



## US HL-LHC Accelerator Upgrade Project

### MQXFA Final Design Report

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## Revision History

Revision	Date	Section No.	Revision Description
V1	5/15/18	All	Initial Release
V2	5/16/18	5.1, 6.2, 7	Updates in coil fabrication tolerances, assembly specifications, magnet test

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## 1 Introduction

The MQXFA Quadrupole magnets will be installed in HL LHC to form the Q1 and Q3 inner triplet optical elements in front of the interaction points 1 (ATLAS) and 5 (CMS). A pair of MQXFA units is assembled in a stainless steel helium vessel, including the end domes, to make the Q1 Cold Mass or the Q3 Cold Mass. The US HL LHC Accelerator Upgrade Project is responsible for the design, manufacturing and test of the Q1/Q3 Cold Masses and the complete MQXFA magnets [1]. CERN provides the cryostat components and is responsible for integration and installation in HL LHC [2].

The MQXFA quadrupoles have 150 mm aperture, 4.2 m magnetic length, nominal gradient of 132.6 T/m, and coil peak field of 11.4 T. They use Nb<sub>3</sub>Sn conductor and a support structure made of segmented aluminum shells pre-loaded by using bladders and keys. The Q2 optical elements will be based on the same quadrupole design with a longer magnetic length of 7.15 m. These units are called MQXFB and MQXF is used as a general reference to both MQXFA and MQXFB.

The design criteria for MQXF are documented in [3-5]. These criteria were developed based on experience from the US LHC Accelerator Research Program (LARP) and other high field magnet R&D programs in the US and Europe [6]. In particular, the 120 mm aperture High-gradient Quadrupole by LARP provided the main design reference for MQXF.

A 1<sup>st</sup> generation short model (MQXFS1) [7] was developed by LARP and CERN and tested in 2016. Additional feedback from conductor development and magnet analysis was implemented in the 2<sup>nd</sup> generation (final) design [8]. The final design was tested through a series of 1.5 m short models (MQXFS3/4/5) developed in close collaboration by LARP and CERN, and implemented in the MQXFA long prototypes fabricated and tested by LARP. The first prototype (MQXFA1) has coils of 4 m magnetic length in a full-length structure. The MQXFA2/3 prototypes have the final 4.2 m magnetic length.

## References

1. US HL-LHC Accelerator Upgrade Project, Q1/Q3 Cryo-Assemblies Conceptual Design Report, US-HiLumi-doc-140, July 17, 2017
2. G. Apollinari et al., “High-Luminosity Large Hadron Collider (HL-LHC) Technical Design Report” CERN Yellow Reports: Monographs, Vol. 4/2017, CERN-2017-007-M (CERN, Geneva, 2017) <https://doi.org/10.23731/CYRM-2017-004>
3. Design Criteria for MQXFA Superconducting Elements, US HiLumi Doc 885, <https://us-hilumi-docdb.fnal.gov/cgi-bin/private/ShowDocument?docid=885>.
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5. 4. MQXFA Structural Design Criteria, US HiLumi Doc 909, <https://us-hilumi-docdb.fnal.gov/cgi-bin/private/ShowDocument?docid=909>
6. G. Sabbi, “Nb<sub>3</sub>Sn IR Quadrupoles for the High Luminosity LHC”, IEEE Transactions on Applied Superconductivity, Vol. 23, No. 3 (June 2013) 4000707
7. “MQXFS1 QUADRUPOLE DESIGN REPORT”, edited by G. Ambrosio and P. Ferracin, FERMILAB-TM-2613-TD, 2014.

8. P. Ferracin et al., “Development of MQXF: The Nb<sub>3</sub>Sn Low  $\beta$  Quadrupole for the HiLumi LHC”, IEEE Trans. Appl. Supercond. Vol. 26, No. 4 (June 2016) 4000207.

## 2 Requirements

The MQXFA functional requirements are classified into two groups: “Threshold” requirements and “Objective” requirements. Threshold requirements are requirements that contain at least one parameter that the project must achieve, and Objective requirements are requirements that the project should achieve and will strive to achieve.

The Functional Requirements Specification for the MQXFA magnets can be found in [1]. The Functional Requirements Specification for the LMQXFA cold-masses can be found in [2]. The LMQXFA Cold Mass, when surrounded by the QXFA or QXFC cryostat shields, piping, and vacuum vessel, is then the LQXFA cryo-assembly for Q1 and the LQXFB cryo-assembly for Q3, as installed in the tunnel of LHC. CERN is responsible for the design and fabrication of the QXFA and QXFC cryostats. The Functional Requirements Specification for the LQXFA and LQXFB Cryostat Assembly can be found in [3].

A summary of the MQXFA threshold and objective requirements is provided in Hi-Lumi-Doc 36 Functional Requirements Specification and in Hi-Lumi-Doc- 1103 Acceptance criteria part A: MQXFA magnet (EDMS:2031083) [1]

### References

[1] Acceptance Criteria part A: MQXFA magnets, US HiLumi DocDB # 1103

[https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=1103&filename=HL\\_Acceptance\\_criteria\\_part-A\\_MQXFA\\_v1.0.pdf&version=6](https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=1103&filename=HL_Acceptance_criteria_part-A_MQXFA_v1.0.pdf&version=6) MQXFA Magnets Functional requirements specification, US HiLumi DocDB # 36 (EDMS 1535430)

[2] LMQXFA Functional Requirements Specifications, US HiLumi DocDB # 64, <https://us-hilumi-docdb.fnal.gov/cgi-bin/private/ShowDocument?docid=64>.

[3] LQXFA/LQXFB Cryostat Assembly Functional Requirements Specification, US HiLumi DocDB # 246. <https://us-hilumi-docdb.fnal.gov/cgi-bin/private/ShowDocument?docid=246>.

## 3 Superconductor

The Rutherford cable for the MQXF magnets is fabricated using 40 Nb<sub>3</sub>Sn strands of diameter 0.85 mm. The baseline strand is a Rod-Restack-Process RRP® strand manufactured by Oxford-Instrument Superconducting Technology (OST), a company of Bruker Energy & Supercon Technologies (BEST). Another option is the Powder-In-Tube PIT strand produced by Bruker Energy & Supercon Technologies (BEST). The prototype coils fabricated by US LARP (LHC Accelerator R&D Program) are using RRP conductor, whereas those made by CERN are using both RRP and PIT conductors.

### 3.1 Strand

Initial acceptance tests of several billets at OST and within LARP for a wire diameter of 0.778 mm (this diameter wire was used for the 120 mm aperture HQ magnets) showed that, although the wires meet the critical current requirement, the residual resistance ratio (RRR) was in many cases barely above the minimum requirements when reacted using the standard reaction schedule of 210°C/72 h + 400°C/48 h + 650°C/48 hr. The reaction used by OST to qualify the strand before delivery of strand to LARP is 210°C/48 h + 400°C/48 h + 650°C/50 h.

To increase the manufacturing margin and increase the likelihood of RRR exceeding 150 in the round wire, the tin content in the sub-element core was reduced by 5% from the standard amount. The wires from these “Reduced-Sn” billets showed a marked increase in RRR to values over 300, demonstrating that MQXF conductor requirements can be met by RRP conductor. The protection offered by the “Reduced-Sn” modification also allowed the final heat treatment temperature to be more aggressive for increasing critical current at 15 T, where the reaction used by OST changed the final stage to 665°C/75 h. The resulting statistical distribution of properties exhibited acceptable margins above both the RRR and critical current.

The number of superconducting filaments shall be equal to or larger than 108, and the mean copper/non-copper ratio shall be 1.2. These requirements imply that the sub-element diameter by design is ~ 55 µm. The US HL-LHC-AUP strand specification and requirements [1] are based on the LARP strand specification and requirements used to procure strands for the MQXF prototypes [2]. The main characteristics of the strand are summarized in Table 3.1.

Table 3.1 : Main Parameters of the HL-LHC AUP Strand.

Parameter or characteristic	Value	Unit
Superconductor composition	Ti-alloyed Nb <sub>3</sub> Sn	
Strand Diameter	0.850 ± 0.003	mm
Critical current at 4.2 K and 12 T	> 632	A
Critical current at 4.2 K and 15 T	> 331	A
<i>n</i> -value at 15 T	> 30	
Count of sub-elements	≥ 108	



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(Equivalent sub-element diameter)	$(\leq 55)$	( $\mu\text{m}$ )
Cu : Non-Cu volume Ratio	$\geq 1.2$	
Variation around mean	$\pm 0.1$	
Residual Resistance Ratio <i>RRR</i> for reacted final-size strand	$\geq 150$	
Magnetization at 3 T, 4.2 K (reported for information)	$< 256$ ( $< 320$ )	$\text{kA m}^{-1}$ (mT)
Twist Pitch	$19.0 \pm 3.0$	mm
Twist Direction	Right-hand screw	
Strand Spring Back	$< 720$	arc degrees
Minimum piece length	500	m
High temperature HT duration	$\geq 40$	Hours
Total heat treatment duration from start of ramp to power off and furnace cool	$\leq 240$	Hours
Heat treatment heating ramp rate	$\leq 50$	$^{\circ}\text{C per hour}$
Rolled strand (0.7225 mm thick) critical current at 4.2 K and 12 T	$> 600$	A
Rolled strand critical current at 4.2 K and 15 T	$> 314$	A
Rolled strand <i>RRR</i> after reaction	$> 100$	

The QXF coil heat-treatment schedule for cables using this RRP strand is the following: 210°C/48h + 400°C/48h + 665°C/50h. This is based on supplier recommendation, and is consistent with past observations by LARP experts, showing that the reduction of the final stage duration, compared to the duration previously applied by the supplier, improved *RRR* for extracted strands at locations of the kinked edges from cabling, with negligible reduction in critical current.

## 3.2 Cable

The MQXFA cables have a reduced keystone angle of 0.40° (cf. first generation: 0.55°). They will have a minimum length of 455 m, respooled from 500 m of strands. The strand maps will be drawn up by LBNL to optimize wire usage with a reasonable billet blending. The strands will be respooled as-received (i.e. without pre-cable annealing). An online dual-axis optical micrometer will be used during respooling to verify diameter. The cables will be fabricated according to the latest “US-HiLumi Cable Specification” [3], which is based on the LARP specification used for the cables of the MQXF prototype coils fabricated by LARP. The salient cable parameters are listed below in Table 3.2.

Table 3.2 : MQXFA Cable Parameters.

Number of Wires in Cable	40
Cable Mid-Thickness	$1.525 \pm 0.010$ mm
Cable Width	$18.15 \pm 0.05$ mm
Cable Keystone Angle	$0.40^\circ \pm 0.1^\circ$
Cable Lay Direction	Left
Cable Lay Pitch	$109 \pm 3$ mm
Cable Core Material	316 L Stainless Steel
Cable Core Width	12 mm
Cable Core Thickness	0.025 mm
Cable Core Position	Biased towards the major edge
Maximum Cable Residual Twist	$150^\circ$

The cables will be identified using the following scheme, which is compatible with the CERN system.

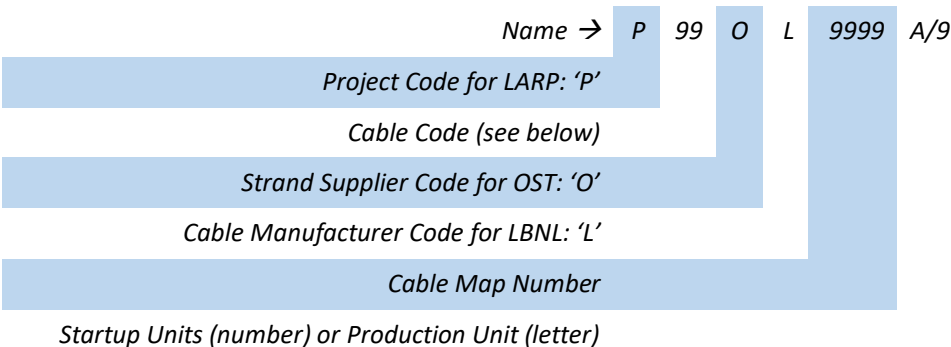


Figure 3.1: Cable ID Scheme based on US HiLumi DocDB # 41.

Table 3.3: Cable codes relevant to MQXF 2<sup>nd</sup> generation cable designs used during R&D and production.

Cable code	2nd Generation Cable Description
43	QXF R&D w/ Core, using un-annealed 108/127 wires
45	QXF R&D w/ Core, using un-annealed 132/169 wires
47	QXF R&D w/ Core, using un-annealed 144/169 wires

Each cable unit length will be accompanied by a Release Note (a.k.a. Cable Report), including a cable summary, the Respool Log (identifying the strand-spool-brake-fork relationship), charts of the cable dimension parameters (keystone angle, width, and mid-thickness) from the online measurements, optical micrograph (for assessing strand damage), and a report of any non-conformity. It will be formatted to allow exporting the required data to the Vector Database.

Strands representative of the billet blend will be extracted according to the Respool Log for  $I_c$  and RRR measurements. The heat treatment schedule used will be that specified for the coil heat treatment.

### 3.3 Cable Insulation

The MQXFA cables are insulated according to the HL-LHC AUP specification [5] based on LARP specification [6] using a high-strength glass yarn (S-2 Glass® direct sized yarn) made of 9  $\mu\text{m}$  continuous glass strands twisted together and treated with an inorganic sizing (“933”), supplied by AGY (2558 Wagener Road, Aiken, South Carolina, USA 29801). The single-ply yarn is then made into a 2-ply yarn with a twist pitch of 3 inches (i.e. 0.34 twist per inch) by an undisclosed subcontractor of New England Wire Technologies (NEWT, 130 North Main Street, Lisbon, NH 03585), who braids the yarns of fiberglass onto our superconducting cables. The yarn is identified by HL-LHC-AUP and its vendors as “SCG75 1/0 0.7Z fiber with 933 sizing”. For completeness, Table 3.4 translates the US- and EU-style nomenclature.

Table 3.4: US- and EU-style nomenclature.

US style	S	C	G	75	1/0	0.7Z
EU style	S	C	9	66	1x0	Z28
Meaning	High-strength glass	Continuous filament, aka strand	Filament diameter = 9 $\mu\text{m}$	Yield is 7500 yd/lb = 66 g/km (TEX)	1 strand twisted into continuous filament ends, no piling	Right hand twist at 0.7 turns per inch = 28 turns per meter

The braiding is done using a 48 bobbin-carrier braiding machine at NEWT, set to achieve 18 picks per inch in a vertical orientation. The bobbin payoff tension is between 1/4 to 3/8 lbs, and the cable payoff and take-up spool tensions are 2 and 12 lbs, respectively. The insulation specification thickness is  $0.145 \pm 0.005$  mm, common between CERN and HL-LHC-AUP. The insulation thickness is checked at the start of the insulation run using a 5-foot sample according to a 10-stack measurement procedure agreed between CERN and HL-LHC-AUP. The insulated 10-stack cable is measured at 5 MPa during three loading cycles, repeated using the same stack with the insulation removed. The per-side insulation thickness (calculated by subtracting the bare-stack average from the insulated-stack average and then divided by two) measured by the vendor is communicated to HL-LHC-AUP and must be within the tolerance before commencing further work. A second 5-foot sample is sent to HL-LHC-AUP for verification measurements. At the end of the run, another 5-foot sample is taken and measured by the vendor using the same procedure.

### References





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- [1] Specification for Quadrupole Magnet Conductor, US-HiLumi-doc-40.
- [2] Specification for Quadrupole Magnet Conductor, US-HiLumi-doc-40; Original Release.
- [3] US-HiLumi Cable Specification, US-HiLumi-doc-74.
- [4] Nb<sub>3</sub>Sn Superconductor Cable for LARP 150 mm Aperture Quadrupole Magnets, LARP-MAG-M-8005, and relevant amendments.
- [5] Cable Insulation Specification, US-HiLumi-doc-75.
- [6] QXF Magnet Cable Insulation Specification, LARP-MAG-R-8006-A (2014).

## 4 Magnet Design

### 4.1 2D Magnetic Design

#### 4.1.1 Coil main parameters

The cross-section of the MQXFA is based on the  $\cos 2\theta$ -layout with two conductor blocks in each layer and similar pole angle in both layers. These features are based on the 120 mm HQ design in order to achieve the following design objectives:

- Minimize the peak stress by optimizing the balance of Lorentz force and pre-load among the two layers.
- High conductor packing to maximize the engineering current density and increase the operating margin
- Minimize field errors, in particular the high order harmonic components, by optimizing the position and angle of each conductor block
- Incorporate to the extent possible the HQ experience in tooling design and coil fabrication,.

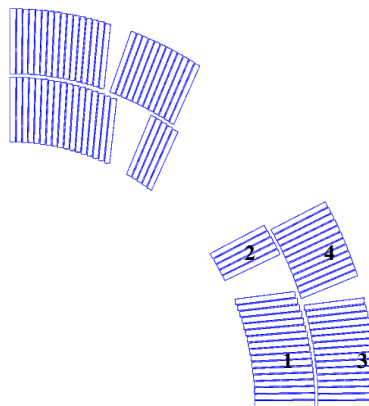


Figure 4.1: Cross-section of the MQXF coil.

Figure 4.1 shows the cross-section design for the second generation coil (MQXF\_v2) implementing various improvements with respect to the original design [1], which was used for the first practice coils and short model (MQXFS1). In order to minimize the impact on coil fabrication and tooling the guidelines for coil re-optimization were to 1) to keep same number of conductors per block; 2) to keep the pole turns of the inner and outer layer aligned so as to have the same concept of layer jump (only hard way bending); 3) to keep the same coil inner and outer diameters.



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The main coil parameters are summarized in Table 4.1. Based on the measurements performed to characterize the conductor dimensional change during heat treatment [1], and in order to find the best compromise between performance and field quality, for the second generation design it was decided to: 1) reduce the radial space in the tooling to accommodate for a cable width expansion to 1.2% instead of 2%; 2) keep the same azimuthal space, corresponding to a thickness expansion of 4.5%. The reduction of the nominal insulation thickness from 150  $\mu\text{m}$  to 145  $\mu\text{m}$  without changing the actual insulation thickness will help to assure a better azimuthal position of the coil turns. Dimensions of the cable before and after reaction are both given in Table 4.1. Design calculations are based on the dimension of the reacted cable.

The additional radial space due to the decreased cable width after reaction is partially absorbed by the increased inter-layer insulation (from 0.500 mm to 0.660 mm) and the outer layer of S2-glass that is installed in the outer coil diameter before impregnation (which increases from 0.150 mm to 0.310 mm). For the second generation design, we also consider a thicker mid-plane and pole insulation to allow fine tuning of field quality. The insulation between the mid-plane and the first insulated conductor increases from 0.250 mm to 0.375 mm, and from 0.350 mm to 0.500 mm between the pole and the insulated conductor. More information about the modifications implemented in the second generation design can be found in [3].

Table 4.1: Nominal parameters of the MQXF coil.

	unit	
Coil aperture radius	mm	75.000
Layer 1 outer radius	mm	93.653
Inter-layer thickness	mm	0.660
Outer layer inner radius	mm	94.313
Outer layer outer radius	mm	112.966
Mid-plane shim thickness (per coil)	mm	0.375
Number of turns in block 1		17
Number of turns in block 2		5
Number of turns in block 3		16
Number of turns in block 4		12
Bare unreacted/ <b>reacted</b> conductor width	mm	18.150/ <b>18.363</b>
Bare unreacted/ <b>reacted</b> conductor thickness	mm	1.525/ <b>1.594</b>
Nominal keystone angle	deg	0.40
Nominal insulation thickness	mm	0.145

The relative position of the block number 2 and 4 (pole block of layer 1 and pole block of layer 2) is such that the broad face of the layer jump turn (orange conductor) is parallel to the broad face of the top conductor of the upper block outer layer (see Figure 4.2). This way a shim with a

uniform thickness ( $\sim 0.25$  mm) can be used. Fabrication tolerances for cable and insulation are provided in the conductor section.

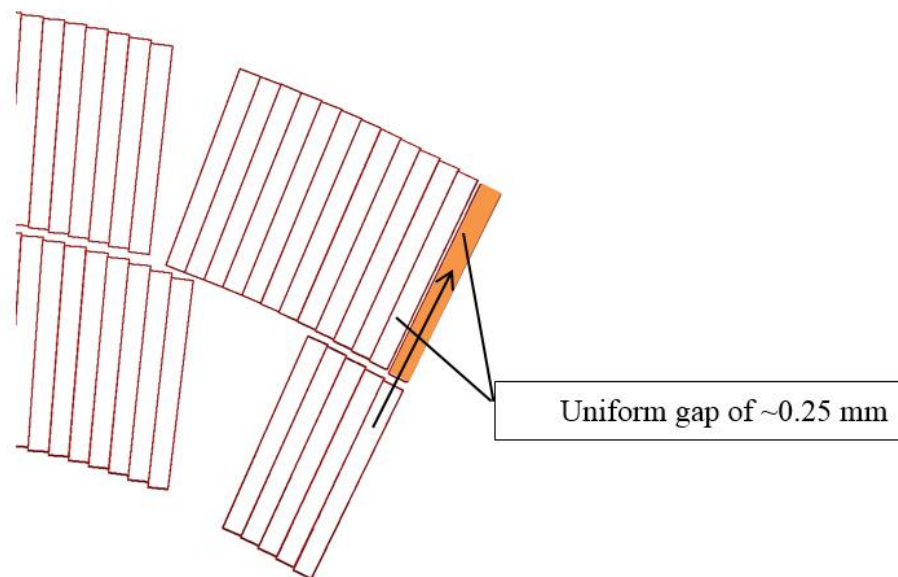


Figure 4.2: Coil layer jump.

Figure 4.3 compares the turn position for the first and second generation coil design.

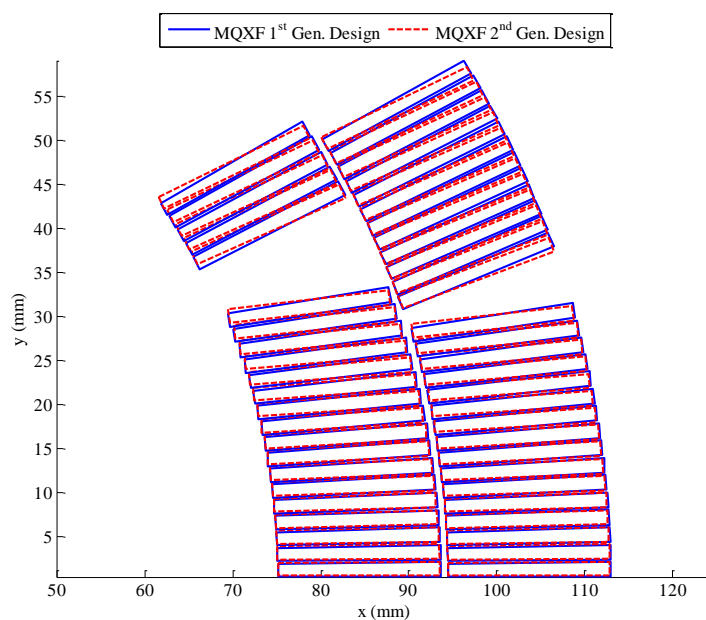


Figure 4.3: Cross-section of the MQXF second generation coil (red) superimposed to the cross-section of the first generation coil (blue).

## 4.1.2 Roxie model

The computation of the magnetic field was performed with the Roxie software [7]. In Figure 4.4 it is given the 2D data table as implemented in Roxie. The option “alignment of the conductor on the coil OD” was selected (ODFAC = 1) since it provides the best results based on the experience from previous magnets.

Block Data 2D											
No	Type	NCab	X	Y	$\alpha$	Current	Cable name	N1	N2	Imag	Turn
1	Cos	17	75	0.28648	0	16471	XF145H5TH5	2	20	0	0
2	Cos	5	75	28.5	24	16471	XF145H5TH5	2	20	0	0
3	Cos	16	94.313	0.22782	0	16471	XF145H5TH5	2	20	0	0
4	Cos	12	94.313	19	20.8049	16471	XF145H5TH5	2	20	0	0

Figure 4.4: Input-file of the MQXF coil used in ROXIE.

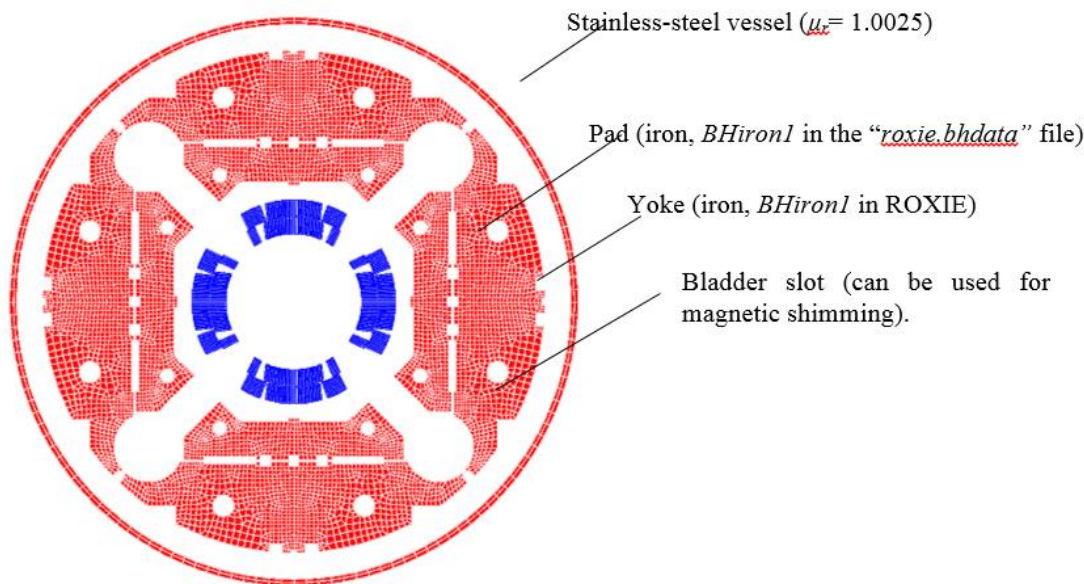


Figure 4.5: MQXF magnet model used in ROXIE.

In the MQXF assembly the superconducting coil is surrounded by iron pads and yokes which reinforce the field in the aperture and reduce the stray field outside the magnet. These elements are also integral components of the shell-based support structure. As a consequence the yoke and the pad implement slots for the insertion of the bladders and grooves for the keys. The 2D FEM model used for the computation of the magnetic field is shown in Figure 4.5. The *BH* characteristic used for the iron components is defined as “BHiron1” in the *roxie.bhdata* file. This *BH* curve assumes a filling factor of 1 (full body). Note that no thermal contraction factor was used for the computation of the harmonics, *i.e.*, the coil is assumed to be at room temperature. The impact of cool-down and mechanical deformation on field quality will be discussed later.



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## 4.1.3 Magnet performance

Minimal requirements for wire manufacturing set by CERN and HL-LHC-AUP require a critical current larger than 632 A and 331 A in respectively 12 T and 15 T applied field and at a temperature of 4.2 K. For the computation of the magnet short sample current 5% degradation on the current due to cabling is assumed and a correction factor of 0.429 T/kA is used to take into account the strand self-field. It corresponds to the magnetic field produced at 89% of the radius of a straight wire. For the characterization of the critical surface the scaling law developed in [8] is used. In Table 4.2 the magnetic parameters of the MQXF magnet when powered at short sample ( $I_{ss}$ ), nominal ( $I_{nom}$ ) and ultimate-operation, or maximum ( $I_{max}$ ) currents are given (Figure 4.6). The operational temperature of the MQXF magnet is 1.9 K.

In Figure 4.7 the magnetic field density in the coil (left) and in the yoke (right) at nominal current are plotted. At  $I = I_{nom}$  the peak field in the coil reaches 11.41 T. The peak field is located in the pole block of the inner layer (block 2). The proximity of the yoke to the coil results in a highly saturated iron yoke that translate in a ~9% reduction in the transfer function from injection to nominal current (Figure 4.8-left). For the same reason the differential inductance  $L_d$  is non-linear (Figure 4.8-right). In spite of being highly saturated the iron yoke still contribute to enhancing the magnet gradient by ~ 8% at  $I_{nom}$  (from 121.7 T/m to 132.6 T/m).

Table 4.2: Main magnetic parameters of the MQXF cross-section considering an operational temperature of 1.9 K.

Parameters	Units	$I_{ss}$	$I_{max}$	$I_{nom}$
Current	kA	21.24	17.89	16.47
$I/I_{ss}$	%	100	84	78
Gradient	T/m	168.1	143.2	132.6
Nominal peak field on the coil	T	14.5	12.3	11.4
Stored energy	MJ/m	1.89	1.38	1.18
Current sharing temperature	K	1.9	5.8	6.8
Differential inductance	mH/m	8.13	8.18	8.21
Superconductor current density ( $j_{sc}$ )	A/mm <sup>2</sup>	2059	1734	1596
Engineering current density ( $j_{eng}$ )	A/mm <sup>2</sup>	936	788	726
Forces x	MN/m	3.83	2.85	2.47
Forces y	MN/m	-5.68	-4.08	-3.48

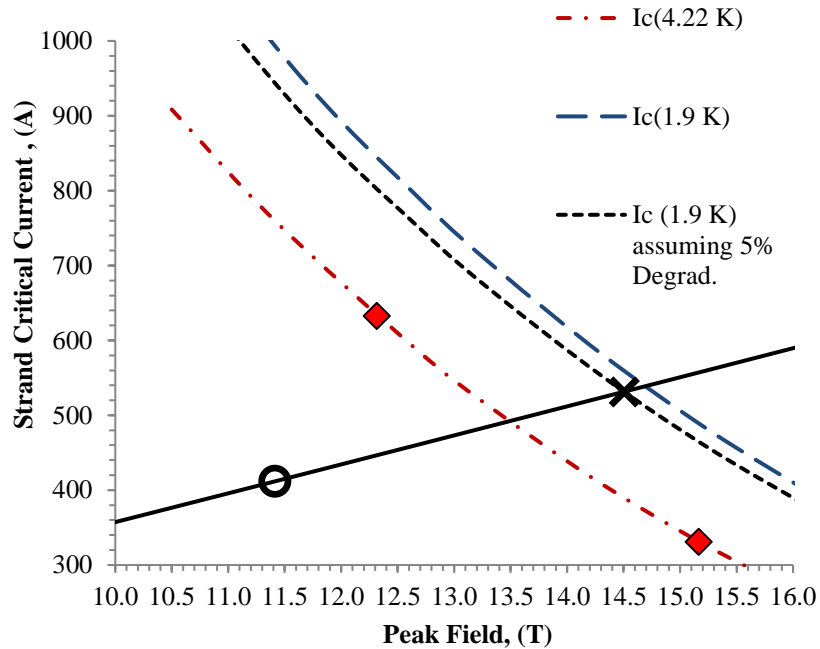


Figure 4.6: MQXF quadrupole load line (current in the cable versus peak field in the coil). The peak field is always located in block 2. The load line has been obtained by gradually increasing the current in the coil. This way the non-linearity of the load line is taken into account.

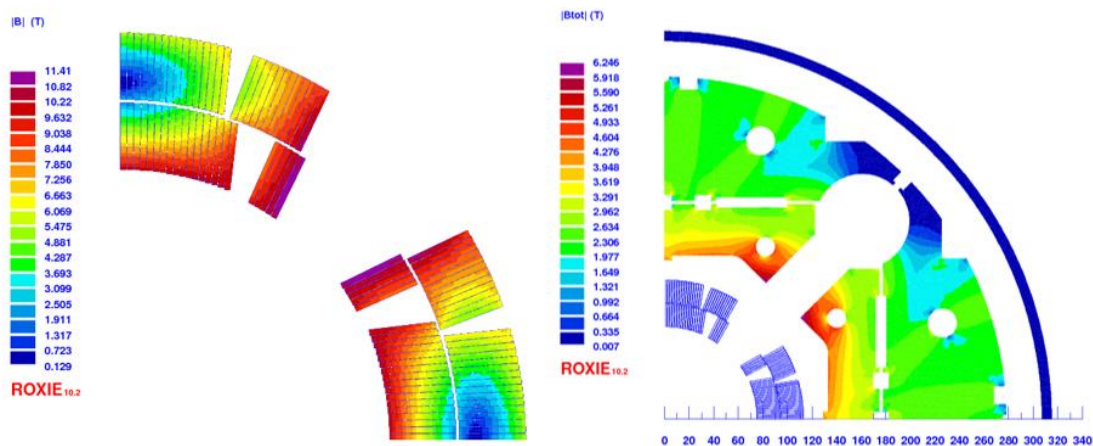


Figure 4.7: Magnetic flux density in the coil (left) and in the yoke (right) at nominal current ( $I_{nom}$ ).



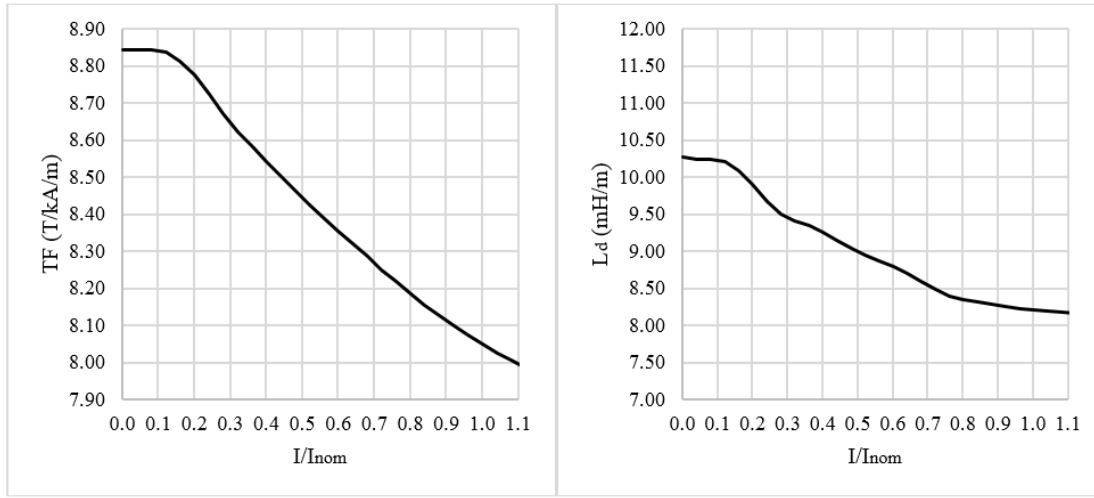


Figure 4.8: Left: Transfer function defined as the ratio between the gradient and the current and expressed in [T/m/kA] plotted versus  $I/I_{nom}$ . Right: differential inductance  $L_d$  in mH/m. Roxie was used for the computations.

