

# Recent Progress on MARS15 Studies for Mu2e-II. HRS optimization

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# Outline

- DPA in PS coils as a critical parameter for Mu2e magnet design
- DPA and power density values and limits for baseline Mu2e
- HRS material and inner bore optimization @ 100 kW
  - Single event sensitivity vs inner bore radius
  - DPA/power density vs inner bore radius
- Feasibility of tungsten/bronze HRS @ 100 kW
- Conclusions

# Radiation studies for Mu2e: aims and issues

## Main optimization goal:

- Maximize useful particle production, maximize lifetime of the apparatus

## Issues:

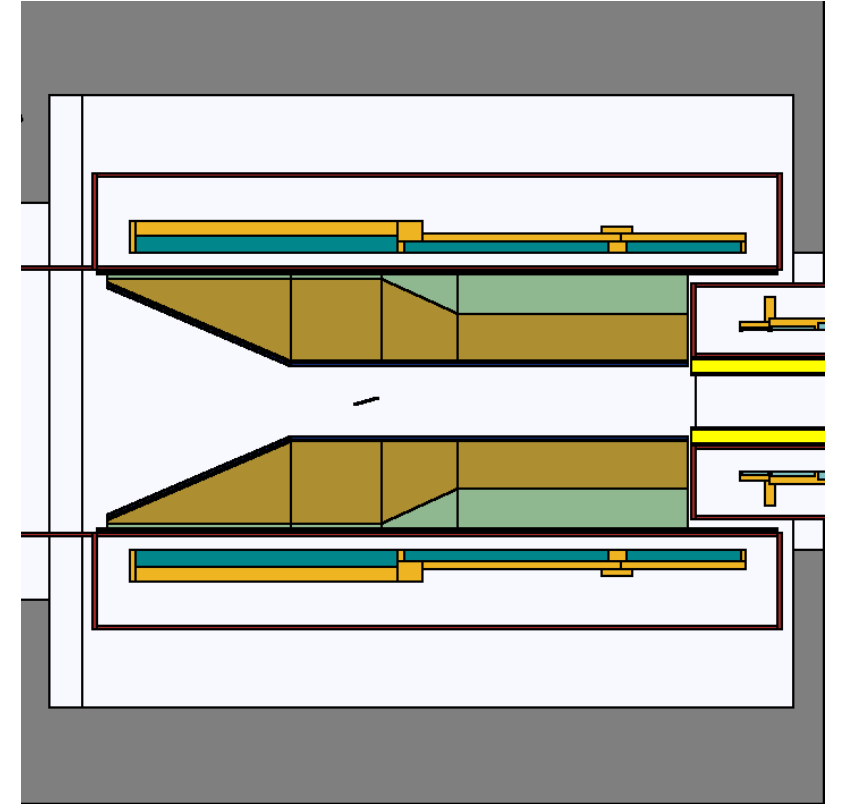
- Quench: power density and dynamic heat load of superconducting (SC) coils.
- Integrity and lifetime of critical components: integrated dose in organic materials, i.e. epoxy, insulator.
- Radiation damage to superconducting and stabilizing materials: atomic displacements (DPA), integrated particle flux
- Safety aspects: shielding, nuclide production, residual dose.

# Heat and Radiation Shield

- **Absorber** (Heat and Radiation Shield) is intended to prevent radiation damage to the magnet coil material and ensure quench protection and acceptable heat loads for the lifetime of the experiment

## Quantities simulated:

- Total dynamic heat load on the coils
- Peak power density in the coils
- Peak radiation dose to the insulation and epoxy
- Displacements Per Atom (DPA) to describe how radiation affects the electrical conductivity of metals in the superconducting cable (RRR degradation)

