

Quantum Sensors and the Fundamental
Limits of Electromagnetic Axion and Hidden-
Photon Searches

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3rd Workshop on Workshops on Microwave
Cavities and Detectors for Axion Research

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1. Fundamental limits

- What is the fundamental limit of sensitivity of a search using a single electromagnetic mode, passive impedance matching, and a phase-insensitive amplifier at the quantum limit?
- What is the optimal scan strategy, given a set of priors?
- Is a single-pole resonant circuit optimal, or can we do better?
- *The above strongly motivate quantum sensors*

2. Quantum sensors < 300 MHz:

- backaction evasion and the Zappe Photon Upconverter (ZPU)

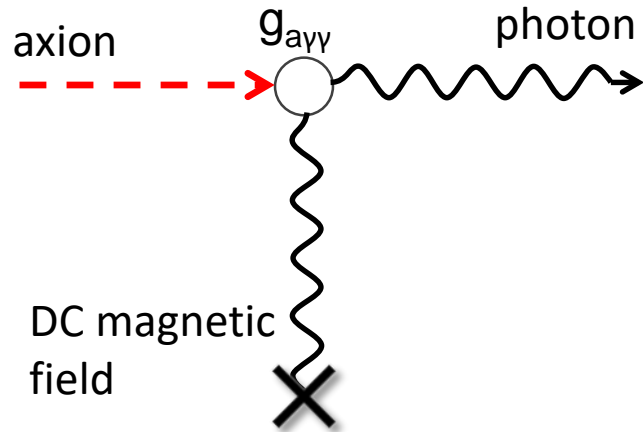
Stanford: Arran Phipps, Dale Li, Saptarshi Chaudhuri, Peter Graham, Jeremy Mardon, Hsiao-Mei Cho, Connor FitzGerald, Stephen Kuentner, Carl Dawson, Betty Young, Cyndia Yu, Kent Irwin

Arxiv:1803.01627, “Quantum Limits for Electromagnetic Axion and Hidden-Photon Dark Matter Searches”

S. Chaudhuri, K. Irwin, P. Graham, J. Mardon



Axions (spin 0)



- Solves strong CP problem
- Converts to photon via inverse Primakoff effect- requires background EM field
- Photon frequency gives mass, $h\nu=mc^2$
- $\sim 10^{-6}$ bandwidth set by DM virial velocity

Hidden Photons (spin 1)



- Appears in generic extensions of Standard Model, may be produced by cosmic inflation
- Converts via kinetic mixing
- Photon frequency gives mass, $h\nu=mc^2$
- $\sim 10^{-6}$ bandwidth set by DM virial velocity

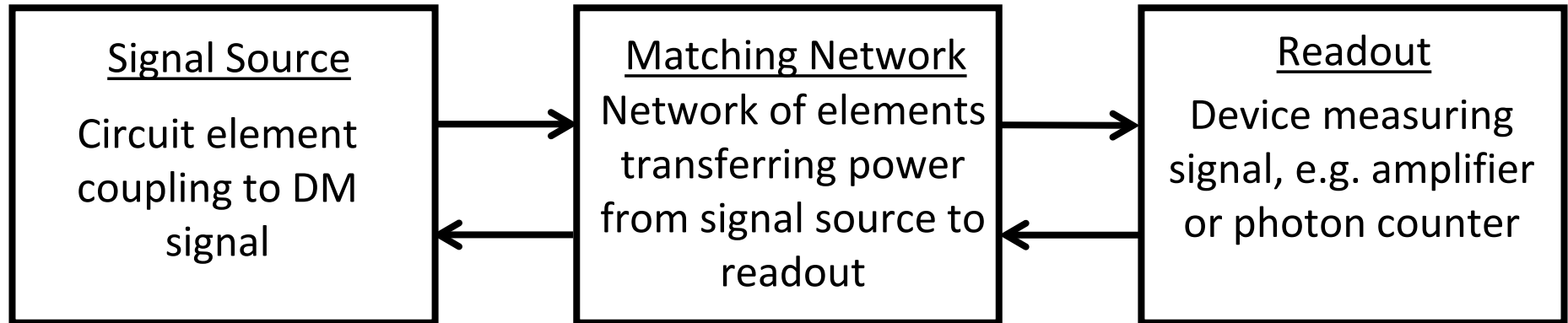
Ultralight, high number density \rightarrow Look for classical, oscillating EM field

- Receiver circuit model
- Standard quantum limit
- Optimizing the matching network
 - Integrated sensitivity
 - Bode-Fano Limit
 - Single-pole resonators are 75% of Bode-Fano Limit
- How do we improve our science limit?
 - Use multiple modes
 - Get colder
 - Use active feedback matching circuits
 - *Measure below SQL with quantum sensors*
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Receiver circuit model: schematic

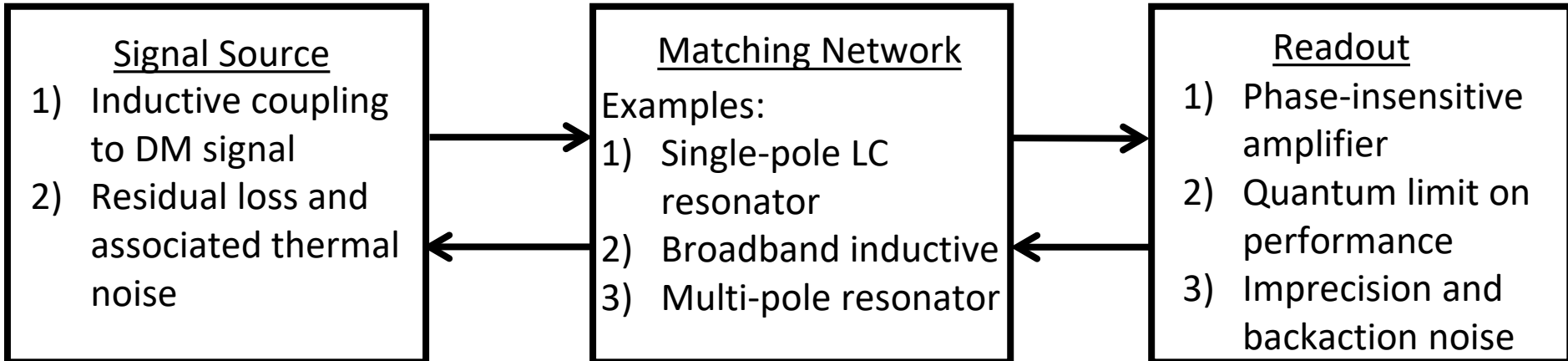
What is the fundamental limit of sensitivity of a search using

- a single electromagnetic mode
- passive impedance matching, and
- a phase-insensitive amplifier at the quantum limit?

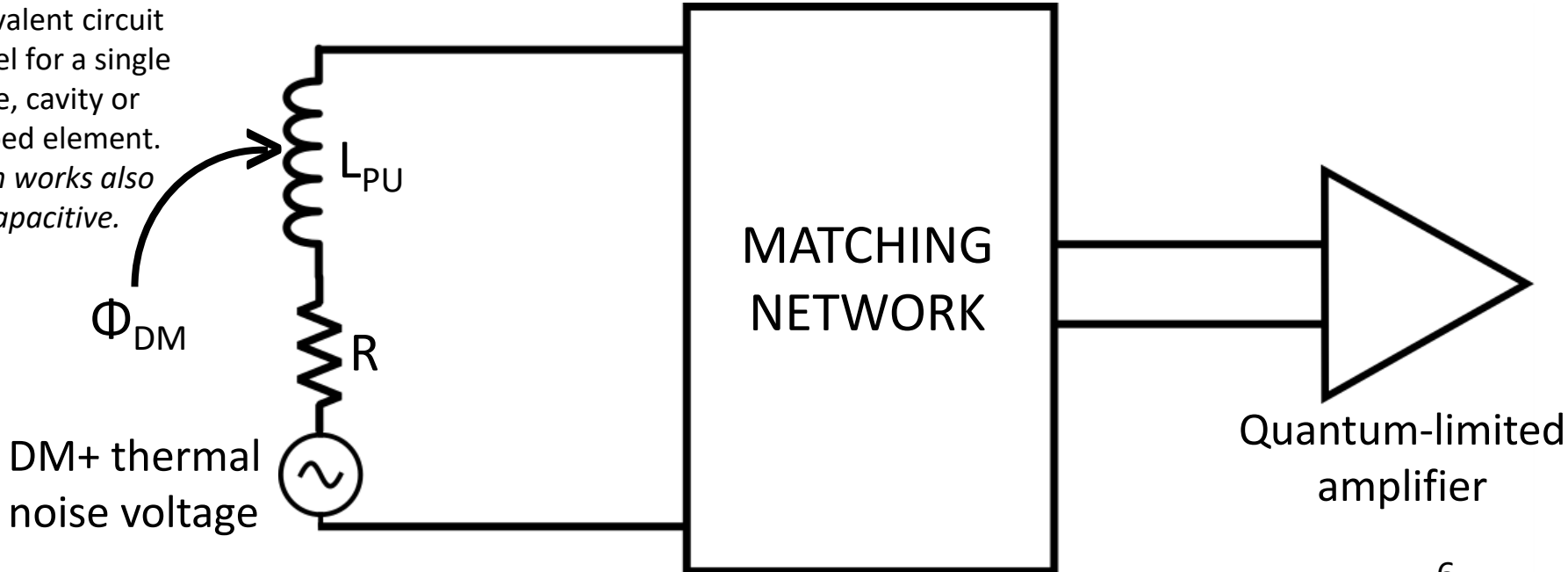


To arrive at fundamental limits, optimize each block and interactions across blocks.