#### 4.1.4 Field quality

Due to the large beam size and orbit displacement in the final focusing triplet, these magnets have challenging targets for field quality requirements at nominal operating current. The coil cross section is optimized such that all allowed harmonics are within one unit at 6.5 TeV. Field quality is optimized at 123 T/m (6.5 TeV) because the triplet will operate between 100% and 90% of the nominal gradient (132.6 T/m, 7 TeV) [3]. The following convention for the definition of the multipoles is used, taking as reference radius  $2/3$  of the coil aperture radius ( $R_{ref} = 50$  mm).

$$B_y + iB_x = 10^{-4} B_2 \sum_{n=1}^{\infty} (b_n + ia_n) \frac{(x + iy)^{n-1}}{R_{ref}^{n-1}}$$

For the second generation design, coil cross section has been re-optimized to account for the effect of coil deformation on field quality [5] and the contribution of the splices and connection leads [6] to the integral field quality. The impact of coil deformation is an offset of +0.9 units on  $b_6$ , mostly caused by the azimuthal coil deformation during cool down as it can be observed in Figure 4.9. The evaluation of the impact of coil deformation on field quality was carried out by importing the coil displacement map extracted from the ANSYS solution into the 2D magnetic model implemented in Roxie. The displacement map corresponds to the state of the coil after the room temperature pre-load, the cool-down and the excitation to  $I_{nom}$ , and it is estimated with respect to the design coil geometry at room temperature without any pre-load. The computed displacements were applied to every strand of the magnetic model and a harmonic analysis was performed with the displaced strand distribution. The deformation of the iron yoke was not taken into account during this analysis. The results of the mechanical analysis indicate a radial displacement of the blocks of -0.3 to -0.4 mm and an azimuthal displacement of -0.04 to -0.05 mm. The output of the numerical



magnetic model showed a change in the normalized  $b_6$  harmonic of about 0.9 units and a negligible change of other allowed harmonics such as  $b_{10}$  and  $b_{14}$ . The offset of the  $b_6$  is mostly caused by the azimuthal coil deformation, which results from the pre-load applied to the structure during the assembly and the structure contraction during the cool-down phase. As expected for quadrupole magnets, the deformations resulting from the electro-magnetic forces have a negligible effect on the  $b_6$ .

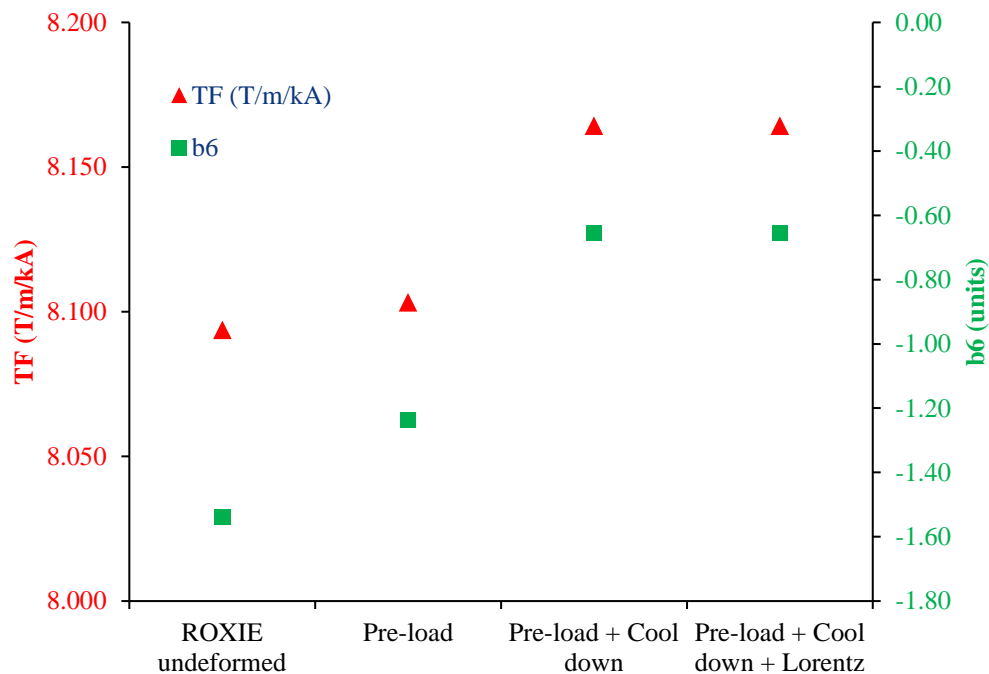


Figure 4.9: Impact of coil deformations due to cool-down, pre-loading, and energizing on the gradient and  $b_6$  at 6.5 TeV. In order to retain only the effect of the mechanical deformation, the magnet current is the same for the different steps to have the same contribution from the iron.

The contribution of the  $\text{Nb}_3\text{Sn}$ - $\text{NbTi}$  splices and connection leads is an offset of +0.5 units on  $b_6$  as it will be described in 3D section. The change on the rest of the harmonics is negligible. Figure 4.10 shows the evolution of  $b_6$  as a function of the current including the mechanical deformations and 3D effects. As it can be seen from the plot, the main contribution to  $b_6$  is coming from the iron saturation. Even if the difference between injection and nominal current is less than one unit, the maximum variation of  $b_6$  for the full range of current is 4 units.

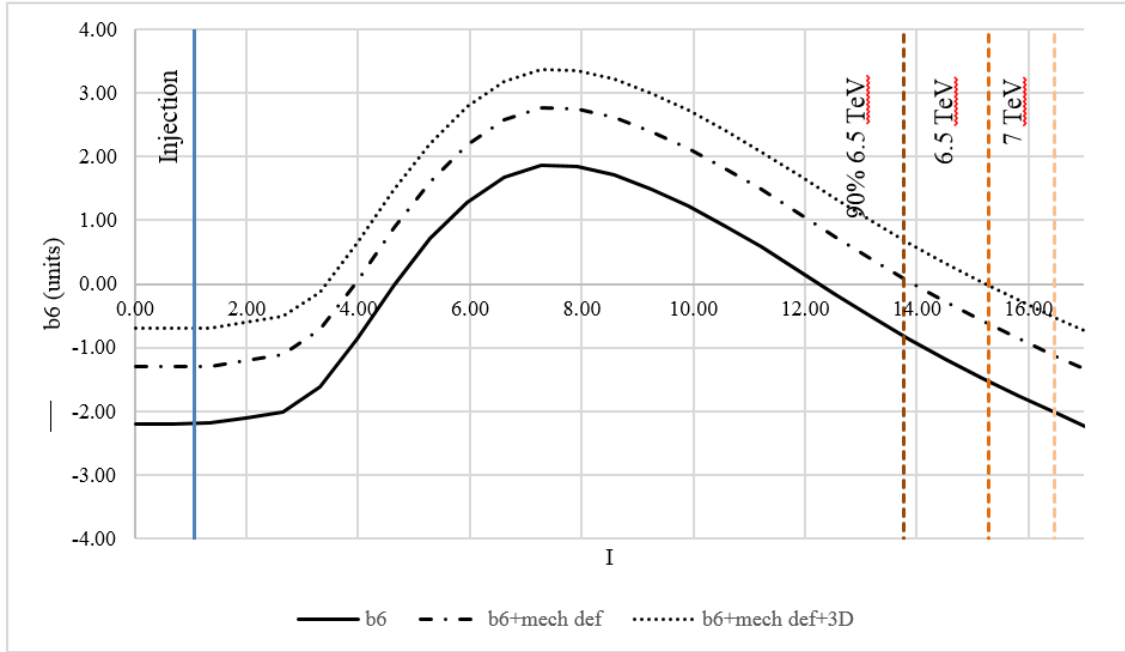


Figure 4.10: First allowed harmonic ( $b_6$ ) plotted versus the current, including the contribution of the mechanical deformation and 3D effects. Harmonics are expressed in units.

The evolution of the first four allowed harmonics ( $b_6$ ,  $b_{10}$ ,  $b_{14}$  and  $b_{18}$ ) with the current is plotted in Figure 4.11. Numerical values of the field components calculated for 7 TeV, 6.5 TeV and 5.85 TeV are given in Table 4.3.

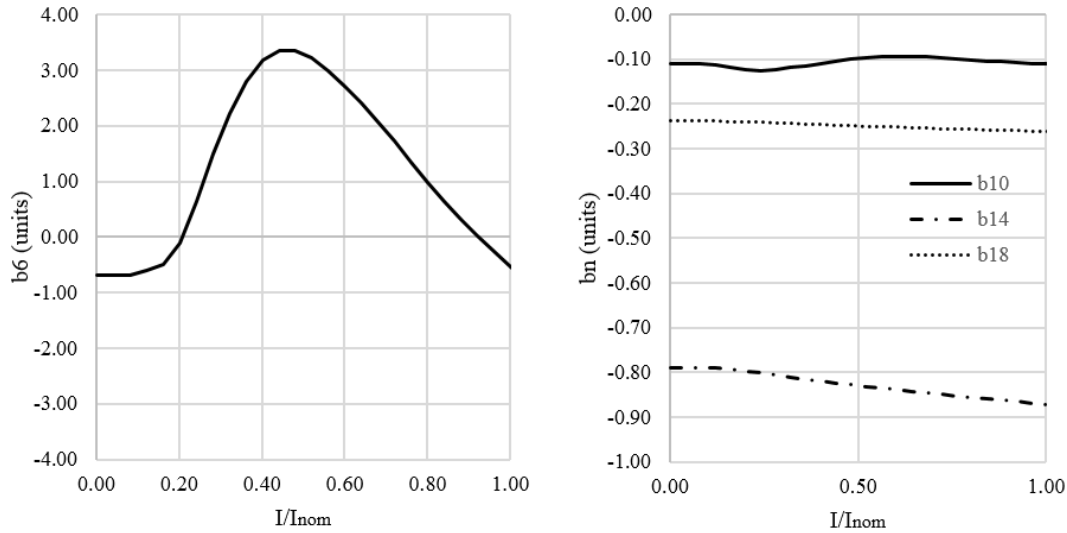


Figure 4.11: First four allowed harmonics ( $b_6$ ,  $b_{10}$ ,  $b_{14}$  and  $b_{18}$ ) plotted versus the  $I/I_{nom}$  ratio. Harmonics are expressed in units.

Table 4.3: Field Harmonic components calculated for 7 TeV (Nominal), 6.5 TeV and 5.85 TeV.

	unit	7 TeV	6.5 TeV	5.85 TeV
Current	kA	16.47	15.29	13.76
Gradient	T/m	132.6	123.8	112.3
$b_6$	unit	-0.69	-0.03	0.63
$b_{10}$	unit	-0.11	-0.11	-0.11
$b_{14}$	unit	-0.26	-0.26	-0.26
$b_{18}$	unit	-0.86	-0.86	-0.86

## 4.1.5 Systematic field error

Field calculations are performed assuming that conductors are aligned on their OD based on the experience from previous (NbTi) magnet. However, it is clear that one does not totally control the position of the cable in the impregnation cavity due to the necessity to allow space for the cable to grow during heat treatment. Here we estimate the field errors due to various defects in tooling, coil size and asymmetry, and turn shifts.

Certain coil variances are observed from 1<sup>st</sup> generation coil cross section and CMM. At the winding and block level there are azimuthal and radial shifts and rotations. The position of turns near the pole and near the midplane have very little displacement as observed in coil cross sections. Therefore, shifts mostly affect the middle turns of each level near the wedge. The variability along the magnetic length alone is the subject of this analysis. A demonstration of each turn shift is shown in Figure 4.12 at greatly exaggerated magnitudes. Coil size and asymmetry is also included in this analysis based on 1<sup>st</sup> generation coil CMM data. Field errors due to tooling defects were calculated in the first generation MQXF design report and are included in this analysis.

A Monte-Carlo code was written in Java in conjunction with COMSOL Multiphysics to calculate the harmonics based on 40 line currents uniformly distributed within each cable. The code neglects effects from iron. Random turn/block/coil shifts have a normal distribution with a standard deviation of 50  $\mu\text{m}$ . Errors larger than 1 standard deviation are not included.

The normal and skew harmonic standard deviations are presented in Table 4.4. All random harmonics assume a 50  $\mu\text{m}$  independent RMS displacement. This level of RMS aberration is based on initial coil cross section analysis and coil CMM variance. Machining tolerance for coil parts is consistent with this choice of RMS aberration. Radial variation seems to have the largest effect on harmonics. This is partly an artifact that the entire block is shifted for radial variation as seen in coil cross sections while rotational and azimuthal variation principally is a shift of only the central turns between the midplane and pole. Regardless this analysis indicates that attention should be paid on the materials and thickness of radial insulation.

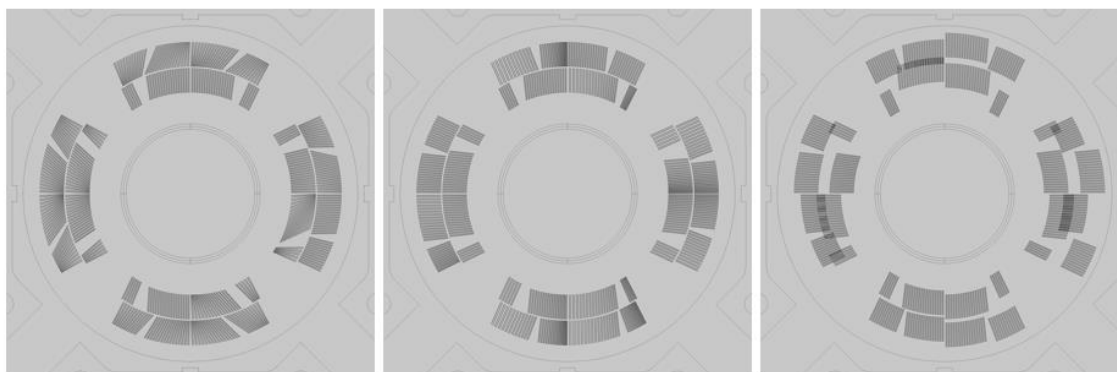


Figure 4.12: On the left a magnet cross section as displayed in COMSOL with random block rotations. The middle image has random azimuthal shifts. The right image has random radial shifts. Each type of shift has a standard deviation and peak greatly exaggerating displacements for demonstration purposes only.

Table 4.4: Random Harmonics based on 50  $\mu$ m RMS variation in tooling defects, coil CMM, and turn shifts.

	b3	b4	b5	b6	b7	b8	b9	b10	b11	b12	b13	b14
<b>Total Random Normal</b>	<b>1.560</b>	<b>1.070</b>	<b>0.680</b>	<b>1.880</b>	<b>0.270</b>	<b>0.160</b>	<b>0.100</b>	<b>0.220</b>	<b>0.041</b>	<b>0.024</b>	<b>0.015</b>	<b>0.032</b>
Coil Size and Asymmetry	0.859	0.331	0.134	0.002	0.027	0.005	0.005	0.000	0.000	0.001	0.001	0.001
Tooling Defects	0.829	0.623	0.412	0.301	0.159	0.121	0.061	0.040	0.028	0.018	0.011	0.007
Radial Shifts	0.761	0.564	0.418	0.195	0.173	0.029	0.068	0.029	0.024	0.016	0.008	0.003
Azimuthal Shifts	0.650	0.566	0.317	0.287	0.128	0.096	0.047	0.022	0.015	0.004	0.005	0.000
Rotational Shifts	0.093	0.105	0.072	0.074	0.038	0.031	0.016	0.008	0.006	0.001	0.002	0.000

	a3	a4	a5	a6	a7	a8	a9	a10	a11	a12	a13	a14
<b>Total Random Skew</b>	<b>1.550</b>	<b>0.960</b>	<b>0.680</b>	<b>0.390</b>	<b>0.280</b>	<b>0.180</b>	<b>0.100</b>	<b>0.066</b>	<b>0.036</b>	<b>0.021</b>	<b>0.010</b>	<b>0.008</b>
Coil Size and Asymmetry	0.846	0.302	0.142	0.083	0.028	0.016	0.004	0.001	0.000	0.001	0.001	0.000
Tooling Defects	0.849	0.585	0.406	0.192	0.161	0.069	0.060	0.030	0.020	0.012	0.008	0.005
Radial Shifts	0.784	0.628	0.421	0.328	0.181	0.155	0.069	0.050	0.025	0.011	0.008	0.006
Azimuthal Shifts	0.594	0.311	0.305	0.007	0.124	0.052	0.043	0.030	0.015	0.012	0.005	0.004
Rotational Shifts	0.098	0.063	0.070	0.001	0.037	0.017	0.016	0.011	0.006	0.005	0.002	0.002

Coil size and asymmetry harmonics decay much quicker than other block or winding level aberrations as a function of harmonic order. This is expected because the aberration is applied over an entire coil rather than a single turn or block. Thus, the coil size and asymmetry has seemingly negligible effect on high order harmonics. This partly explains the larger than expected  $a_3$  and  $b_3$  harmonic seen in MQXFS01 assembly test for example.

The 2<sup>nd</sup> generation MQXF design has increased radial and azimuthal insulation and has reduced the free space by roughly half the 1<sup>st</sup> generation design. It is expected therefore that 2<sup>nd</sup> generation MQXF should likewise have reduced longitudinal variability of turns.

## 4.2 3D Magnetic Design

### 4.2.1 Design objectives and process

From the magnetic point of view, the design objectives for coil ends optimization are:

- to limit the peak field enhancement in the ends;
- to keep the coil end as compact as possible in order to increase the magnetic length for a given coil length;
- to minimize the multipole content of the integrated field.

Magnetic and mechanical optimization of the coil ends for the first generation coil design is described in [6]. Following the positive feedback from winding and destructive inspection of the first generation practice coils, the overall shape of the coil ends was not modified. Only a fine tuning was needed to adapt to the new cable geometry and optimize field quality. In order to compensate the non-negligible positive contribution of the coil layer jump and Nb<sub>3</sub>Sn/NbTi splice to  $b_6$  [6], the following actions were taken: 1) The magnet longitudinal loading system has been moved from the connection side to the non-connection side of the magnet to minimize the length of the current leads; 2) Re-optimization of the longitudinal position of the coil blocks at the ends. Figure 4.13 compares the conductor longitudinal position for the first and second generation design; 3) Coil cross section has been optimized aiming to a  $b_6$  close to -0.5 units in the straight section to minimize the  $b_6$  integrated over the entire magnet length.

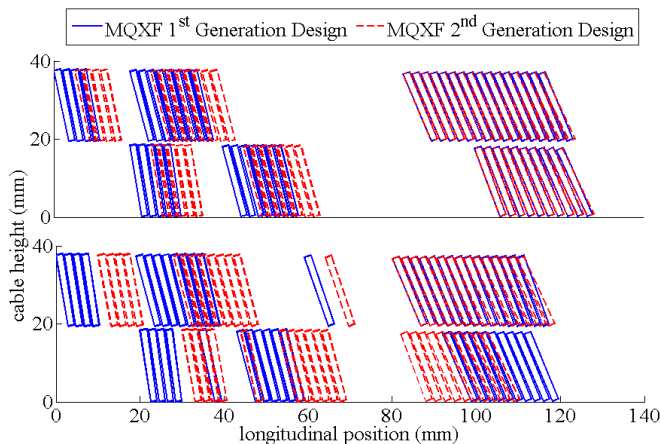


Figure 4.13: Comparison of the conductor position on coil ends for the first and second generation coil design.

Figure 4.14 to Figure 4.17 provide the 3D data table as implemented in ROXIE for each coil end.

Block Data 2D

No	Type	NCab	R	$\phi$	$\alpha$	Current	Cable name	N1	N2	Imag	Turn	Ne
1	Cos	10	75	0.28648	0	15310	XF145HTH5	2	20	0	0	1
2	Cos	7	75	14.2547	3.9938	15310	XF145HTH5	2	20	0	0	2
3	Cos	5	75	28.5	24	15310	XF145HTH5	2	20	0	0	3

More options :

No	String	N/a	N/a

Block Data 3D

No	Type	$\beta$	Bo	zo	Wi	Wo	Hwed	Horder
1	Diff. Geometry f	71	2	266	0.35	0.02	18.5	3.2
2	Diff. Geometry f	76	1.9	211	0.17	0.02	18.5	3
3	Diff. Geometry f	81	2.23	189	0.15	0.02	18.5	2.8

Figure 4.14: ROXIE input-file of the MQXF\_V2 return end, inner layer.

Block Data 2D

No	Type	NCab	X	Y	$\alpha$	Current	Cable name	N1	N2	Imag	Turn	Ne
1	Cos	10	75	1.6762	0.3994	-15310	XF145HTH5	1	1	0	0	1
2	Cos	6	75	15.6684	4.3932	-15310	XF145HTH5	1	1	0	0	2
3	Cos	1	75	28.5	24	-15310	XF145HTH5	1	1	0	0	3
4	Cos	4	75	29.8946	24.3994	-15310	XF145HTH5	1	1	0	0	4
5	Cos	10	75	0.28648	0	15310	XF145HTH5	1	1	1	90	1
6	Cos	6	75	14.255	3.9938	15310	XF145HTH5	1	1	1	90	2
7	Cos	1	75	22.8184	6.3901	15310	XF145HTH5	1	1	1	90	3
8	Cos	4	75	28.5	24	15310	XF145HTH5	1	1	1	90	5

More options :

No	String	N/A	N/A

Block Data 3D

No	Type	$\beta$	Bo	zo	Wi	Wo	Hwed	Horder
1	Diff. Geometry f	71	2	382	0.35	0.02	18.5	3.2
2	Diff. Geometry f	76	1.9	353	0.17	0.02	18.5	2.8
3	Diff. Geometry f	78	1.85	344	0.17	0.02	18.5	2.5
4	Diff. Geometry f	80	2.5528	330	0.15	0.02	18.5	2.8
5	Diff. Geometry f	80	2.2305	330	0.15	0.02	18.5	2.5

Figure 4.15: ROXIE input-file of the MQXF\_V2 lead end, inner layer.

Block Data 2D

No	Type	NCab	R	$\phi$	$\alpha$	Current	Cable name	N1	N2	Imag	Turn	Ne
1	Cos	16	94.313	0.22782	0	15310	XF145HTH5	2	20	0	0	1
2	Cos	8	94.313	19	20.8049	15310	XF145HTH5	2	20	0	0	2
3	Cos	4	94.313	27.8448	23.9999	15310	XF145HTH5	2	20	0	0	3

More options :

No	String	N/a	N/a

Block Data 3D

No	Type	$\beta$	Bo	zo	Wi	Wo	Hwed	Horder
1	Diff. Geometry f	68.5	2	249	0.2	0.02	18.5	3
2	Diff. Geometry f	76	1.9	189	0.15	0.02	18.5	2.8
3	Diff. Geometry f	79	1.804	171	0.15	0.02	18.5	2.3

Figure 4.16: ROXIE input-file of the MQXF\_V2 return end, outer layer.

Block Data 2D											
No	Type	NCab	R	$\phi$	$\alpha$	Current	Cable name	N1	N2	Imag	Turn
1	Cos	15	94.313	0.22782	0	-15310	XF145HTH5	1	1	0	0
2	Cos	1	94.313	16.9004	5.9907	-15310	XF145HTH5	1	1	0	0
3	Cos	8	94.313	19	20.8049	-15310	XF145HTH5	1	1	0	0
4	Cos	4	94.313	27.8448	23.9999	-15310	XF145HTH5	1	1	0	0
5	Cos	15	94.313	1.3329	0.3994	15310	XF145HTH5	1	1	1	90
6	Cos	1	94.313	19	20.8049	15310	XF145HTH5	1	1	1	90
7	Cos	8	94.313	20.1054	21.2043	15310	XF145HTH5	1	1	1	90
8	Cos	3	94.313	28.9526	24.3993	15310	XF145HTH5	1	1	1	90
9	Cos	1	94.313	32.4347	25.5974	15310	XF145HTH5	1	1	1	90

More options :			
No	String	N/a	N/a

Block Data 3D									
No	Type	$\beta$	$B_0$	$z_0$	$W_1$	$W_0$	Hvcd	Order	
1	Diff. Geometry f	68.5	2	380	0.2	0.02	18.5	3	
2	Diff. Geometry f	72	1.95	364	0.15	0.02	18.5	2.9	
3	Diff. Geometry f	76	1.9	328	0.15	0.02	18.5	2.8	
4	Diff. Geometry f	80	1.788	310	0.15	0.02	18.5	2.3	
5	Diff. Geometry f	80	2.042	310	0.15	0.02	18.5	2.5	
6	Diff. Geometry f	79.9968	2.042	311.996	0.15	0.02	18.5	2.5	

Figure 4.17: ROXIE input-file of the MQXF\_V2 lead end, outer layer.

## 4.2.2 Study of Integrated Field Harmonics

The objective is to have an integrated multipole content lower than the random components, defining the integrated multipole content as

$$\bar{b}_n = \frac{\int_{-\infty}^{+\infty} B_n(I, z) dz}{B_2^{ss} l_{mag}(I)}$$

where  $B_n$  follows the convention

$$B_y + iB_x = \sum (B_n + iA_n)(x + iy)^{n-1},$$

$B_2^{ss}$  is the main field in the straight section and  $l_{mag}$  is the magnetic length defined as

$$l_{mag}(I) = \frac{1}{B_2^{ss}(I)} \int_{-\infty}^{+\infty} B_2(I, z) dz.$$

Integration limits are  $\pm\infty$  when providing the total integral of the harmonic content. The contribution of each magnet end is also provided in a separate column in Table 4.5. As it can be observed, even if the integral of  $b_6$  over the connection side of 400 mm length is close to 9 units, the total integral is 0.32 units for Q1/Q3 and -0.07 units for Q2a/b. The rest of the harmonics are also summarized in the table, providing the local contribution on the magnet connection side (RE), non-connection side (LE) and the total integral. Only the harmonics where the end contribution is larger than 0.1 units are included in the table.

Table 4.5: Field Harmonics ( $R_{ref} = 50\text{mm}$ ).

	Straight part	Ends		Integral	
		RE	LE	Q1/Q3	Q2a/Q2b
Magnetic length	--	0.400	0.341	4.2	7.15
$b_6$	-0.640	8.943	-0.025	0.323	-0.075
$b_{10}$	-0.110	-0.189	-0.821	-0.175	-0.148
$a_2$	0.000	-31.342	0.000	-2.985	-1.753
$a_6$	0.000	2.209	0.000	0.210	0.124

### 4.2.3 Magnetic and Physical Lengths

In order to minimize the impact on beam dynamics of the reduction of the nominal gradient from 140 T/m to 132.6 T/m, the magnetic length has been increased by 200 mm for Q1/Q3 and by 350 mm for Q2a/b. Table 4.6 summarizes the magnetic and physical lengths of the coil, pad and yoke for MQXFS, for the 4.2-m length magnet (Q1/Q3) and for the 7.15-m length magnet (Q2a/Q2b).

Table 4.6: Magnetic length and physical lengths

Parameters	UNITS	MQXFS	Q1/Q3	Q2
Magnetic length at 1.9 K	mm	1196	4200	7150
Magnetic length at RT	mm	1200	4213	7172
Overall coil length at RT (including splice extension)	mm	1510	4532	7482
Magnetic yoke extension at RT	mm	1552	4565	7524
Magnetic pad extension at RT	mm	975	3988	6947
Cable length per coil	m	126	431	721
Cable unit length (including winding margin)	m	150	455	750

Changing the number of iron yoke laminations on the magnet's ends, the magnetic length will be affect.

The maximum increase of magnetic length we could achieve is around 18 mm (peak field enhancement on the coil ends of 0.4 T). The maximum decrease of magnetic length is around 23 mm (Figure 4.18).



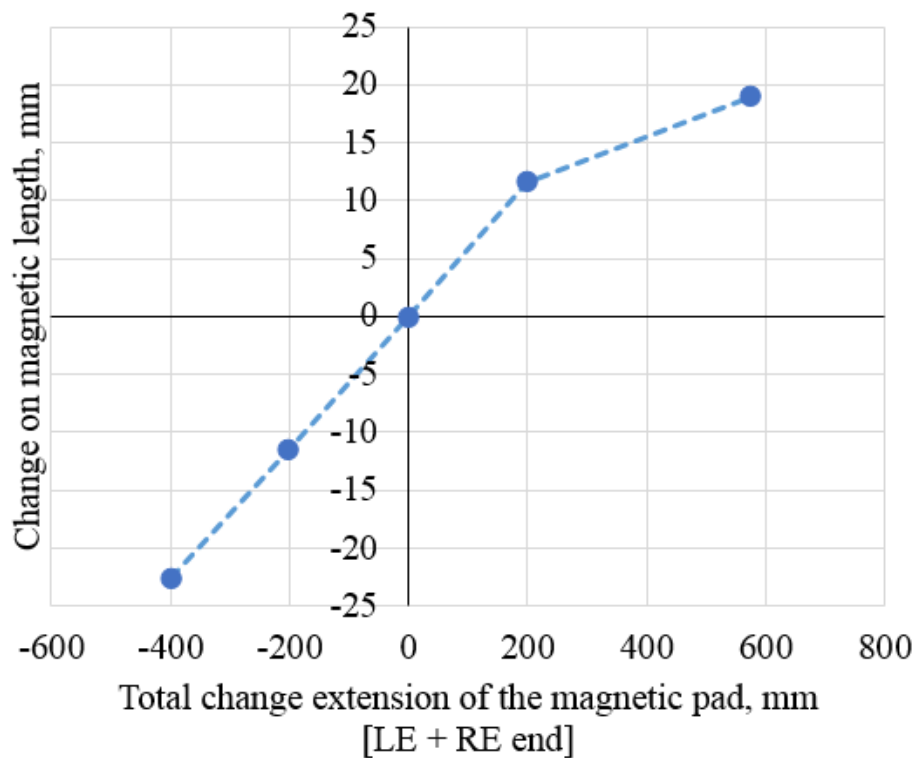


Figure 4.18: Magnetic length change respect to the extension of the magnetic pad change.

## 4.2.4 Fringe Field

The maximum field in a circular path 20 mm from the outer surface of the cryostat will be 0.0068T (Figure 4.19).

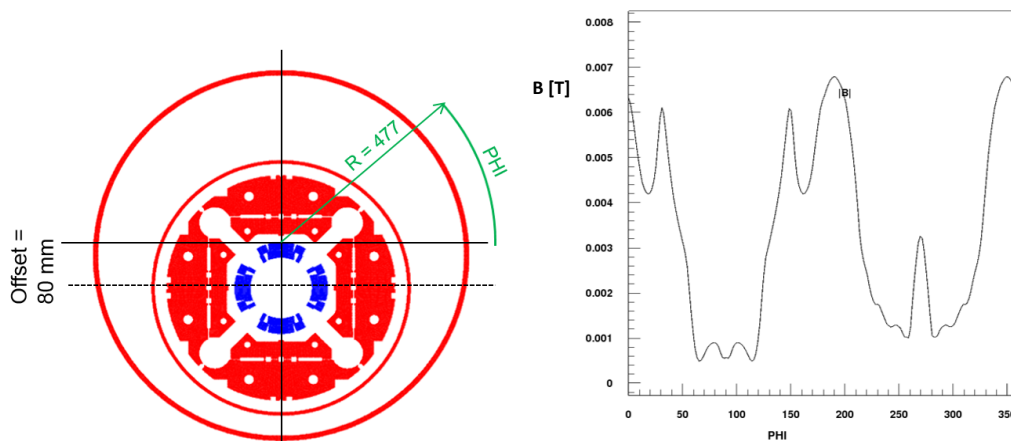


Figure 4.19: Magnetic field around the cryostat at 20 mm (function of the angle).

## References

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## 4.3 Structural Design

### 4.3.1 Design features and goals

The support structure of MQXF relies on an aluminum shell pre-stressed at room temperature with bladders and interference keys (i.e. bladder and key technology), which has been demonstrated in the previous successful series of LARP magnets such as HQ. The cross section of the structure of MQXF is a direct scale-up from the HQ models which featured a 120 mm aperture [1]. As shown Figure 4.20, the MQXF quadrupoles feature an aperture of 150 mm and provides a nominal field gradient of 132.6 T/m by utilizing Nb3Sn superconductor over a magnetic length of 4.2 m (MQXFA) and 7.15 m (MQXFB) at cold [2].

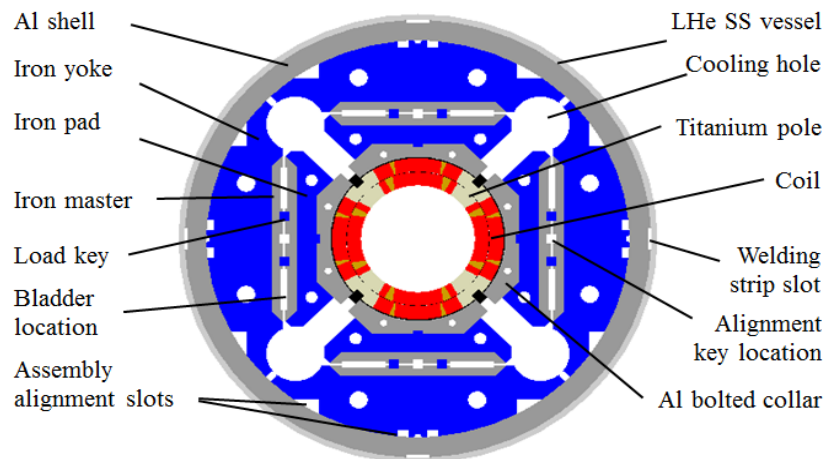


Figure 4.20: Cross section of the MQXF.

The design of the structure comprises an iron yoke assembly surrounded by a 29 mm thick aluminum shell, also includes four iron pads, and the coil-collar subassembly which includes four aluminum collars bolted around the coils engaged by the G11 pole alignment key. The yoke, pads and collars are made of thin laminations assembled with tie rods. Between each pad and yoke, there is master package per quadrant including two interference keys to balance the azimuthal tension in the outer shell with the azimuthal compression in the inner coils.

Maintaining contact between the coils and poles pieces at all stages is achieved by azimuthal load applied on the shell: it relies on a system of water-pressurized bladders and keys to apply a partial pre-load to coil-pack and to pre-tension to aluminum shell at room temperature. During the preload operation, the pressurized bladders open up the master pack and allow inserting the load keys with shims of the designed interference. The final pre-load is achieved during the cool-down phase, when the tensioned aluminum shell compresses the structure components because of its high thermal contraction.

Upon the magnetic design (see Section 2D Magnetic Design), the MQXFA magnet will experience a total Lorentz force in the axial (Z direction, parallel to the magnet's bore) direction on the order of 1.17 MN at nominal current. Axial pre-stress is therefore designed to withstand the total axial forces generated by the coil ends. Four tensioned steel rods within the yoke's cooling holes are connected to endplates to provide the pre-stress. As same as the radial pre-stress, the initial designed axial pre-stress is tuned as to counteract 0.2 MN at room temperature and 0.55 MN

after cool down (see Section *3D Results*)

In brief, the main features of the MQXF structural design are:

- (1) Shell-based support structure replying on “bladder and key” technology to perform azimuthal pre-loads, which allows reversible assembly process and tunable preload;
- (2) G11 alignment keys inserted into the pole pieces provide the coil alignment and intercept forces from the shell in pre-loading and cool-down;
- (3) The aluminum shell is segmented into sections to minimize axial tension in the shell and to ensure a uniform azimuthal load on the coil;
- (4) Axial pre-load is provided by four SS rods with a certain amount of pre-strain.

### 4.3.2 Graded Approach of Structural Analysis

Structural failure can occur via one of the followings:

- a) Plastic collapse typically associated with "tough" materials that yield in a smooth manner under the influence of large loads;
- b) Linear elastic fracture, typically associated with brittle materials under significant loads coupled with stress concentration factors such as defects or voids;
- c) Ductile tearing, i.e. materials subjected to a combination of the elements above.

MQXFA structural designs account the failures above by referencing ASME FFS-1 as a standard to accept use of nominally ‘brittle’ materials with assumed flaws. A graded approach [3] which is expected to yield structural designs that are safe for operation in the Large Hadron Collider is developed and used in MQXFA designs, shown in Figure 4.21, wherein the design criteria are evaluated using consecutively more advanced and detailed analysis as the component and load case are found to result in reduced margin with respect to relevant mechanical figures of merit.

Due to the complexity of the magnet design and the various load conditions encountered during fabrication, assembly, and operation, most structural elements of the MQXFA magnet are subjected to 2D and/or 3D FEA. At each grade level criteria are defined which, if FEA results exceeded, will trigger the next level of analysis and/or require modifications to the design.