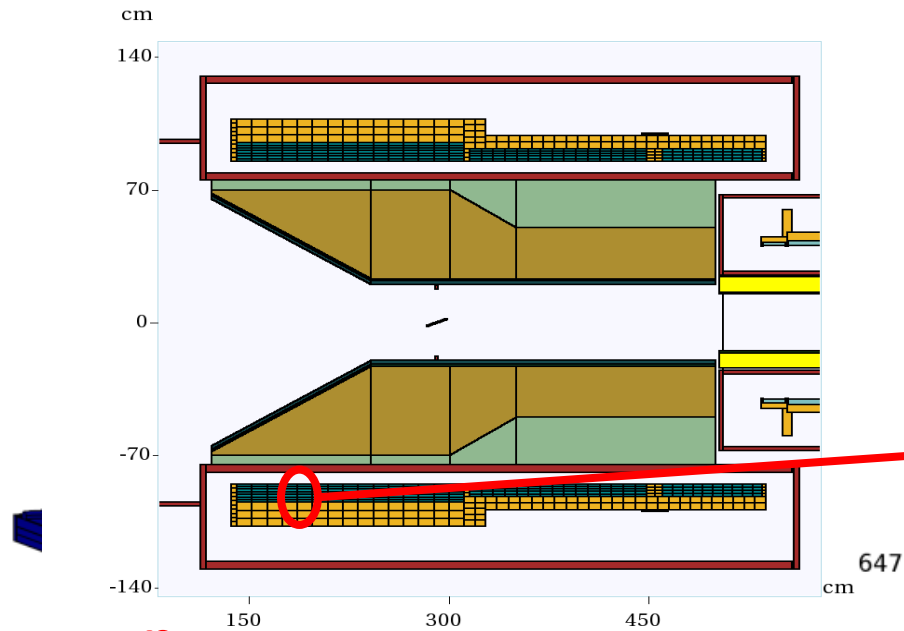


# Mu2e radiation quantity dose limits

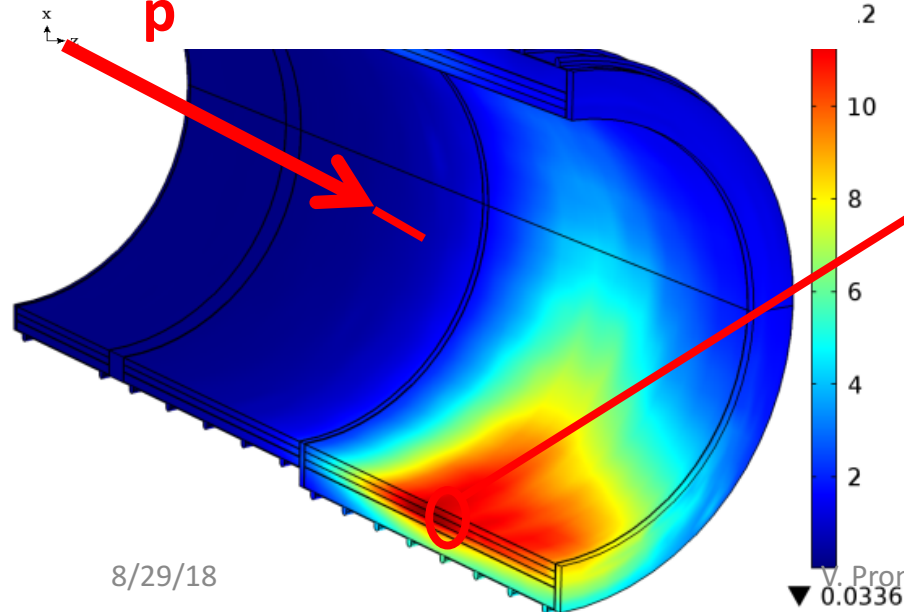
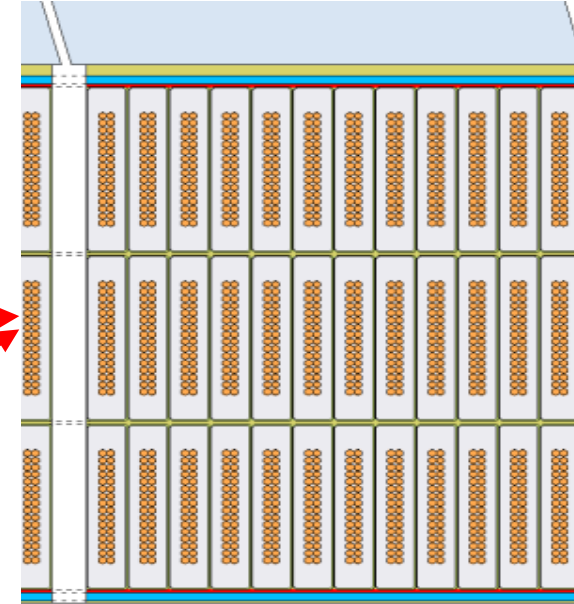
Quantity	DPA, $10^{-5}$	Power density, $\mu\text{W/g}$	Absorbed dose, MGy/yr	Dynamic heat load, W
Specs	4-6	30	0.35	100