Model for axion / hidden photon detection through electromagnetism



Equivalent circuit model for a single mode, cavity or lumped element. *Math works also for capacitive.*



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Standard Quantum Limit (SQL) on amplification

- Phase-insensitive amplifier: both sine and cosine components of signal (“quadratures”) are amplified equally
- Subject to Standard Quantum Limit: Heisenberg uncertainty on noise performance
 - H.A. Haus and J.A. Mullen, Phys. Rev. **128**, 407 (1962)
 - Caves, PRL **26**, 1817 (1982)
 - Modern review: Clerk et al, RMP **82**, 1155 (2010)
- SQL=1 photon of noise added by the measurement
 - 1 photon= increase required in thermal occupation number of circuit for change in thermal noise to equal amplifier noise

Standard Quantum Limit (SQL) on amplification

SQL=1 photon

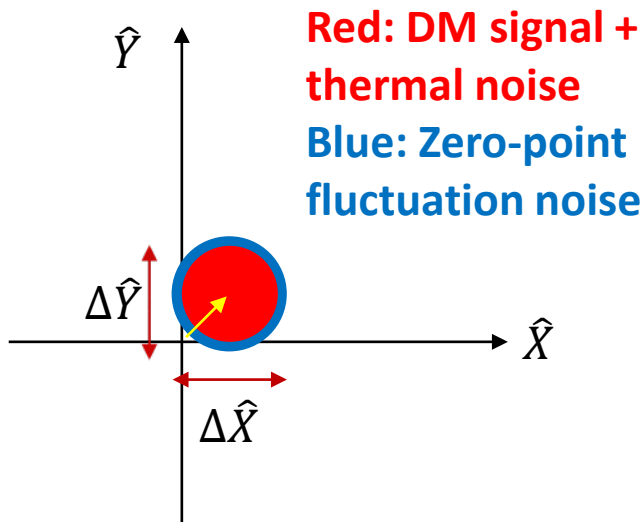
Zero-point fluctuation noise (1/2)

- Quadrature measurements \hat{X} (cosine) and \hat{Y} (sine) applied to vacuum have nonzero variance \rightarrow noise

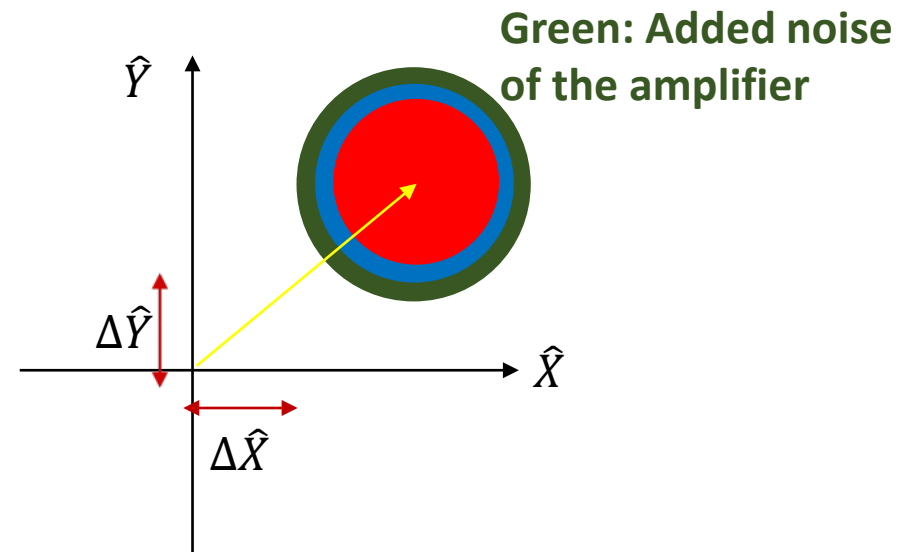
Amplifier noise (1/2)

- Noise added upon amplification from simultaneously measuring two noncommuting operators, $[\hat{X}, \hat{Y}] = i$

Amplifier Input



Amplifier Output



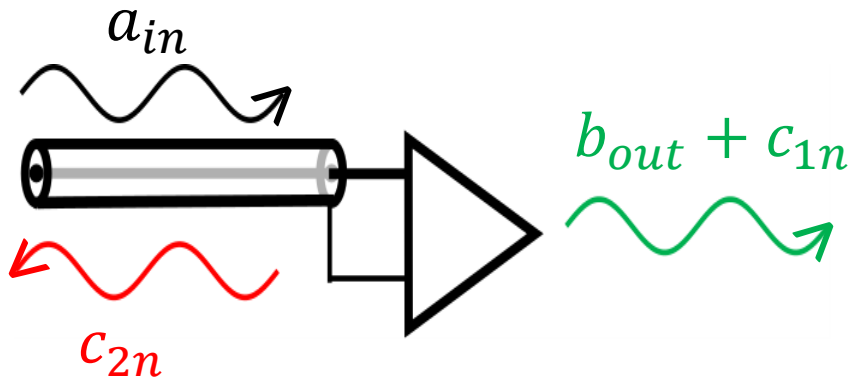
Amplifier noise = imprecision + backaction

Amplifier has two effective noise modes

- Imprecision noise: independent of input circuit
- Backaction noise: dependent on input circuit

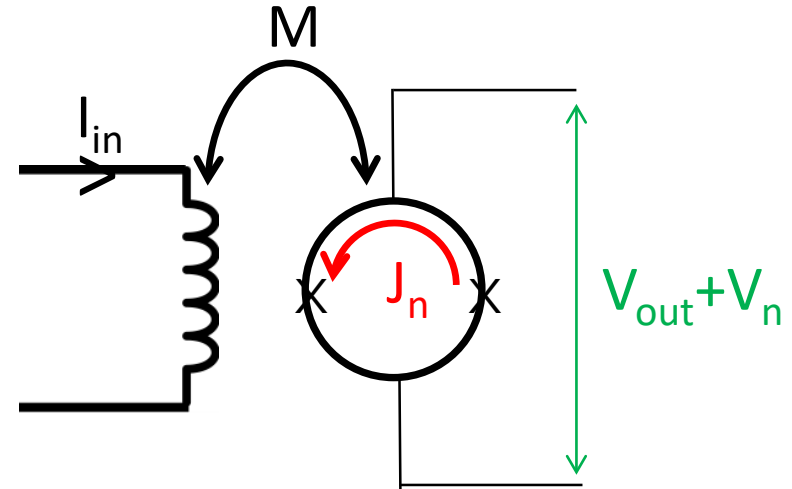
Amplifier noise = imprecision + backaction

Scattering-mode Amplifier



- E.g. JPAs, used in ADMX, HAYSTAC
- Incoming wave a_{in} amplified, giving output wave b_{out}
- Imprecision noise: intrinsic noise wave c_{1n} at output
- Backaction noise: noise wave c_{2n} injected into input circuit
- Reflects off input circuit, appears as more noise at output