The graded procedure consists of four levels analysis from ‘hand calculations’ to FEA, advance FEA to LEFM—in order of complexity. MQXFA structural design uses FEA for every structural component; In the grade I and II analysis, the FEA results will be evaluated with the material properties, parts could be reported to be satisfactory when the results meet Von Mises criteria; Grade III will be required when the results show stress singularity or concentration, or any other cases that exceed the Von Mises criteria. Grade IV analysis will be triggered when the material is brittle and indicates high stress in the structure. Associate with grade III and IV analysis, mitigations were performed as well to ensure the design is deemed appropriate.

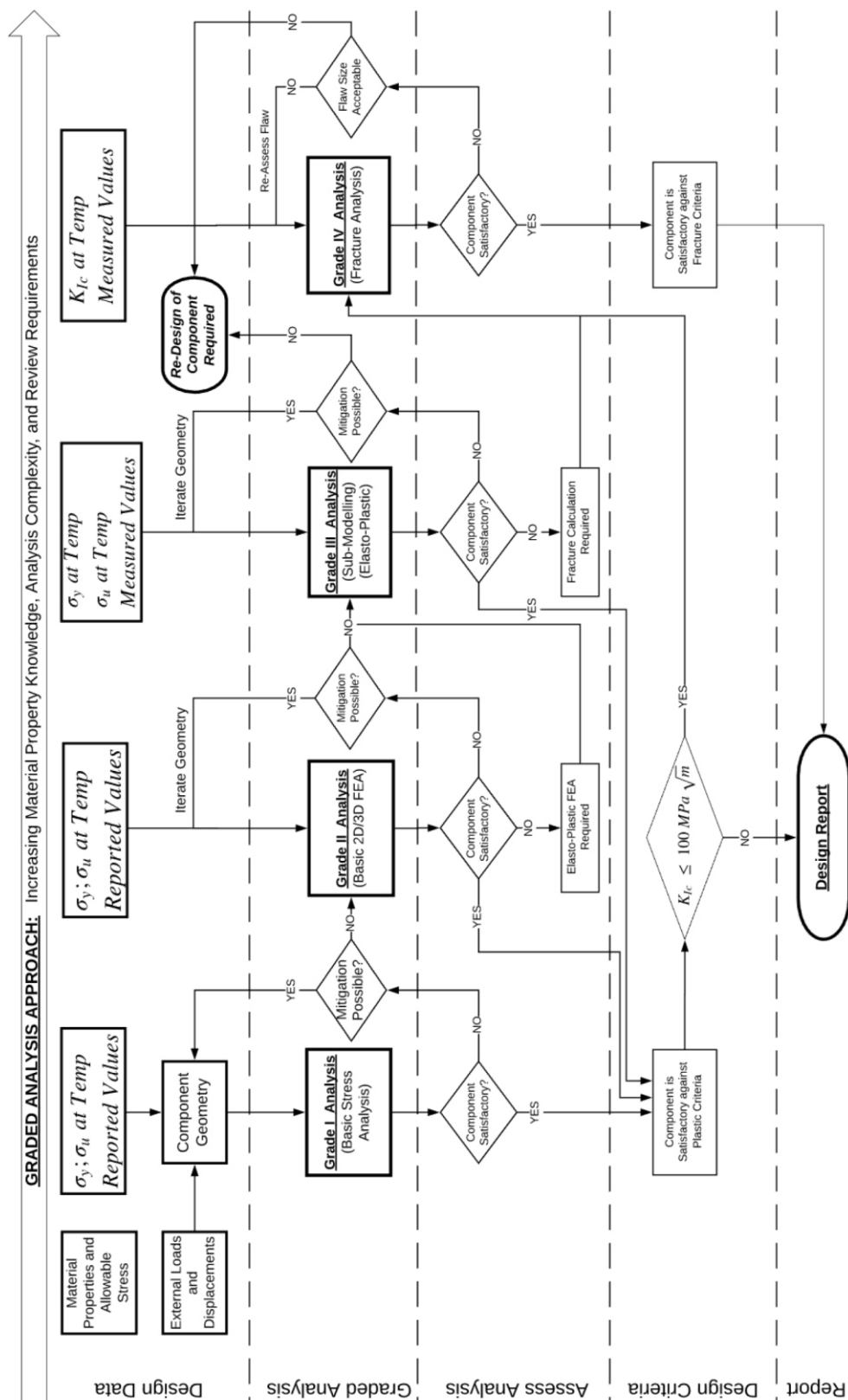


Figure 4.21: Schematic of Graded Approach to Analysis Procedures.

## 4.3.3 Grade II Analysis

### 4.3.3.1 Model Description

Standard ANSYS 2D/3D finite element models are used in grade II analysis. The ANSYS models' parameters are defined based on the experiences of the previous QXF magnets. The models are octant symmetric azimuthally. Each coil block, including cables, epoxy resin and fiberglass, is modeled as a homogenous object with average properties determined in [2]. The 2D model, as shown in Figure 4.22, employs high order 8-node element (plane183) for the main structures; uses elements of CONTA172 and TARGE169 to model the contact interfaces. The half-length 3D model (Figure 4.23) uses higher order 20-node elements (SOLID186) for all volumes. Similarly, 3D contact elements CONTA174 and TARGE170 with similar contact parameters are used in the 3D model. Every part inside a coil, in either 2D or 3D models, is bonded at all steps; frictional contact with frictional coefficient 0.2 was used at each interface of all the other components.

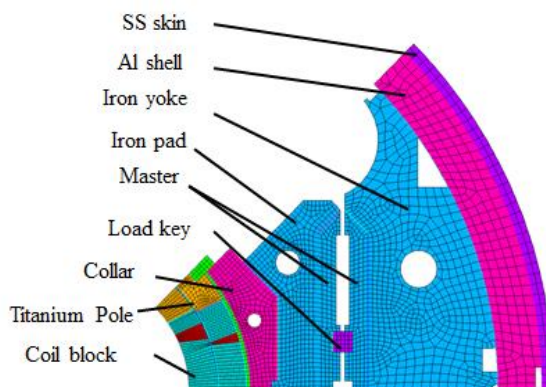


Figure 4.22: Mesh view of the 2D octant model (materials are displayed by colors).

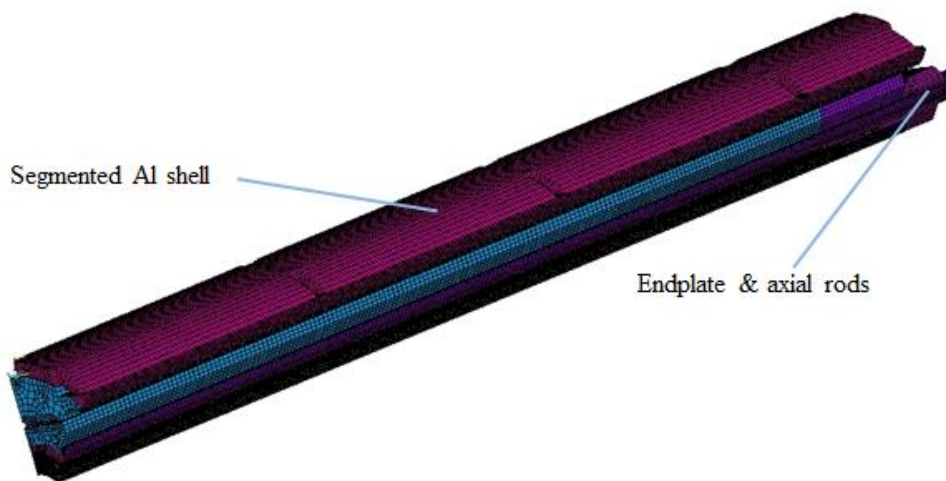


Figure 4.23: Mesh view of the 3D model (materials are displayed by colors).

Material properties used in the MQXFA design are shown in Table 4.7. The operation process was simulated by the following four steps as defined in [3] for MQXFAP1 magnet:

- A. Room-temperature load (load 1b) --- Azimuthal and axial pre-load at room temperature; The models utilize contact offset between load key / pad-master contact interface to



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simulate the azimuthal preload shims, and 3D model applies displacement on rod to simulate axial preload.

- B. Cool-down to 1.9 K: the temperature of all solids was changed from 300 K to 1.9 K.
- C. Operation (normal current of 16.47 kA): Import the coil from ROXIE to opera, and then compute forces in opera and import from opera to ANSYS.
- D. Operation (ultimate current of 17.89 kA): scale the imported Lorentz force to the level of ultimate current.

Table 4.7 Material Properties used in FE models

Materials	E at 293K	E at 4.2K	Poisson Ratio	Integrated thermal contraction (293K-4.2K)
	GPa	GPa		
Coil	20	20	0.3	3.88E-03
Aluminum bronze	110	120	0.28	3.24E-03
Aluminum 7075T6	70	79	0.34	4.20E-03
Iron	213	224	0.28	2.00E-03
G10 (normal direction)	10	10	0.3	7.30E-03
G10 (layer direction)	15	15	0.3	2.44E-03
Notronic 50	210	225	0.28	2.60E-03
Stainless Steel	193	210	0.28	2.90E-03
Titanium	115	125	0.3	1.70E-03

The analysis in this report focuses on the MQXFAP1 design as instance. The design of MQXFAP1 defined the azimuthal interference is 640  $\mu\text{m}$ , and the pre-tension on each rod is 580  $\mu\text{E}$ . (MQXFAP2 will use 750  $\mu\text{m}$  based on the test performance of MQXFAP1).

The computations in both the 2D and 3D (discussed in next section) models were carried out in light of the structural design criteria [3] and superconducting elements design criteria [4] (*detailed definition of the design procedures and calculation approaches could be found in [3] and [4], this report mainly focuses on the results computed in the work frame defined by the design criteria*):

- 1) Limit the coil peak stress to 120MPa at room temperature and 200 MPa at 1.9 K;
- 2) Coil axial stain remains below 0.2% with axial preload >50% of the full axial Lorentz force.
- 3) The coil preload is selected to maintaining contact between the coils and poles pieces up to the operating gradient. Localized tension up to 20 MPa at the pole-coil interface is acceptable provided that average compression is maintained across the pole width.
- 4) Maintain the stress in the support structure components within the material limits (Discussed in next section);



## 4.3.3.2 2D Results

Stresses in the coils have been computed and displayed in a cylindrical coordinate system. Azimuthal stress distribution is checked in the coil as shown in Figure 4.24. The coils are compressed from the bladder operation to cool-down; as mentioned above, the inner and outer layers at the coil/pole interface show an average tension of about 22 MPa when energized to the normal gradient. The maximum  $\sigma_\theta$  in coil is -94 MPa at room temperature; and -158 MPa after cool-down. Coil stress from the 2D computation is within the limit; more detailed coil stress will be further discussed in next section (*3D Results*).

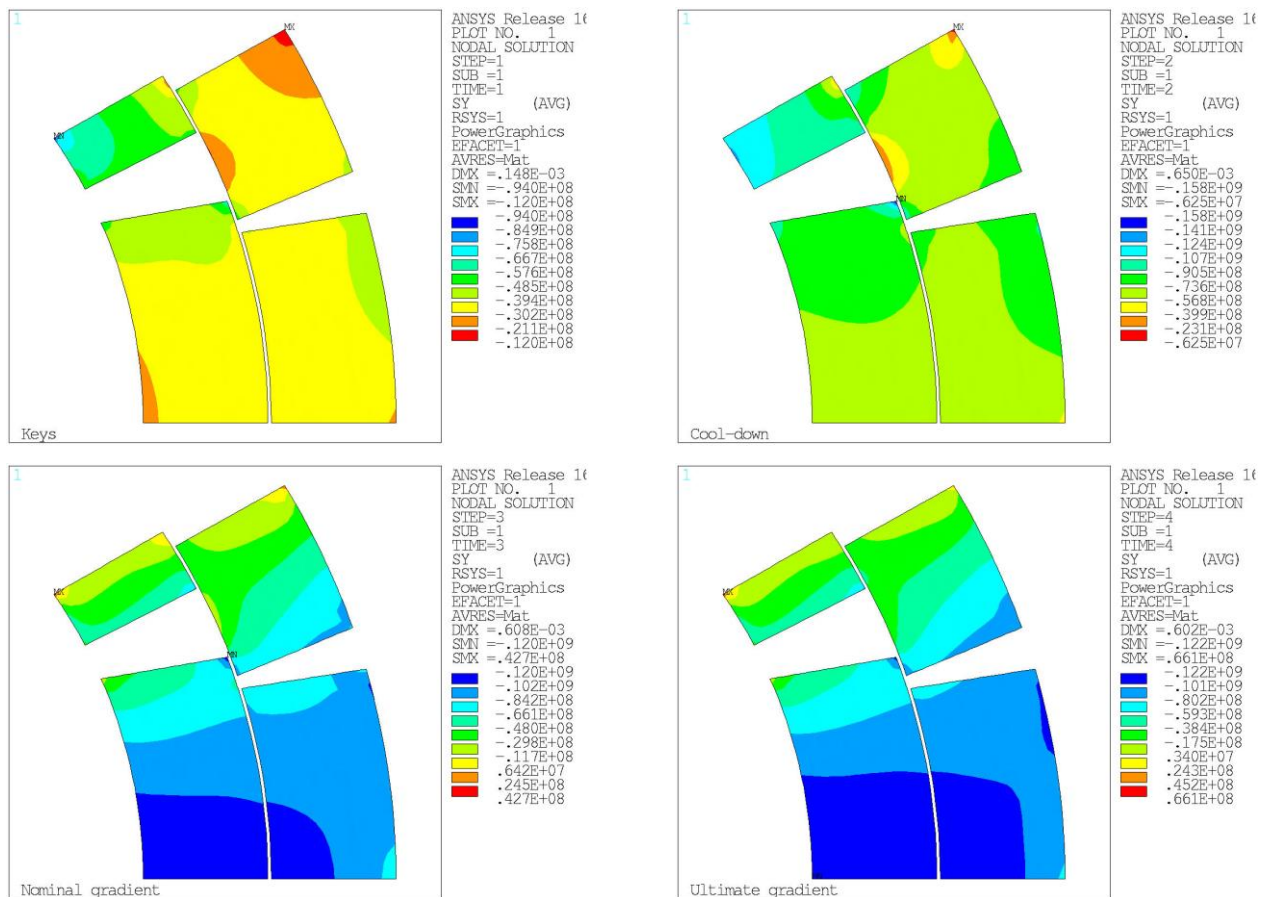


Figure 4.24: Azimuthal stress distribution of MQXFAP1.



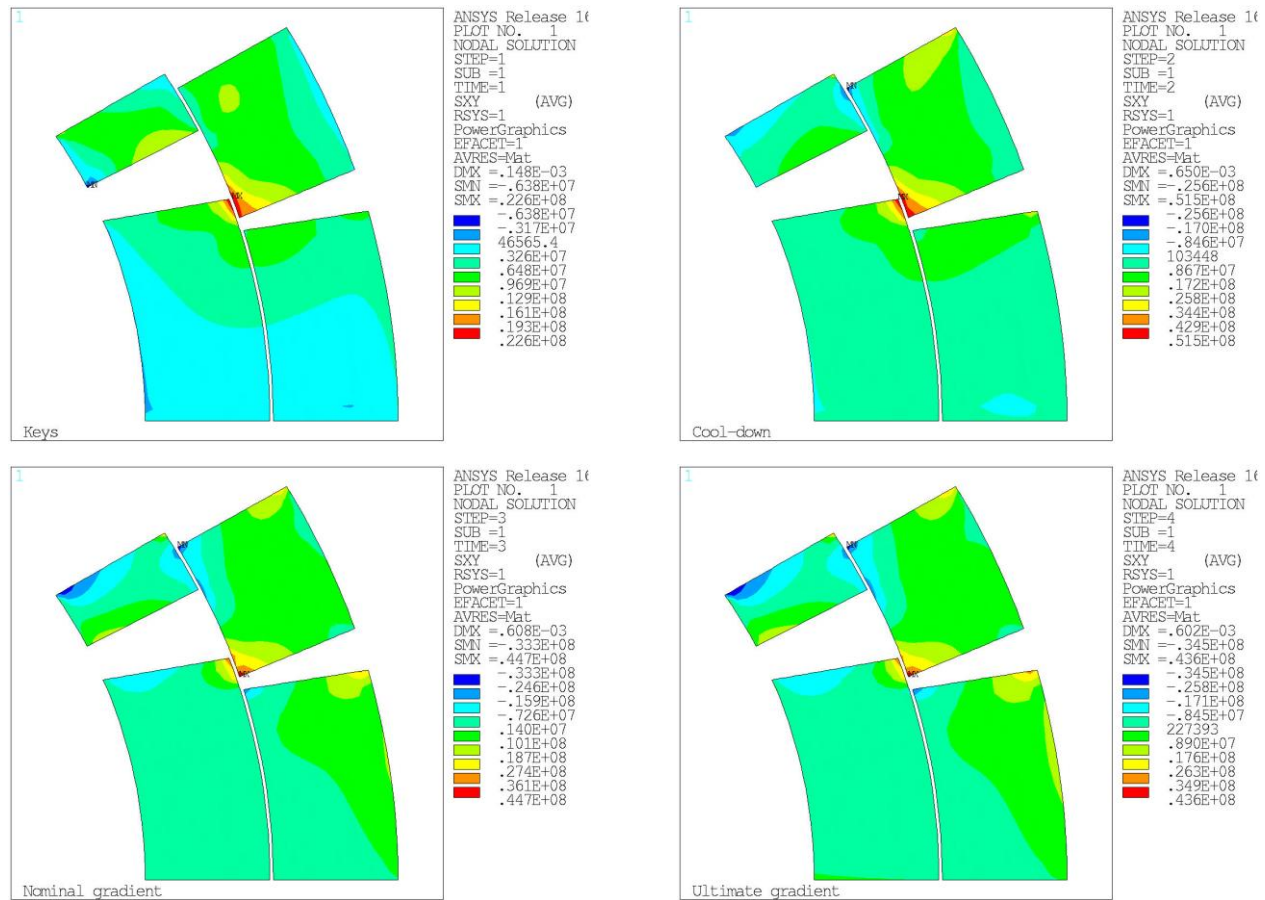


Figure 4.25: Shear stress distribution of MQXFAP1.

Shear stress in the coils after cooldown varies in the  $\pm 25 \sim 35$  MPa range with the exception of a few corners (the outer corner of layer 1 pole turn and the inner corner of layer 2 pole turn, (Figure 4.25). A peak shear stress of 51 MPa is observed after cool-down at the corners on the coil/wedge interface. According to measurements performed at 77K [5], the shear stress in side coil keeps in the acceptable range.

The 2D results (mainly coils) are close to the average stress, detailed analysis on the support structure (metallic parts) was performed with 3D results.

### 4.3.3.3 3D Results

The 3D model applies the same azimuthal interference of  $640 \mu\text{m}$  as the baseline. Axial preload is provided by pre-tensioning  $-580 \mu\text{e}$  on the axial steel rods.

The coil azimuthal stress over load steps is shown in Figure 4.26. Peak coil stress usually appears on the ends of the coil straight section. Compared with the 2D solution, the coil azimuthal stress reaches the maximum compression of  $-102$  MPa at room temperature after the bladder operations; and  $-165$  MPa at 1.9 K. When the coils are energized, the location of the peak coil stress moves from the pole-turn to the mid-plane, the magnitude also reduces to 125 - 127 MPa.

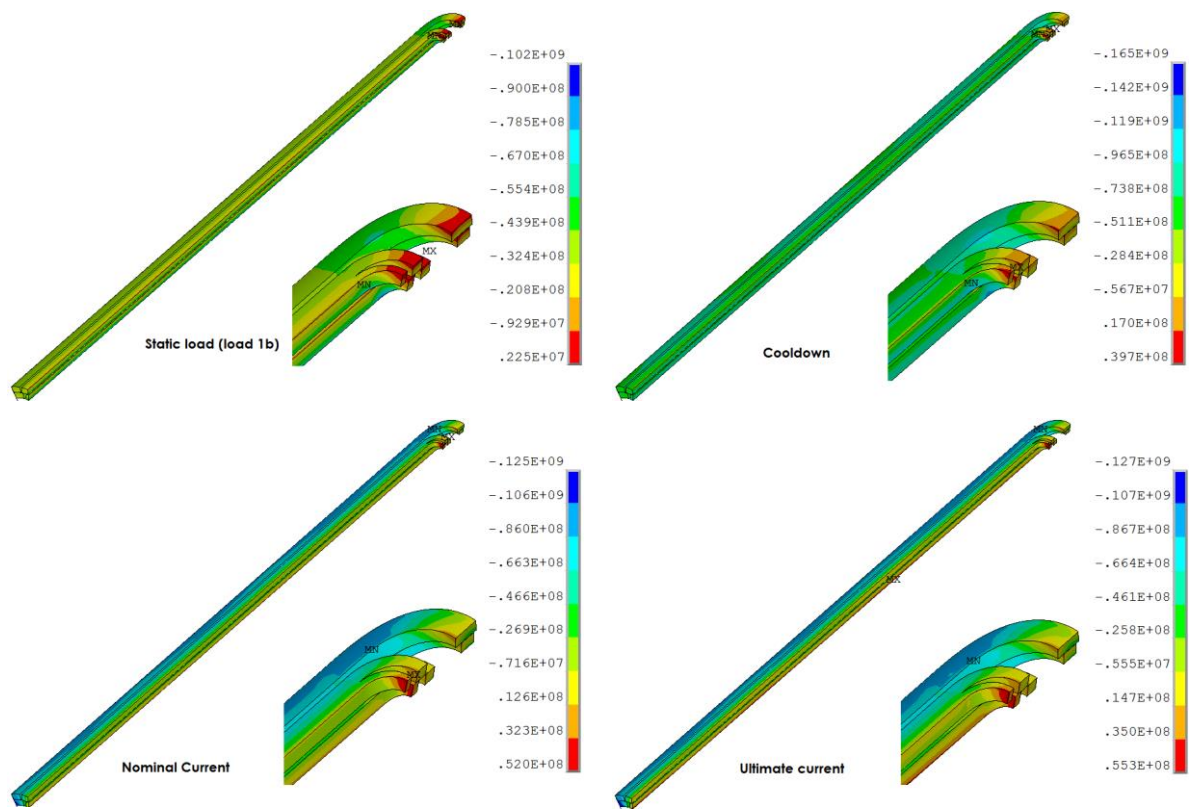


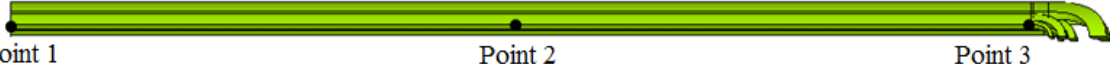
Figure 4.26: Coil azimuthal stress distributions (Unit: Pa)

The axial load that counteracts the axial Lorentz force of 1.17 MN on the coils is provided by four pre-tensioned 32 mm diameter steel rods and two Nitronic 50 end plates, which prevent the coils from detaching from the pole or end-spacers. Although the rods and plates were sized to accommodate the full axial load ( $F_z$ ), in the simulation the magnet was axially preloaded to only ~54% of this value due to friction forces between the coils and the support structures, which is based on previous experience on the HQ series.

The longitudinal strain in the coil straight section is listed in Table 4.8. It's dominantly affected by the difference of thermal contraction rate of coil blocks and Titanium poles. The coil stress and longitudinal strain of the baseline case are within the design criteria defined in [4].

Table 4.8 Longitudinal strain on coil straight section

Load steps	Point 1	Point 2	Point 3
Cooldown	0.180%	0.170%	-0.002%
Nominal Current (16.47 kA)	0.183%	0.176%	0.162%
Ultimate Current (17.89 kA)	0.184%	0.177%	0.191%



Point 1                      Point 2                      Point 3

The peak stresses in the metallic parts are listed in Table 4.9. Please note, ARMCO steel is ultra-low carbon steel with low very impurities produced by AK steel, was tested at CERN at both room temperature and 4 K. It shows purely brittle at 4 K thus no yield strength was determined.

From the Table 4.9, most of the structural components are within the yield limits; those parts can stop with a report after a successful Grade II analysis is completed. Shell and yoke clearly exceed their yield limits at either room temperature or 1.9 K. The peak stresses in the end shell and yoke locate at the cut-out inner corners, as shown in Figure 4.27, which are considered stress concentrations due to the sharp corners in the model.

Table 4.9 Peak stresses in the metallic parts

Part	Material	Principal Stress (MPa)		Von Mises Stress (MPa)		$\sigma_y$ (MPa)	
		293 K	1.9 K	293 K	1.9 K	293 K	1.9 K
Collar	Al 7075 [6]	-	-	121	273	420	550
SS Pad	SS 316 [6]	-	-	82	277	289	375
Iron Pad	ARMCO [7]	98	152	-	-	223	-
Yoke	ARMCO	246	306	-	-	223	-
Shell	Al 7075	280	610	320	573	420	550
Endplate	Nitronic 50	-	-	137	333	517	-

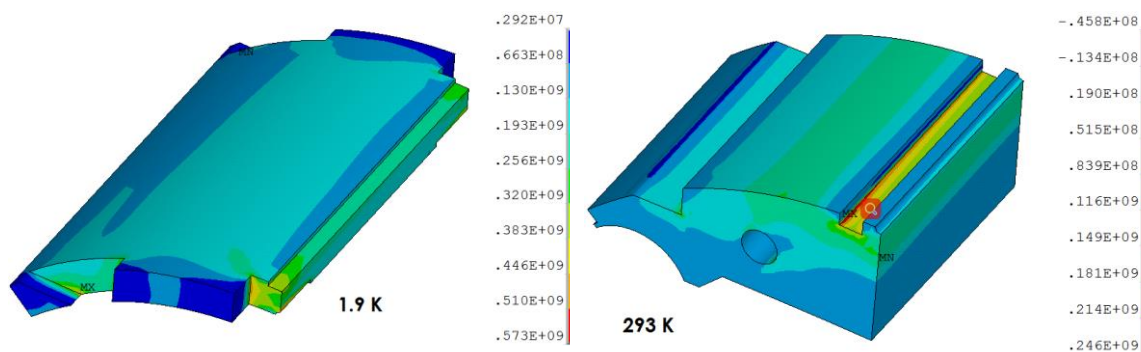


Figure 4.27: Peak Von Mises stress (Pa) in the end shell (Left) and peak principal stress (Pa) in yoke(Right)

The stress concentration can not readily resolved when increased the local mesh density; it usually means the model needs to include the actual geometry features such as fillets or chamfers. On the other hand, Al 7075 and ARMCO steel are considered as brittle material due to low fracture toughness. Therefore, the end shell and yoke need to be analyzed in Grade III with detailed features and mesh refinements, then Grade IV is also triggered for fracture assessment.

#### 4.3.4 Grade III Analysis

For components exhibiting stress concentrations that cannot be readily resolved via routine mesh refinement studies in the primary FEA model, sub-modeling was employed to evaluate the stress distribution around the particular concerning area.

Sub-model is a separate finite element model of the local region of interest, which imposes displacements on the cutting boundaries from the original model. The basis of a sub-model is St. Venant's principle when picking the cutting boundary locations from the original model.

Use the end shell for instance: Figure 4.28 illuminates the verification of the end shell sub-model. The Von Mises stress on the picked locations of the cutting boundary has compared with the stress on the same locations of the original model. The agreement of the two sets of stress indicates that the cutting boundaries are remote enough to meet St. Venant's principle.

Same verification process has been performed on the yoke sub-model.

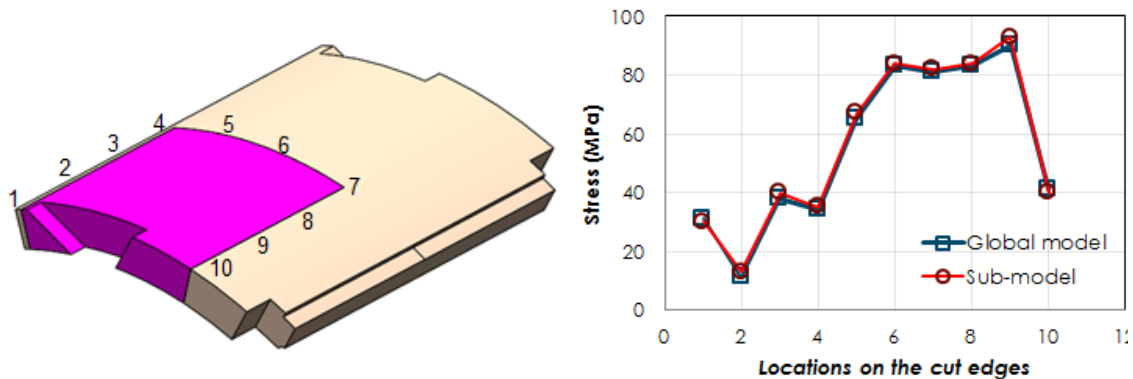


Figure 4.28: End shell sub-model verification

#### 4.3.4.1 End shell sub-model results

Once the sub-model has been verified, mesh refinements have been performed on the sub-model. There are additional cases with different fillet sizes were performed for the end shell as well.

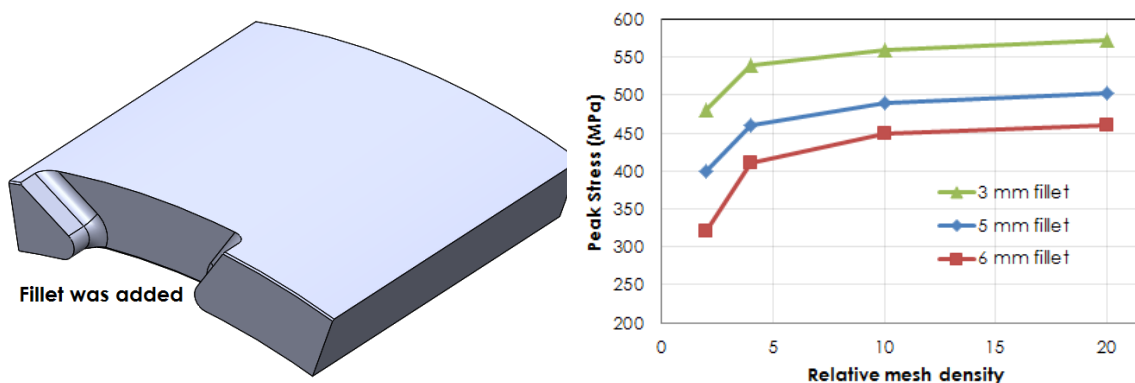


Figure 4.29: End shell sub-model (left) and Peak Von Mises stress at 1.9 K vs. relative mesh density (right)

The initial elements size in the original model was 8 mm. The mesh refinement studies (Figure 4.29) show the peak stress in end shell increases and converges finally with increased the mesh density. Thus, the following studies then used relative mesh density of 10 (element size 0.8

mm). Elasto-plastic study has been performed for the end shell sub-model at 1.9 K to obtain the plastic zone size.

Fillet certainly reduces stress concentrations at the local corner; the peak stress decreases to 490 MPa with 5 mm fillet at 1.9 K, which dropped within the yield limits of 550 MPa for Aluminum 7075.

Although there was no plastic deformation occurred with 5 or 6 mm fillet, Grade IV analysis will be performed due to low fracture toughness of Al 7075.

#### 4.3.4.2 Yoke sub-model results

The yoke is considered brittle at room temperature and 1.9 K according to the test results conducted by CERN [7]. But it still shows yielding point at room temperature. Sub-model was used to determine the plastic deformation and the stress on the likely path if part-through a crack presents itself. Similarly, the yoke sub-model also includes different fillet radiuses (Figure 4.30).

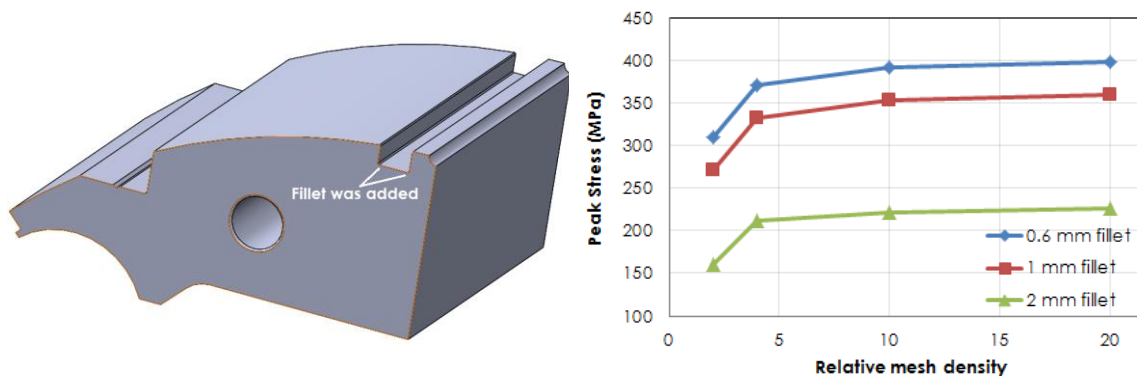


Figure 4.30: Yoke sub-model (left), Peak principle stress at room temperature vs. relative mesh density(right)

The initial elements size of the yoke was 6 mm. As shown in Figure 4.30, the mesh refinement studies show that the peak stress at room temperature in the yoke has similar trends as seen in end shell sub-model. It converges finally once the mesh density larger than 10. Thus, the following studies then used relative mesh density of 10 (element size 0.6 mm). Elasto-plastic study has been performed for the yoke sub-model at room temperature.

Adding a fillet lowers the peak stress at the corner, too; however, plastic deformation still occurs at room temperature. As a fracture dominated material, the yoke will be analyzed in Grade IV to determine the plastic deformation and load factor with fillets.

#### 4.3.5 Grade IV Analysis

Grade III analyses for the end shell and yoke show that fillets around the corner are recommended. As defined in the work flow (Figure 4.31), end shell and yoke will be analyzed in grade IV.

Grade IV analysis will determine if their load factor meet the design criteria with different fillet sizes. The approach in this grade relies on the R6 FAD (Failure Assessment Diagram) [8], captures failure by LEFM (elastic fracture), and plastic collapse simultaneously.

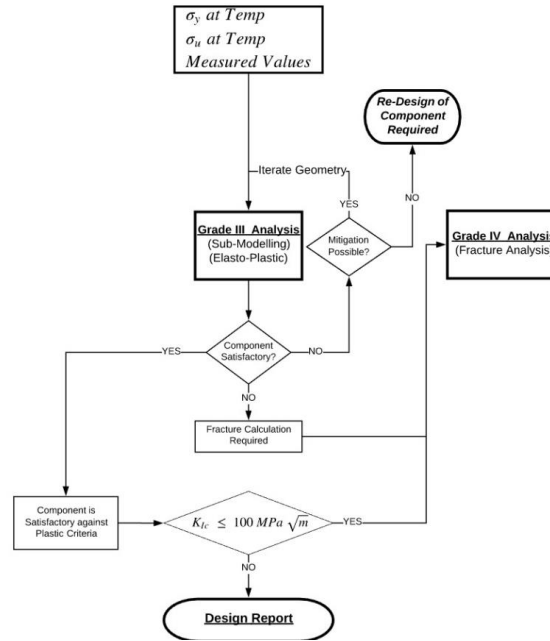


Figure 4.31: Flow chart describing procedure from Grade III to Grade IV

For the purposes of design, semi-elliptic part-through cracks are assumed with flaw features intersecting and centered on the components surface as these typically have the highest stress intensities. The major process of fracture analysis is to determine the applied stress intensity  $K_I$ . For part-through cracks subject to primary stresses,  $K_I$  can be written in the following form:

$$K_I = F\sigma(x) \sqrt{\frac{\pi a}{Q}} \quad (4-1)$$

$$Q = 1 + 1.464\left(\frac{a}{c}\right)^{1.65} \quad (4-2)$$

where  $a$  and  $c$  are the elliptical radius of a crack,  $F$  is geometry constants that can be obtained from FEA or published data.  $\sigma(x)$  can be approximated as a cubic expansion of a load profile extracted from an unflawed elastic analysis in the direction of assumed crack propagation through part thickness  $x = a$  direction.  $F\sigma(x)$  can be approximated as:

$$F\sigma(x) = \sum_{i=0}^3 G_i A_i x^i \quad (4-3)$$

where  $G_i$  is shown in [10] appendix A.2;  $A_i$  is the curve-fitting coefficient. The stress on the path of assumed crack propagation has been defined in the end shell and yoke sub-models. The path direction of a crack growth is normal to the max. principal stress and in the most energetic direction (the direction of lowest stress gradient).

