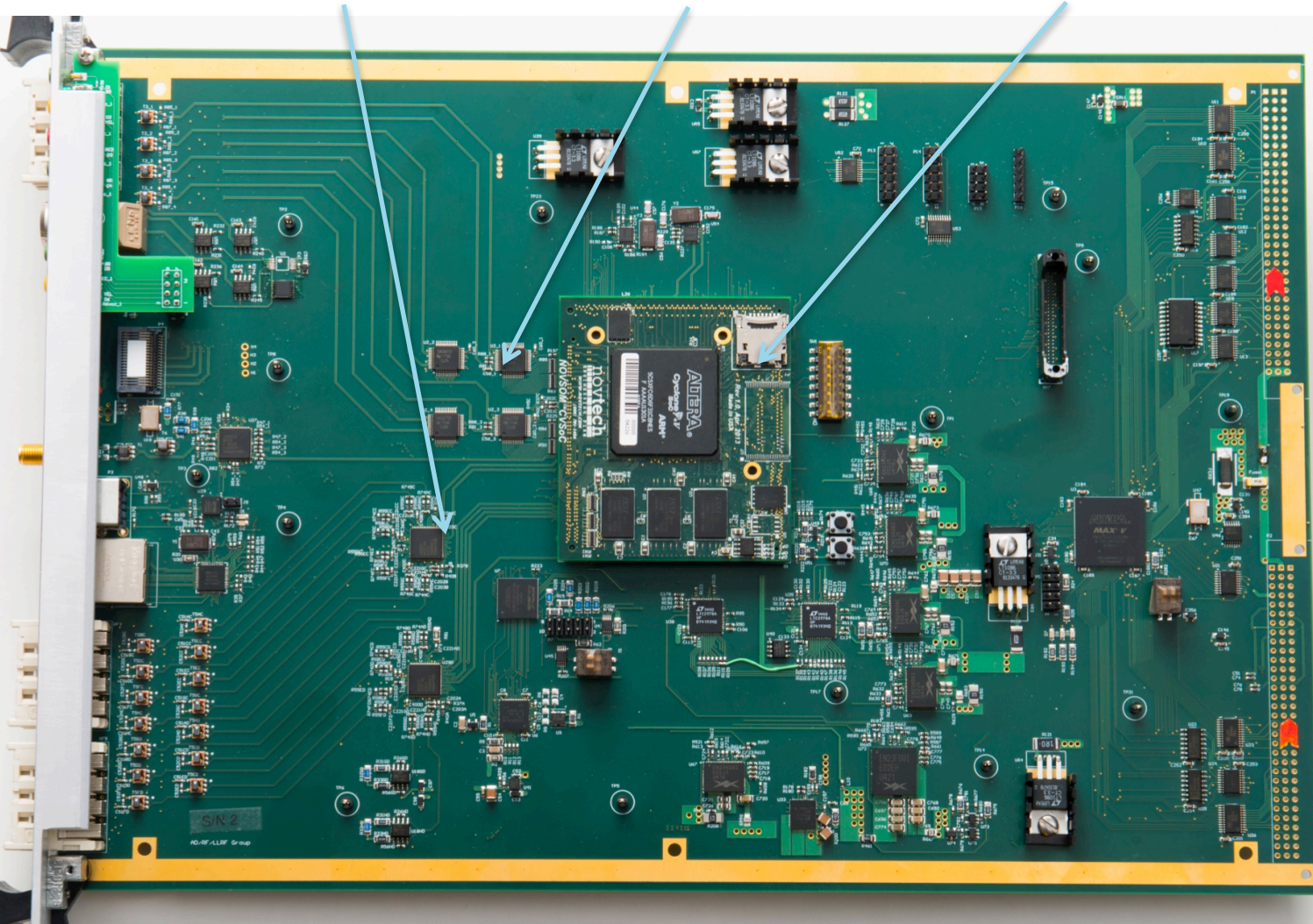
1.3 GHz 100 kW magnetron test results

- 100 kW injection locked power with 5 msec. pulses
- Good phase modulation bandwidth
- Expect no problem with 10kw average power



LLRF Digital Control Card for Phase Modulation Scheme

(16) 14 bit ADCs (8) 14 bit DACs System on Module



Dual core Arm processor with FPGA eliminates the need for a crate and external processor.