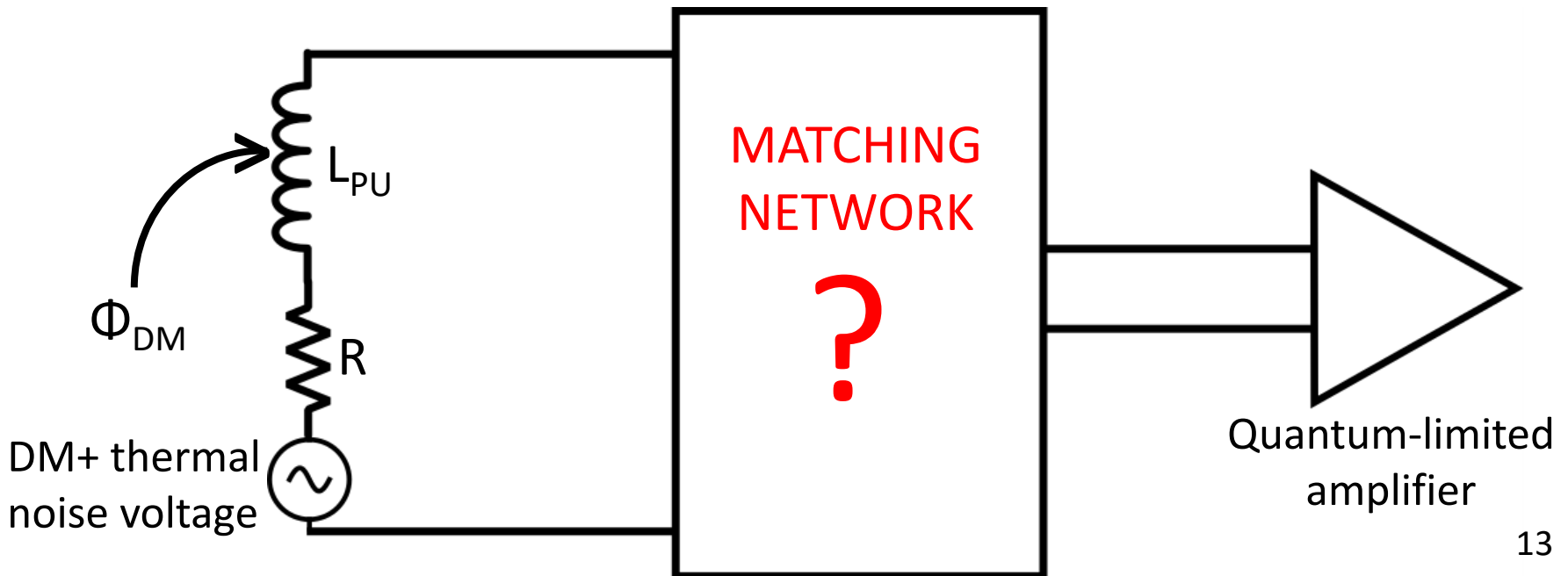
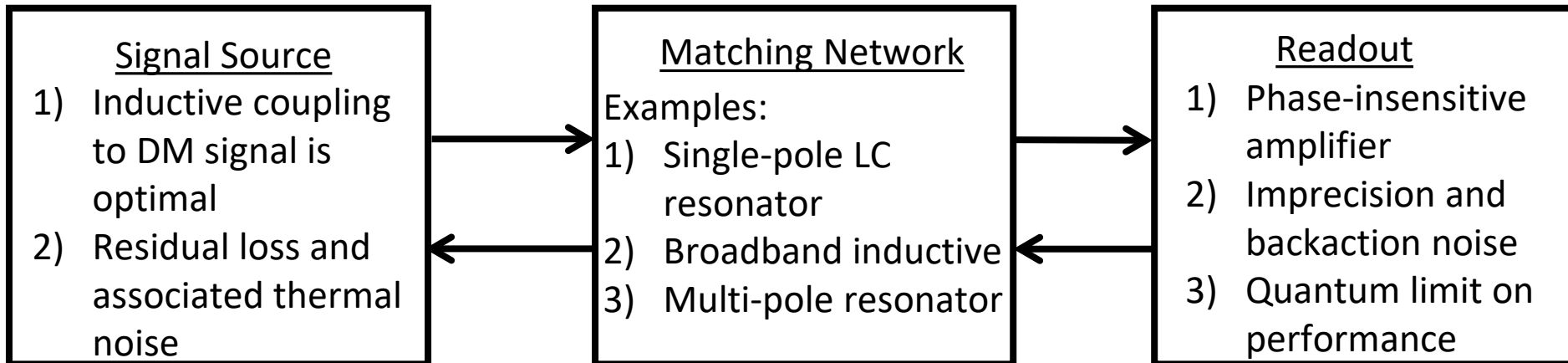
Flux-to-Voltage Amplifier



- E.g. SQUIDs, used in DM Radio, ABRACADABRA
- Input current I_{in} feeds flux into loop, giving output voltage V_{out}
- Imprecision noise: intrinsic voltage fluctuations V_n at output
- Backaction noise: circulating noise currents J_n couple voltage to input
- Creates noise currents in input, appears as more noise at output

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How do we optimize matching network?



Value function for matching optimization

- Value function needs to reflect:
 - Signal-to-noise ratio (SNR)
 - Priors- Favored mass or coupling range? Candidate signal to validate?
- Value function is expectation value of SNR squared:
$$U[S(\nu)] = E[SNR^2 [S(\nu)]]$$
- $S(\nu)$ =scattering matrix for the network
- Expectation is evaluated with user-defined preference functions for DM properties, e.g. mass
- *Log-uniform search*
 - Uninformative priors on DM
 - DM mass uniformly likely in log space
 - Want sensitivity as large as possible over as wide a bandwidth as possible

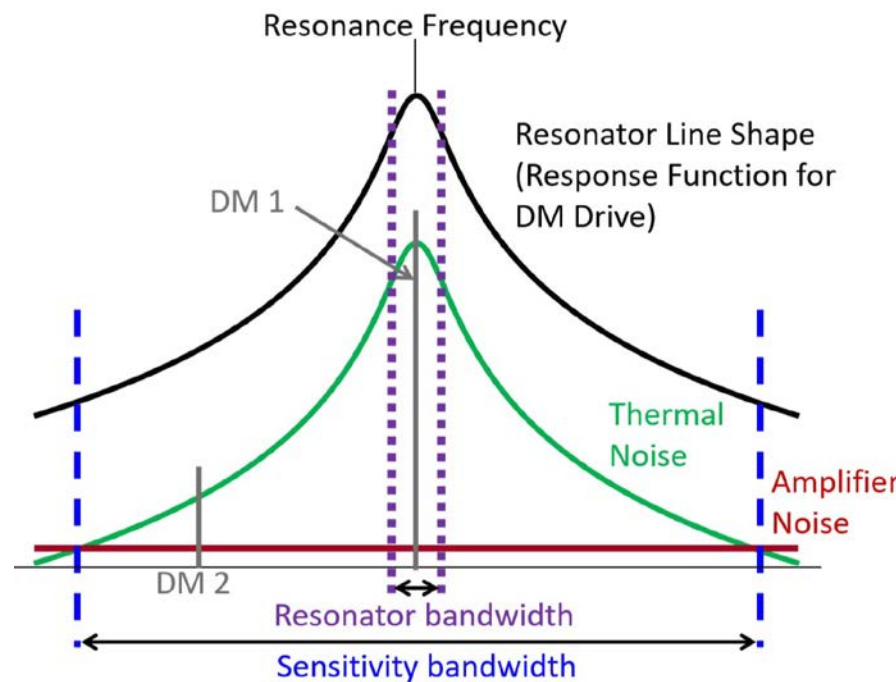
Log-uniform search: optimize integrated sensitivity

Example: single-pole resonator

- Maximize integrated sensitivity across search band, between ν_l and ν_h
- Figure of merit with quantum-limited amplifier:

$$U[S(\nu)] = \int_{\nu_l}^{\nu_h} d\nu \left(\frac{|S_{21}(\nu)|^2}{|S_{21}(\nu)|^2 n(\nu) + 1} \right)^2$$

- $n(\nu)$ = signal source thermal occupation number
- “+1” is standard quantum limit



Substantial sensitivity available outside of resonator bandwidth for thermal resonator states. Substantial scan rate enhancement.

Quantum-limited amplifiers highly desirable even for thermal states $hf < kT$. (Measuring below SQL even better)

How large can sensitivity U be? Bode-Fano limit

- Constraint provided by Bode-Fano criterion for matching LR to a quantum-limited amplifier with a real noise impedance:
 - H.W. Bode, "Network Analysis and Feedback Amplifier Design" (1946)
 - R.M. Fano, *Journal of the Franklin Institute* (1950)
- *Assume matching network is linear, passive, and reciprocal.*

Bode-Fano
$$\int_{\nu_l}^{\nu_h} d\nu \ln \left(\frac{1}{|S_{22}(\nu)|} \right) \leq \frac{R}{2L_{PU}} \Rightarrow$$

Bode-Fano-limited U
$$U[S(\nu)] \leq \begin{cases} \frac{1}{4n(\nu_h)} \frac{R}{L_{PU}}, & n(\nu_h) \gg 1 \\ 0.41 \frac{R}{L_{PU}}, & n(\nu_h) \ll 1 \end{cases}$$