#### 4.3.5.1 End shell fracture analysis at 1.9 K

Use the path as described above, the total Von Mises stresses on this path of the end shell with different fillets at 1.9 K are shown in Figure 4.32, because the end shell did not yield at room temperature, the analysis focuses on the stress at cold.



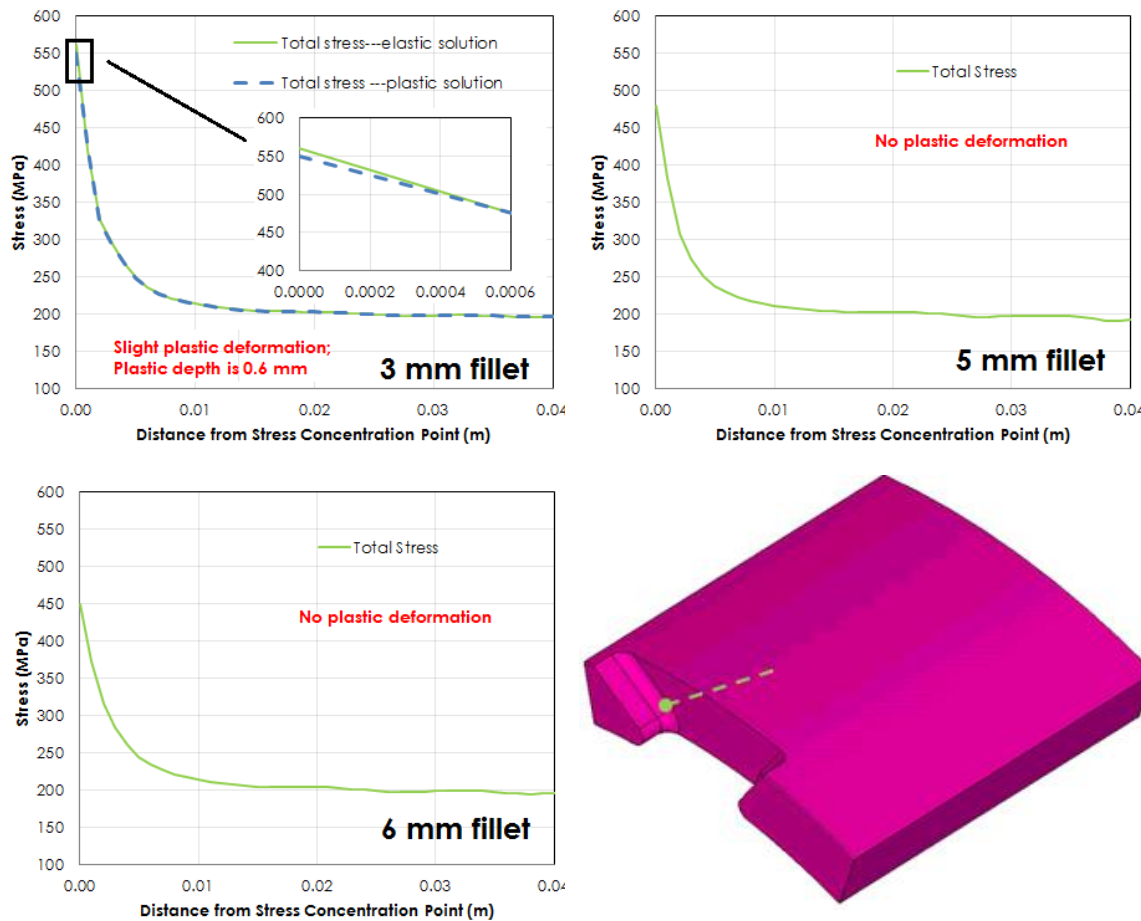


Figure 4.32: Total stress on the path of a crack is most likely to propagate

The local stress concentration results in local plastic deformations that limit the effective stress state. The fully elastic analysis will coincide with the elasto-plastic model at some distance from the structural discontinuity. The distance to the coincidence is considered as the plastic depth on the defined path. With 3 mm fillet, plastic deformation occurred around the stress concentration area, results in a 0.6 mm plastic depth along the path; the peak stress dropped when increasing the fillet radius.

Take the total stress illustrated in Figure 4.32 and a given crack length, the “load point” of each case can be determined in FAD. Load points inside of the FAD curve are safe from failure, load points falling outside or on the curve may fail. Each load point determines a “load line” by connecting the original point. The load factor in the plot is defined as:

$$\text{Load factor} = \frac{L}{L'} \quad (4-4)$$

where  $L$  is the length from the original point to the load point;  $L'$  is the length from the original point to the “projected load point”, which is the intersection of load line and the FAD curve. A flaw is considered critical in size if its Load Factor is unity.

The critical flaw sizes at 1.9 K for 5 mm fillet is 2 mm. Accordingly, critical flaw sizes are 1.6 mm and 2.5 mm for 3 mm and 6 mm fillet end shell, respectively. Assuming 2 mm crack started at the stress concentration spot, the load points in FAD of the stress concentration area of different cases can be seen in Figure 4.33.

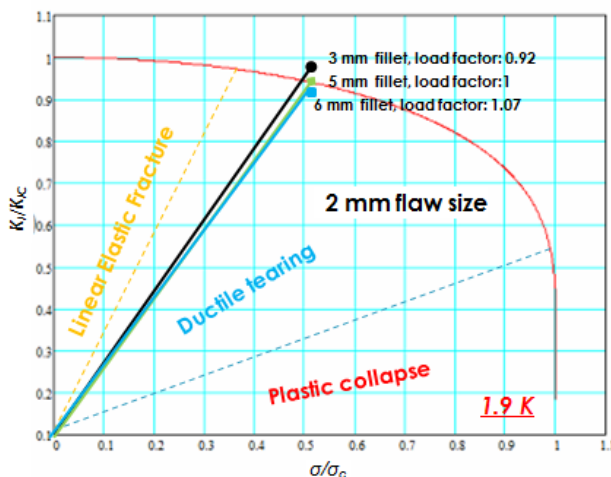


Figure 4.33: FAD for 2 mm crack in stress concentration area of end shell with different fillet sizes

The plastic deformation depth in the case of 3 mm fillet is less than the critical flaw size of 1.6 mm, thus the plastic deformation will not affect the crack propagation. However, according to the flaw sizes correlated to Inspection Grades for Aluminum Forgings [11], if a flaw is 2 mm, an inspection Class of “AA” is required; a higher Class of “AAA” is required if a flaw is less than 1.77 mm.

Based on the calculations above, the end shell cut-out corners were rounded up to 5 mm fillet radius, each batch of the forging material will be inspected in the Class of “AA”. Please note that the load factor of 1 is only at this stress concentration area, load factor in the major part of shells are larger than 1.4.

## 4.3.5.2 Yoke fracture analysis results

The yoke yields at the notch corner at room temperature in the cases of fillet radius from 0.6 mm to 2 mm. The path of a crack likely grow along on the yoke is shown in Figure 4.34, pointing to the tie-rod hole.

Figure 4.35 shows the total stress on the path at room temperature. The yield depths at room temperature of the cases are 2.1 mm and 0.8 mm for 1 mm and 2 mm fillet radius, respectively.



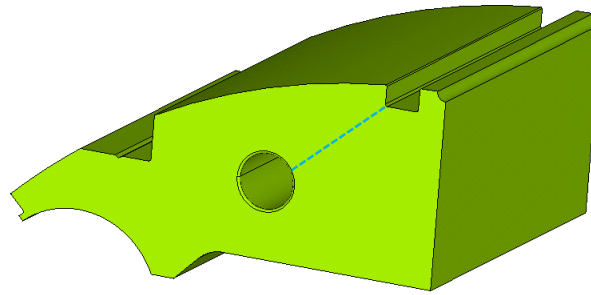


Figure 4.34: Path of a crack is most likely to propagate on yoke

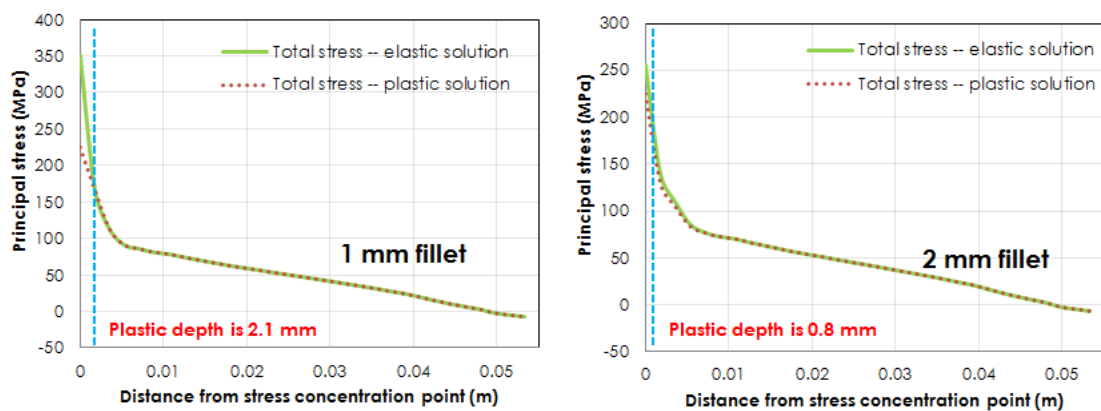


Figure 4.35: Total stress on the path at room temperature

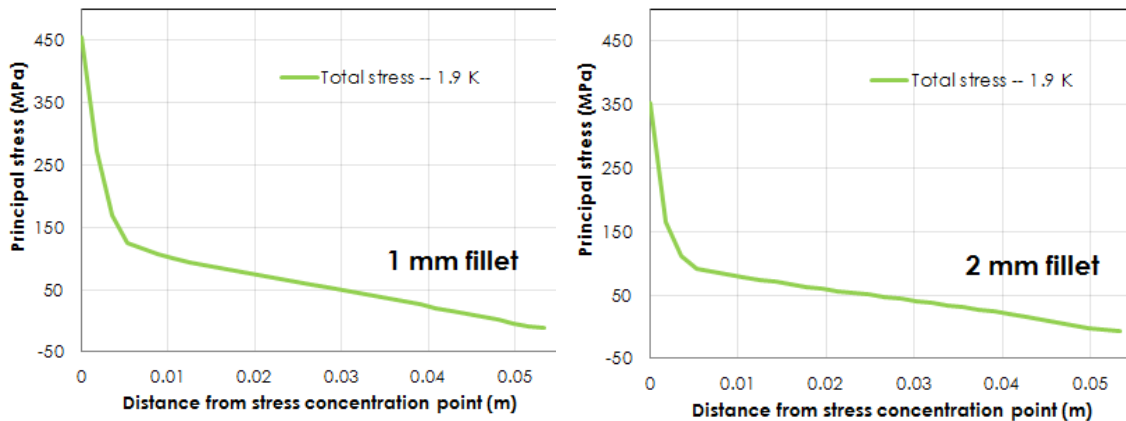


Figure 4.36: Total stress on the path at 1.9 K

Use the total stress illustrated in Figure 4.35 and Figure 4.36, the critical flaw sizes for 1 mm fillet case are calculated as 8.6 mm and 5.5 mm at room temperature and 1.9 K. The plastic zone seen on yoke is much smaller than the critical flaw size.

The FAD of yoke is shown in Figure 4.37 when use 5 mm flaw size to check the yoke. For all the cases of 1 mm and 2 mm fillets, the load points of yoke are within the envelope of the FAD, which indicates that 2 mm fillet will be adequate for yoke at both room temperature and 1.9 K.

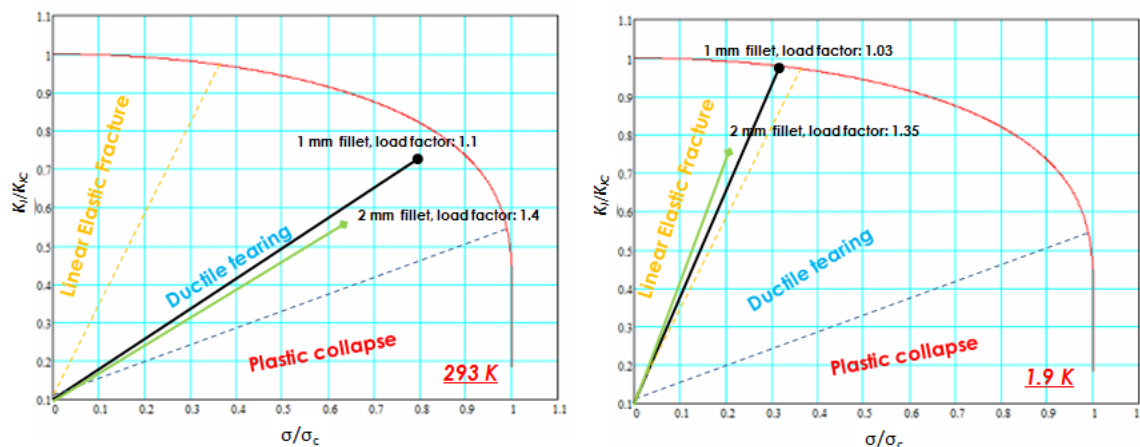


Figure 4.37: FAD for 5 mm thumbnail crack in end shell with different fillet radii

With 2 mm fillet radius, the load factor at both room temperature and 1.9 K are about 1.4.

## 4.3.6 Peak Stresses in MQXFAP2

MQXFAP2 will have an azimuthal preload target of 750  $\mu\text{m}$  interference at room temperature; which increases by 17.2% compared with MQXFAP1. The axial preload of MQXFAP2 will remain the same as applied in MQXFAP1.

Table 4.10 lists the peak azimuthal stress of coils abstracted from the models of MQXFAP1 and MQXFAP2. The alignment G11 pole key used in MQXFAP1 is only for the coil straight section; the coil stress can be lowered by extending the pole to the same length of the entire coil. Therefore, MQXFAP2 intends to use the full length pole key. The coil peak stress predicted by the MQXFAP2 model is certainly higher than that from MQXFAP1, but it's within the design criteria of superconducting elements.

Table 4.10 Peak coil azimuthal stress of MQXFAP1 and MQXFAP2

	MQXFAP1	MQXFAP2
293 K	-101	-110
1.9 K (on entire coil, keys for straight sections)	-164	-180
1.9 K (on entire coil, full length key)	-157	-174

Table 4.11 lists the peak stresses in metallic parts abstracted in MQXFAP1 and MQXFAP2. Most of the parts are still within the yielding limits. Higher peak stresses are foreseen in the shell and yoke. The peak stresses increase by 13% maximally in the shell and yoke. The redesign of the corresponding parts still applicable for MQXFAP2.



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Table 4.11 Peak stresses in the metallic parts of MQXFAP1 and MQXFAP2

Part	Principal Stress (MPa)				Von Mises Stress (MPa)			
	293 K		1.9 K		293 K		1.9 K	
	MQXFAP1	MQXFAP2	MQXFAP1	MQXFAP2	MQXFAP1	MQXFAP2	MQXFAP1	MQXFAP2
Collar	-	-	-	-	121	162	273	276
SS Pad	-	-	-	-	82	98	277	286
Iron Pad	98	119	152	154	-	-	-	-
Yoke	246	255	306	311	-	-	-	-
Shell	280	320	610	635	320	329	573	610
Endplate	-	-	-	-	137	140	333	335

## 4.3.7 Conclusion

The MQXFAP1 has been designed according to the structural design criteria [3],[4]. The coil stress and strain has been evaluated in both 2D and 3D finite element models, and the results meet the requirements defined in [4].

The structural metallic parts have been designed in light of a graded approach designed in [3]. Most of the structural components meet the design criteria at grade II level; End shell and yoke presented stress concentration in Grade II analyses, Grade III and Grade IV then were performed. The analysis suggests adding fillets on the cut-out corners of these components. The end shell eventually added 5 mm fillet on the corner; and yoke added 3 mm fillet. The load factors of the shells and yokes are at least 1.4 after the adding the fillets.

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## 4.4 Radiation Effects

Proton-proton collisions at 7 TeV generate about 120 secondary particles per interaction. Many of these particles, and their decay products, are intercepted by the detector components. However, those emitted at small angles with respect to the beam direction exit the detector region through the TAS, a 60 mm aperture, 1.8-m long absorber located at 20 m from the IP. While less than 10% of the secondary particles cross the TAS, they carry a large fraction of the total energy, resulting in 3.8 kW of power on each side of IP1 and IP5 at the nominal HL-LHC luminosity of  $5 \times 10^{34} \text{cm}^{-2} \text{s}^{-1}$ . This has a critical impact on both thermal loads and radiation dose to the IR quadrupoles.

The protection strategy of the IT magnets is centered on a tungsten absorber placed in the magnet bore between the beam pipe and the coil. The absorber is mounted on the beam screen, which is made of stainless steel and has an octagonal shape. This assembly allows both shielding the cold mass from a large fraction of the secondary particles, and collecting their energy at a higher temperature, reducing the heat load on the 1.9K system.

Detailed simulations of the radiation load for HL-LHC were carried out using FLUKA at CERN [1-2] and MARS at Fermilab [3-4]. Both codes have been extensively used and validated in past studies for LHC and many other applications. Both FLUKA and MARS simulations used identical models of the HL-LHC machine geometry and materials, and the results are in close agreement. A comprehensive analysis of the radiation effects for the High Luminosity LHC is reported in [5] and references therein. Details of the IR quadrupole model are shown in Figure 4.38.

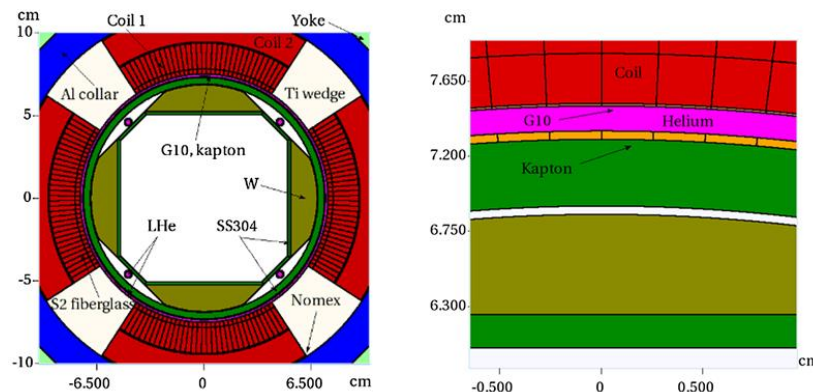


Figure 4.38: Details of the model used both in FLUKA and MARS for the inner region of the IR quadrupole Q1 (in Q2-Q3 a thinner tungsten absorber is used). [5]

The power density and dynamic heat load are normalized to a luminosity of  $5 \times 10^{34} \text{cm}^{-2} \text{s}^{-1}$ . The absorbed dose, neutron fluence and DPA are normalized to an integrated luminosity of  $3000 \text{fb}^{-1}$ . Figure 4.39 shows the longitudinal profile of the peak power density on the inner coils of the IT magnets. The peak value in the  $\text{Nb}_3\text{Sn}$  quadrupoles is  $2 \text{ mW/cm}^3$ , considerably lower than the quench limit at the operating point. For the total length of the cold mass, the average dynamic heat load on it is  $\sim 14 \text{ W/m}$ . This is within a design range of 10–15 W/m used for the LHC and assumed for the HL-LHC.

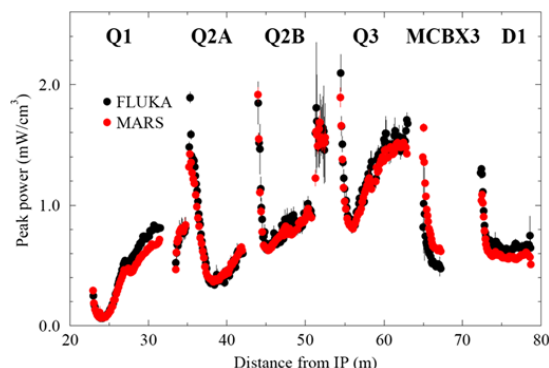


Figure 4.39: Longitudinal peak power density profile on the inner coils of the IT magnets [5].

Figure 4.40 shows the longitudinal profile of peak dose on the inner coils and insulating materials. Thanks to the increased aperture and tungsten absorbers, the dose in the HL-LHC inner triplet at  $3000 \text{ fb}^{-1}$  is comparable that of the present LHC at  $300 \text{ fb}^{-1}$ . The peak dose in the insulation reaches 28-30 MGy. The results of a detailed characterization of the radiation resistance of the ceramic epoxy used for MQXF are reported in [6]. The materials have been irradiated with 50 MGy, using 4 MeV electron beam at 77 K which well reproduces the expected radiation spectrum for the IR magnet case. The electrical strength of the irradiated samples was found to be between 45 kV/mm and 65 kV/mm, which is still significantly higher than the required 5 kV/mm. This provides adequate margin for the HL-LHC integrated luminosity target. Further studies of the beam screen and absorber configuration are underway to guide the engineering design incorporating all details required for fabrication and installation of these components.

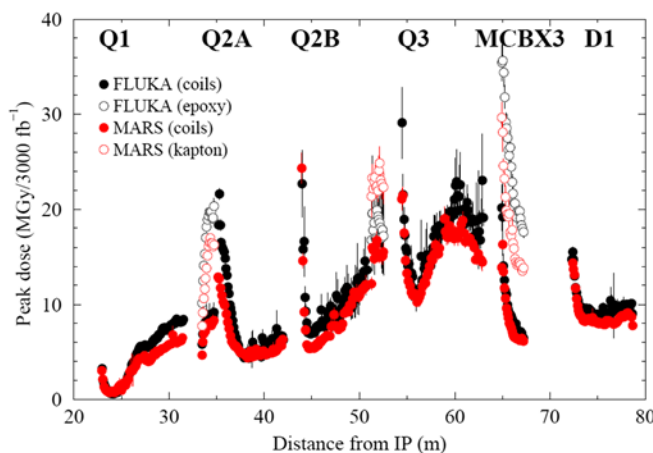


Figure 4.40: Longitudinal peak dose profile on inner coils and nearby insulators. [5]

The radiation effect on  $\text{Nb}_3\text{Sn}$  superconductor, copper stabilizer and structural components is best characterized by integrated neutron fluence and DPA over the expected magnet lifetime. Figure 4.41 shows the corresponding profiles on the quadrupole inner coils, where the peaks are located.

The highest DPA is about  $2 \times 10^{-4}$  DPA per 3000 fb<sup>-1</sup> integrated luminosity, which is acceptable for the superconductor. A similar conclusion can be reached by comparing the neutron fluence in the coils with the known limits. In the quadrupole coils, the peak fluence is  $\sim 2 \times 10^{17} \text{ cm}^{-2}$  which is substantially lower than the  $3 \times 10^{18} \text{ cm}^{-2}$  limit used for the Nb<sub>3</sub>Sn superconductor. The integrated DPA in the magnet mechanical structures is 0.003 to 0.01 in the steel beam screen and tungsten absorber,  $\sim 10^{-4}$  in the collar and yoke, and noticeably less outside. These are to be compared to a  $\sim 10$  DPA limit for mechanical properties of these materials. Neutron fluence in the IT mechanical structures range from  $3 \times 10^{16} \text{ cm}^{-2}$  to  $3 \times 10^{17} \text{ cm}^{-2}$  compared to the  $10^{21} \text{ cm}^{-2}$  to  $7 \times 10^{22} \text{ cm}^{-2}$  limits.

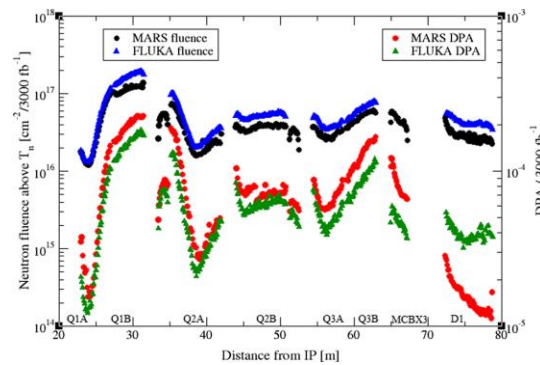


Figure 4.41: Longitudinal peak neutron fluence and peak DPA profiles along the hottest regions in the IT magnet coils [5].

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## 4.5 Thermal Design

The final focusing magnets will receive a heat load due to debris coming from the adjacent particle interaction points: the computed peak heat deposition in the coil is of the order of  $7 \text{ mW/cm}^3$  ([1], [2]).

The cooling method is based on the one used in the present LHC, and the overall cryogenic infrastructure needed is similar to the existing configuration. The cooling performance is evaluated in terms of temperature margin of the magnets under full steady state heat load conditions, and in terms of local maximum sustainable load.

An annular gap, filled with He, separates the cold bore from the superconducting coil, which is surrounded by the mechanical support structure to form the cold mass. The cold-mass is enclosed in a vessel, to be kept at the chosen operating temperature and supported in a vacuum insulated cryostat. This section is focused on the cooling configuration specific to the cold mass.

The heat loads due to debris from the adjacent interaction point are intercepted at two distinct magnet locations and temperature levels. A first heat intercept is on tungsten absorbers which are placed inside the beam pipe vacuum and which will be cooled in the 40 K to 60 K range. The remaining heat load will fall on the cold mass volume comprised of the yoke, collars and coils. For the purpose of the evaluation of the cooling, the heat load to the cold masses is taken at 1050 W for an ultimate luminosity of  $7.5 \times 10^{34} \text{ cm}^{-2} \text{ s}^{-1}$ .

### 4.5.1 Cooling requirements for magnet cold masses

The cooling principle, depicted in Figure 4.42 is an evolution of the one proposed for the LHC-Phase-I Upgrade [3]. The cold masses will be cooled in a pressurized static superfluid helium bath at 1.3 bar and at a temperature of about 1.9 K. The heat generated in the magnets will be extracted by vaporization of superfluid helium which travels as a low pressure two-phase flow in two parallel bayonet heat exchangers (HX) protruding the magnet yokes (depicted as one bold line in Figure 4.42). The low vapor pressure inside the heat exchanger is maintained by a cold compressor system, with a suction pressure of 15 mbar, corresponding to the saturation temperature of 1.776 K.

The flow diagrams for the four site implementations (Left of IP1, Right of IP1, Left of IP5, and Right of IP5), are very similar. They differ in orientation left-right, so Q1 will always face the IP, and have slope dependence for the He II two-phase flow in the HX, so the flow is always downstream. Figure 4.43 shows the flow diagram version applicable to the right side of IP5. On top are depicted the supply headers for cryogens, with two jumper connections between it and the magnet cryostats. All cryogenic valves are on the supply header-side.



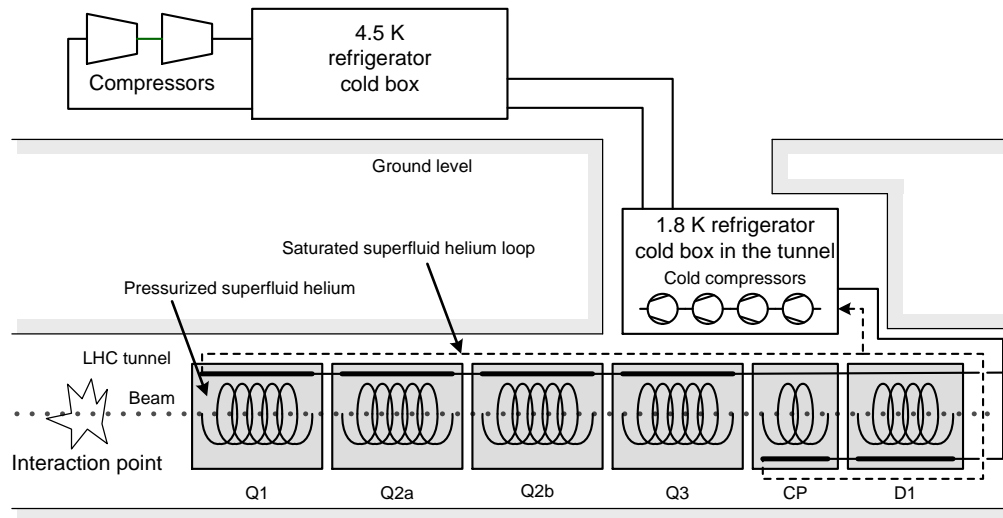


Figure 4.42: Architecture of the cooling by using superfluid helium.

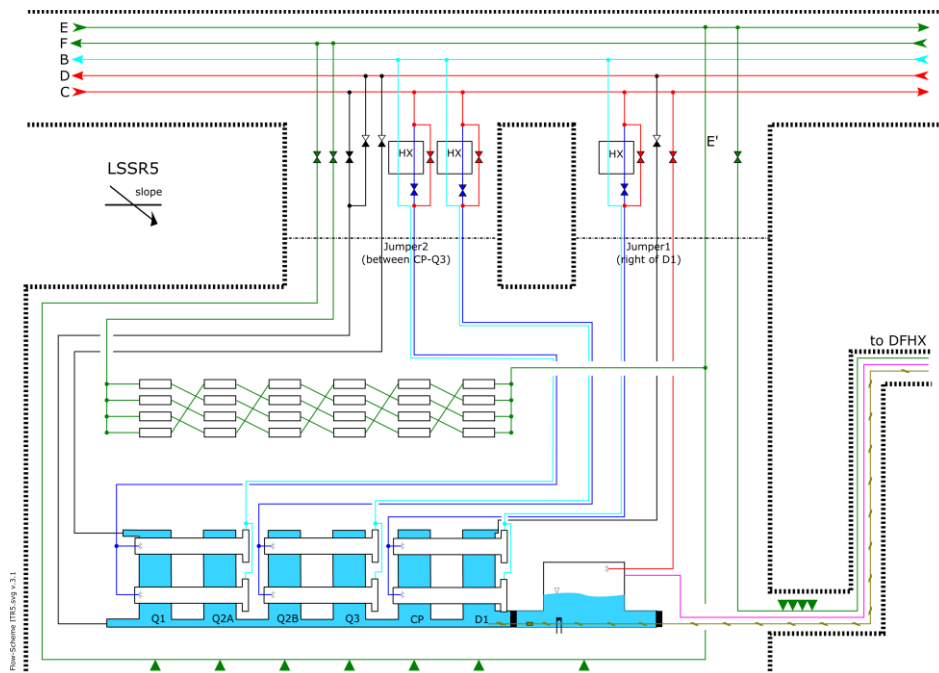


Figure 4.43: flow diagram for inner triplets, right of IP5

Due to constraints on magnet design, the bayonet heat exchangers cannot be continuous all the way from the quadrupole magnets through the corrector package and D1 dipole. The size and number of heat exchangers is determined by the maximum vapor velocity of 7 m/s above which the heat exchangers do not function anymore and the total available heat exchange area, when they are

wetted over their full length. For the quadrupole heat exchangers, the vapor velocity limit is the more stringent condition and is met if one uses two heat exchangers in parallel with inner diameters greater than 68 mm and lengths limited to two quadrupoles in series. As a consequence, the flow diagram exhibits three sets of bayonet heat exchanger cooling-units (D1+CP, Q3+Q2b, Q2a+Q1), each with their own supply and low vapor pressure return. These supplies and return lines are forcibly proper to the cooling loops such as to keep the counter flow heat exchangers, situated on the cryogenic supply headers' side, balanced. Each of these cooling loops integrates a phase separator at its end. These have to absorb the liquid present in the bayonet heat exchangers in case magnet quenches would drive it out. The liquid volumes to accumulate, without obstructing the low-vapor pressure return inlet, are estimated to be 12.5 ℓ for each of the quadrupole cooling loops and 5.5 ℓ for the D1+CP cooling loop.

The heat exchangers themselves are to be made of copper to assure proper heat conduction across the walls. A wall thickness of about 3 mm is required to sustain the external design pressures of 20 bar. With, in addition, an annular space of 1.5 mm between the HX and the yoke to allow contact area of the pressurized superfluid helium on the coil-side, the yoke-hole size required is 77 mm minimum. With this configuration about 800 W can be safely extracted. The 77 mm yoke-hole size is compatible with the mechanical design of the magnet, but should not be increased otherwise one would need to increase as well the overall diameter of the cold mass. Coping with the remaining 250 W is to be done via active cooling of the D1 and CP. Two parallel bayonet heat exchangers of 51 mm ID through D1 and CP are foreseen, requiring yoke holes of 60 mm diameter.

For correct functioning of the two-phase heat exchanger configuration, heat must be given some freedom to redistribute along the length of the cold-masses. This is no hard criterion, and a free longitudinal area of  $\geq 150 \text{ cm}^2$  through the Q1, Q2a, Q2b, Q3, and their interconnections and  $\geq 100 \text{ cm}^2$  through D1, CP and their interconnections are deemed to be sufficient.

Two pressure relief devices are foreseen as safety in case of sudden energy release to the cold mass helium due to either magnet quenches or catastrophic loss of insulation vacuum. The quench energies released are substantial for the MQXF – quadrupoles and D1 – dipole only. The energy per local helium volume for the magnets in the corrector package are so low that they can be absorbed by the surrounding helium without consequences for the neighboring magnets

## 4.5.2 Radial heat extraction in IR quadrupoles

The Nb<sub>3</sub>Sn quadrupole coils are fully impregnated, without any helium penetration. The heat loads from the coils and the beam-pipe area can only evacuate to the two heat exchangers by means of the pressurized He II. To this end, the cold mass design needs to incorporate the necessary radial helium passages.

Figure 4.44 shows the typical heat flow path: out from the coil areas, through the annular spacing between cold bore and inner coil-block, and subsequently via free passages through the titanium pole pieces and G11-alignment key, and around the axial rods towards the cooling channels where the two-phase flow bayonet heat exchangers will be inserted. They will occupy the two-upper yoke-holes marked “Cooling channel”. Since only two of the four possible cooling channels will house bayonet heat exchangers, free helium paths interconnecting these four cooling channel holes shall be implemented in the cold mass design. Doing so allows for equilibrating the heat flows and increasing the heat extraction margins as a whole.

The annular space between cold bore and inner coil block is set at 1.5 mm and the free passage needed through the titanium insert and G11-alignment key should be of the order of 8 mm holes

repeated every 40 mm – 50 mm along the length of the magnet. Magnet design is presently integrating 8 mm diameter holes every 50 mm. This value and repetition rate will be used in the temperature margin evaluation in subsequent paragraphs. Around the axial rods a free passage of 1.5 mm has to be guaranteed.