- DPA damage we can get so that RRR degrades from  $\sim 600$  to 100. After this RRR reduction we must warm-up and anneal Al (once a year).
- The cooling requirements lead to limits on peak power density calculated based on the heat map
- Dynamic heat load limit depends on cooling system

# HRS and solenoid MARS15 baseline Mu2e model



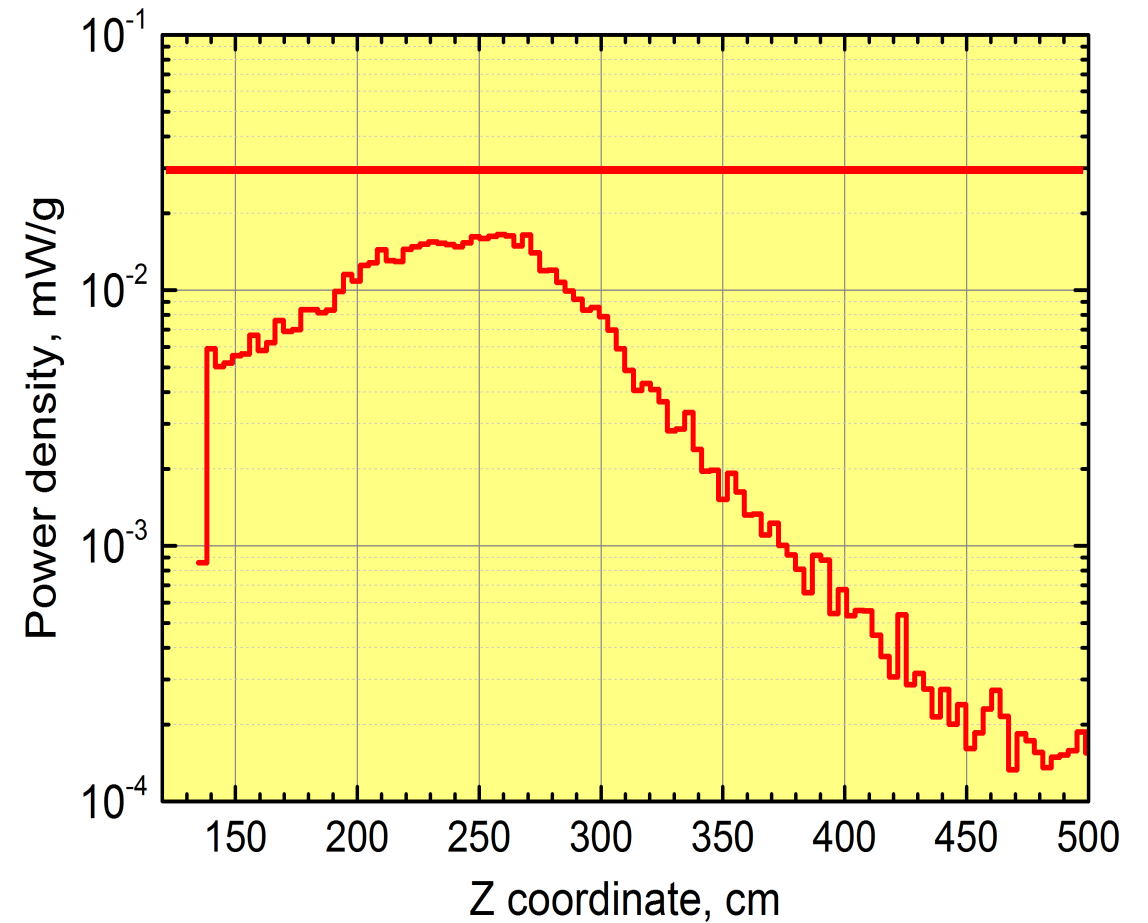
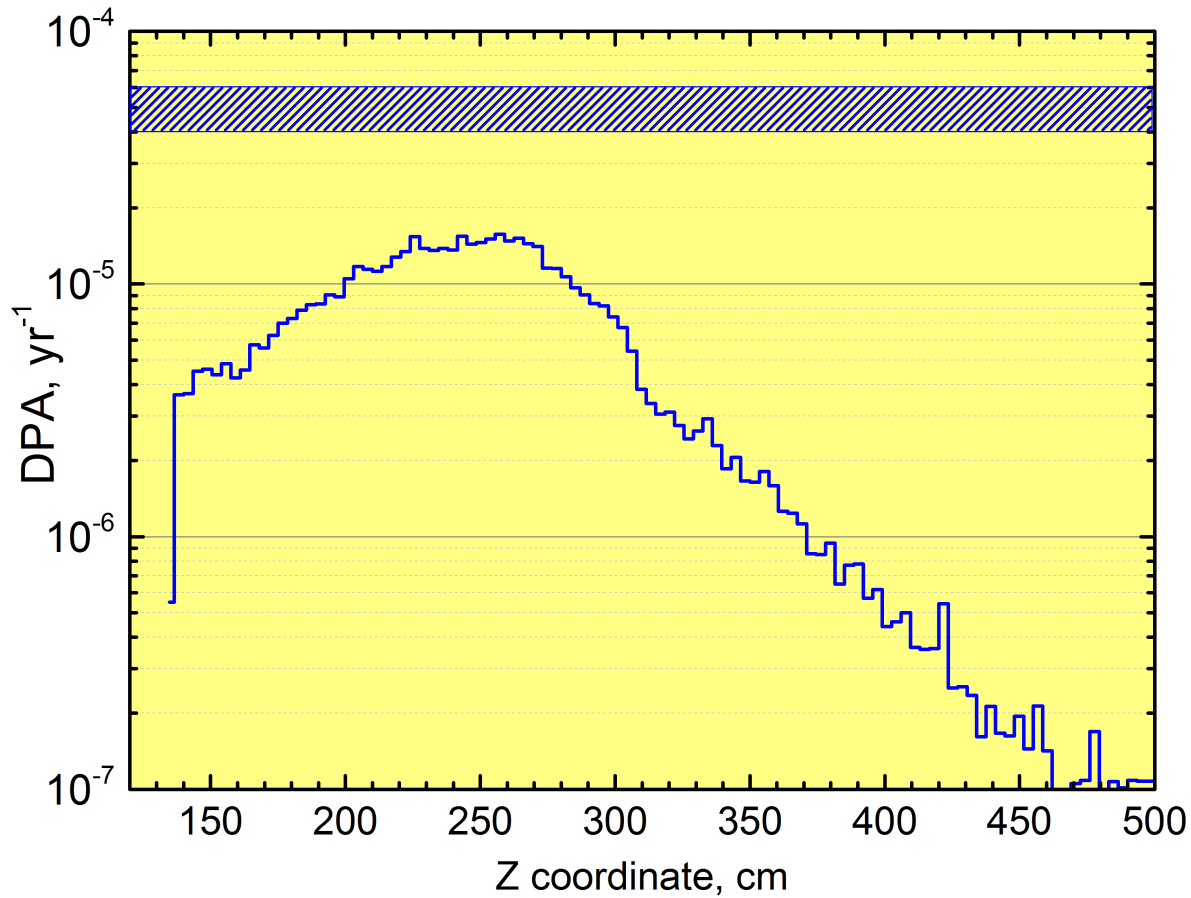
High-resistivity bronze C63200,  $7.64 \text{ g/cm}^3$ ,  $\sim 33$  tonnes