- Analogous constraint for RC signal source

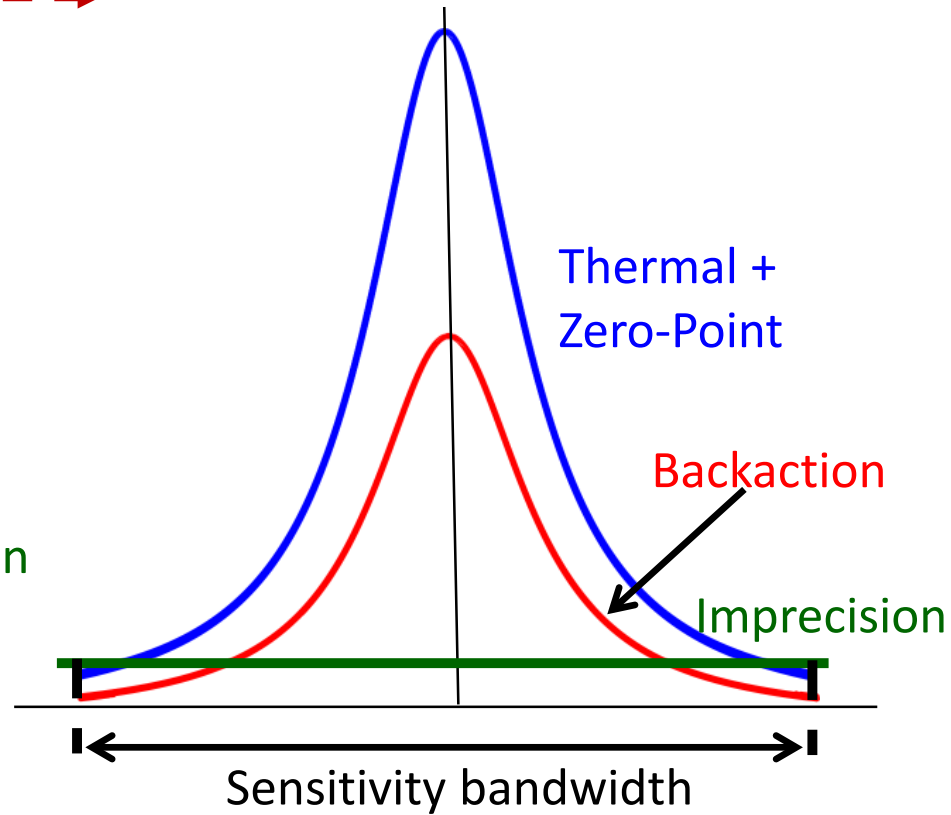
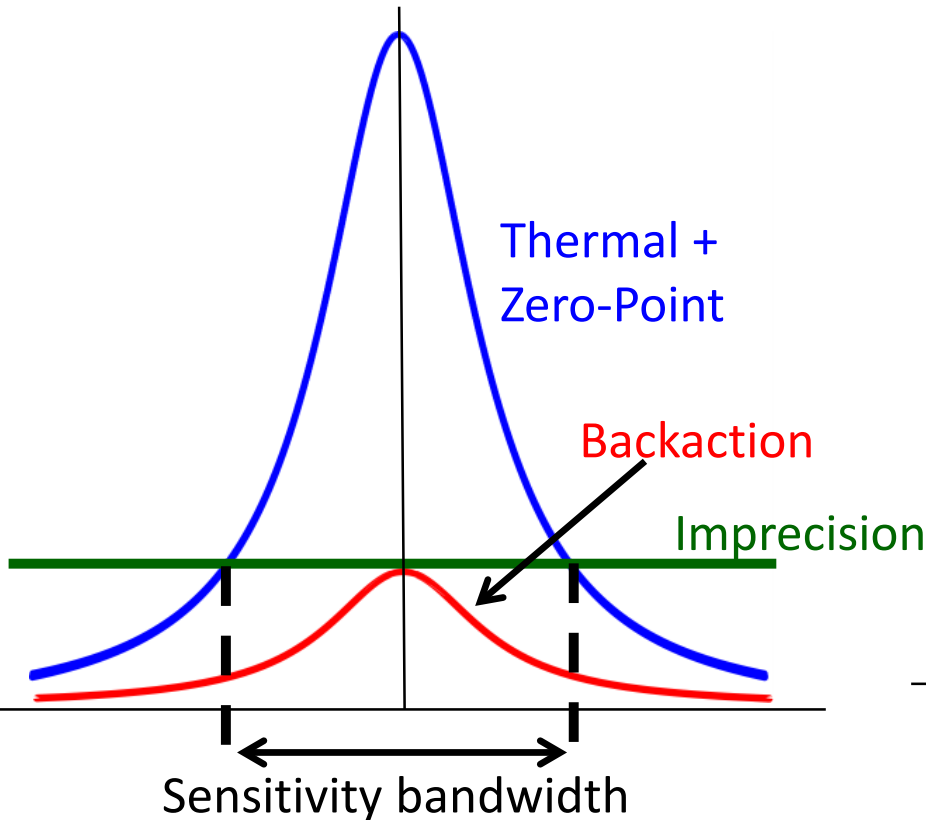
An **optimal** single-pole resonator can have a figure of merit U that is $\sim 75\%$ of the fundamental limit (pretty good!)

Optimize coupling strength with respect to integrated sensitivity

Noise-matched
on resonance

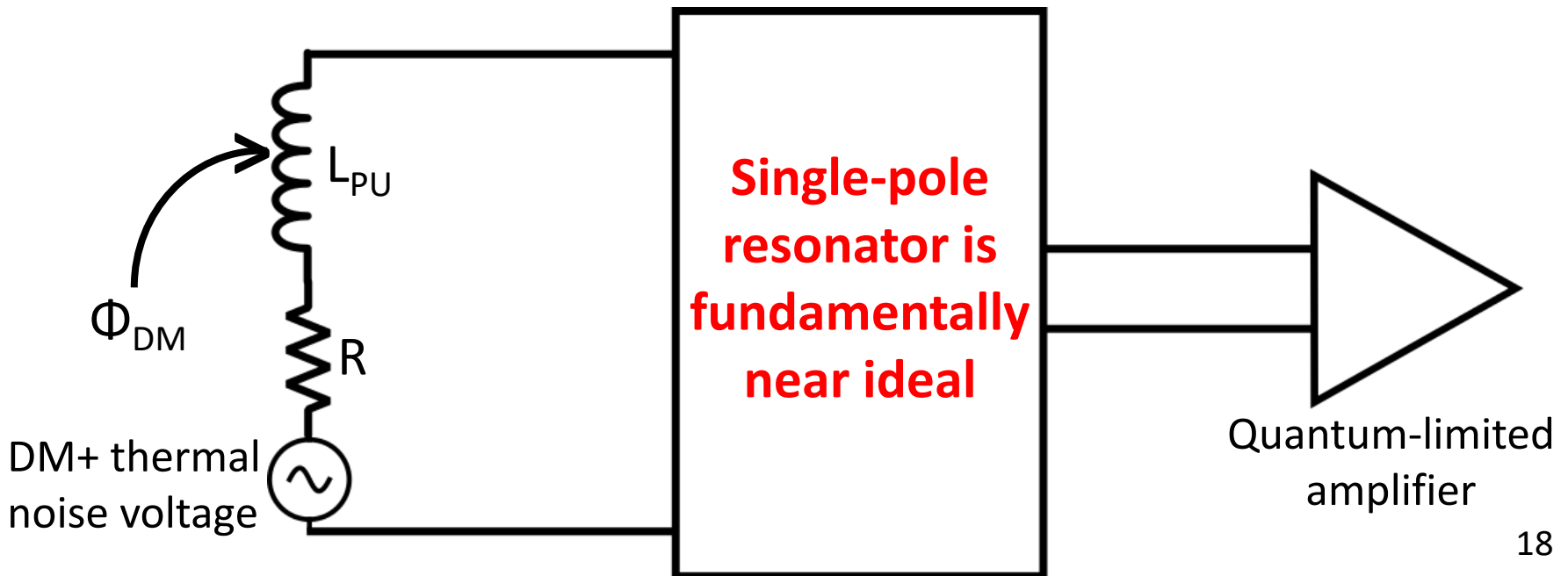
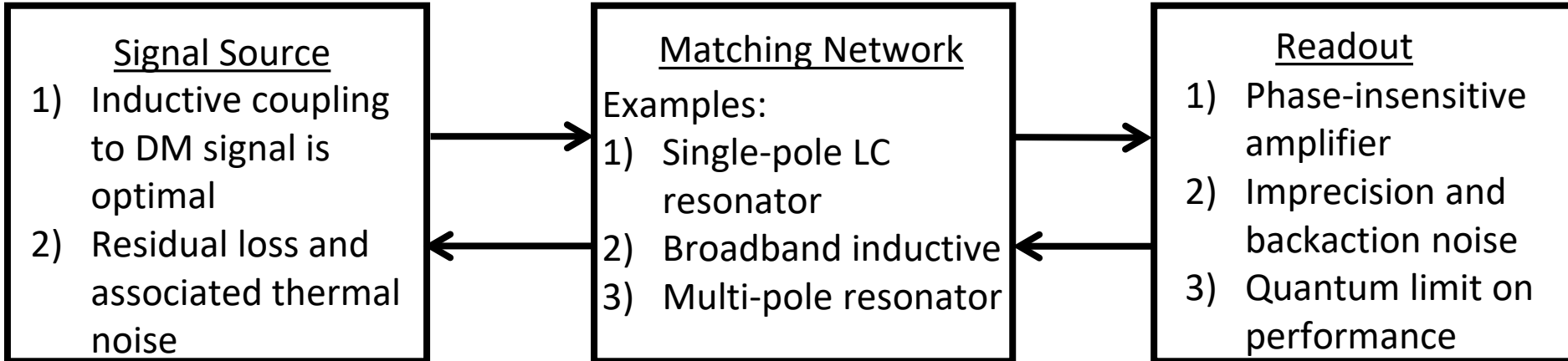
Increase coupling
to QL amplifier
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Noise-mismatched on
resonance