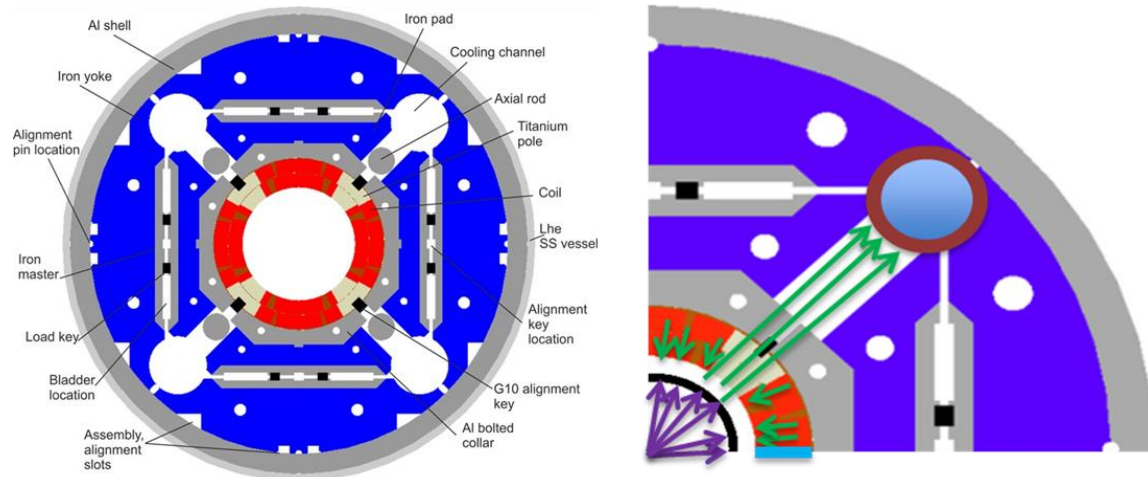


Figure 4.44: Heat flow paths from coil to one of the two-phase heat exchangers located in the upper right quadrant

### 4.5.3 Thermal performance evaluation

The heat load distribution at the most unfavorable location is used as reference (Figure 4.45) [3]. The peak power densities reached in the quadrupoles are close to  $7 \text{ mW/cm}^3$ .

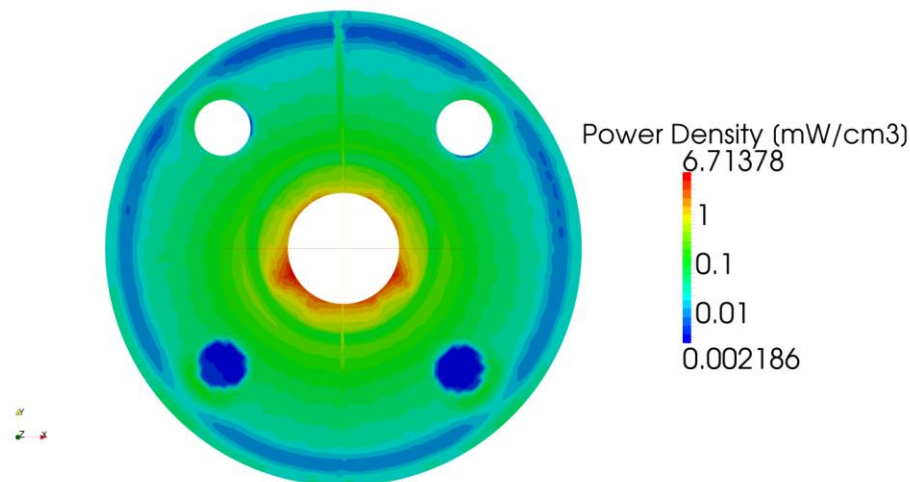


Figure 4.45: Power deposition map for Q3 at ultimate peak luminosity.

These power deposition maps are used as input to produce temperature distribution maps of the cold masses. The results are then converted into temperature margin maps by comparison with the

respective current sharing maps, calculated on an assumed homogeneous temperature distribution of 1.9 K (Figure 4.46).

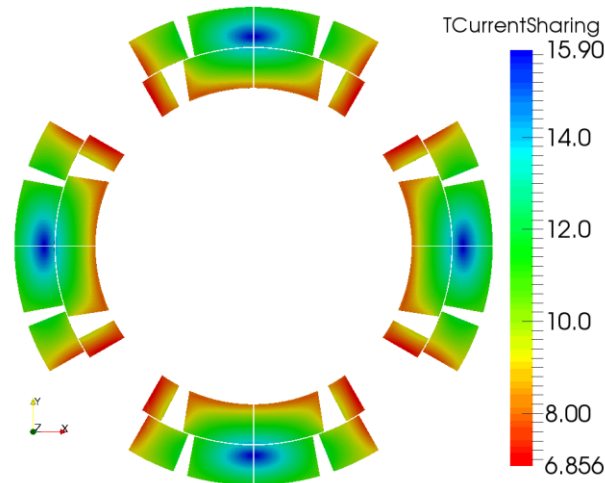


Figure 4.46: Current sharing map of MQXF quadrupole.

The MQXF-quadrupole coil materials were implemented with the coil pack details as shown in Figure 4.47. “Porous” quench heater traces were assumed to be placed on the MQXF inner coil layer (Figure 4.48) to perform the analysis. Since inner layer quench heater traces have been later removed from the quench protection scheme, these results are conservative (being the traces right in the heat extraction path).

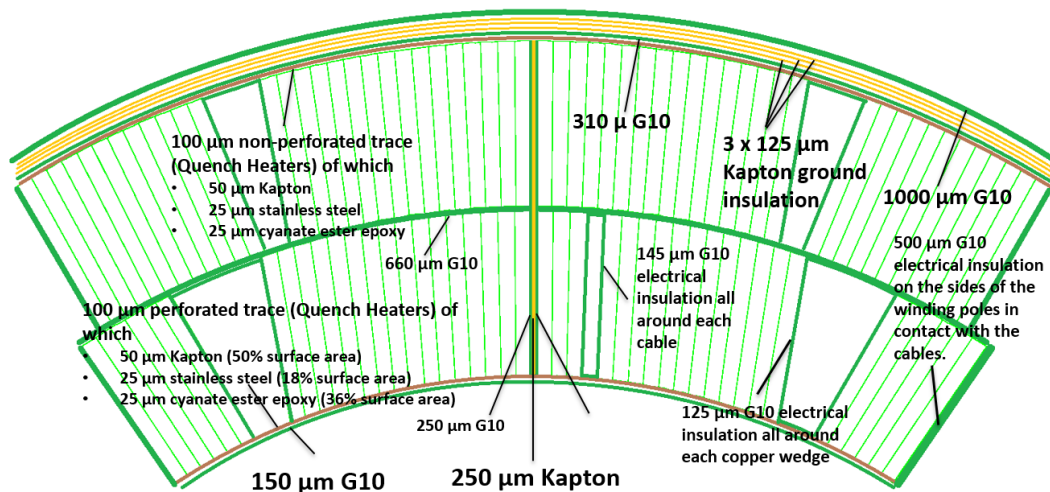


Figure 4.47: Quadrupole Nb<sub>3</sub>Sn coil materials assumed for the calculations.

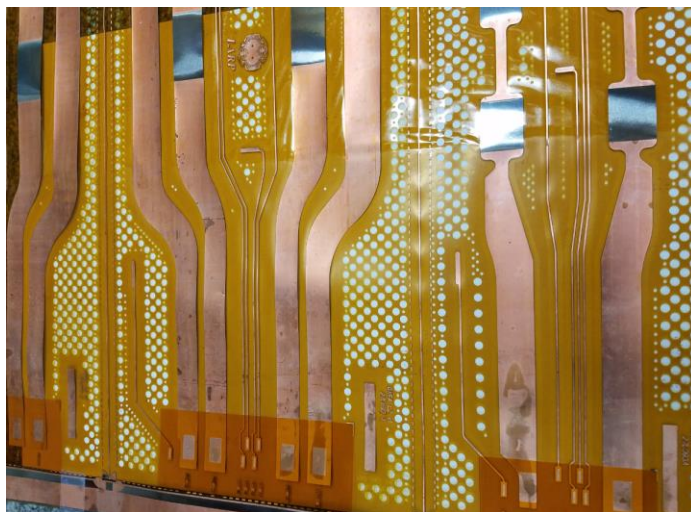


Figure 4.48: Perforated Kapton quench heater traces.

#### 4.5.4 Steady state temperature distribution, T margin and local maximum-sustainable load

Figure 4.49, Figure 4.50, Figure 4.51 and Figure 4.52 show the temperature and temperature-margin maps with their respective zooms. These were all calculated assuming a 1.9 K cold source (bayonet heat exchanger) temperature. Although the highest temperatures of about 3.15 K are reached in the outer coil layer, when combined with the current sharing maps, we find the most critical zones at the inner layer pole edges. There, the temperature margin goes down to about 4.1 K. Note that the value of 4.1 K is reached in a small fraction of the coil (Figure 4.52), and further optimization of the beam screen W absorber could remove this singularity and bring the temperature margin above 5 K all over the coil.

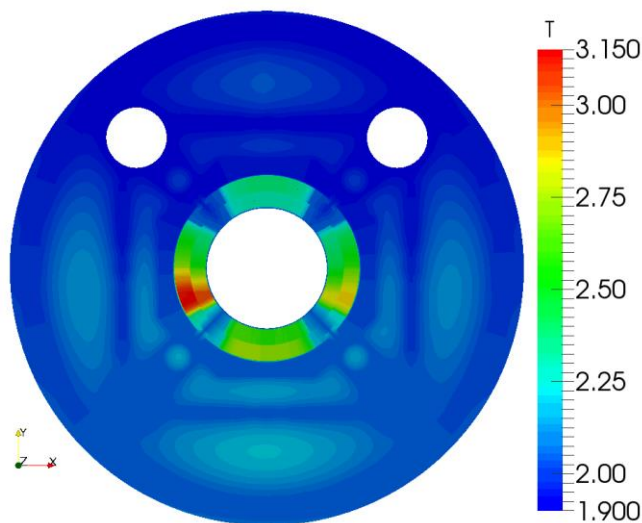


Figure 4.49: MQXF quadrupole temperature map; full section.



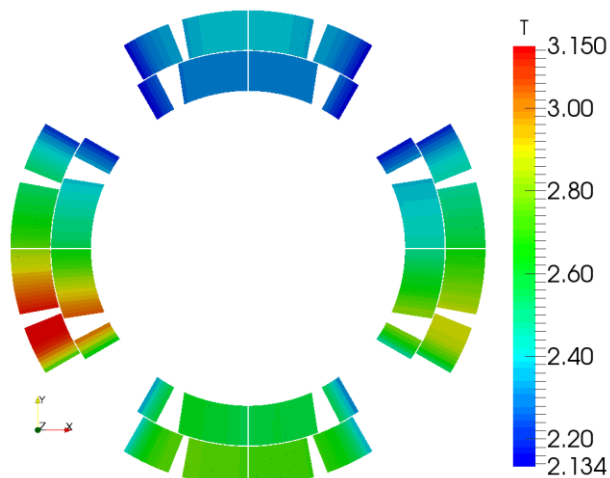


Figure 4.50: MQXF quadrupole temperature map; coil section.

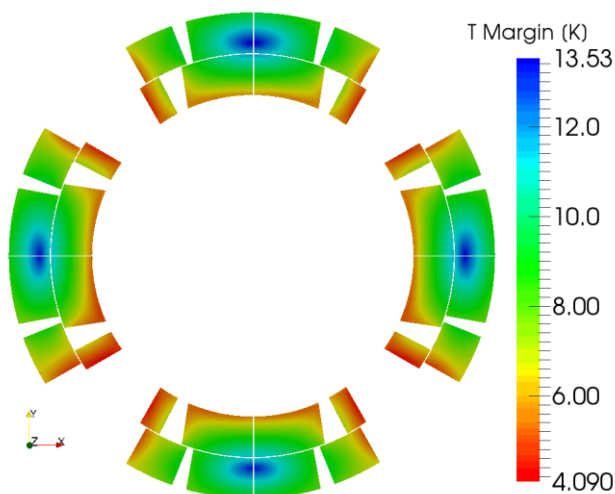


Figure 4.51: MQXF quadrupole temperature-margin map.

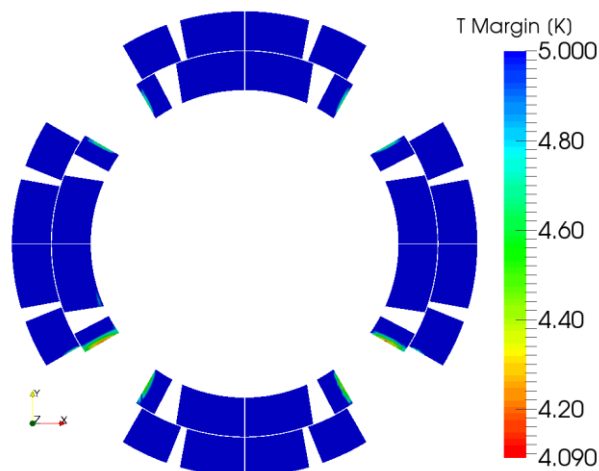


Figure 4.52: MQXF quadrupole temperature-margin map, capped off at 5 K to expose the critical zones.

The robustness of the MQXF thermal design is addressed by steady state local power deposit values that the coil can withstand without either the cooling breaking down or the cable reaching a temperature margin of 0 K. We found that in these steady state cases the local cooling break-down occurs first. Figure 4.53 shows that locally we can sustain powers from 56 mW/cm<sup>3</sup> at 1.9 K down to 19 mW/cm<sup>3</sup> at 2.1 K bayonet heat exchanger temperature. This constitutes a factor 8 at 1.9 K down to 3 at 2.1 K with respect to the expected peak load of 6.7 mW/cm<sup>3</sup> at ultimate luminosity.

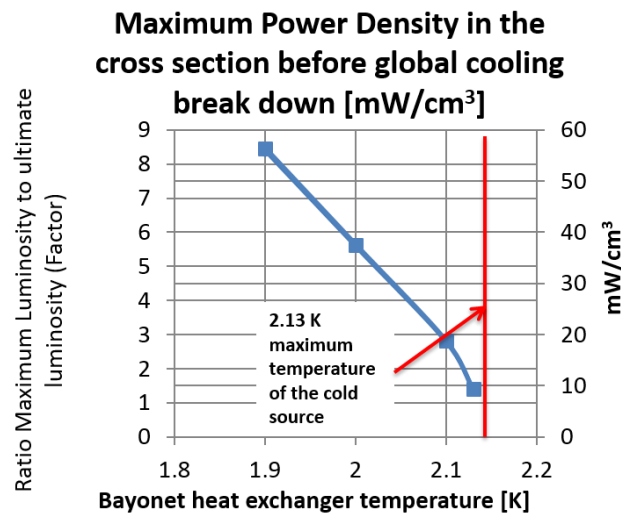


Figure 4.53: MQXF Quadrupole steady state power margin.

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## 4.6 Quench Protection

The requirements for MQXFA magnets protection in operating conditions are: hot-spot temperature  $< 350$  K [1,2] coil-ground voltages  $< 670$  V [3] and, turn-to-turn voltages  $< 160$  V [4].

The MQXFA is protected with a combination of quench heaters (QH) and Coupling-Loss Induced Quench (CLIQ) system [5-8]. Upon quench detection, both QH and CLIQ units are triggered simultaneously. The QH units introduce a current through the QH strips attached to the coil and heat up the conductor by heat diffusion through a thin  $50\text{ }\mu\text{m}$  insulation layer. The CLIQ units introduce oscillations in the magnet transport currents. The resulting local magnetic-field change introduces high inter-filament and inter-strand coupling loss, which heats the copper matrix of the strands. The two systems together constitute an effective synergy since they are based on different heating mechanisms and they deposit energy mainly in different parts of the winding pack.

Following a detailed study and evaluation of both Inner Layer (IL) and Outer Layer (OL) quench heaters, the configuration selected for the production magnets includes only the outer layer quench heaters [9]. Each magnet is equipped with 16 quench heater strips glued to the outer layers, and with two CLIQ terminals. This system has been optimized by assessing the performance of different types of quench heater strips, of alternative CLIQ configurations, and of combinations of these. Dedicated experimental studies have confirmed that adequate quench protection of the MQXF magnets in the LHC tunnel can be achieved in both nominal conditions and failure scenarios

### 4.6.1 Quench heater strips

Four quench heater strips are glued to the outer layer of each pole:

- Two strips (one on each side of the pole) in the low-field region near the magnetic mid-plane
- Two strips (one on each side of the pole) in the high-field region near the magnetic pole (B02, B03)

The quench heaters are made of stainless steel strips with copper plated sections to lower the resistance between heating stations, as shown in Figure 4.54. Their position in the coil cross-section and naming conventions are shown in Figure 4.55. Note that the strips of each pole are numbered starting from the strip closest to the lead end.



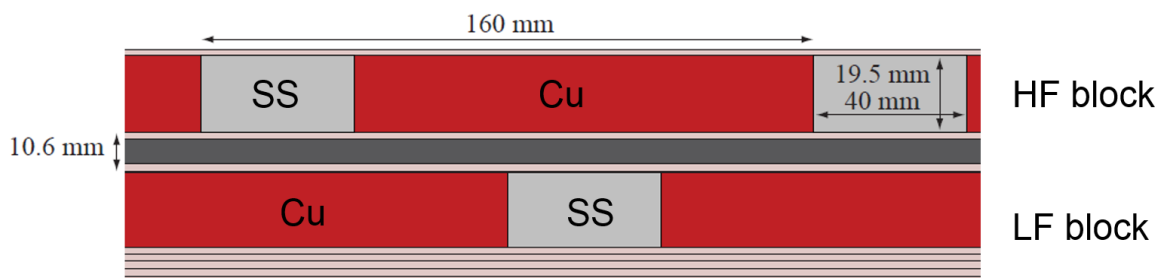


Figure 4.54: Design of the MQXFA outer layer quench heaters.

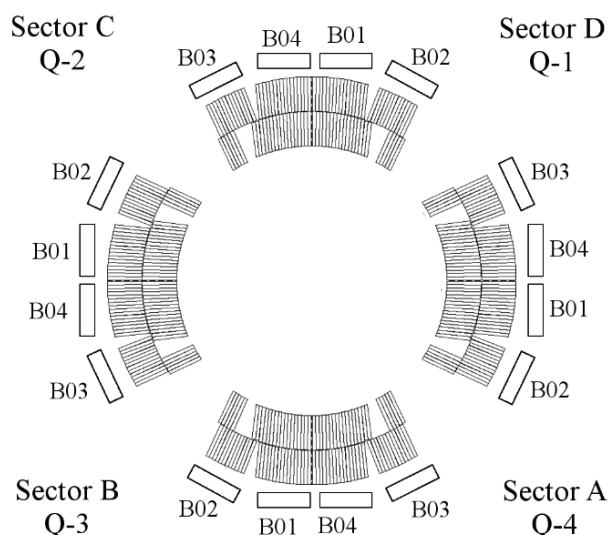


Figure 4.55: Position of the heater strips attached to the MQXFA magnets, viewed from the lead side.

The main parameters of the two types of heater strips and their estimated resistances at cryogenic and room temperature are summarized in Table 4.12. For the resistance calculations, the applied magnetic field is considered nihil, the resistivity of stainless steel is assumed to be  $5.45\text{E-}7$  and  $7.31\text{E-}7$   $\Omega\text{m}$  at 10 and 293 K, respectively (RRR=1.34), and that of copper  $6.00\text{E-}10$  and  $1.76\text{E-}8$   $\Omega\text{m}$ , respectively (RRR=29).

Table 4.12: Parameters of the quench heater strips attached to the MQXFA magnet

QH strip location	High-field outer layer	Low-field outer layer
QH design type [10]	Cu-plated 2 OL	Cu-plated 2 OL
Strip length [m]	4	4
Heater SS width [mm]	20	20
Heater Cu width [mm]	20	20
Heater SS thickness [mm]	0.025	0.025
Heater Cu thickness [mm]	0.01	0.01
Station length [mm]	40	40



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Station period [mm]	160	160
Number of stations	25	26
Strip resistance @ 10 K [Ω]	1.10	1.14
Strip resistance @ 293 K [Ω]	1.73	1.80

Each pair of QH strips is connected in series to an LHC standard QH power supply, featuring a capacitor bank of 7.05 mF charged to 600 V. In order to reduce the peak voltages to ground in the case of QH failures, the pairs are composed of strips glued to poles that are opposite to each other (P1-P3 and P2-P4), as shown in Figure 4.55. The resistance of the copper leads connected to the strips is assumed to be 0.6 Ω per circuit, the same as the present LHC QH circuits. The expected performances of the QH circuits are summarized in Table 4.13.

Table 4.13: Expected performances of the QH circuits protecting MQXFA

QH strip location	High-field outer layer	Low-field outer layer
Number of strips in series	2	2
Strip resistance @ 10 K [Ω]	1.10	1.14
Resistance of the warm leads [Ω]	0.60	0.60
QH circuit resistance @ 10 K [Ω]	2.80	2.89
QH supply charging voltage [V]	600	600
QH supply capacitance [mF]	7.05	7.05
Peak QH current [A]	214	208
QH discharge time constant [ms]	20	20
Peak QH power density [W/cm <sup>2</sup> ]	250	235
QH energy density [J/cm <sup>2</sup> ]	2.47	2.40

## 4.6.2 CLIQ terminals and leads

Each cold mass (Q1/Q3) is composed of two MQXFA magnets, powered in series. The MQXF electrical circuit is presented in [11]. The presence of parallel elements (thyristors, diodes) across each cold mass allows analyzing the discharge of each cold mass separately. In Figure 4.56, the part of the circuit corresponding to one cold mass is schematized. Each two MQXFA magnets are protected by two CLIQ units connected as shown in Figure 4.56. Two CLIQ leads are attached to each magnet, located at the joint between two electrically connected poles (see taps ‘a’ and ‘b’ shown in Figure 4.56). Their terminals are connected at the coil ends in the “pizza box” in Figure 8.10. The electrical order of the four poles is as follows: Q-1, Q-4, Q-2, Q-3 [12]. The resulting configuration, called “Crossed-Poles”, allows introducing opposite current changes in poles which are physically adjacent (P1-P3 and P2-P4), which is the most effective option for this magnet [5,8].

Each CLIQ unit features a 40 mF capacitor bank charged to 600 V.

The parameters of the conductor used for the CLIQ leads are summarized in Table 4.14. The copper cross-section of the leads is dimensioned to avoid overheating during the CLIQ discharge and to not limit the CLIQ performance due to an excessive electrical resistance. The temperature in the leads is expected to remain well below 300 K.

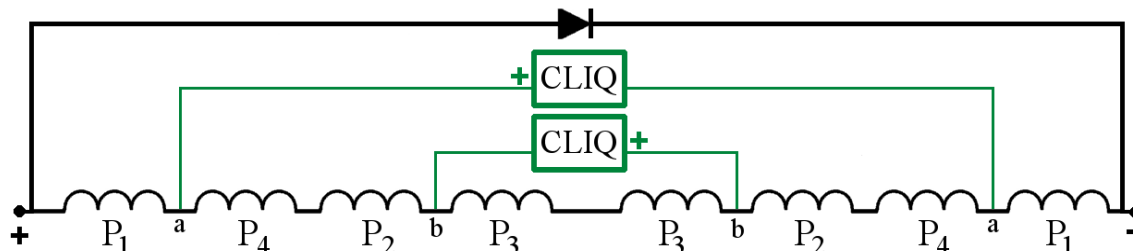


Figure 4.56: MQXFA electrical order of the poles and position of the CLIQ terminals.

Table 4.14: Parameters of the conductor used for the CLIQ leads of the MQXFA magnet

Parameter	Value
Material	Silver Plated Copper
Construction	133 filaments
Filament diameter	0.287 mm
Strand diameter	4.09 mm
Conductor area	8.60 mm <sup>2</sup>
Conductor resistance per unit length	0.217 $\Omega$ /100m
Insulation material	Extruded polyimide
Strand diameter with insulation	4.95 mm
RRR	>100

### 4.6.3 Expected quench protection performance

The detailed study of the MQXF quench protection and redundancy is presented in [11]. This analysis actually shows the performance of the protection system in the case of the 7.15 m long Q2a/Q2b magnets, which have the same cross-section and conductor parameters but different length. However, the same limits and safety factors on the coil's hot-spot temperature and peak voltage to ground are assumed for the longer and shorter magnets. In particular, the electrical quality assurance of the 4.2 m long MQXFA magnet will be performed at the same voltages as the 7.15 m long magnet.

Two options for the quench protection system are analyzed in the above-mentioned report:

- QH attached to the coil's outer layers (O-QH)
- QH attached to the coil's outer layers and CLIQ (O-QH + CLIQ).

The main quench protection simulation results, at nominal and ultimate current, are summarized in Table 4.15. Sensitivity to strand parameters and initial quench position are included in the analysis. It is shown that a protection system including only quench heaters attached to the coil's outer layers does not offer the required level of redundancy and barely maintains the coil's hot-spot temperature below 350 K, which is considered a conservative limit against permanent degradation. On the contrary, the other protection option effectively protects the magnet and limit the hot-spot temperature well below 350 K.

The consequences of QH circuit failures are studied, and the results reported in Table 4.16. The worst-case considered in the analysis is the failure of two independent QH circuits. Before the publication of the report [11], the worst-case  $U_{g,peak}$  reference value was 520 V, calculated in the case of O-QH+CLIQ [12]. The increase with respect to this value comes from the improvement in the model accuracy and from the detailed analysis of the effect of the initial hot-spot position. However, it is recommended that no correction of the test values during electrical quality be asked, considering that prudent safety margins were applied.

We assume that the total detection plus validation time is 15 ms [11]. This number is compatible with a voltage threshold of 100 mV, and a validation time of 10 ms.

Table 4.15: Simulated coil hot-spot temperature  $T_{hot}$ , peak voltage to ground  $U_{g,peak}$  and peak turn to turn voltage  $U_{t,peak}$  obtained after a quench at nominal and at ultimate current, for varying fraction of copper in the conductor, RRR and strand diameter. Uncertainty ranges also include the effect of different quench locations.

Configuration	$T_{hot}$ [K]	$U_{g,peak}$ [V]	$U_{t,peak}$ [V]
Nominal current			
O-QH	293-364	304-619	62-123
O-QH + CLIQ	215-248	521-658	49-90
Ultimate current			
O-QH	312-389	362-860	72-145
O-QH + CLIQ	237-273	664-924	61-109

Table 4.16: Failure case analysis. Simulated hot-spot temperature, peak voltage to ground and peak turn to turn voltage obtained for one failure or two simultaneous failures of QH circuits, at nominal and at ultimate current. Uncertainty ranges are due to the different locations of the initial quench and of the failing QH circuits.

Configuration	$T_{hot}$ [K]			$U_{g,peak}$ [V]			$U_{t,peak}$ [V]		
	No f	1	2	No f	1	2	No f	1	2
Nominal current									
O-QH	330-345	345-362	363-384	577	702	868	113	122	132
O-QH + CLIQ	236-237	238-240	239-242	641	668	666	83	84	86
Ultimate current									

O-QH	352-369	364-385	379-406	808	916	1068	133	141	152
O-QH + CLIQ	260-262	261-264	262-267	874	910	909	101	103	105

## 4.6.4 Failure analysis of the coil-to-heater insulation

The insulation between coils and quench heaters is constituted by 150  $\mu\text{m}$  of cable insulation (epoxy), plus 50  $\mu\text{m}$  of polyimide sheets. In case of damage of the polyimide insulation, since the epoxy cracks due to thermal contractions and electromagnetic forces, the electrical robustness of the coil is not trivial. Indeed, the crack is filled by superfluid helium, which during a quench evaporates. Helium gas is a “good” conductor, and can induce a short between heater and coil.

The peak heater-to-coil voltage during a quench in MQXFA is 400 V [13], when the temperature of the coil is 110 K. Assuming that the helium reaches the same temperature, this voltage is considerably larger than the helium breakdown voltage of a 200  $\mu\text{m}$  path ( $\sim 300$  V at 75 K [13]), at a pressure of 1 bar. Nevertheless, the helium pressure is expected to increase: indeed, starting from 1 atm pressure at 1.9 K, the helium pressure grows to  $\sim 530$  atm at 100 K. At such a large pressure, some helium is expected to flow out. Modeling this scenario is not trivial. However, the outer surface of the coil is pushed against the structure due to the electromagnetic forces. The contact pressure is  $\sim 100$  bar [13]. Assuming that the helium can keep at least 10% of this pressure, i.e. 10 bar, the breakdown voltage would be  $\sim 1\text{kV}$ , giving a certain margin to the peak heater-to-coil voltage (400 V). Therefore, this scenario can be reasonably considered safe; nevertheless, more detailed modelings are undergoing. A detailed analysis of this process is presented in [13]

## 4.6.5 Quench protection during single magnet tests

During the test of a single MQXFA magnet, one 40 mF, 600 V CLIQ unit is connected to the magnet. The resulting configuration, shown in Figure 4.57, allows introducing in the magnet poles the same oscillating currents as in the baseline LHC configuration.

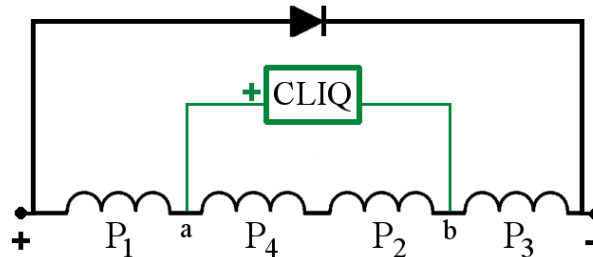


Figure 4.57: MQXFA electrical order of the poles and position of the CLIQ terminals.

## 4.6.6 Quench protection during cold mass tests

During the test of an entire cold mass, composed of two MQXFA magnets in series, the CLIQ configuration is identical to the final LHC machine case. Accordingly, the CLIQ connection scheme is presented in Figure 4.56.

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## 5 MQXFA Coils

### 5.1 Coil Technical Specification and QA/QC Plan Introduction

The QXFAs coil has a magnetic length of 4.2 m at the magnet operating temperature and is 4.532 m long at room temperature. It consists of Nb<sub>3</sub>Sn cable, stainless steel end parts, copper wedges, titanium pole pieces, and fiberglass insulation all encapsulated by epoxy. Tooling used for reaction and impregnation use numbered laminated pieces that are assemble in the same order for each coil fabrication process step. A work flow document or traveler specifies the order of assembly and process for all the fabrication steps. Coil parts and tooling are made to relatively tight tolerances and inspected by QC inspectors.

#### 5.1.1 Coil Technical Specification

The QXFAs coil is a two-layer cos-2 $\theta$  coil with saddle-shaped ends. The two-layer coil is wound continuously, without a splice at transition between the inner and outer layers, using the double-pancake technique successfully used in all LARP coils and by several other Nb<sub>3</sub>Sn magnets. The cross-section for coil design is shown in Table 5.1. For the inner layer, there are 5 turns in the first conductor group, 17 turns for the second conductor group, and inner layer wedges in between the two conductor groups on both coil sides. For the outer layer, there are 12 turns in the first conductor group, 16 turns in the second conductor group, and outer layer wedges in between the two conductor groups on both coil sides. Table 5.1 lists the coil dimensional specification.

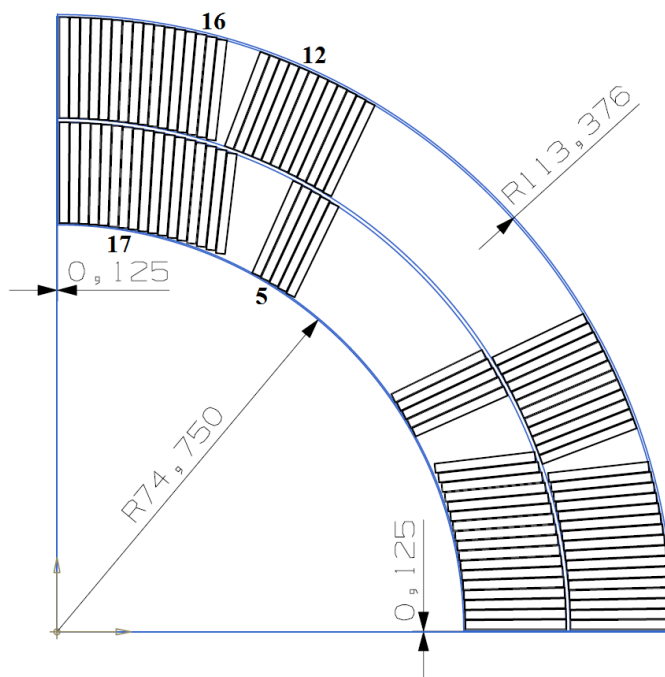


Figure 5.1: Coil Cross-section.



Table 5.1 Coil Dimensional Specification

	Dimension (mm)	Tolerance (mm)
Inner radius	74.750	$\pm 0.25$
Outer radius	113.376	$\pm 0.25$
Coil to midplane gap	0.125	$\pm 0.05$
Coil length	4532	$\pm 5.0$

The coil model is shown in Figure 5.2. To meet the requirement of a magnetic length of 4.2 m, the overall coil length will be 4.532 m.

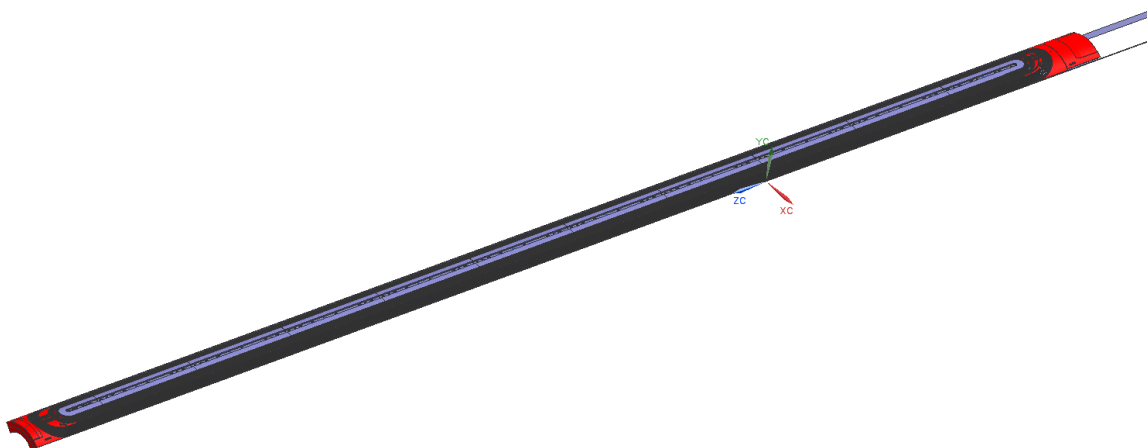


Figure 5.2: QXFA Coil Model

There are poles, end parts and wedges that go into the coil, and Table 5.2 lists the parts dimension with tolerance. Reference drawing is QXFA Coil Assembly Drawing F10030927.

Table 5.2 Coil Parts Dimension and Tolerances

	Inner radius	Outer radius
L1 Pole	$75 \pm 0.025$	$93.65 \pm 0.025$
L2 Pole	$94.31 \pm 0.025$	$112.97 \pm 0.025$
L1 End Part	$75.1 \pm 0.07$	$93.55 \pm 0.07$
L2 End Part	$94.4 \pm 0.07$	$112.87 \pm 0.07$
L1 wedge	$75.127 \pm 0.05$	$93.526 \pm 0.05$
L2 wedge	$94.44 \pm 0.05$	$112.84 \pm 0.05$

## 5.1.2 Coil QA/QC Plan

### a. Coil Electrical Measurements

The coil QA/QC plan consists of electrical measurements made throughout the fabrication process. Electrical continuity check between the coil and the ground, and between the coil and the coil parts is performed during coil winding and curing, and during coil reaction. Electrical continuity check between the coil and the quench heater is performed after coil impregnated. When the coil is transferred to the shipping fixture, coil resistance,  $L_s$  and  $Q$  are measured, and Table 5.3 shows the measurement range for a good coil. Hipot test and impulse test are also performed when the coil is sitting on the shipping fixture, and the specification for these tests are written Electrical Design Criteria document [1].