Magnetron Control R&D moving forward

- Cathode voltage and solenoid current control is a logical choice for slow amplitude control to optimize efficiency for operating conditions
 - there is potential for moderate bandwidth with switch-mode PS
 - should be a part of any scheme
- RF vector control through fast phase modulation is a potential fit for many machine designs
 - single tube design with greatest hardware simplicity
 - at the cost of control complexity
- Working towards a 650 MHz 150 kW magnetron for industrial accelerators

Summary

- The magnetron has been a remarkable RF source for 75 years that is unparalleled in cost and highly efficient. It is widely used for industrial heating and smaller electron accelerators but has had little impact in hadron accelerators
- There are now several control architectures that can take advantage of the processing capabilities of modern FPGAs
- Initial testing with a 1.3 GHz 100 kW 10% duty factor magnetron and controller using fast phase modulation is complete.
- Magnetrons may be a strong contender for high power, high efficiency accelerators

Thank you for your attention!

Backup slides

References

- B. Chase, R. Pasquinelli, E. Cullerton, and P. Varghese, “Precision Vector Control of a Superconducting RF Cavity driven by an Injection Locked Magnetron,” *Journal of Instrumentation*, no. 10 P03007, 2015.
- H. Wang *et al.*, “USE OF AN INJECTION LOCKED MAGNETRON TO DRIVE A SUPERCONDUCTING RF CAVITY,” in *Proceedings of IPAC’10*, Kyoto, Japan, THPEB067.

Efficiency Goals

ADS Accelerator Efficiency

$$P_{GRID} = P_{beam} \left[\frac{\eta_{el} G_0 k}{1-k} - \frac{1}{\eta_{acc}} \right]$$

For a typical ADS (Rubbia) the first term is of the order of 50

- ❑ The electric power to run the accelerator must be small compared to the power produced in the ADS core:

$$\frac{1}{\eta_{acc}} \ll 50 \Rightarrow \eta_{acc} \gg 0.02$$

- ❑ Minimum is $\eta_{acc} = 0.2$, but $\eta_{acc} = 0.4$ should be achievable and in that case the accelerator takes only 5% of the electric power produced by the ADS, which seems reasonable
- ❑ For very high power beams (≥ 10 MW), every MW saved matters, and it is useful to have the highest possible accelerator efficiency, if it does not compromise other properties (cost, reliability, etc.)



Revol/PSI/2016

- For high power SRF linacs the RF sources are a key component in overall wall-plug efficiency

Phase locked magnetrons

Varian Associates (MA) (1991)	Treado, Hansen, Jenkins	(Short pulse)
Univ. Michigan (-2013)	Gilgenbach et al.	(Relativistic Magnetrons)
Univ. Lancaster (2003 – 2010)	Dexter, Tahir, Carter, Burt	(CW Cooker type)
J-Lab (2006 – 2013)	Wang	(CW Cooker type)
Muon Inc. , Fermi-Lab & (2007 – 2013)	Kazakevich, Yakovlev	(Power combining)

Efficient L Band Magnetrons

SLAC, CTL, Raytheon	Tantawi et al. (2004)	(CW Coaxial? 300kW)
Diado Instit. Tech. Japan (1991)	Shibata (1991)	(CW Coaxial 600kW)