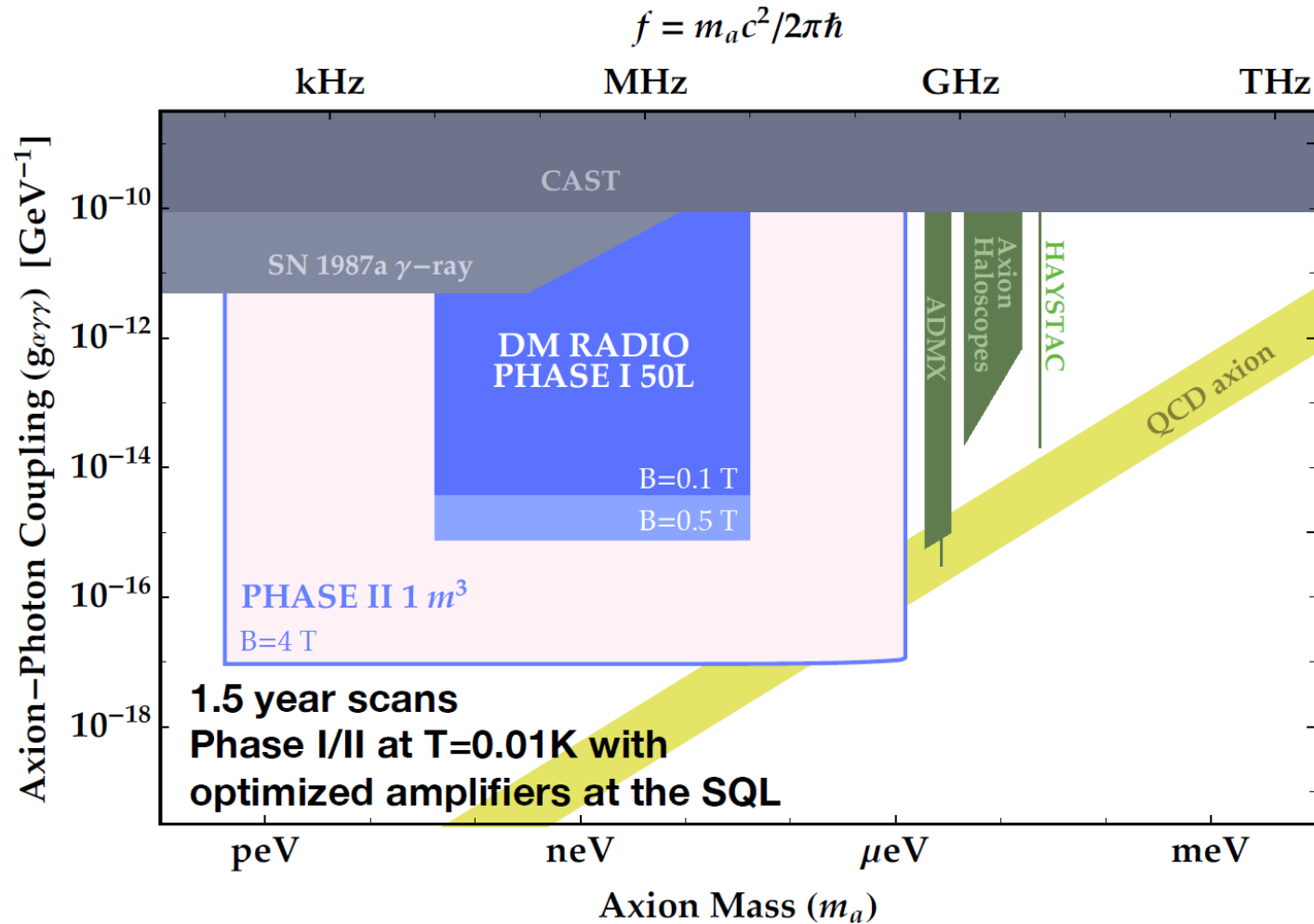
- Increased coupling: reduced imprecision, increased backaction
- 50% on-resonance noise penalty. Much larger sensitivity bandwidth

Completing our optimal detector!



SQL for DM Radio from Arran's Talk

Axion Sensitivity



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Quantum noise in a harmonic oscillator

The Hamiltonian of a harmonic oscillator is

$$\hat{H} = \hbar\omega(a^\dagger a + 1/2)$$

The Hamiltonian can be written in the cosine component (\hat{X}) and the sine component (\hat{Y})

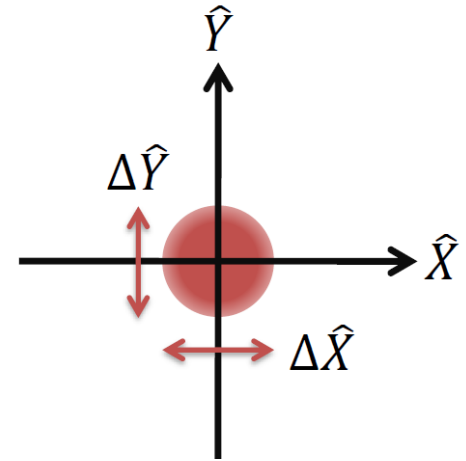
$$\hat{H} = \frac{\hbar\omega}{2}(\hat{X}^2 + \hat{Y}^2)$$

$$[\hat{X}, \hat{Y}] = i$$

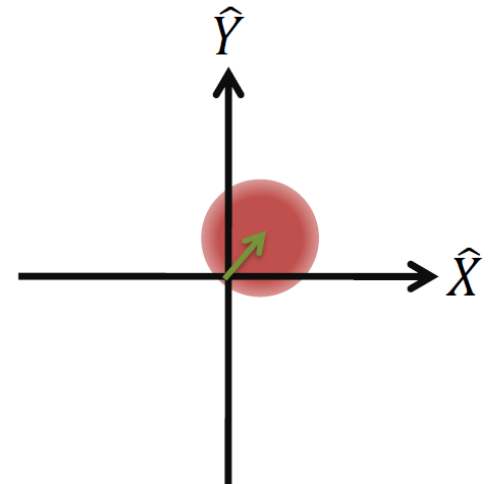
$$\Delta\hat{X}\Delta\hat{Y} \geq \frac{1}{2} \quad \text{vacuum noise}$$

When amplified, add one more $\frac{1}{2}$ quantum

$$N_{add} \geq \frac{1}{2}$$



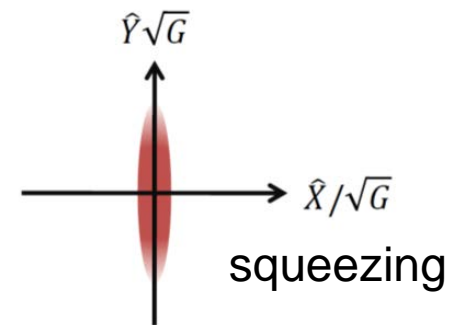
With nonzero expectation value



Quantum sensing

- If we don't need to measure both quadratures of a field, we don't have to be limited by the standard quantum limit.
- The standard quantum limit can be evaded using quantum correlations. These techniques are deeply related:
 - Photon counting
/ quantum nondemolition
 - Squeezing
 - *Backaction evasion*
 - Entanglement
 - Cooling
 - Quantum nondemolition