Coils: Al stabilizer + NbTi+Al+ insulation. Homogeneous model In MARS15.

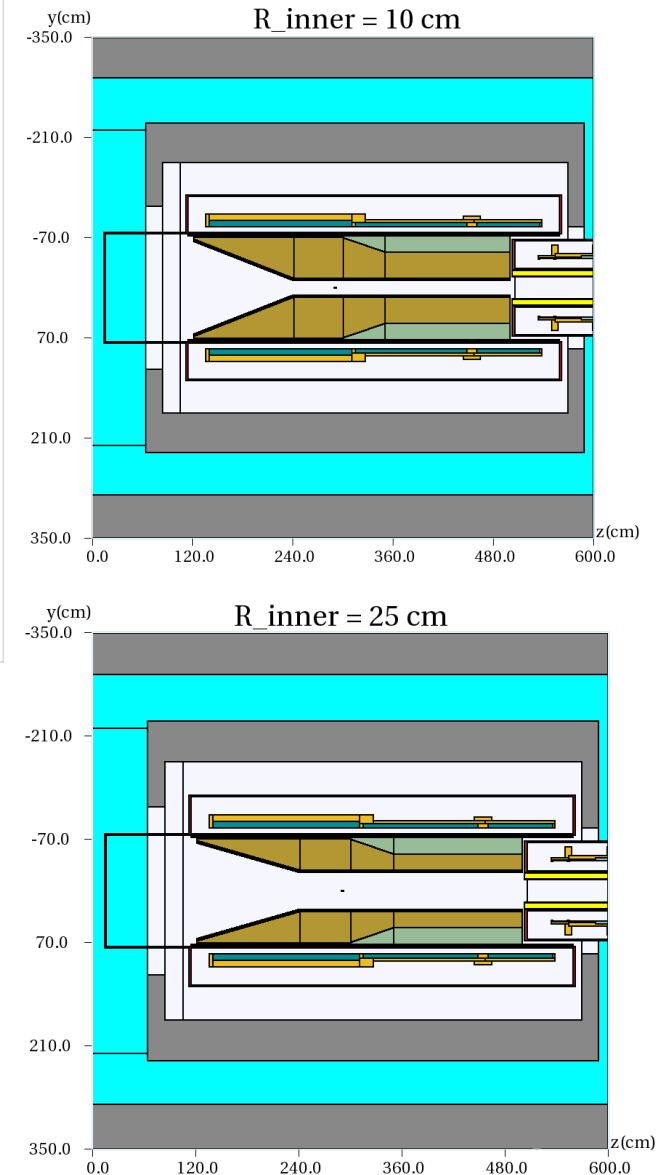
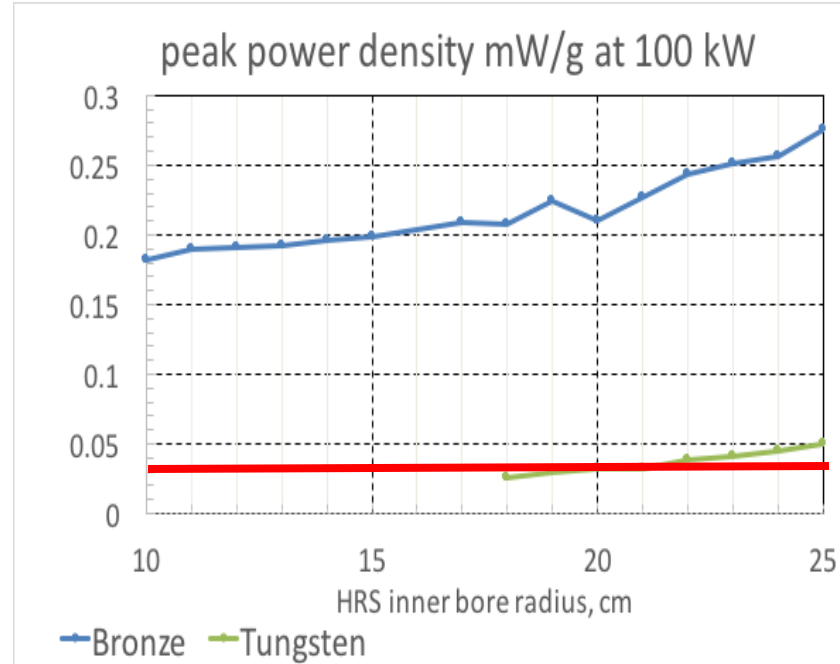
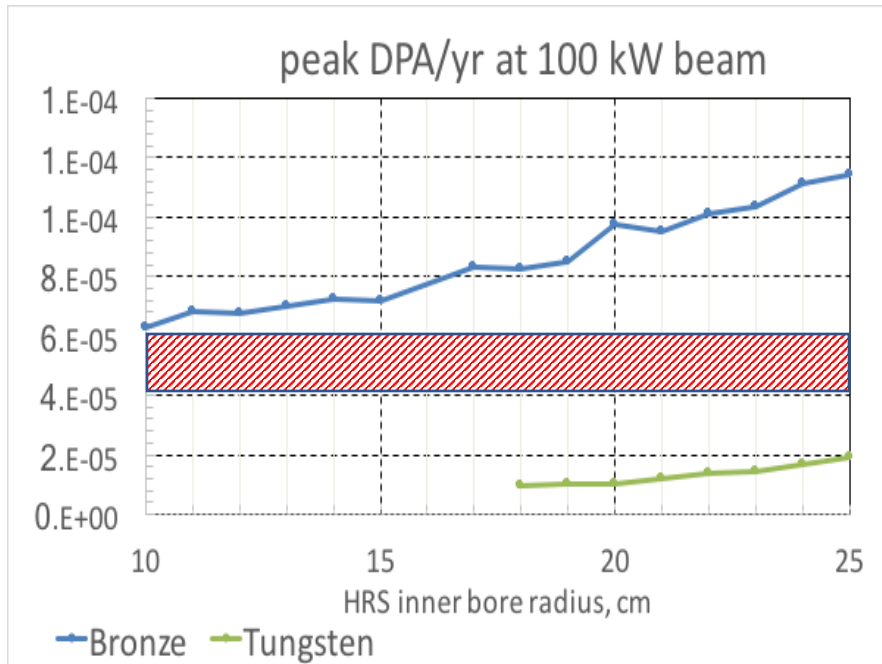
Coil materials:  
8.35% NbTi 8.35%  
Cu 17.33% G10  
65.97% Al