Gyro Klystrons

IAP Nizhny Novgorad	Lebedev
Univ. Maryland	Lawson
Calabazas Creek	

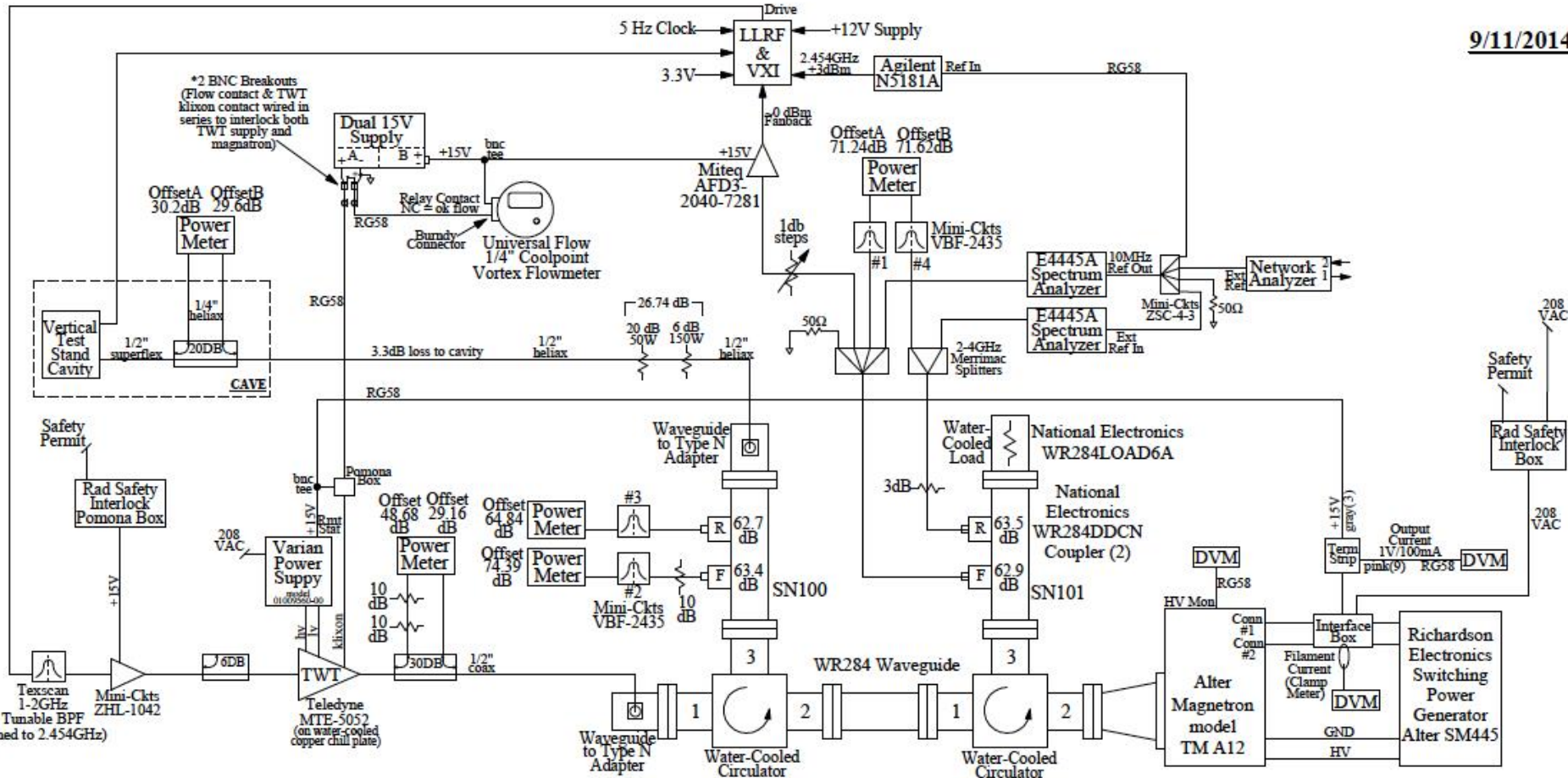
Gyro TWT

Univ. Strathclyde
MIT
IAP Nizhny Novgorad
Univ. Maryland
NRL Washington
Univ. Michigan

Amos Dexter

A0 Vertical test stand, Jlab 2.45 GHz single cell undressed cavity RF block diagram

9/11/2014



1950s transmitter using 2 magnetrons and out-phasing

Patent awarded in 1952 for a transmitter design using cathode voltage modulation and out-phasing with two magnetrons

Why was this technology discarded?
- Possibly just too many parts and expense.

Dec. 2, 1952 J. S. DONAL, JR. 2,620,467
AMPLITUDE MODULATION OF MAGNETRONS
Filed Jan. 25, 1950 5 Sheets-Sheet 3

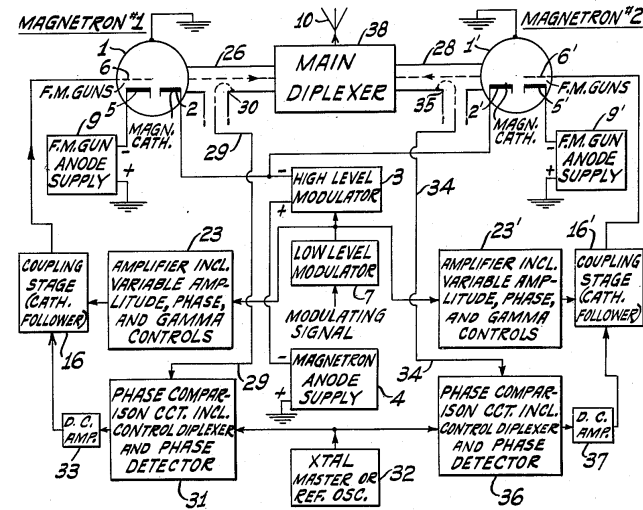


Fig-6

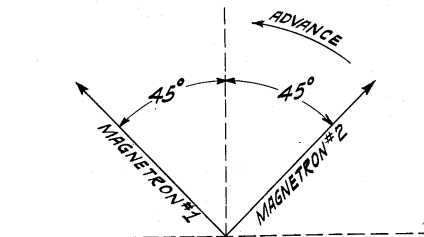


Fig-7

INVENTOR
John S. Donal, Jr.
BY *Jerry Tunkie*
ATTORNEY