Table 5.3 Coil Electrical Measurement Range

Measurement	Ref. Min-Max
<i>Coil Resistance @ 1A</i>	590.00-610.00 mV
<i><math>L_s</math> @ 20 Hz</i>	4.80-5.10 mH
<i><math>Q</math> @ 20 Hz</i>	0.80-0.90
<i><math>L_s</math> @ 100 Hz</i>	3.20-3.50 mH
<i><math>Q</math> @ 100 Hz</i>	1.50-1.70
<i><math>L_s</math> @ 1 kHz</i>	1.80-2.00 mH
<i><math>Q</math> @ 1 kHz</i>	1.90-2.10

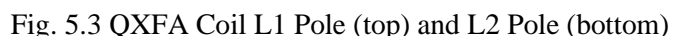
### b. Coil Mechanical Measurements

The coil QA/QC plan consists of mechanical measurements made throughout the fabrication process. After impregnation, the coil is measured at 14 cross sections with a coordinate measurement machine, the coil CMM location based on the drawing 27K975.

## 5.2 Coil Parts

### • Poles

The QXFA coil is wound around the pole parts, and there are 1 piece of lead end pole, 9 pieces of center pole and 1 piece of return end pole for both the inner and the outer layer coil, as shown in Fig. 5.3 The pole parts are made of Ti-6Al4V STA (solution treated aging process) to have better straightness and strength. Table 5.4 lists the part name and the drawing ID for the poles, which can be found in Teamcenter, the FNAL drawing system. Each pole part has the profile tolerance bilateral 0.05 mm, which is defined as critical in AQL for inspection.



Name	Drawing ID	Qty. per coil
Pole, Lead End L1	F10039540, Rev. C	1
Pole, Layer 1	F10039545, Rev. C	9
Pole, Return End L1	F10005738, Rev. C	1
Pole, Lead End L2	F10039541, Rev. C	1
Pole, Layer 2	F10039546, Rev. C	9
Pole, Return End L2	F10005750, Rev. C	1

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For L2 pole, the keyway is designed to align the coil during coil fabrication and the magnet assembly. The 14 mm wide keyway is defined within (+0.02 mm, 0) profile tolerance, as shown in Fig. 5.5, which is defined as major in AQL for inspection.

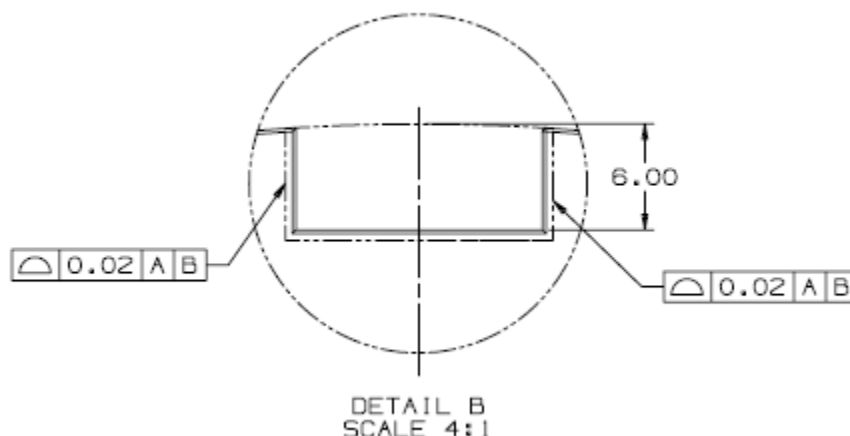
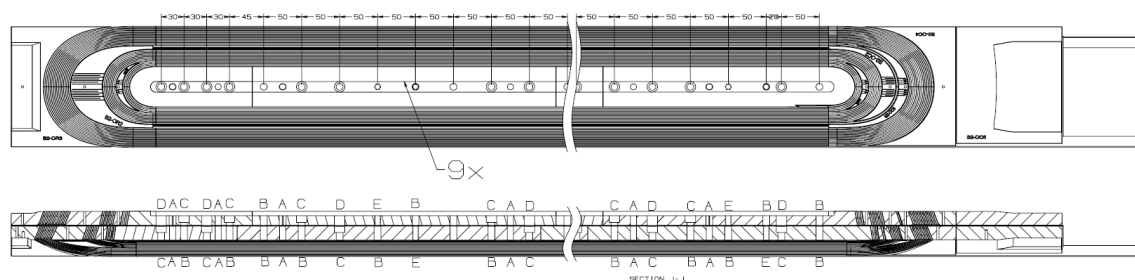


Fig. 5.5 Keyway Profile Tolerance

Pole parts between inner and outer layers are aligned through the 8 mm dowel pins. The poles are bolted to the winding anchor bars through clearance holes. The fabricated coil is lifted through lifting holes. Both clearance holes and lifting holes are designed with minimum 8 mm diameter and 50 mm spacing. These holes are used as cooling channels, shown in Figure 5.6, to extract the heat from the coil aperture to the heat exchangers in the yoke.



Pin Hole A:  $\varnothing 8.02\text{mm}$  for 8 mm dowel pin  
 Clearance Hole B:  $\varnothing 9\text{mm}$  thru for 5/16" or M8x1.25 SHCS  
 Clearance Hole C:  $\varnothing 9\text{mm}$  thru, L  $\varnothing 13.8\text{mm}$   $\varnothing 8.8\text{mm}$  for 5/16" or M8x1.25 SHCS  
 Clearance Hole D:  $\varnothing 13.8\text{mm}$  thru for 5/16" or M8x1.25 SHCS  
 Lifting Hole E: M8x1.25 threaded  
 After coil fabrication, hole B, C, D and E will be used as cooling channel for the magnet

Figure 5.6: Cooling holes through coil pole

## Wedges

The wedge is fabricated through the extrusion process to have the best uniform shape for each coil, with the profile tolerance defined as bilateral 0.05 mm. Witness notches are added to each wedge for identification and orientation. Figure 5.7 shows the wedges cross-section for both the inner layer and the outer layer coil. The wedges are made of phosphor bronze to have the similar thermal properties as Nb<sub>3</sub>Sn cable. Table 5.5 lists the part name and the drawing ID for the wedges.

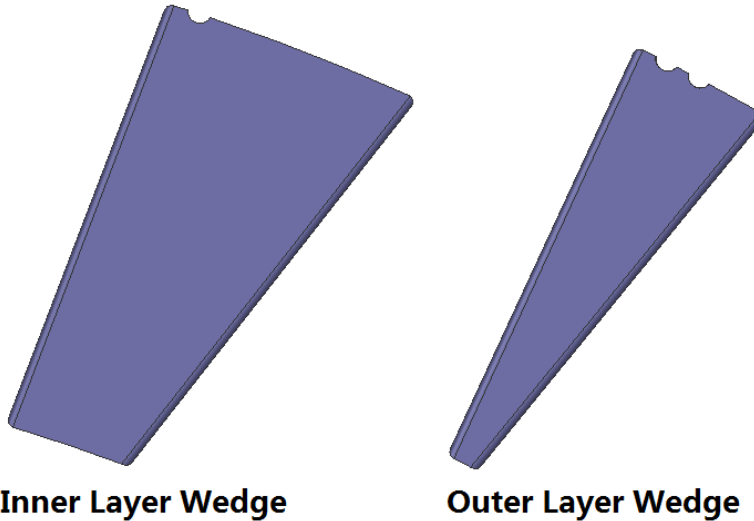


Figure 5.7: Wedges.

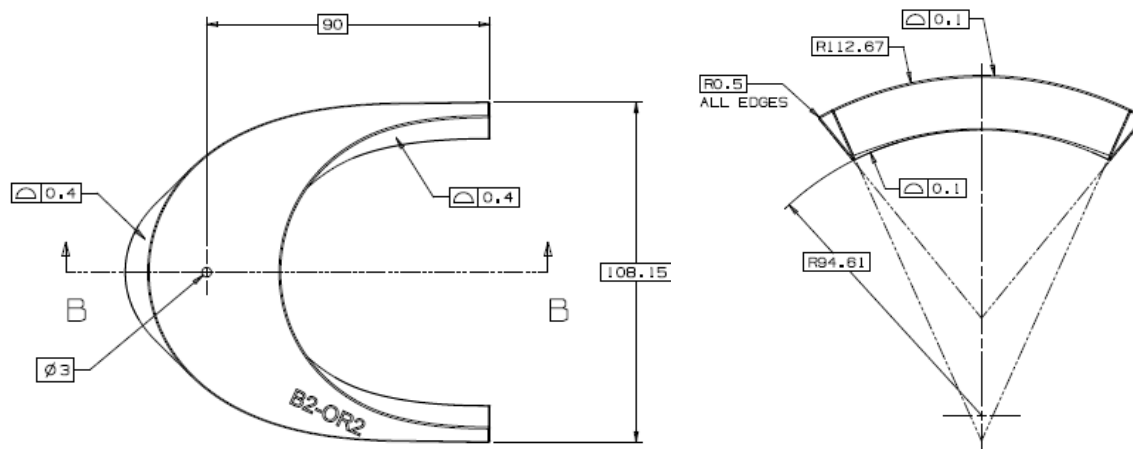
Table 5.5 QXFA Coil Wedge Components

Name	Drawing ID	Qty. per coil
QXFA Coil L1 Wedge_Long	F10068150, Rev. B	10
QXFA Coil L1 Wedge_Short	F10068151, Rev. A	2
QXFA Coil L2 Wedge_Long	F10068148, Rev. B	10
QXFA Coil L2 Wedge_Short	F10068149, Rev. A	2

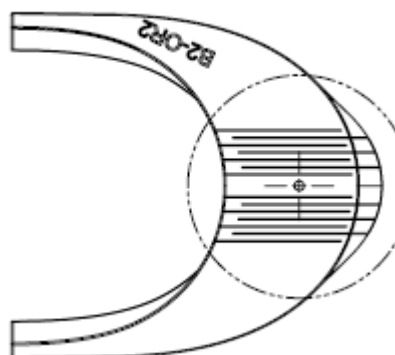
## • End Parts

End parts, saddles and splice block are designed based on the nominal coil size after reaction. End parts have been designed and optimized using BEND and ROXIE, and both designs work well. LARP uses BEND parts, while CERN uses ROXIE parts.

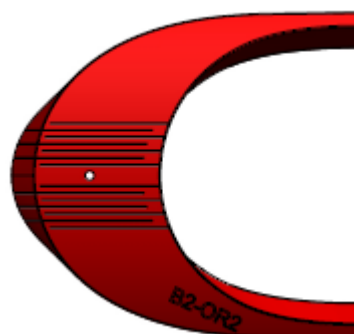
During winding, the coil is not fully constrained inside the envelope. This effect is most pronounced at the ends. Prior to curing, the cable tries to separate from radial surface of the mandrel in some areas (springback), causing the shape of the turn not to match the shape of the end parts. The springback is larger with larger coil aperture and cable size. Therefore, flexible features (slits) have been introduced in QXFA coil design. This is an incremental change with respect to single slit design previously used in LARP coils. The end parts are made of SS 316L. End parts are plasma coated at 250  $\mu\text{m}$  thickness to increase the dielectric strength. One of the parts is shown in Figure 5.8, 0.1 bilateral profile tolerance on OD and ID is defined as critical in AQL for inspection, 0.2 bilateral profile tolerance on bend surfaces is defined as critical, the slits feature is defined as minor, and the coating thickness  $0.008'' \pm 0.002''$  is defined as major.



(a) Part with no slits



(b) Part with slits



(c) Part after plasma coating

Figure 5.8: QXFA Coil End Spacer

For identification number, instead of using the drawing number, Bx-xxx is adopted, where B represents BEND, the first “x” after B represents the design generation (the latest design generation is 2), the second “x” shall be either I (inner layer) or O (outer layers), the third “x” shall be either R (return end) or C (lead end), and the fourth “x” represents end part’s number. For example, 2<sup>nd</sup> generation design, inner layer LE spacer 2, the identification number is B2-IC2. The identification number for each part is shown in Figure 5.9, which is laser cut on the surface of the

part, and after coating it is still visible. Table 5.6 lists the part name and the drawing ID for the end parts at different fabrication stages.

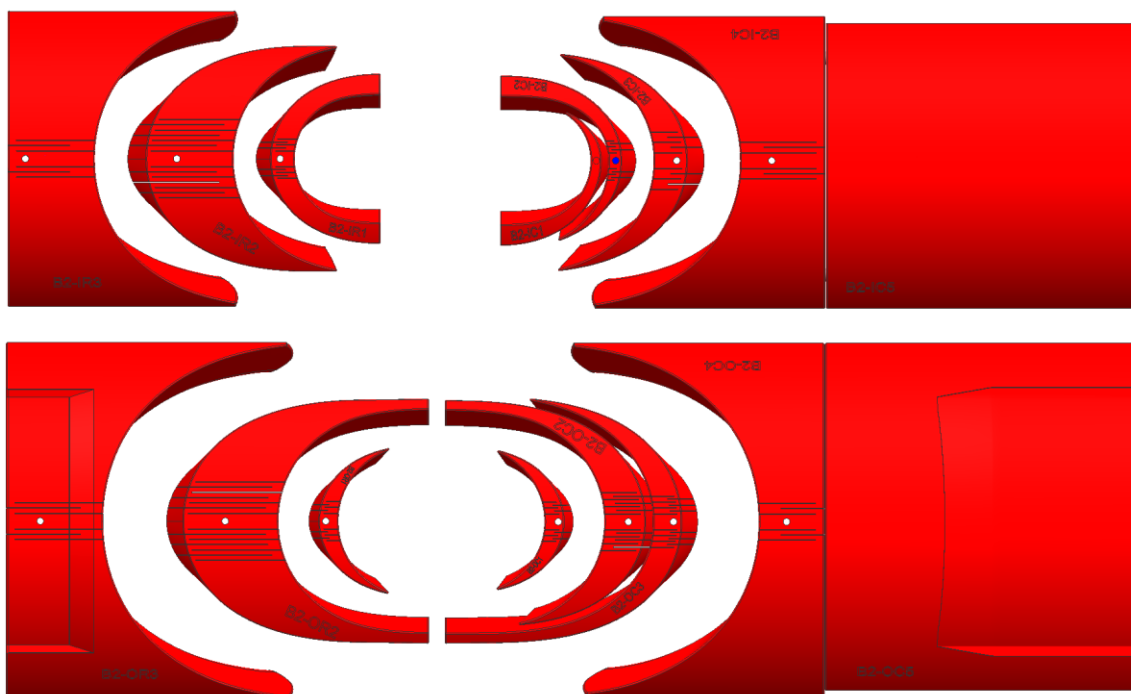


Figure 5.9: QXFA Coil End Parts for L1 (top) and L2 (bottom)

Table 5.6 QXFA Coil End Parts Identification

Name	ID #	Drawing/Solid Part	Drawing/ Slit Part	Drawing/Coated Part
Spacer 1, Lead End L1	B2-IC1	F10039749 Rev. A	-	F10088257 Rev. -
Spacer 2, Lead End L1	B2-IC2	F10039750 Rev. A	F10041400 Rev. -	F10042026 Rev. -
Spacer 3, Lead End L1	B2-IC3	F10039751 Rev. A	F10041401 Rev. -	F10042027 Rev. -
Saddle, Lead End L1	B2-IC4	F10039752 Rev. C	F10041397 Rev. A	F10042022 Rev. A
Splice block, Lead End L1	B2-IC5	F10039892 Rev. A	-	F10042599 Rev. A
Spacer 1, Return End L1	B2-IR1	F10039746 Rev. A	F10041413 Rev. -	F10042035 Rev. -
Spacer 2, Return End L1	B2-IR2	F10039747 Rev. A	F10041414 Rev. -	F10042036 Rev. -
Saddle, Return End L1	B2-IR3	F10039748 Rev. D	F10041415 Rev. B	F10042037 Rev. B
Spacer 1, Lead End L2	B2-OC1	F10039756 Rev. A	F10041409 Rev. -	F10042032 Rev. -
Spacer 2, Lead End L2	B2-OC2	F10039757 Rev. A	F10041410 Rev. -	F10042033 Rev. -
Spacer 3, Lead End L2	B2-OC3	F10039758 Rev. A	F10041412 Rev. -	F10042034 Rev. -



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Saddle, Lead End L2	B2-OC4	F10039759 Rev. D	F10041408 Rev. A	F10042031 Rev. A
Splice block, Lead End L2	B2-OC5	F10039893 Rev. A	-	F10042600 Rev. -
Spacer 1, Return End L2	B2-OR1	F10039753 Rev. A	F10041403 Rev. -	F10042029 Rev. -
Spacer 2, Return End L2	B2-OR2	F10039754 Rev. A	F10041406 Rev. -	F10042030 Rev. -
Saddle, Return End L2	B2-OR3	F10039755 Rev. D	F10041402 Rev. B	F10042028 Rev. C

## • NbTi Cable

After the coil reaction, the Nb<sub>3</sub>Sn lead is soldered to two pieces of NbTi cable which is provided by CERN, with the strand specification and cable specification shown in Table 5.7 and Table 5.8. The cable dimension is shown in Figure 5.10. The minimum length for IL and OL NbTi coil lead are reported in the interface control document # 252 and # 309 [2]. After cable lead soldering, 3 mil (75  $\mu$ m) thick Kapton insulation is wrapped around the splice ground insulation, see Figure 5.11 . Two (2) redundant voltage taps are used for quench detection in each internal MQXFA Nb<sub>3</sub>Sn-NbTi splice.

Table 5.7: NbTi Cable Strand Specification.

NbTi Cable Strand	
Coating type	Sn5wt%Ag
Diameter after coating (mm)	1.065 $\pm$ 0.0025
Copper to superconductor ratio	1.65 $\pm$ 0.05
Filament diameter ( $\mu$ m)	7
Number of filaments	~ 8900
RRR	$\geq$ 150
Twist pitch after cabling (mm)	18 $\pm$ 1.5
Critical current (A) 10T, 1.9 K	$\geq$ 515
9 T, 1.9 K	
$\Delta$ M at 0.5 T and 1.9 K (mT)	$\leq$ 30

Table 5.8: NbTi Cable Specification.

Strand Type	NbTi
Strand Diameter	1.065 mm
Number of Strands	34
Width	18.15 mm
Height	1.92 mm



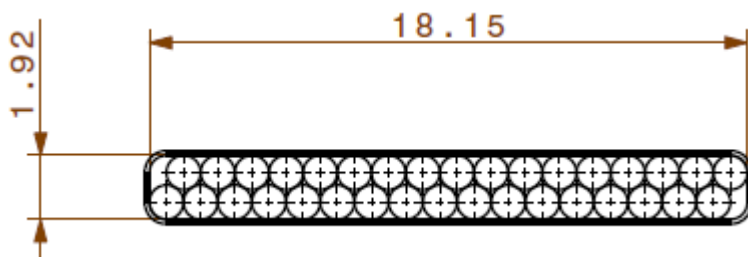


Figure 5.10: NbTi Cable.

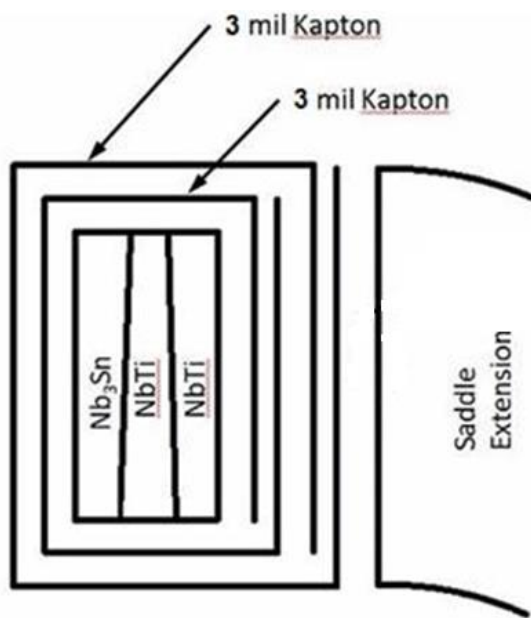


Figure 5.11 Insulation around the coil lead.

## • Quench Heater Circuits

Flexible quench heater circuits are used in the protection of MQXF superconducting magnets for the HiLumi Upgrade of the LHC. These circuits consist of heater strips glued on polyimide layer (trace) and are used to trigger a full magnet quench. The trace design (see Fig. 4.48) uses an insulating layer of 50  $\mu\text{m}$  thick polyimide followed by a 25  $\mu\text{m}$  thick resistive layer of 316L stainless steel. A top layer of 10  $\mu\text{m}$  thick copper is then electrodeposited over a large fraction of the stainless to ensure targeted heat application, see the sketch in Figure 5.12. Non-active areas of polyimide are then perforated at  $\sim 50\%$  while maintaining hole to metal spacing of  $>4$  mm. Quench heater traces are placed only on coil outer surfaces. Instrumentation circuits for coil voltage taps on the outer layer are photoetched on the same trace.

Voltage taps on the inner layer are placed on a mini trace.

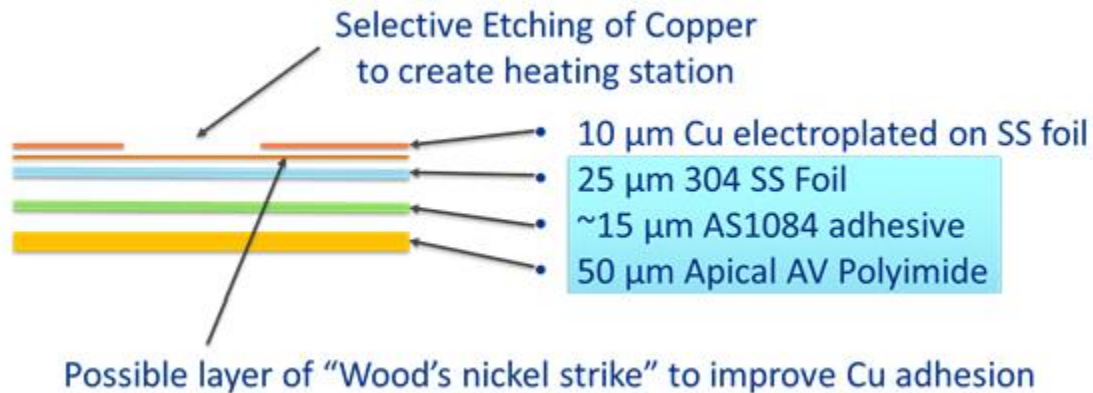


Figure 5.12 Sketch of the Quench Heater Circuits

For the prototype and pre-series magnets, 8 voltage taps are used in the OL and IL coil to monitor coil quench location. The drawing of OL quench heater trace for these magnets is shown in Figure 5.13 (a). Voltage tap mini trace for IL is shown in the drawing and picture of Fig. 5.13 (b).

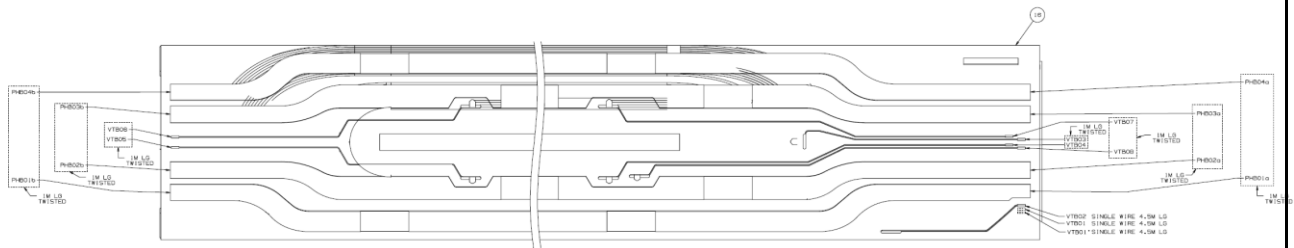


Fig. 5.13 (a): OL quench heater trace and voltage taps drawing for prototype and pre-series magnets

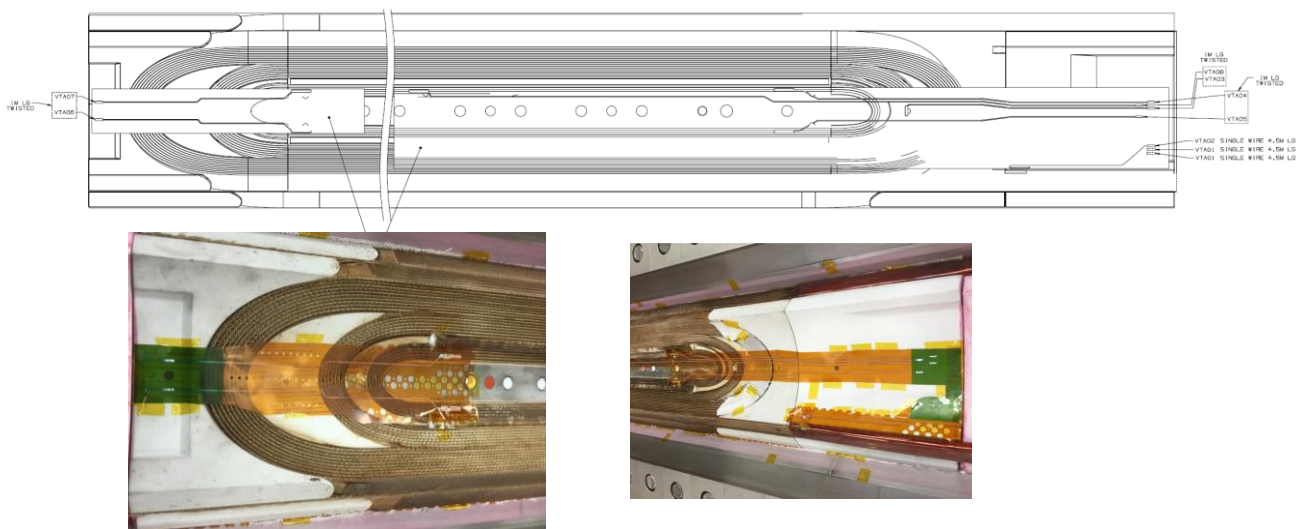


Fig. 5.13 (b): IL voltage taps mini trace drawing and pictures for prototype and pre-series magnets

For production magnet, just 4 voltage taps (two in the IL coil and two in the OL coil) are required to monitor the coil splices. Drawing of the outer layer trace and inner layer mini trace are shown in Figure 5.14 (a) and (b) respectively.

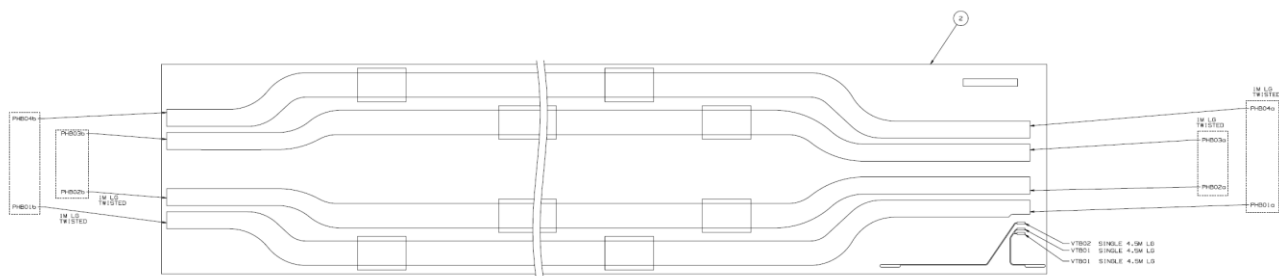


Fig. 5.14(a): Outer Layer quench heater and tap trace for magnet series

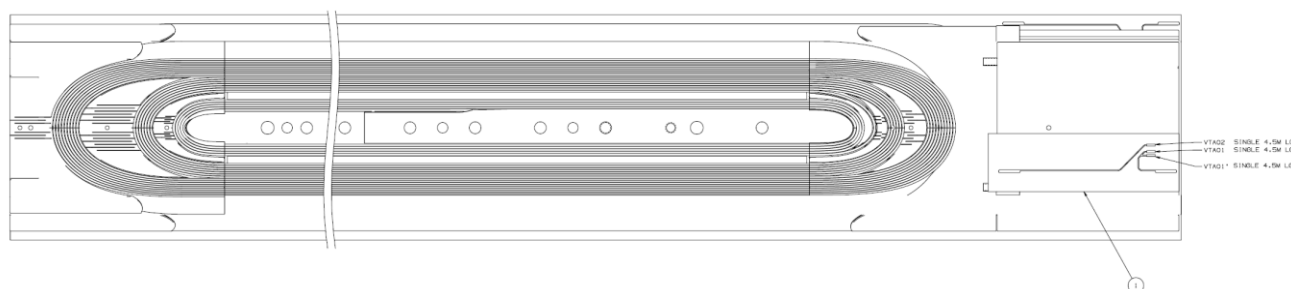


Fig. 5.14(b): Inner Layer voltage tap mini trace (bottom right) for magnet series

## Other Materials

There are other materials that are going into the coil during coil fabrication. Table 5.9 lists these materials.

Table 5.9 Other Materials in the Coil

Name	Material	Drawing ID
Pole Insulation	S2 glass tape	FC0066103
Wedge Insulation	S2 glass sleeve	FC0060196
Ramp turn Shim	S2 glass	F10039954
Interlayer Insulation	BGF 6781 and Hexcel 4522 S2 glass	F10052204
Impregnation Cloth for Outer layer	Hexcel 4522 S2 glass	F10058890
Impregnation Cloth for Inner layer	BGF 6781 S2 glass	F10059904
8 mm Dia. 24 mm Length Dowel Pin	SS 316	-
Curing Binder	CTD 1202	-
Impregnation Epoxy	CTD 101k	-
Solder	96/4 Tin/silver	-

Soldering Flux

MOB 39

## 5.3 Coil Fabrication at FNAL

### 5.3.1 Winding and Curing

Fermilab will perform 46 QXFA coils winding and curing with equipment, tooling and processes successfully used for the prototype coils by LARP. SELVA winder, as shown in Fig. 5.15, which was used during LHC low beta quadrupole coils fabrication, is used to wind the QXFA coils for LHC upgrade.

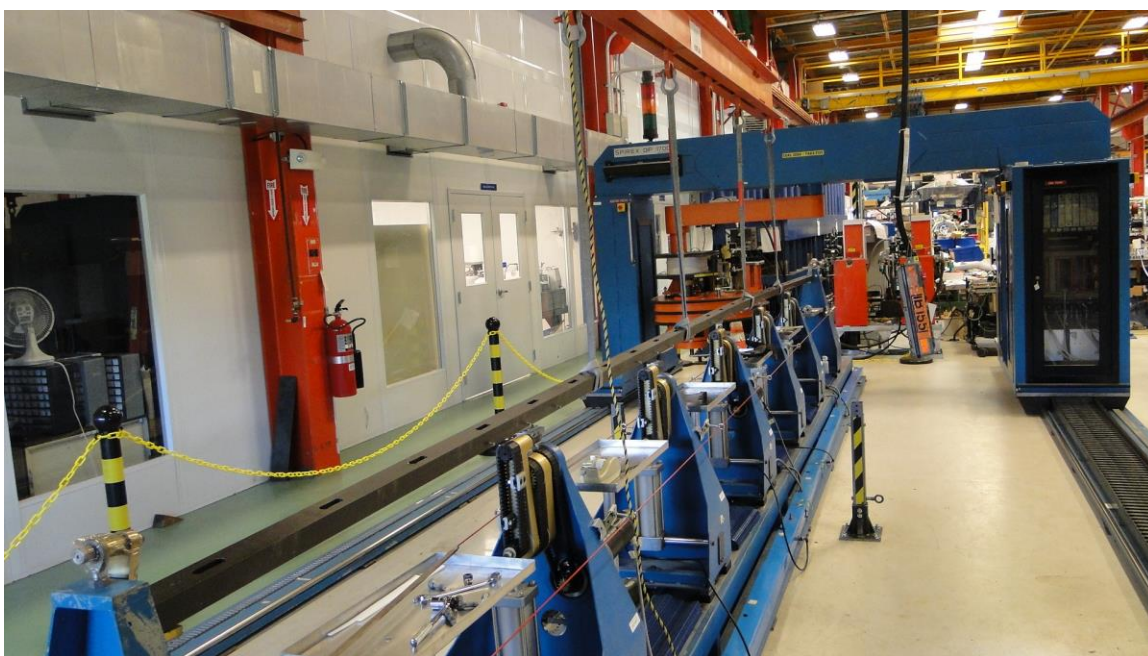


Figure 5.15: SELVA Winder.

The 2-layer QXFA coil is wound without a cable splice between the layers. The insulated cable, with minimum length 441 m, is measured to verify the overall length and then split into two spools for the inner layer and the outer layer.

Before winding, the inner pole parts are prepared and setup on the winding mandrel with 4 layers of 0.125 mm thick S2 glass insulation wrapped around. To accommodate the coil length shrinking due to the tension release after curing and thermal effects during reaction, pole gaps totaling 12.7 mm are introduced to the 2<sup>nd</sup> generation coil fabrication, based on prototype coil experience. The total gap along the wedge is required to be no less than 2 mm/m longer than the pole gap, considering the thermal shrinkage difference between the wedge and the coil.

The coil winding and curing process is shown in Figure 5.16. The inner layer is wound first. The wound inner coil is uniformly painted with binder (CTD-1202) at a rate of 1.7 g/m per cable, packaged with the curing tooling and shims, as shown in Figure 5.17. It is transferred to the curing mold through the rollover fixture. The inner layer coil is cured in the curing mold at 150°C for 1 hr

and 45 mins, and after curing it is transferred back to SELVA through the rollover fixture. The 0.66 mm pre-cured interlayer insulation is placed on top of the inner layer coil, and the outer layer pole parts are set up on top of it with 4 layers of 0.125 mm thick S2 glass insulation wrapped around continuously from the inner layer. When the outer layer winding is completed, the outer layer is uniformly painted with binder at a rate of 1.7 g/m per cable, packaged as shown in Figure 5.17. It is transferred through the rollover fixture to the curing mold for 1 hr and 45 mins curing at 150°C. Each layer is cured under pressure in a precise closed cavity mold at 150 °C in air. While the coil is inverted relative to winding orientation, the pole is radially compressed with mandrel cylinders. Subsequently the coil is azimuthally compressed with the platen cylinders until closure which typically occurs at 13 MPa coil pressure. Curing is performed on the coil to set the coil size for reaction, as well as allow the coils to be easily handled, facilitating insertion into the reaction fixture without damage. Spacers simulating the outer layer are used during the curing of the inner layer. The outer layer is cured on the top of the inner layer. Therefore, the same mandrel and mold are used to cure both the inner and the outer layer.