# MARS15 baseline Mu2e radiation quantities



**Distribution in slice:  $\pm 10$  cm in Y, 6 cm in X (thickness)**

# Optimization for 800 MeV@100 kW Mu2e-II

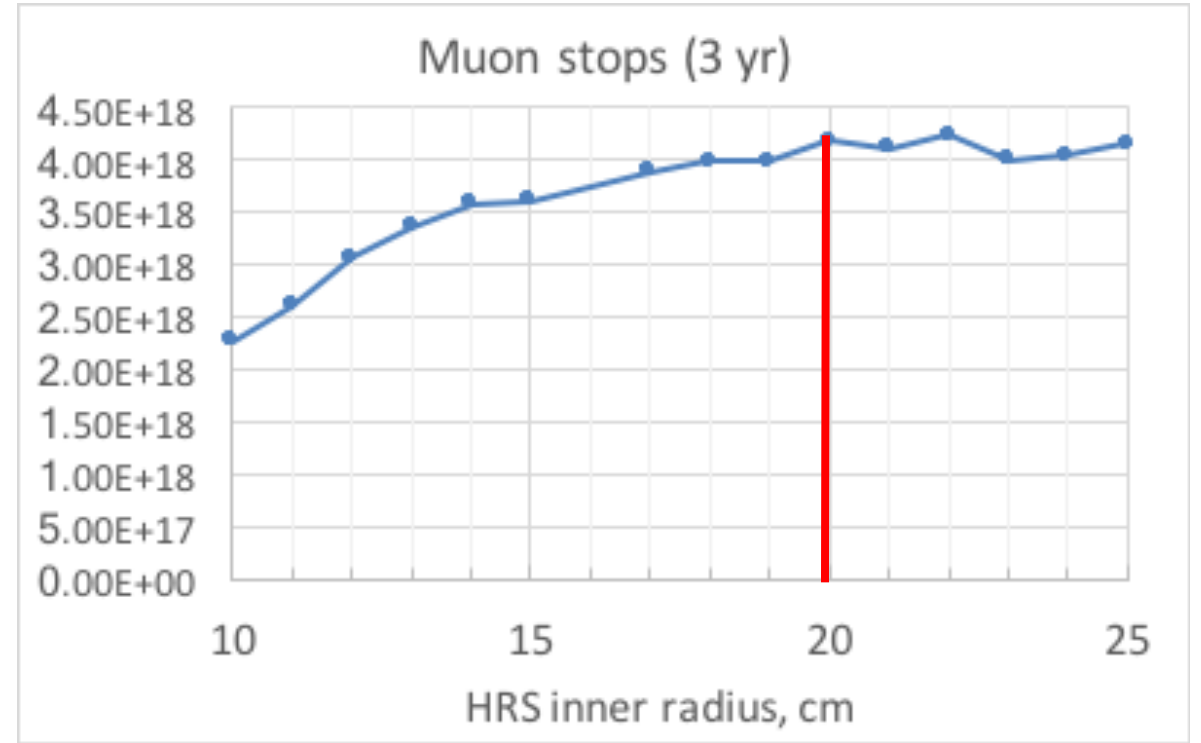
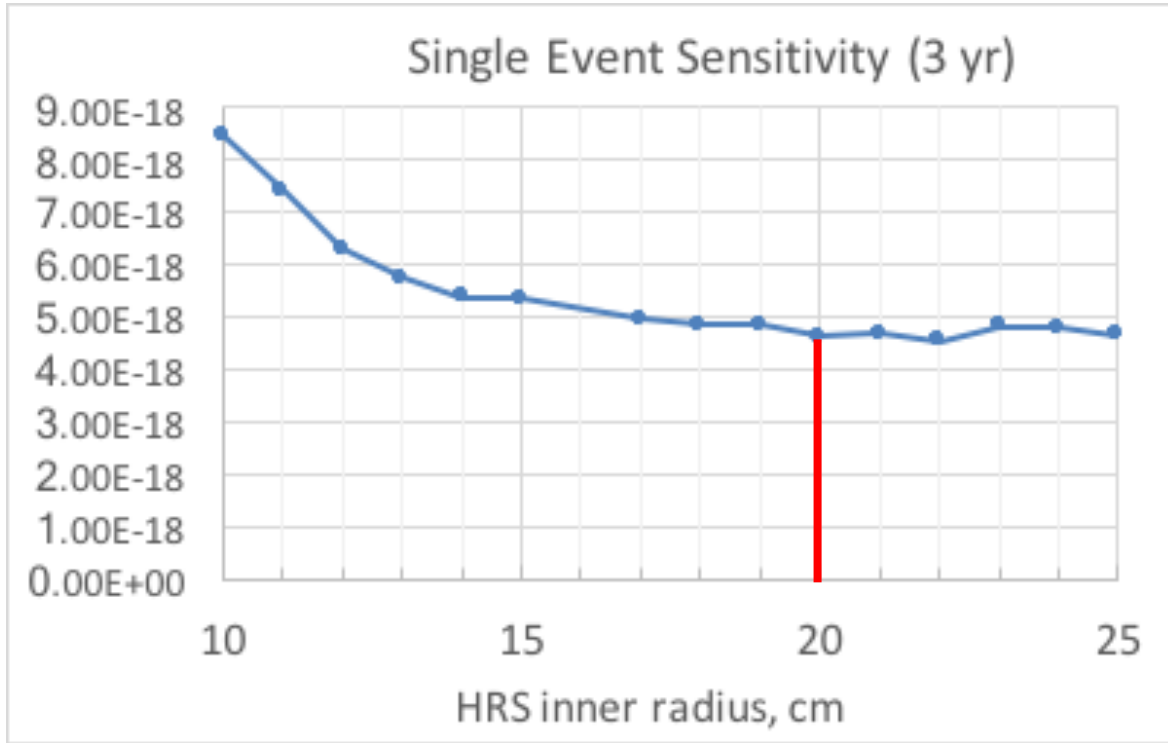


**DPA:** W HRS of all radii satisfy the limits (bronze with R=10cm may too).

**Power density:** Only W HRS with  $R \leq 20$  cm satisfies the requirements



# Muon stops and SES @ 100 kW



Red line: maximum radius to satisfy peak power density limit.

Optimum for W HRS is at R=17-20 cm.

Based on SES:  $\Lambda_{\text{mu2e-II}}/\Lambda_{\text{mu2e}} = 1.56$  ( $\kappa=0.01$ ) to  $1.88$  ( $\kappa=100$ )

# Conclusions

- Critical radiation quantities for PS coils are DPA and peak power density
- For the baseline Mu2e DPA is the most critical one with the limits 4-6E-5 DPA/yr to allow for annealing one a year
- For Mu2e-II with **800 MeV @ 100 kW** the most critical parameter is the **peak power density**. It constraints HRS to tungsten in inner **bore  $\leq 20$  cm** (and  **$\geq 17$  cm** not to compromise Single Event Sensitivity,  $\Lambda_{\text{mu2e-II}}/\Lambda_{\text{mu2e}} = 1.56$  to  $1.88$ ).
- If peak **power density issue** can be alleviated, **any R tungsten HRS** (or, probably, **R=10 cm bronze HRS**) would satisfy the DPA requirements