$$\hat{H} = \hbar\omega(a^\dagger a + 1/2)$$



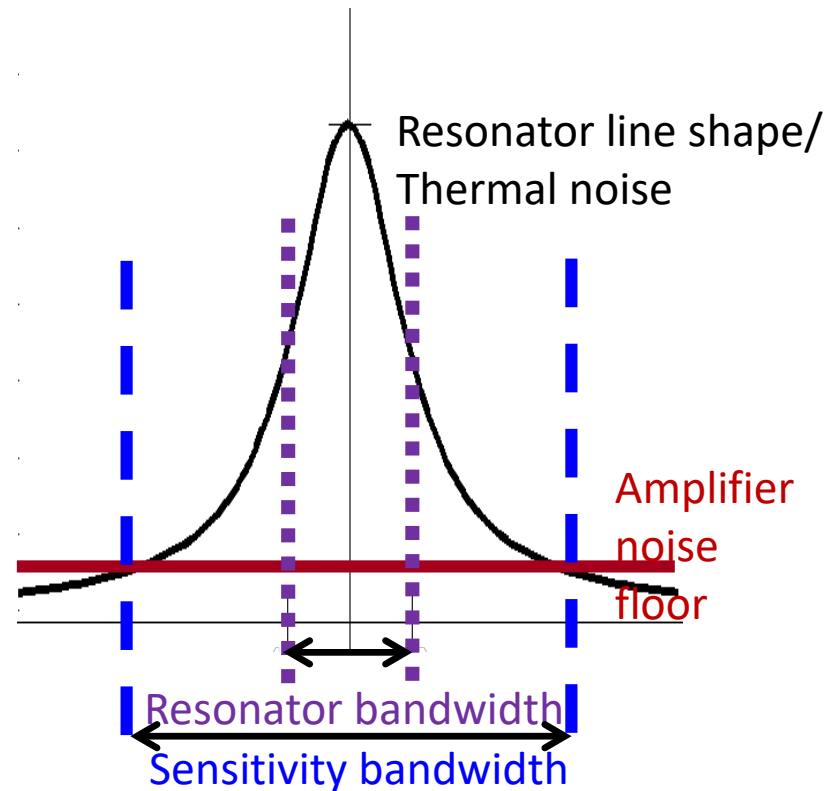
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Quantum sensing of thermal states

$$\hbar\omega < k_B T \quad \text{Thermal state}$$

Why would we use a quantum sensor for a thermal state?

- The signal to noise within the resonator bandwidth is not helped by a better amplifier.
- The sensitivity of the amplifier determines the *sensitivity bandwidth*, and thus the sensitivity of a search for an unknown signal frequency.
- Very large speedup possible for a sensor operating below the standard limit even if $\hbar\omega < k_B T$

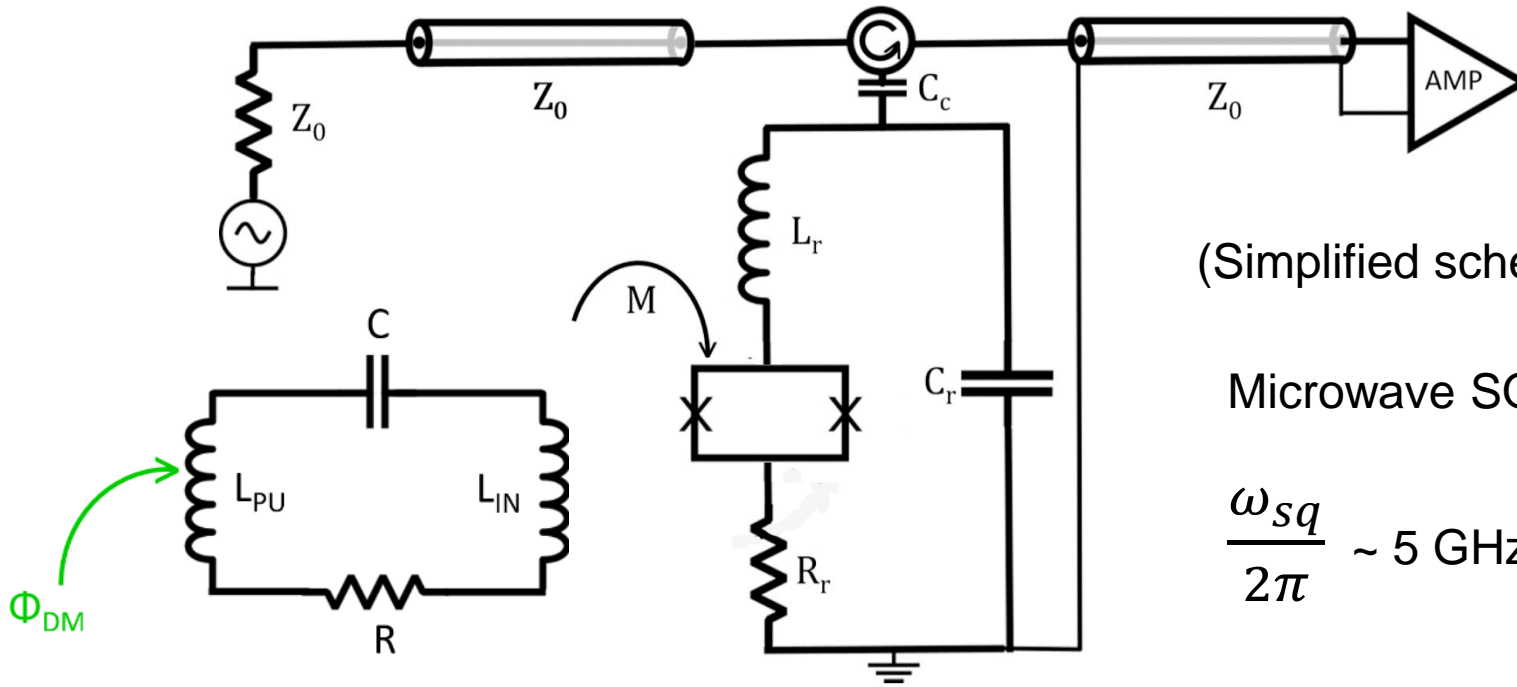


Quantum sensors are needed for low-frequency thermal states too

Measuring a resonator with a dissipationless microwave SQUID frequency upconverter



Dissipationless microwave SQUID flux amplifier



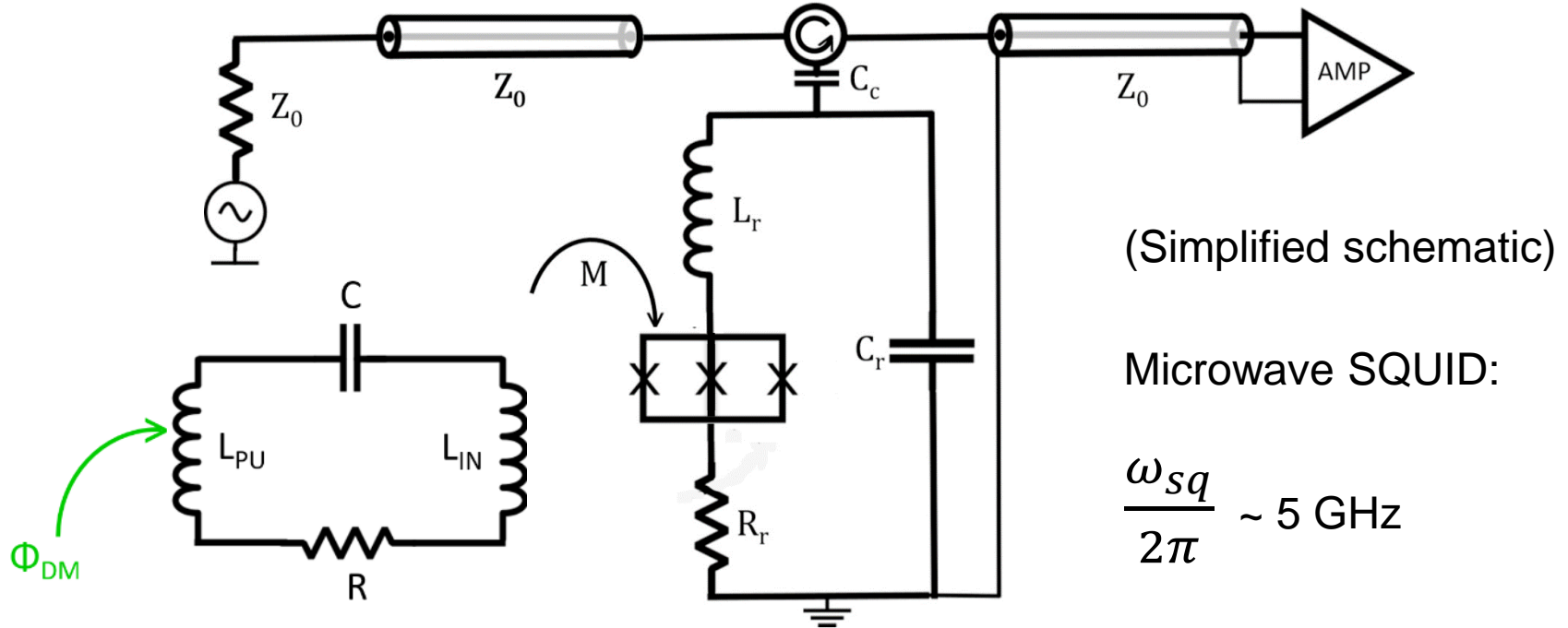
(Simplified schematic)