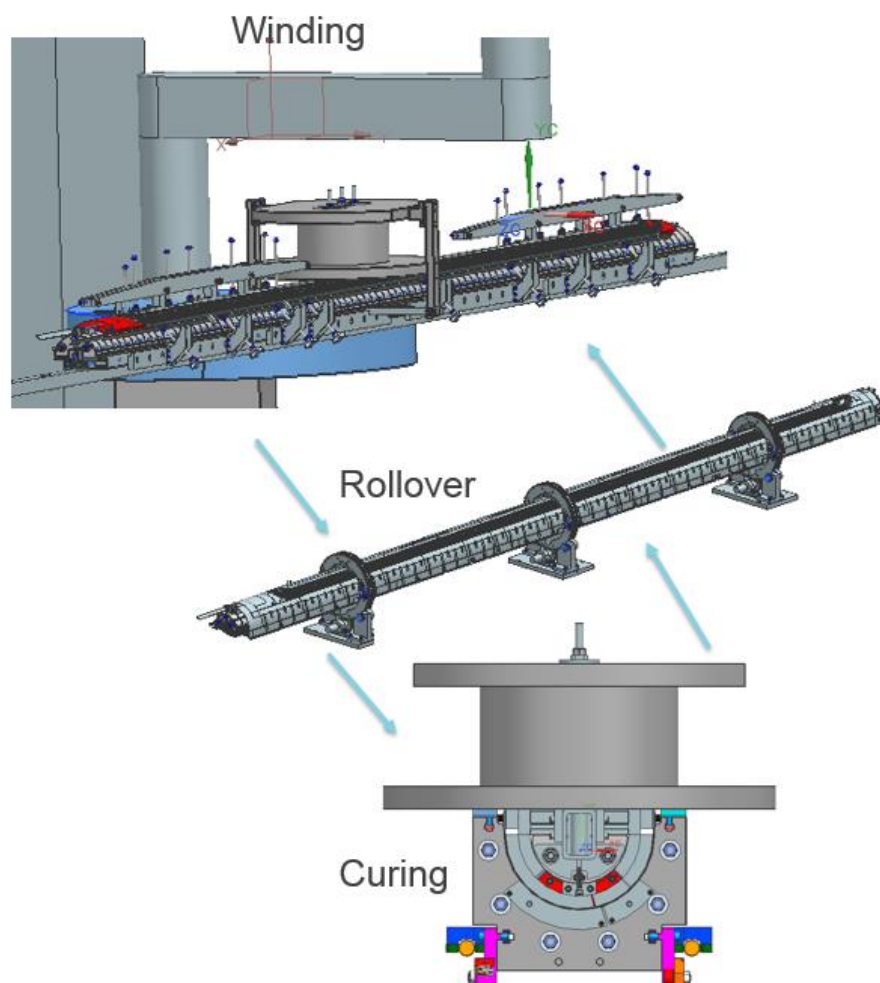
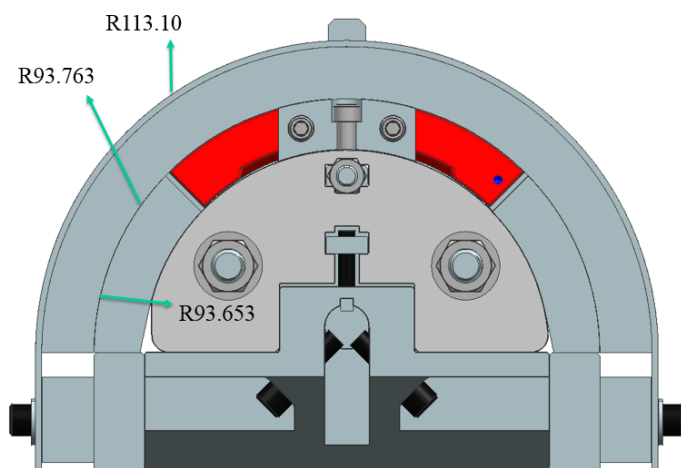


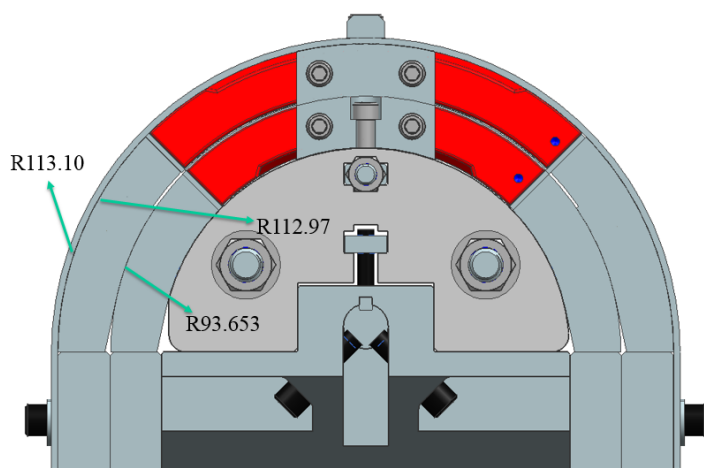
Figure 5.16: Winding and Curing Process.





Tooling/ Shims	R or t (mm)	+ tol. (mm)	- tol. (mm)	Max. (mm)	Min. (mm)
Mandrel	74.873	0.01	0.01		
Kapton	0.127	0.01	0.01		
	75	0.02	0.02		
L1 Sector pusher	75	0.08	0	0.1	-0.02
Coil OD	93.653	0	0.05		
Mylar	0.1	0.01	0.01		
	93.753	0.01	0.06		
Curing spacer	93.763	0.08	0	0.15	0
	113.10	0	0.08		
Curing retainer	113.10	0.05	0	0.13	0
90mil stock	2.286	0.014	0.127		
	115.386	0.014	0.127		
Curing mold	115.4	0.01	0	0.151	0

Figure 5.17: Inner Layer Packaging for Curing.



Tooling/ Shims	R or t (mm)	+ tol. (mm)	- tol. (mm)	Max. (mm)	Min. (mm)
Mandrel	74.873	0.01	0.01		
Kapton	0.127	0.01	0.01		
	75	0.02	0.02		
L1 pusher	75	0.08	0	0.1	-0.02
	93.653	0	0.08		
Interlayer	0.660	0.019	0.048		
	94.313	0.019	0.128		
L2 pusher	93.653	0.08	0	0.16	0
Cutout	94.653	0.08	0	0.321	0.548
Coil OD	112.97	0	0.05		
Mylar	0.1	0.01	0.01		
	113.07	0.01	0.06		
Curing retainer	113.10	0.05	0	0.14	0.02
90 mil stock	2.286	0.014	0.127		
	115.386	0.014	0.127		
Curing mold	115.4	0.01	0	0.151	0

Figure 5.18: Outer Layer Packaging for Curing.

The 8.8 m long curing press is shown in Figure 5.19, and the press load to cure a QXFA coil is shown in Table 5.10. The results of the stress analysis are shown in Figure 5.20. The maximum stress under normal operation is less than 100 MPa, lower than 1/3 of steel 1050's yield strength (580 MPa). A detailed version of the procedures can be found online at [1].



Figure 5.19: Curing Press

Table 5.10: Curing Press Load for Curing QXFA Coil.

	Capacity (pump psi)	Max. force/cylinder kN (ton)	Spacing cm(inch)	Unit Force kN/m/psi (lb/in/psi)
Main Cylinders	10000	1780 (200)	30 (12)	0.6 (3.34)
Mandrel Cylinders	10000	134 (15)	15 (6)	0.09 (0.5)



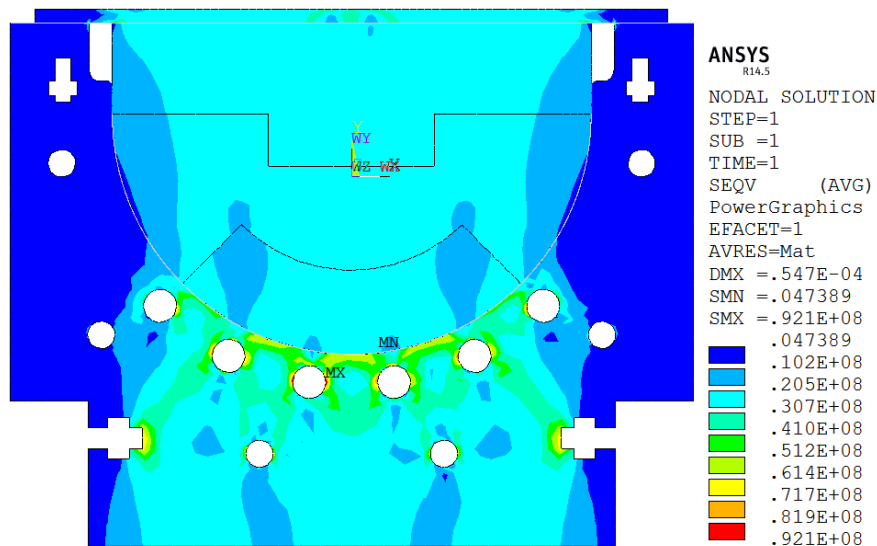


Figure 5.20: QXFA coil curing mold analysis.

To reduce the production risk, the rotation table is prepared as the backup winder for coil winding, as shown in Figure 5.21, which was used for LARP LQ and LHQ coil winding.

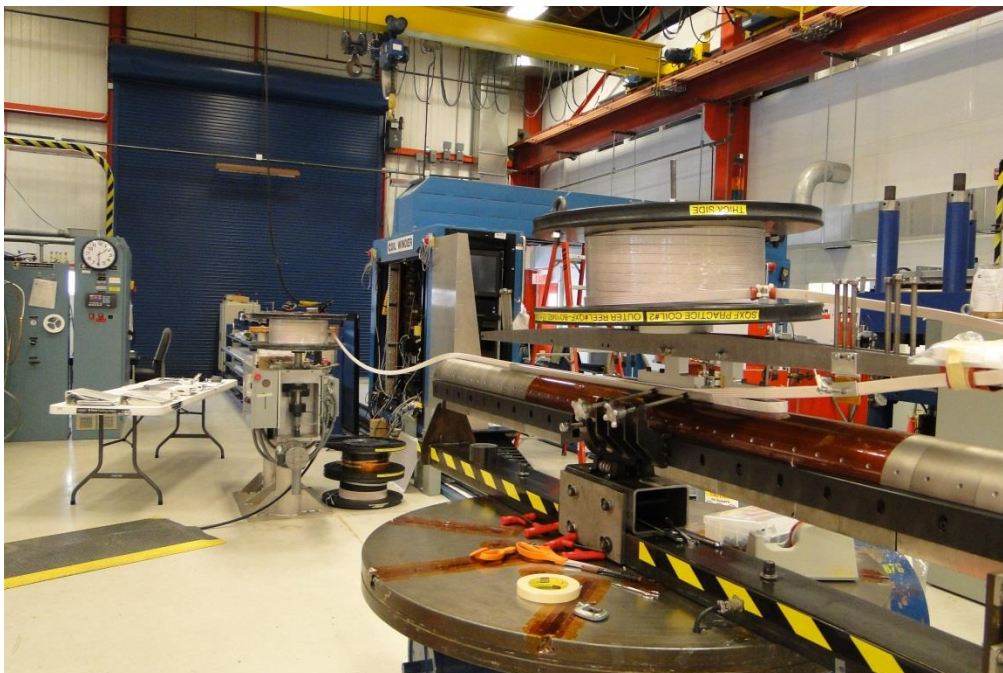


Figure 5.21: Rotation Table.

The coil cross section during winding and curing is shown in Figure 5.22.

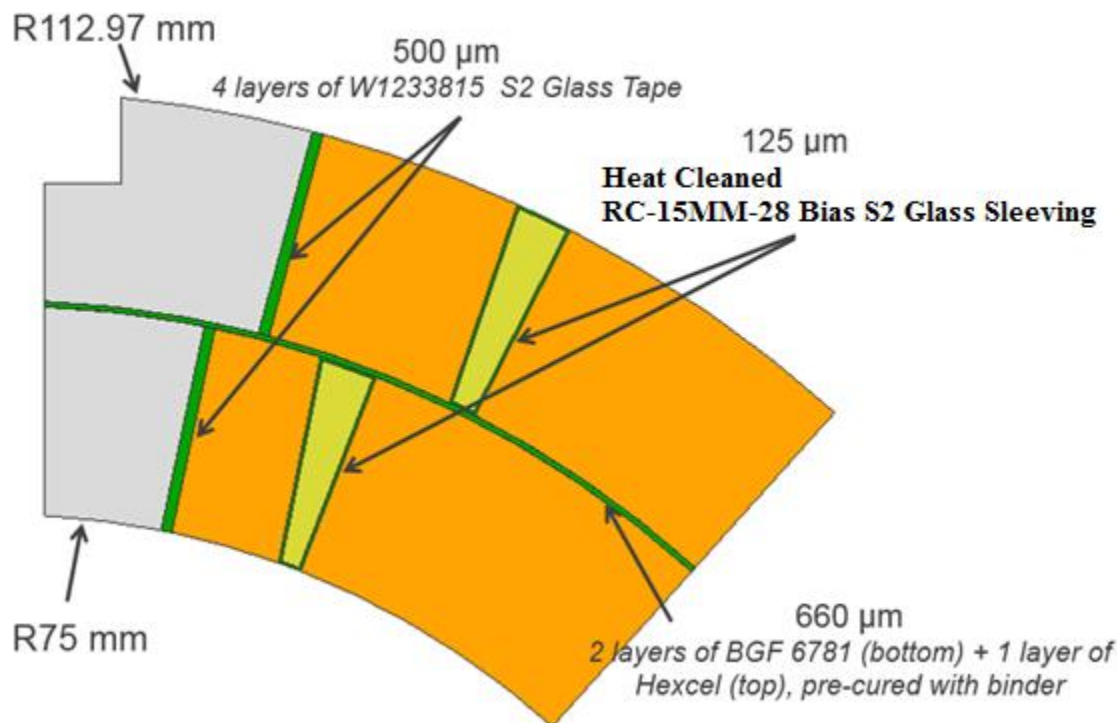


Figure 5.22: Coil cross-section during winding and curing.

#### Materials:

- Pole insulation – S2 glass tape.
- Wedge insulation – S2 glass sleeve.
- Interlayer insulation – BGF 6781 and Hexcel 4522.

### 5.3.2 Reaction

The QXFA coil reaction/impregnation tooling design is based on the designs used for QXFS, HQ and LHQ coils. A cross section of the reaction fixture is shown in Figure 5.23. The closed cavity mold defines the coil size precisely and alignment pins are used to position the pole pieces during reaction and impregnation. The nominal fixture dimensions are shown in Table 5.11. Slender links connect the end saddles to the coil pole to keep the saddles in contact with the cable turns during reaction. A 0.6 mm radial filler is included to allow for the possibility of a small adjustment to the coil outer diameter. The fixture temperature during reaction is monitored continuously by thermocouples bolted to the outside of the reaction fixture.

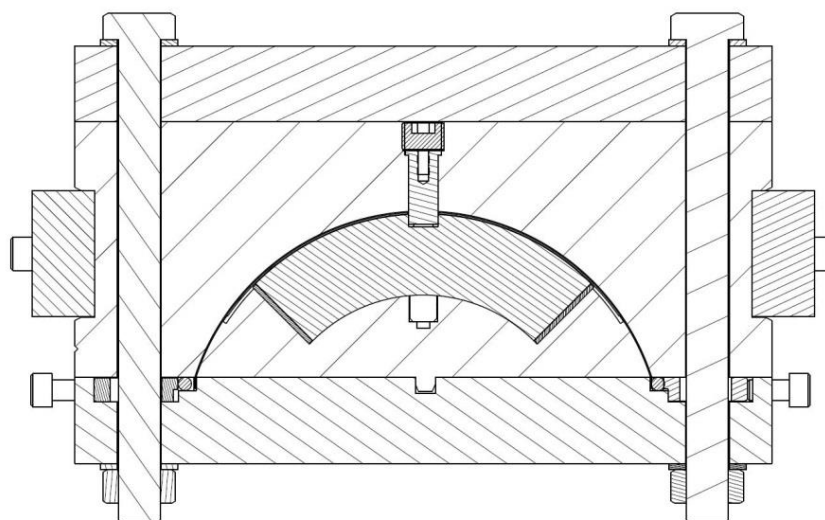


Figure 5.23: Reaction fixture cross section

Table 5.11: QXF Reaction/Impregnation Fixture Dimensions.

Description	Dimension
Inner radius	74.750 mm
Outer radius	113.630 mm
Midplane offset	0 mm

Note:

Dimensions are with liner, radial filler and midplane shims installed.

Reaction takes place in a gas tight oven using an automatic program. The target cycle for the reaction fixture is shown in Table 5.12. The durations and ramp rates for the oven control may be varied in order to achieve the target temperature for the reaction fixture. The reaction fixture is sealed and a continuously flowing argon atmosphere is used to carry away any contaminants that are released during the reaction cycle. Argon flow is supplied independently to the oven at 50 SCFH and to the reaction fixture within the oven at 25 SCFH. Flow rates are sufficient to maintain the oven at a small positive pressure relative to the external atmosphere and the reaction fixture at a positive pressure relative to the internal oven atmosphere. Argon flow is maintained throughout the entire cycle, until the fixture has cooled to a temperature below 100°C. Temperature uniformity within the furnace volume can be maintained to within  $\pm 3^{\circ}\text{C}$  at all three temperature plateaus.

Table 5.12: QXF Coil Reaction Fixture Target Cycle.

	Step	Description	Average Rate	Time
Step 1	Ramp	from 20°C to 210°C	25 C/hour	
Step 2	Soak	210°C		48 hours
Step 3	Ramp	from 210°C to 400°C	50 C/hour	
Step 4	Soak	400°C		48 hours
Step 5	Ramp	from 400°C to 665°C	50 C/hour	
Step 6	Soak	665°C		50 hours
Step 7	Ramp	from 665°C to 20°C		~ 80 hours

Notes:

- Average fixture ramp rate shall not exceed rates listed above.
- Before step 3 the temperature of the reaction fixture shall NOT exceed 215°C.
- Target cycle to be confirmed by the conductor group before each coil reaction.

Mica sheets are set around the coil in preparation for the reaction to reduce friction between materials with different thermal expansions. A sketch of the layers of material installed for reaction is shown in Figure 5.24.

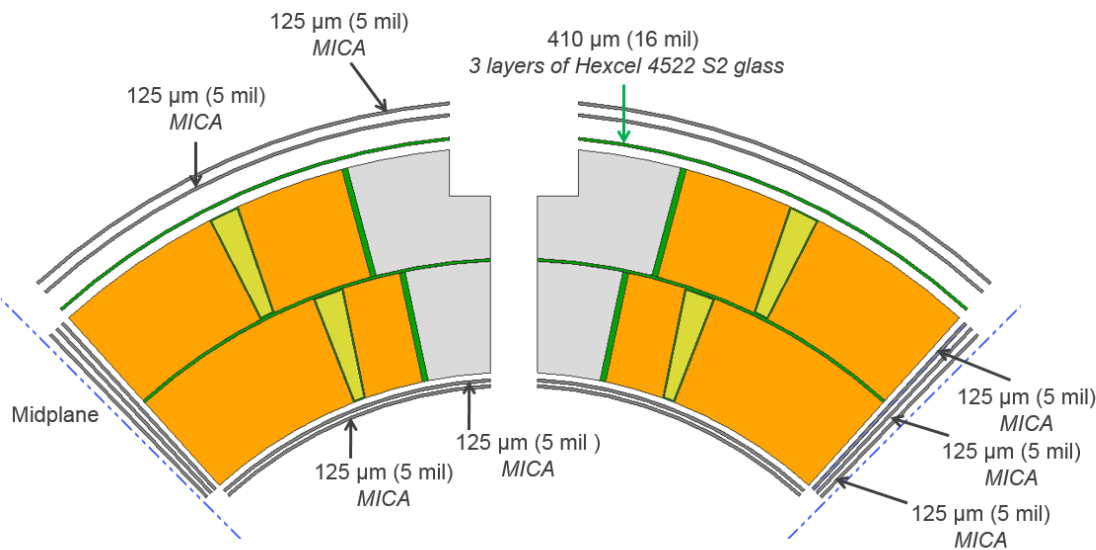


Figure 5.24: Coil cross section during Reaction.

## Materials:

- Mica – Cogebi Cogemica Hi-Temp 710-1.
- Fiberglass – Hexcel 4522.

### 5.3.3 Impregnation

After reaction, coil lead splices are made. The Nb<sub>3</sub>Sn coil leads are soldered to a pair of NbTi cables using MOB39 flux and 96/4 tin/silver solder. Next the outer layer protection heater trace is installed made of copper plated stainless steel foil glued to a layer of polyimide film. Fiberglass cloth and G11 shims are then added to the coil. The fixture is closed and rotated along its long axis to install fiberglass on the coil ID. A sketch of the layers of material installed for impregnation is shown in Figure 5.. The coil is vacuum impregnated with CTD-101k epoxy using a fixture similar to the one used for reaction. The nominal impregnated coil dimensions are shown in Table 5.13.

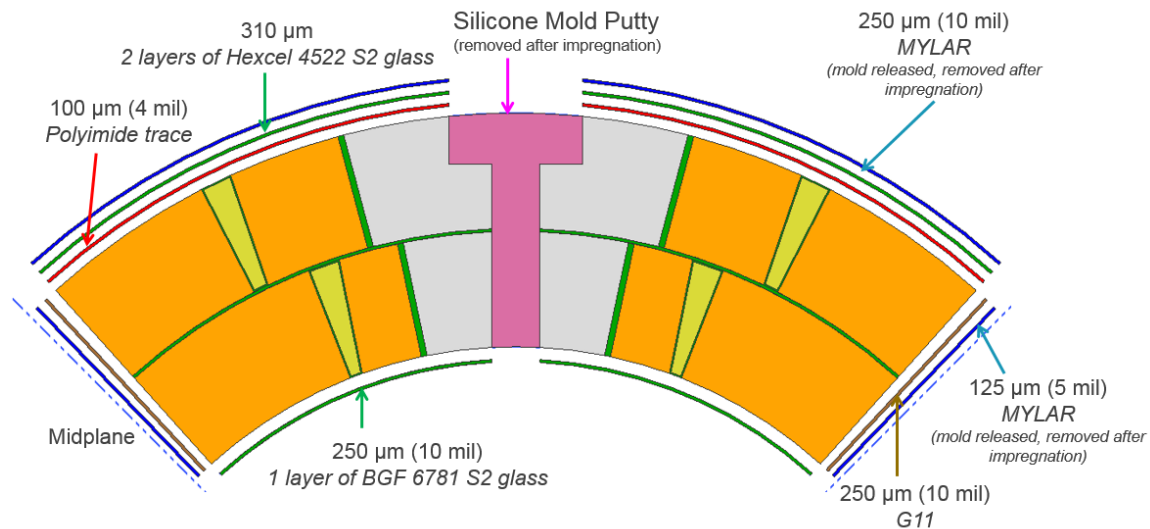


Figure 5.25: Coil cross section during Impregnation.

## Materials:

- Trace – Polyimide + copper plated stainless steel.
- Fiberglass – Hexcel 4522.
- G11 – .250 mm thick.
- Mylar, midplanes – .125 mm thick (mold release applied).
- Mylar, coil OD – .250 mm thick (mold release applied).



Table 5.13: QXF Nominal Impregnation Coil Dimensions.

Description	Dimension
Coil inner radius	74.750 mm
Coil outer radius	113.376 mm
Coil midplane offset	0.125 mm

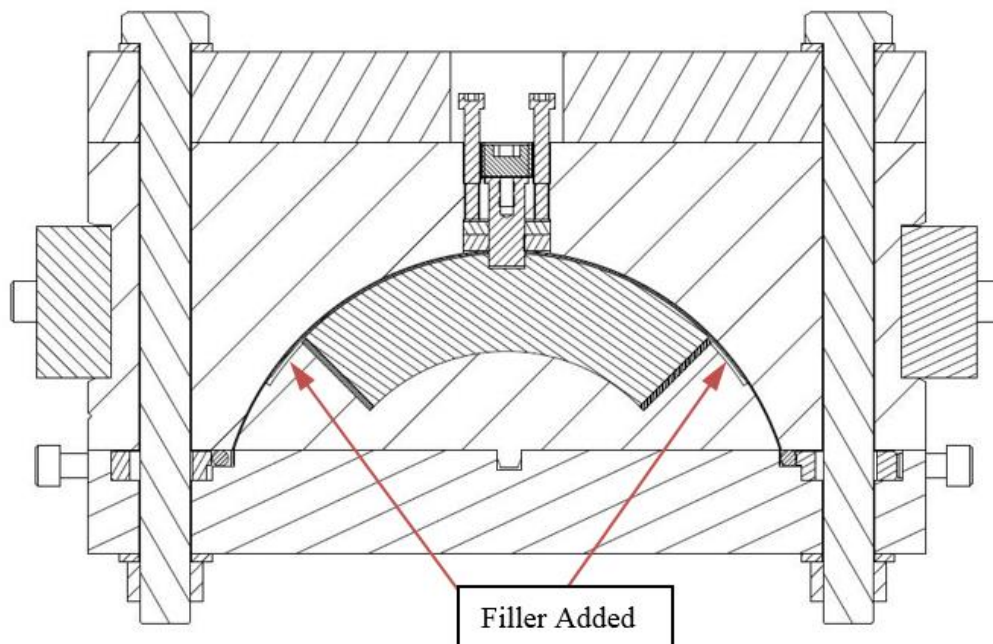


Figure 5.26: Impregnation fixture cross section.

The impregnation tooling is used to epoxy impregnate the coil in a vacuum oven. Fillers are installed to fill the gaps on each side of the mandrel blocks, as shown in Figure 5. This is done to help force the epoxy to flow through the coil instead of through the gaps. The coil is positioned at an incline within the vacuum furnace with the lead end of the coil elevated above the return end. External heaters mounted to the tooling are used for all steps of the impregnation cycle. While under vacuum, the coil is baked at 110° C then cooled back down to 55° C before the impregnation is started. The epoxy is mixed, warmed to 55° C, and degassed to the same vacuum level as the

coil. Once degassed, the vacuum level in the fixture and in the vacuum tank is equalized. The epoxy tank is let up to atmospheric pressure and the pressure differential forces epoxy into the coil. The epoxy is introduced into the return end of the impregnation fixture. The fill rate is controlled by a peristaltic pump, with pump speed set to result in a fill time of about 4 hours. An exit line from the top of the impregnation fixture is connected to an overflow reservoir within the vacuum oven. Once the epoxy flows into the overflow reservoir from the lead end of the coil, the epoxy input hose is clamped off at the return end and a dwell period at atmospheric pressure begins. During the dwell period, small amounts of epoxy back-fills into the coil from the overflow reservoir. After the dwell, the coil is rotated to the horizontal position and the cure cycle in Table 5.14 is used.

Table 5.14: QXF Coil Impregnation Cure Cycle.

Step	Description	Time / Rate
Ramp	from 55°C to 110°C	10 C/hour
Soak	110°C	5 hours
Ramp	from 110°C to 125°C	10 C/hour
Soak	125°C	16 hours

## 5.4 Coil Fabrication at BNL

### 5.4.1 Winding and Curing

Coil winding is done on the existing long shuttle winder using an automated winding program (Fig. 5.27). Insulated cable and coil parts are procured by FNAL and supplied to BNL. The insulated cable is re-spoiled, without any reverse bending of the cable, and split onto two spools for the inner and outer coil layers. The inner layer is wound first. Then it is painted with CTD-1202 binder, packaged for curing and transferred to the curing formblock.





Figure 5.27: Winding Machine.

Coil curing is done utilizing the existing long curing press displayed in Fig. 5.28. The coil mandrel assembly is bolted down into the formblock to set the radial cavity (Figure 5.29). Azimuthal pressure is applied to the coil using 40 six inches diameter hydraulic cylinders. Pressure is applied to close the mold to the nominal coil size. The coil tooling is then heated with electric cartridge heaters installed in both the mandrel and the formblock. The tooling is heated to 150C and held for 1 hour and 45 minutes to cure the binder.

After the inner layer has been cured, the coil is transferred back to the winding machine and the process is repeated for the outer layer. The winding machine is configured so that both layers are wound without any reverse bending of the cable.

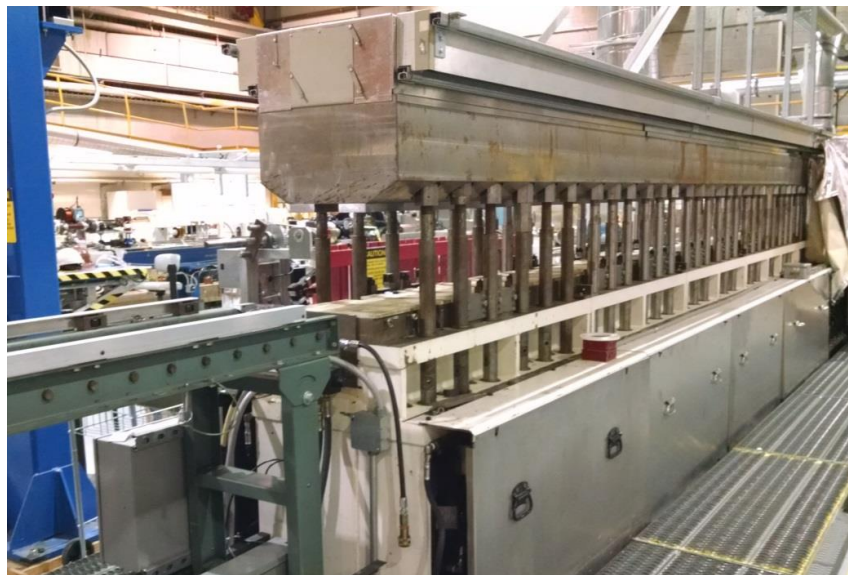


Figure 5.28: Curing Press

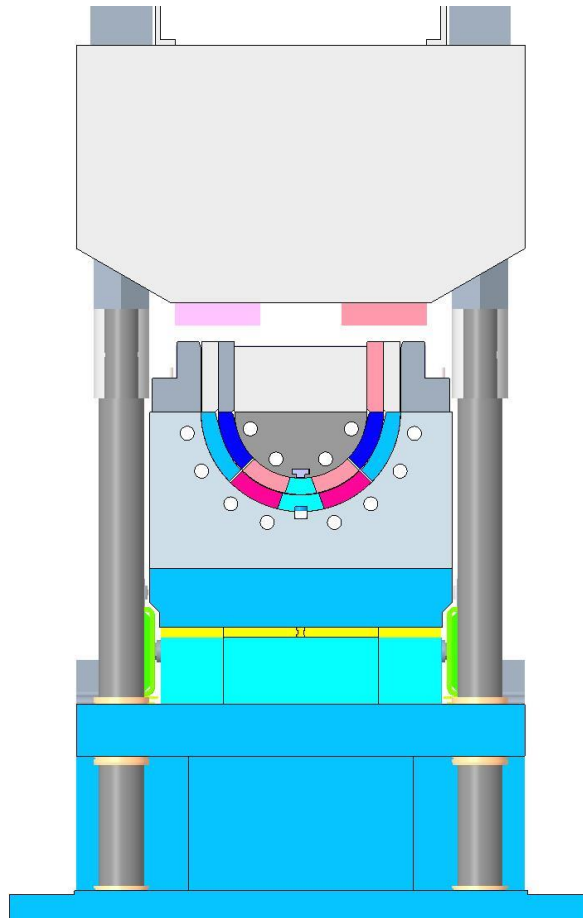


Figure 5.29. Curing tooling in the curing press

Cross sections with tooling dimensions are shown in Figure 5.30.

Tooling Dimensions	in	mm
Mandrel OD	5.906	150.00
L1 Quad Pusher ID	5.906	150.00
L1 Quad Pusher OD	7.374	187.30
L2 Quad Pusher ID	7.382	187.50
L2 Quad Pusher OD	8.895	225.93
Formblock ID	8.903	226.14
L1 Cure Only		
Spacer ID	7.382	187.50
Spacer OD	8.900	226.06
(Teflon wrap)	0.008	0.20

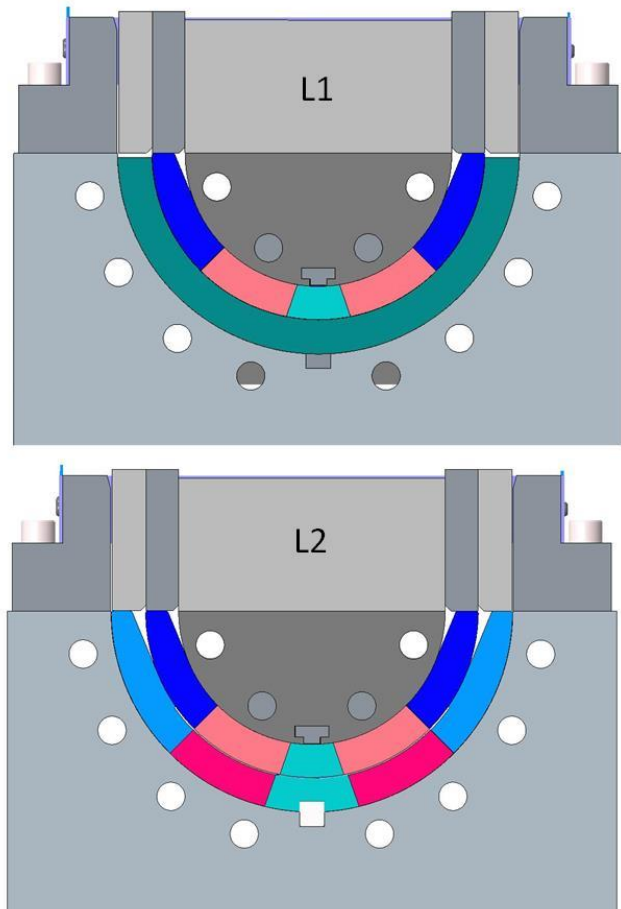


Figure 5.30: Curing tooling dimensions

## 5.4.2 Reaction

The QXF coil reaction/impregnation tooling design is based on the designs used for HQ and LHQ coils. A cross section of the reaction fixture is shown in Figure 5.31. The closed cavity mold defines the coil size precisely and alignment pins are used to position the pole pieces during reaction and impregnation. The nominal fixture dimensions are shown in Table 5.15. Slender links connect the end saddles to the coil pole to keep the saddles in contact with the cable turns during reaction. The fixture temperature during reaction is monitored continuously by thermocouples bolted to the outside of the reaction fixture.

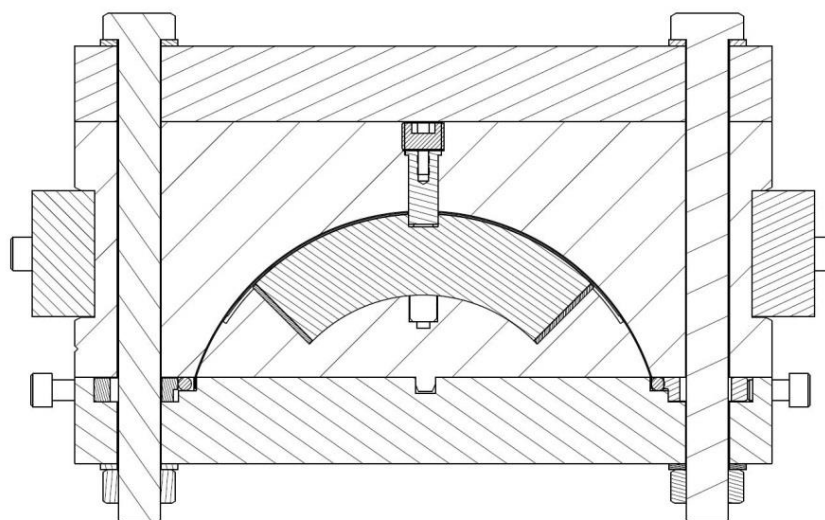


Figure 5.31: Reaction fixture cross section.

Table 5.15: QXF Reaction/Impregnation Fixture Dimensions.

Description	Dimension
Inner radius	74.750 mm
Outer radius	113.630 mm
Midplane offset	0 mm

Note:

Dimensions are with liner, radial filler and midplane shims installed.