Microwave SQUID:

$$\frac{\omega_{sq}}{2\pi} \sim 5 \text{ GHz}$$

DM Radio: $\frac{\omega_r}{2\pi} = 1 \text{ kHz} - 100 \text{ MHz}$

Measuring a resonator with a dissipationless Zappe Photon Upconverter (ZPU)



DM Ratio: $\frac{\omega_r}{2\pi} = \sim 300 \text{ Hz} - \sim 300 \text{ MHz}$

Uncoupled Hamiltonian: $\hat{H}_0 = \hbar\omega_{sq}\hat{a}^\dagger\hat{a} + \hbar\omega_r\hat{b}^\dagger\hat{b}$

Interaction Hamiltonian: $\hat{H}_{int} = -\hbar G\hat{\Phi}_{in}\hat{a}^\dagger\hat{a} = -\hbar g_0\hat{a}^\dagger\hat{a}(\hat{b} + \hat{b}^\dagger)$

Hamiltonian maps onto optomechanical system

DM Radio: $\frac{\omega_r}{2\pi} = \sim 300 \text{ Hz} - \sim 300 \text{ MHz}$ Microwave resonator: $\frac{\omega_{sq}}{2\pi} \sim 5 \text{ GHz}$

Uncoupled Hamiltonian: $\hat{H}_0 = \hbar\omega_{sq}\hat{a}^\dagger\hat{a} + \hbar\omega_r\hat{b}^\dagger\hat{b}$

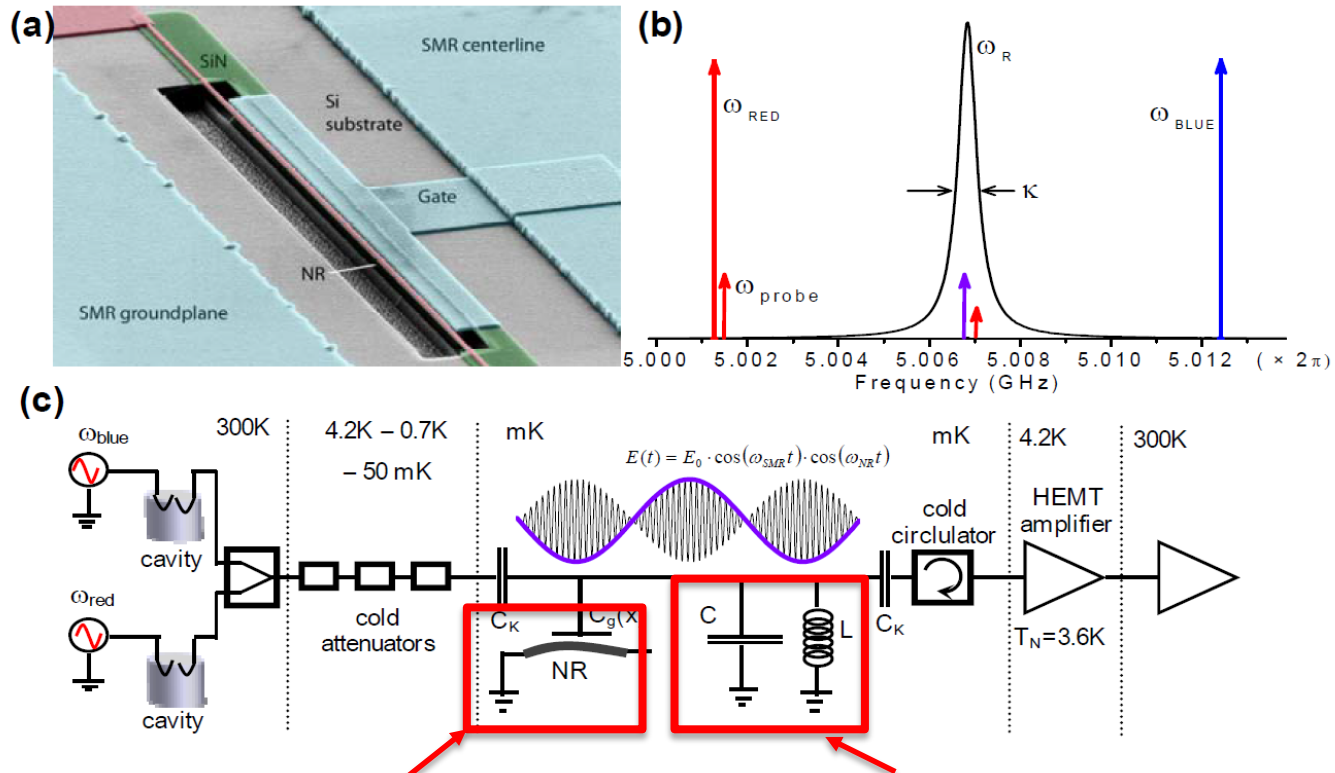
Interaction Hamiltonian: $\hat{H}_{int} = -\hbar G\hat{\Phi}_{in}\hat{a}^\dagger\hat{a} = -\hbar g_0\hat{a}^\dagger\hat{a}(\hat{b} + \hat{b}^\dagger)$

This maps onto the Hamiltonian of an optomechanical resonator with:

Displacement r	\longleftrightarrow	Flux Φ
Momentum p	\longleftrightarrow	Charge Q
Inverse spring constant $1/k$	\longleftrightarrow	Inductance L
Mass m	\longleftrightarrow	Capacitance C

Nonlinear interaction upconverts photons from the DM Radio resonator to the microwave SQUID, downconverts microwave SQUID photons to the DM Radio, leading to backaction

Hamiltonian maps onto optomechanical system



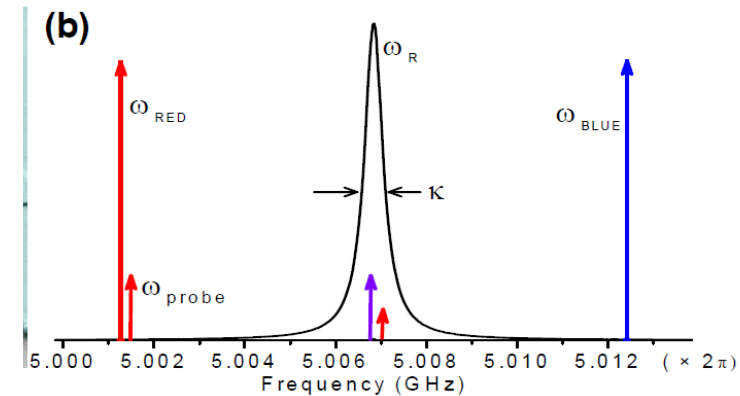
Low-frequency mechanical resonance
(Maps onto DM radio Hamiltonian)

High-frequency LC resonance
(Maps onto uwave SQUID Hamiltonian)

Hertzberg, J. B., Rocheleau, T., Ndukum, T., Savva, M., Clerk, A. A., & Schwab, K. C. (2010). Back-action-evading measurements of nanomechanical motion. *Nature Physics*, 6(3), 213-217.

Back-action Evasion

- Originally proposed by Braginsky (1980) for gravitational wave detectors.
- With proper device symmetry, when both sidebands are pumped, the back-action is applied only to the unmeasured quadrature. Allows much stronger coupling, and reduction of both imprecision and back-action noise.
- Squeezing, cooling, other quantum protocols possible



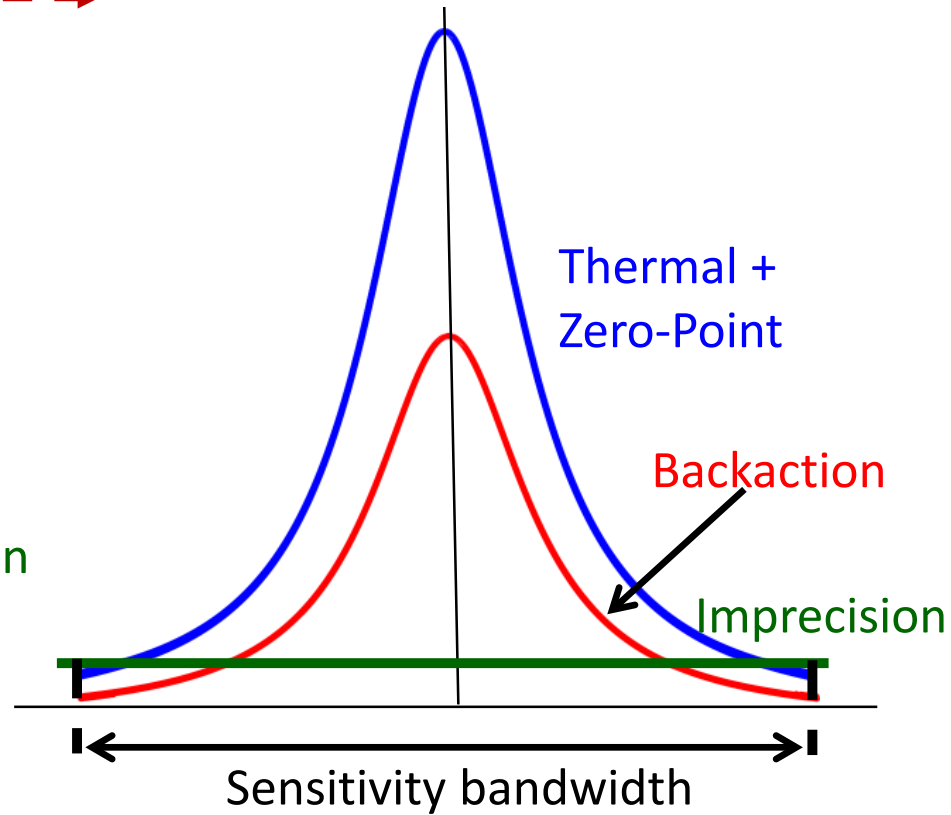
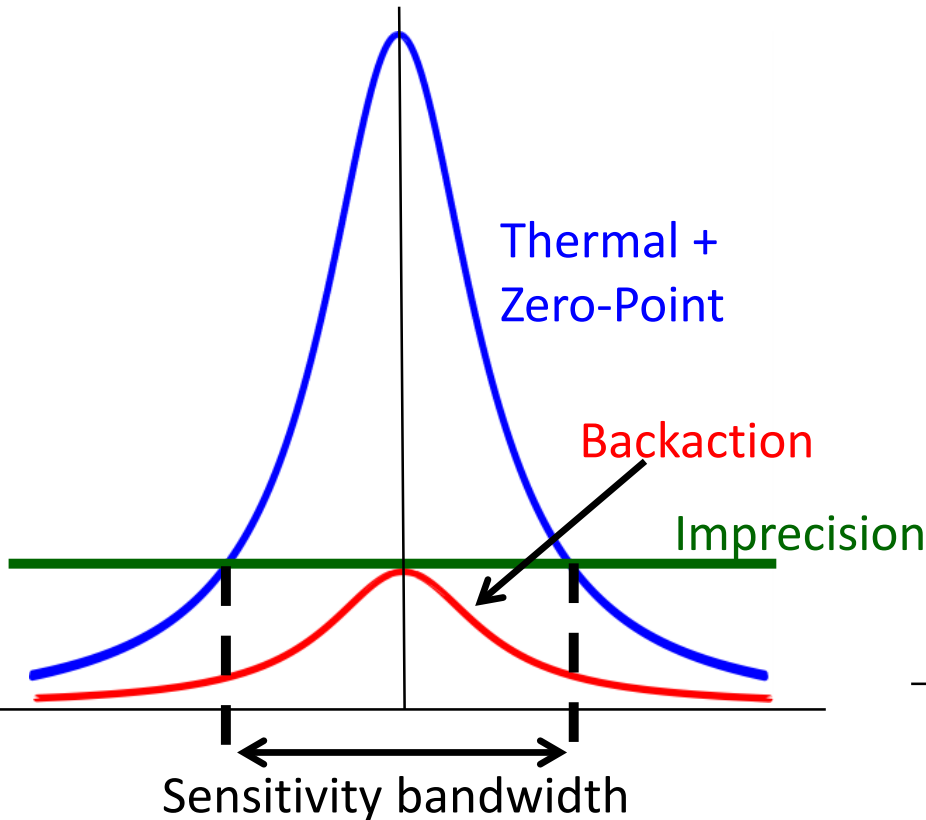
Back-action Evasion with microwave SQUID
frequency upconverters is a promising quantum
protocol for DM Radio

Optimize coupling strength with respect to integrated sensitivity

Noise-matched on resonance

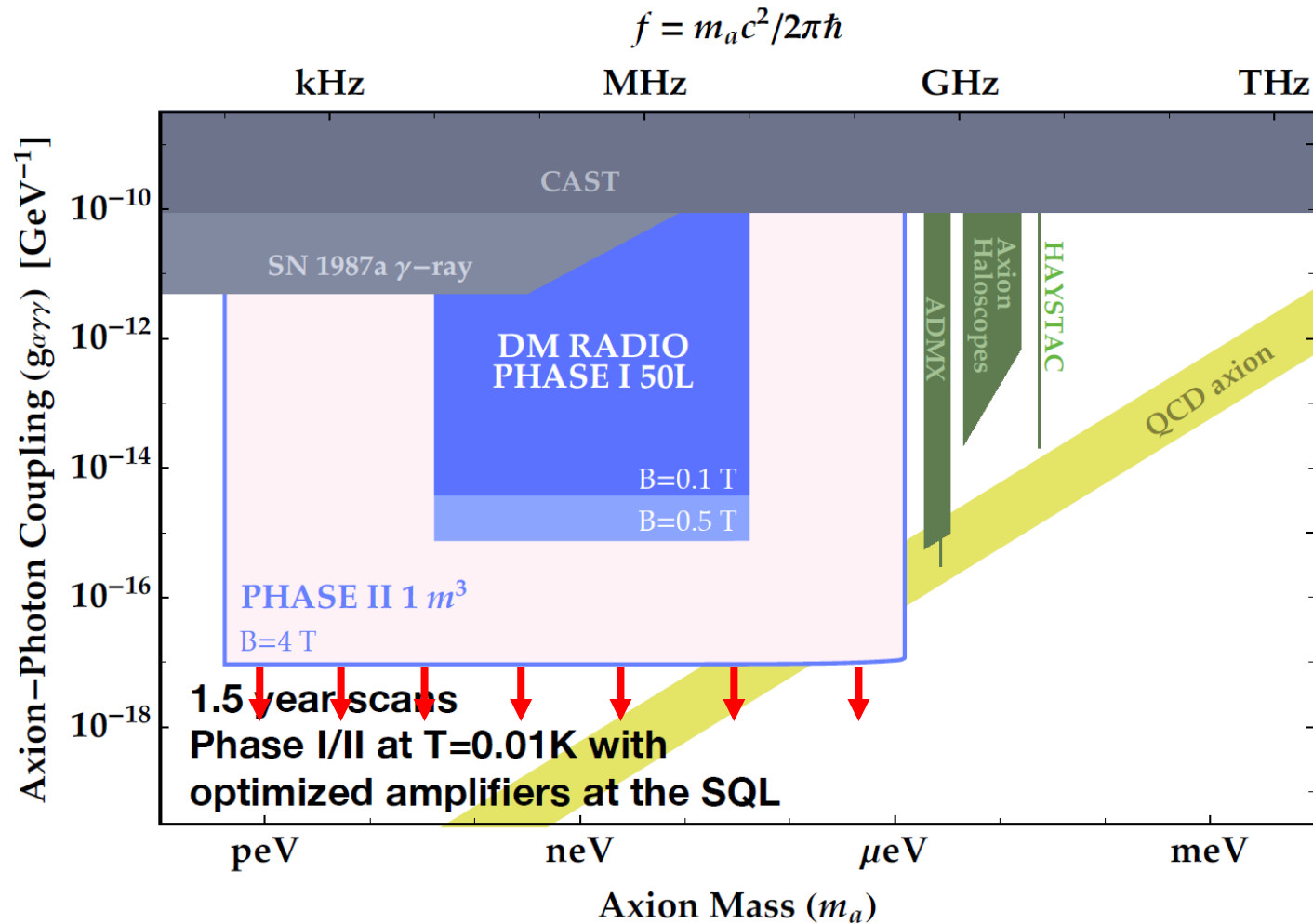
Increase coupling to QL amplifier
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Noise-mismatched on resonance



- Increased coupling: reduced imprecision, increased backaction
- 50% on-resonance noise penalty. Much larger sensitivity bandwidth

Axion Sensitivity



Conclusions

- One-pole resonators are nearly optimal for single-mode dark-matter searches (75% saturation of Bode-Fano Limit)
- Significant sensitivity outside of the resonator bandwidth
 - Larger scan steps possible: with $Q \sim 10^6$, at 1 MHz SQL, we would likely have 40 Hz scan steps, rather than 1 Hz.
- Strong encouragement to improve limits with quantum sensors, even for resonators in a thermal state (< 300 MHz)
- Zappe Photon Upconverters promising for backaction-evasion to measure below the SQL in experiments < 300 MHz, including DM Radio (and others).



STOP

MANUFACTURED BY THE CITY OF LOS ANGELES