Reaction takes place in an existing gas tight 5 meter long oven using an automatic program. The target cycle for the reaction fixture is shown in Table 5.16. The durations and ramp rates for the oven control may be varied in order to achieve the target temperature for the reaction fixture. The reaction fixture is sealed and a continuously flowing argon atmosphere is used to carry away any contaminants that are released during the reaction cycle. Argon flow is supplied independently to the oven at 50 SCFH and to the reaction fixture within the oven at 25 SCFH. Flow rates are sufficient to maintain the oven at a small positive pressure relative to the external atmosphere and the reaction fixture at a positive pressure relative to the internal oven atmosphere. Argon flow is maintained throughout the entire cycle, until the fixture has cooled to a temperature below 100°C. Temperature uniformity within the furnace volume can be maintained to within  $\pm 3^\circ\text{C}$  at all three temperature plateaus.



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Table 5.16: QXF Coil Reaction Fixture Target Cycle.

	Step	Description	Average Rate	Time
Step 1	Ramp	from 20°C to 210°C	25 C/hour	
Step 2	Soak	210°C		48 hours
Step 3	Ramp	from 210°C to 400°C	50 C/hour	
Step 4	Soak	400°C		48 hours
Step 5	Ramp	from 400°C to 665°C	50 C/hour	
Step 6	Soak	665°C		50 hours
Step 7	Ramp	from 665°C to 20°C		~ 80 hours

Notes:

- Average fixture ramp rate shall not exceed rates listed above.
- Before step 3 the temperature of the reaction fixture shall NOT exceed 215°C.
- Target cycle to be confirmed by the conductor group before each coil reaction.

Mica sheets are set around the coil in preparation for the reaction in order to reduce friction between materials with different thermal expansions. A sketch of the layers of material installed for reaction is shown in Figure 5.32.





Figure 5.32: Materials installed for reaction.

#### Materials:

- Mica – Cogebi Cogemica Hi-Temp 710-1.
- Fiberglass – S2 fiberglass cloth.

#### 5.4.3 Impregnation

After reaction, coil lead splices are made. The  $\text{Nb}_3\text{Sn}$  coil leads are soldered to a pair of NbTi cables, using MOB39 flux and 96/4 tin/silver solder. Next the protection heater trace circuits are installed. The trace circuits consist of copper plated stainless steel foil glued to a layer of polyimide film. Fiberglass cloth and G11 shims are then added to the coil. A sketch of the layers of material installed for impregnation is shown in Figure 5.33. The fixture is closed and rotated end-over-end to access the coil ID after work on the OD is complete. The coil is vacuum impregnated with CTD-101k epoxy using a fixture similar to the one used for reaction. The nominal impregnated coil dimensions are shown in Table 5.17.

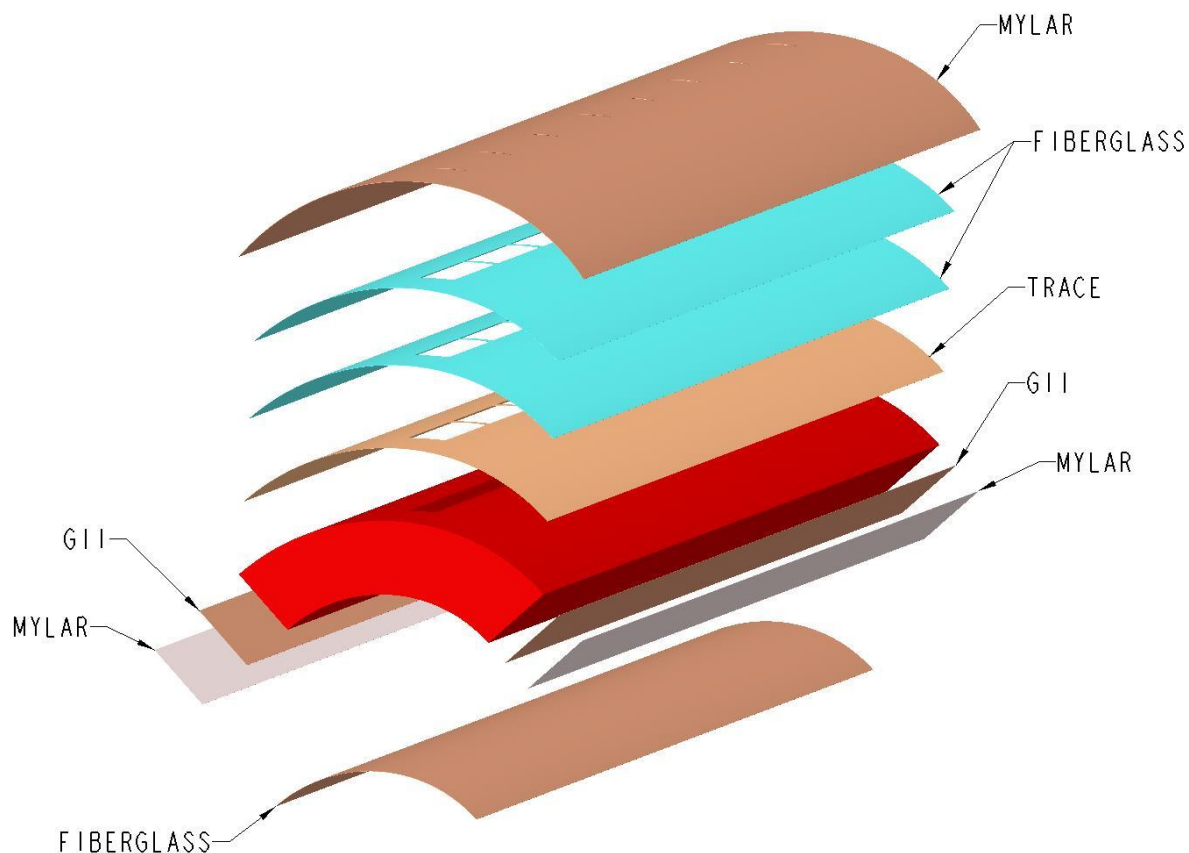


Figure 5.33: Materials installed for impregnation.

## Materials:

- Trace – Polyimide + copper plated stainless steel.
- Fiberglass – Hexcel 4522.
- G11 – .250 mm thick.
- Mylar, midplanes – .125 mm thick (mold release applied).
- Mylar, coil OD – .250 mm thick (mold release applied).

Table 5.17: QXF Nominal Impregnation Coil Dimensions.

Description	Dimension
Coil inner radius	74.750 mm
Coil outer radius	113.376 mm
Coil midplane offset	0.125 mm



The impregnation fixture is closed and sealed. The fixture is hung vertically, lead end up, in a vacuum tank. Strip heaters mounted to the outside of the fixture are used for heating. The fixture and the vacuum tank are evacuated to a vacuum level of 600 mTorr or less. While under vacuum, the coil is baked at 110°C for 8 hours then cooled back down to 55°C before the impregnation is started. The epoxy is mixed, warmed to 55°C, and degassed to the same vacuum level as the coil. Once degassed, the vacuum level in the fixture and in the vacuum tank is brought up to 800 mTorr. The epoxy pot is let up to atmospheric pressure and the pressure differential forces epoxy into the coil. The epoxy is introduced into the bottom of the impregnation fixture. The fill rate is controlled by a peristaltic pump, with pump speed set to result in a fill time of about 4 hours. An exit line from the top of the impregnation fixture is connected to a resin trap outside the vacuum tank. When epoxy reaches the resin trap, the exit line is closed. The supply line remains open, with atmospheric pressure continuing to force resin into the coil. The coil is held overnight, for approximately 16 hours, at 55°C while allowing epoxy to continuously draw into the coil. After the overnight soak, the cure cycle is initiated. The epoxy is cured using an automatic cycle as shown Table 5.18. Vacuum is maintained in the vacuum tank until the cure is complete.

Table 5.18: QXF Coil Impregnation Cure Cycle.

Step	Description	Time / Rate
Ramp	from 55°C to 110°C	10 C/hour
Soak	110°C	5 hours
Ramp	from 110°C to 125°C	10 C/hour
Soak	125°C	16 hours

## 5.5 Coil Handling and Shipment

The MQXFA coil handling and shipping are specified in [3,4]. We provide here a summary for information only. The official document can be accessed through the link provided in [3, 4]

MQXFA coils are made of brittle Nb<sub>3</sub>Sn conductor. In order to prevent conductor degradation, all handling and shipment operations shall meet the following requirement:

**Coil H&S Requirement #1: The conductor strain shall never exceed 500 microstrain in any part of the coils during any handling or shipping operation.**

A coil shipping fixture is used to support the coils for shipment between labs. The fixture consists of an aluminum support tube mounted in an aluminum channel using rubber shock mounts. Side rails support the full length of the coil midplane. A series of clamps are applied over the coil OD. Longitudinal restraint is provided by bolts contacting the ends of the coil saddles. The fixture is shown in Figure 5.34: .

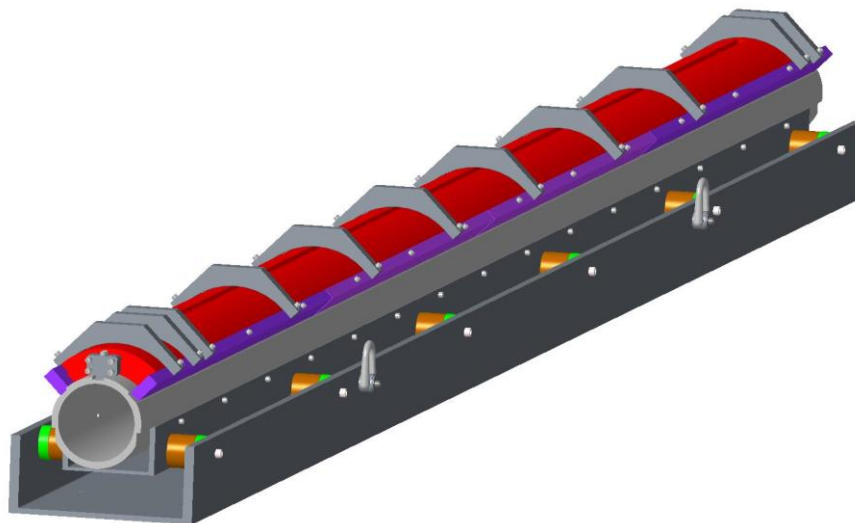


Figure 5.34: Coil shipping fixture.

The shipping fixture is installed inside a wooden crate. Shipment is made using a dedicated truck such that the once the crate is loaded onto the truck at the origin lab, it remains on the truck until it arrives at the destination lab. There is no loading and unloading permitted while on route. The shipping fixture is instrumented with accelerometers and shock watches are placed on the crate [2] If there are no shocks above 5 g the standard QC for coil reception can be performed. This threshold was determined through analysis of coil shipments and magnet test results. FEM analysis confirmed that shocks up to 5 g are acceptable using the AUP MQXFA coil shipping fixture [5].

## References

[1] MQXFA Electrical design criteria, US-HiLumi-Doc-826, April 2018:

[https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=826&filename=AUP\\_Electrical\\_Design\\_Criteria\\_v12.pdf&version=7](https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=826&filename=AUP_Electrical_Design_Criteria_v12.pdf&version=7)

[2] Interface control document, US-HiLumi-Doc-252 and US-HiLumi-Doc-309,

[3] MQXFA Coils Handling & Shipping Requirements, US-HiLumi-Doc-820, January 19, 2018.  
<http://us-hilumi-docdb.fnal.gov/cgi-bin/ShowDocument?docid=820>

[4] MQXFA Coils Handling & Shipping Requirements, US-HiLumi-Doc-1686, November 16, 2018 coil <https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/ShowDocument>

[5] Heng Pan, “FEM analysis of MQXFA coil during shipment” US-Hilumi-DocDB-820

## 6 MQXFA Structure and Magnet Assembly

### 6.1 Magnet Structures Features

As described in the section 4.3 (Structural Design), the main features of the support structure design as shown in Fig. 6.1 are:

1. Shell-based support structure relying on the “bladder and key” technology to perform azimuthal pre-loads, which allows a reversible assembly process and tunable preload;
2. The aluminum shell is segmented into sections to minimize axial tension in the shell and to ensure a uniform azimuthal load on the coil;
3. The use of master key packages between the yokes and the pads allow for assembly clearances prior to preload operations.
4. G11 alignment keys inserted into the pole pieces provide the coil alignment and to also intercept some of the forces from the shell during pre-load and cool-down conditions;
5. Axial pre-load is applied by four stretched axial stainless steel rods that react against endplates on each end that transfer to the forces to the coil.

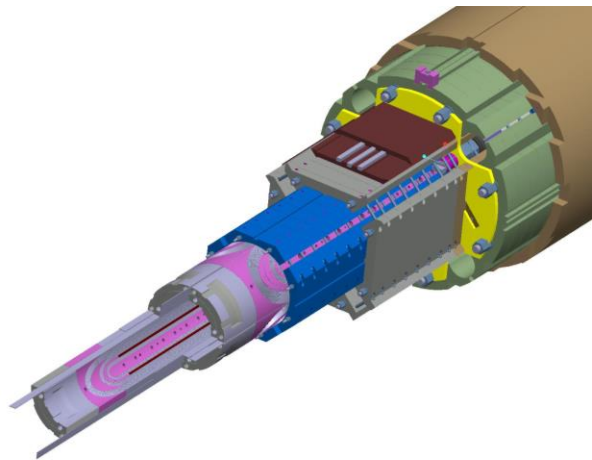


Fig. 6.1: 3D exploded view of the end of an MQXF magnet (axial end loading and splice connection components not shown).

### 6.2 Magnet Assembly Requirements

The Functional Requirements Specification are listed in Section 2, and describe the functional requirements for the MQXFA coldmass structures. Specifically for the MQXFA magnet structures, Table 6.1. lists the relevant requirements from the complete list, and how they are satisfied in this structure design.

Table 6.1. Relevant Functional Requirements for the MQXFA magnet structures

Requirement	Description	Criteria Met
	<b>Threshold Requirements</b>	
R-T-02:	Physical outer diameter must not exceed 614 mm.	O.D of shells are 614 mm.

R-T-06:	The MQXFA cooling channels must be capable of accommodating two (2) heat exchanger tubes running along the length of the magnet in the yoke cooling channels. The minimum diameter of the MQXFA yoke cooling channels that will provide an adequate gap around the heat exchanger tubes is 77 mm.	Yoke cooling hole dimensions are designed to 77 mm.
R-T-08:	The MQXFA structure must have provisions for the following cooling passages: (1) Free passage through the coil pole and subsequent G-11 alignment key equivalent of 8 mm diameter holes repeated every 50 mm; (2) free helium paths interconnecting the yoke cooling channels holes; and (3) a free cross sectional area of at least 150 cm <sup>2</sup>	(1) G11 alignment keys are provided with holes for through passage of helium. (2) Yoke laminations at shell junctions provide a total of 15.5 cm <sup>2</sup> cross talk between each cooling holes. (3) <i>To be verified at the cold mass</i>
R-T-14	Splices are to be soldered with CERN approved materials.	Splice joints are made using CERN-approved Sn96Ag4 solder.
R-T-15	Voltage Taps: the MQXFA magnet shall be delivered with (a) three redundant (3x2) quench detection voltage taps located on each magnet lead and at the electrical midpoint of the magnet circuit; (b) two (2) voltage taps for each quench strip heater; and (c) two (2) voltage taps for each internal MQXFA Nb3Sn-NbTi splice. Each voltage tap used for critical quench detection must have a redundant voltage tap.	<i>*Redundant VTs not yet installed in MQXFAP2. These are planned for MQXFA03 and subsequent production magnets.</i>
R-T-20	All MQXFA components must withstand a radiation dose of 35 MGy, or shall be approved by CERN for use in a specific location as shown in [6]”	Materials chosen for the magnet structures have been approved by CERN.
<b>Objective Requirements</b>		
R-O-01	Variation of local position of magnetic center must be within $\pm 0.5$ mm; variation of local position of magnetic axis within $\pm 2$ mrad. Local positions are measured with a 500 mm long probe every 500 mm.	<i>*Measurements to be performed and analyzed with MQXFAP2 assembly.</i>
R-O-04	Splice resistance target is less than 1.0 n $\Omega$ at 1.9K.	Magnet splices from MQXFS and MQXFAP1 have been measured to have <1.0 n $\Omega$ .

## 6.2.1 MQXFA Magnet Assembly Specification

The magnet assembly must meet two primary specifications:

- Ensure coil preload is uniform to  $\pm 10$  MPa at the pole
- R-O-01: Variation of local position of magnetic center must be within  $\pm 0.5$  mm; variation of local position of magnetic axis within  $\pm 2$  mrad. Local positions are measured with a 500 mm long probe every 500 mm.

### 6.2.1.1 Uniformity of coil preload

The uniformity of the preload will be determined by the tolerances of the parts when fabricated. Figure 6.2 shows a quadrant of the MQXFA magnet cross-section showing the interfaces of the various components when assembled. Table 6.2 lists those parts and their respective allowed manufacturing tolerances. A worst case scenario (though unlikely) would be that the all parts would vary at the maximum extent of the tolerance band and add up (not including the coil variances), which would represent a total of  $\pm 325$   $\mu\text{m}$  of variance, translating to  $\pm 43$  MPa. However, a statistical spread would better represent how all these tolerances stack up. The RMS tolerance stack up is then calculated to be  $\pm 31$   $\mu\text{m}$ , which translates to  $\pm 9$  MPa. It should be noted that although the variances of the impregnated coil can be  $\pm 250$   $\mu\text{m}$ , the radial shims used to build up the coil pack should be able to accommodate gross variances.

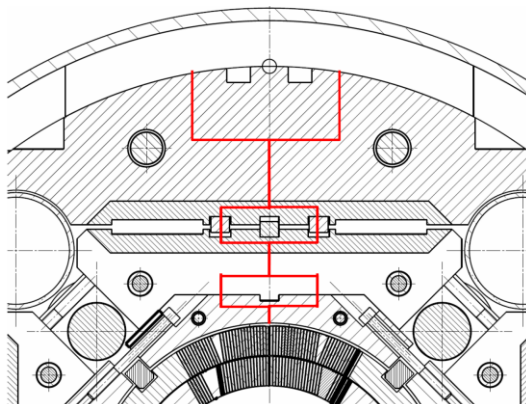


Figure 6.2: Magnet cross-section, showing areas of interfaces.

Table 6.2. Magnet Components Dimensional Specifications.  
Different colors represent subassembly interfaces.

Comp	Description	Stack tol. [ $\mu\text{m}$ ]
Shell	Inner radius	$\pm 25$
Yoke	Outer radius	$\pm 25$
	Main master contact	$\pm 25$
Master 1&2	Main yoke/pad contact x2	$\pm 50$
	Load key x2	$\pm 25$
Pad	Main master contact	$\pm 25$
	Main collar contact	$\pm 25$
Collar	Main pad contact	$\pm 25$
	Inner radius	$\pm 25$
Coil (see Section 5.1)	Outer Radius	$\pm 250$



6.2.2 Magnet QA/QC Plan

c. Magnet Structures Components Mechanical Measurements

The magnet structure parts will be inspected by the respective vendors where the parts will be fabricated. Components that consist of large quantities of parts (ie. Yoke laminations, etc.) will have only 10% of the batch measured, with an incoming inspection of a random sample performed at LBNL.

d. Magnet Electrical Measurements

At various stages of the magnet assembly process electrical QC measurements will be taken. This will ensure that throughout the entire assembly process the electrical integrity of the magnet is maintained. US-Hilumi Doc 956 describes the details, but the various measurement hold points are listed in Table 6.3.

Table 6.3. Magnet Assembly Electrical Measurement hold points.

Hold Point	Measurement
<i>Coil Reception</i>	Hipot, Impulse, Seq. R, Inductance
<i>Coil Pack Assembled</i>	Basic R checks
<i>Magnet Azimuthally loaded</i>	Basic R checks, Impulse, Hipot (optional)
<i>Magnet Axially loaded</i>	Hipot, impulse (individual coils)
<i>Magnet spliced and connectorized</i>	Seq. R, Inductance, Impulse (magnet), PH R, Hipot
<i>Magnet Pre-shipment</i>	Basic R checks to ground

6.3 Magnet Assembly Breakdown Structure

Fig. 6.3 shows the magnet assembly breakdown structure (ABS) flowchart of the long magnet assembly. The ABS shows the subassemblies that make up the assembled magnet and helps to organize the required processes and captured data. The primary assembly drawings are listed in Table 6.4, although the full complement of approximately 130 drawings for the magnet structures components are listed elsewhere. Uncontrolled versions of the drawing package can be found in US-HiLumi Doc 953; all current version-controlled drawings are maintained on the LBNL Windchill document database.



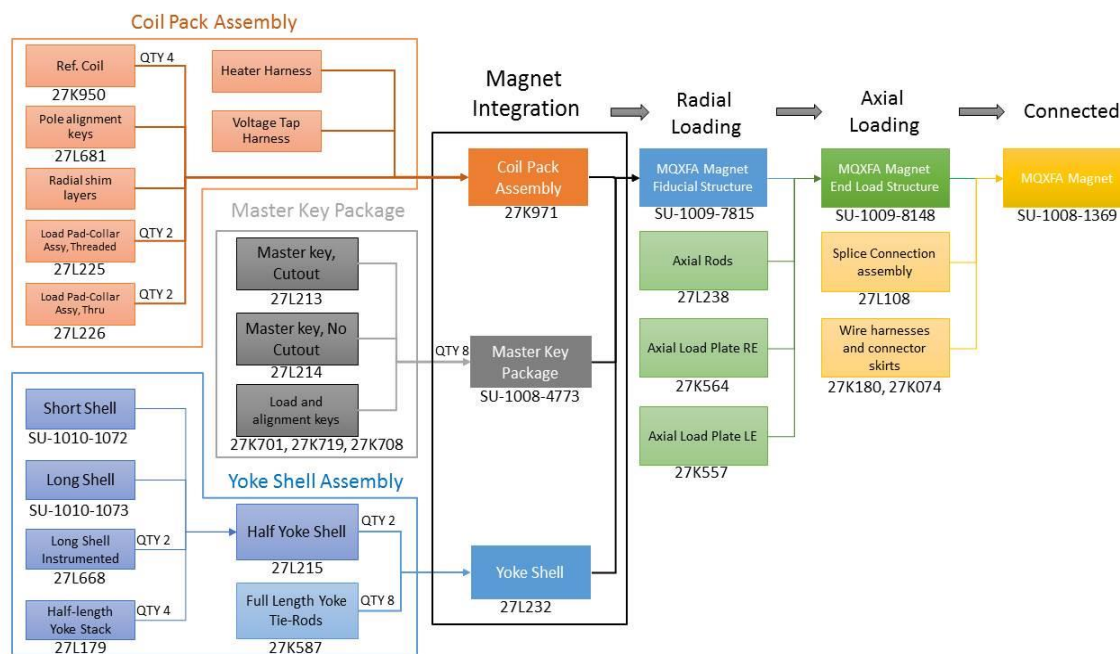


Fig. 6.3: MQXFA magnet assembly breakdown structure flowchart with associated drawings.

Table 6.4. Magnet Assembly drawing packages.

Description	Drawing #	Notes
MQXFA Magnet Assembly	SU-1008-1369	26 additional dwgs in this package
MQXFA Axial loaded structure	SU-1009-8148	11 additional dwgs in this package
MQXFA Magnet fiducial structure	SU-1009-7815	
Coil Pack Assembly	27K971	47 additional dwgs in this package
Master Key Package	SU-1008-4773	10 additional dwgs in this package.
Yoke-shell Subassembly	27L232	31 additional dwgs in this package
		<b>131 Total drawings</b>

## 6.3.1 Shell-Yoke Subassembly

### 6.3.1.1 Shells

The shells are 614 mm O.D. by 556 mm I.D. The MQXF magnet adopts segmented shells to minimize the axial tension in the shell segments and to ensure a uniform azimuthal load on the coils. There are two lengths of shell segments used in the assembly: a 325.65 mm long segment (two ea.) used at each extremity; and six 651.29 mm long segments stacked in between the short ones.

As shown in the Fig 6.4 each shell segment has various cutouts on each end, for alignment, tooling, and supports. There are pin slots machined into each quadrant of the ID on each end of the shells, though pins will be used only in one quadrant during magnet assembly operations.

The shells are fabricated and inspected by the vendor, then each individual shell will then be measured again upon receipt. The average I.D. will also be measured at five axial locations along the length of each shell segment: approximately 25 mm from each end, and three equally spaced mid-length locations. These measurements are used to determine an optimal arrangement and order that will be used when assembling these shells in the magnet structure. Once the order of shells is determined, three of the six long shells will be instrumented with strain gauges so that preload operations can be measured against the analytical targets.

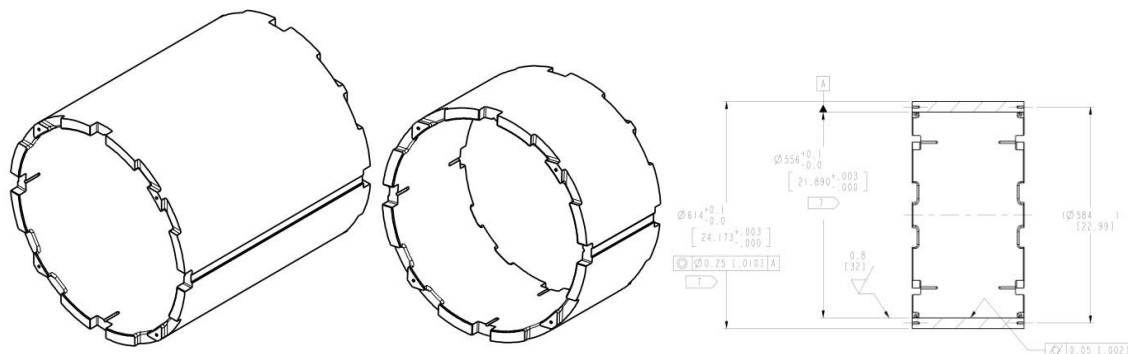


Fig. 6.4: The long and short shell segments, and dimensions of the cross section of the short shells.

## 6.3.1.2 Yokes

The iron yoke laminations are typically 49 mm (~1.93 in.) thick and made of ARMCO Pure Iron (Grade 4). Each quadrant of the yoke stacks is joined using two 19.05 mm (¾ in.) diameter stainless steel tie rods, and aligned by close-fitting aluminum bronze bushing sleeves. Each tie rod is pre-tensioned to 40,000 N (9000 lbs). Since the cooling holes in the MQXFA magnet are found in each quadrant, the required 77 mm clearance bore is actually formed by two adjacent yoke profiles.

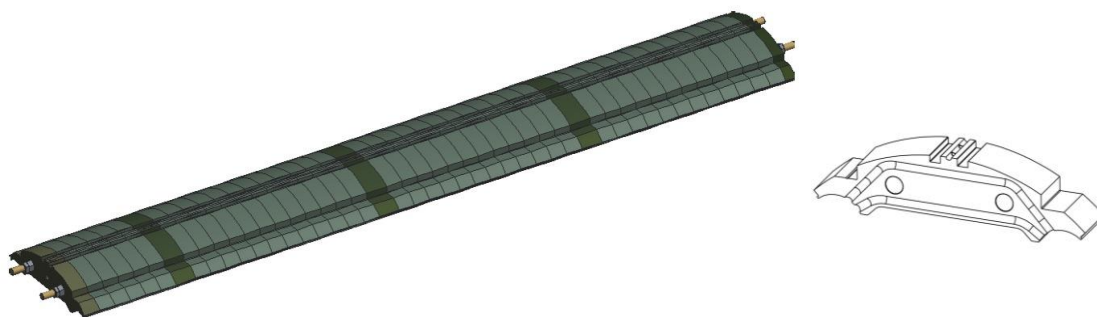


Fig. 6.5. (L) 3D model of a half-length yoke stack, and (R) a typical yoke lamination used at the junction between shells.

The yoke laminations are initially stacked into “sub-stacks” corresponding to the junction of the shell segments. These sub-stacks are then assembled into eight 2281.5 mm (89.82”) long sub-assemblies, which is half the length of the magnet. See Fig. 6.5. Four of these subassemblies will be assembled per half-length shell-yoke subassembly prior to the final integration of the full-length structure. The fact that these laminations bridge between shell segments increases the longitudinal stiffness of the shell assembly. However, when joined together the half-length shell-yoke subassemblies are not bridged at the center: only the yoke bushings and the coil pack assembly components bridge the full-length structure. It is for this reason that the yoke tie rods must be



tensioned properly, since the tensioned yoke stacks provide the stiffness for the structure; the next section describes this process.

Special intermediate yoke laminations separate these pre-stacks in a half-length assembly. Though keeping the same basic geometry, the laminations located at the junction between two shell segments have additional features. First, there are two grooves cut into the mating faces of these yoke laminations to satisfy the cooling requirements (R-T-08(3)) when the magnet is in service, with each groove providing about  $0.48 \text{ cm}^2$  of clear passage. A full-length yoke stack therefore provides approximately  $15.5 \text{ cm}^2$  passage between each quadrant's cooling holes. Secondly, there are tapped holes at the crown, which are provisions for the welding block that will be attached when the SST LHe cryostat shell is welded over the magnet structure after a successful cold test.

### 6.3.1.3 Shell-Yoke Subassembly Operations

When assembling the shell-yoke subassembly, four shells (three long, one short) are initially stacked vertically on the assembly stand. Pins are inserted only in the “Top” quadrant slots initially to align the shells prior to the insertion of the half-length yoke stacks.

The four yoke stacks are then inserted vertically inside the stack of shells (Fig 6.6). A bladder operation is performed to insert the gap keys and constrain the yokes against the shells. The cooling holes in the yokes are utilized as the bladder locations to open up the gaps, which is more efficient than the operating the bladders at the internal cross support geometry. The nominal yoke gap is 12 mm, but the gap keys are shimmed to approximately 12.1 mm total to achieve a shell strain of approximately  $200 \text{ } \mu\text{m/m}$ .

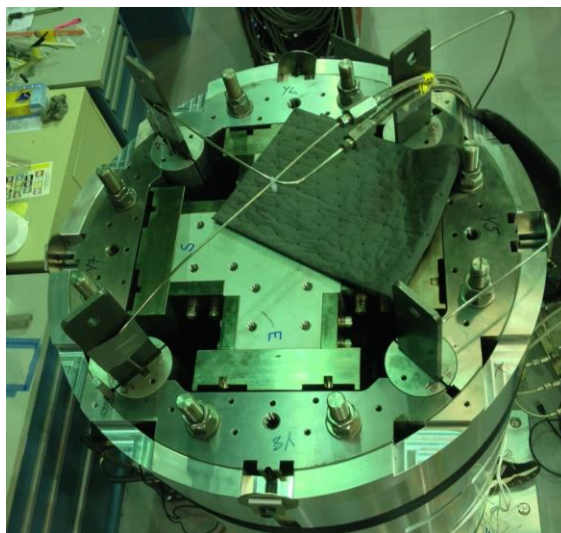


Fig. 6.6. (L) Half-length shell stack on the assembly stand. (R) View from the top, with the yoke quadrants ready to be preloaded.

Once the tooling is removed and the assembly has been moved, the process is repeated for the second half-length subassembly, after which they are both placed on the magnet integration table; see Figure 6.7. The dimensional size of the yoke opening is measured, and these values are used to calculate the master key initial shim package. When both half-length assemblies are joined

together the centermost bronze bushing sleeves are replaced to span the halves, in addition to the short yoke tension rods being replaced with full-length ones. A hydraulic rig is used to pre-tension these full-length yoke tension rods to carry 9000 lbs. each. See Fig. 6.8. This completes the shell-yoke subassembly.

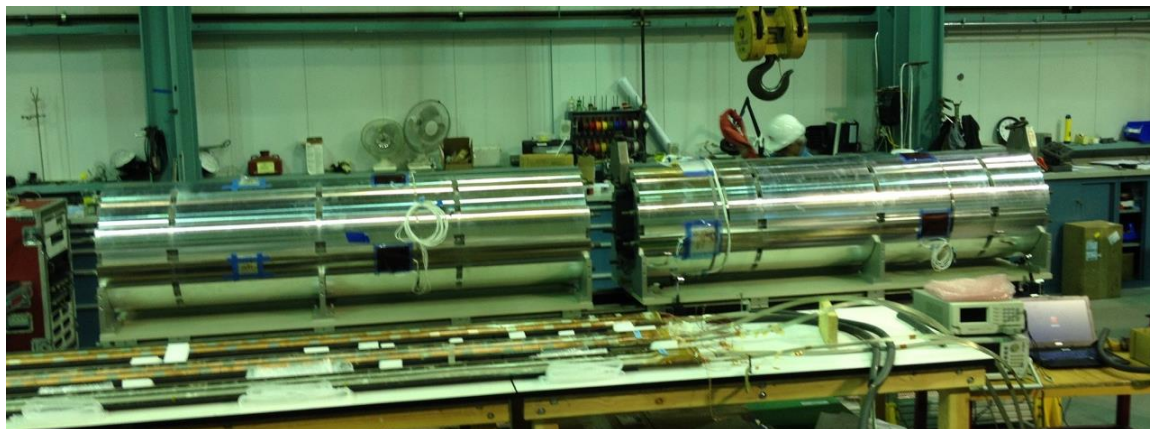


Fig. 6.7. Two half-length yoke-shell subassemblies, ready to be joined.



Fig. 6.8. Hydraulic rig for pre-tensioning the yoke tie rods.

## 6.3.2 Coil Pack Subassembly

### 6.3.2.1 Dressed Coils

When received, each impregnated coil undergoes a series of electrical and mechanical CMM measurements. These measurements will be used to determine the order and placement of each coil in the coil pack assembly. Once complete, a ground plane insulation (GPI) layer, made up of 75  $\mu\text{m}$  polyimide and a 37  $\mu\text{m}$  B-stage epoxy layer, is attached to each coil around the OD and midplanes. The CMM measurements may also define whether an additional shim layer at the midplane, or additional radial shims, are required in later assembly operations. Support pads, called pions (CERN drawings: LHCMQXFMO347), for the eventual beam tube will also be attached to the coils at this point while the coil poles are accessible before the coil pack is assembled. These

will be nominally spaced 800 mm apart, but the bottom pair of coils will have theirs offset by 400 mm with respect to those found on the upper pair of coils.

Presently, coils are instrumented with strain gauges on the pole islands in three axial locations allowing for strain measurements in the azimuthal and axial directions. The expectation is that the final design will utilize only a single axial station on the coil at the return end of the magnet, which would then be removed after a successful magnet test, before the insertion of the beam tube as part of the cryostat and cold mass assembly. Finally, the G-11 pole keys are installed (but not shimmed to size yet) at this time. Note again, that these G11 pole keys also have 50 mm spacing of 8 mm holes to provide for the cooling required through the coil poles.

### 6.3.2.2 Pad-Collar Stacks

The aluminum collar laminations and the load pad laminations will be assembled together in four full-length stacks, one for each quadrant. Both lamination types are typically 50 mm (1.969 in) thick. While the collars are all 6061 aluminum, the load pads are made of ARMCO Pure Iron (Grade 4) in the straight section; each end must be stainless steel (304CO, low-cobalt) on the ends, in order to reduce the peak magnetic field.

The load pad is assembled first using short “sub-stacks” that correspond to the length between particular collar laminations. These sub-stacks are assembled into a full-length load pad assembly stack, aligned by aluminum bronze bushing sleeves, and joined using two 11.11 mm (7/16”) pre-tensioned stainless steel tie rods.

Collar laminations are then stacked upon each assembled load pad. The collars are also aligned by aluminum bronze bushing sleeves, as well as by the key feature of the load pad geometry. Two 6.35 mm (1/4 in.) stainless steel tie rods are tensioned to 1000 lbs. each. The collars assembly is held to the load pads via bolts through five load pad and collar lamination pairs along the length. These bolts are removed prior to the final assembly. See Fig 6.9.

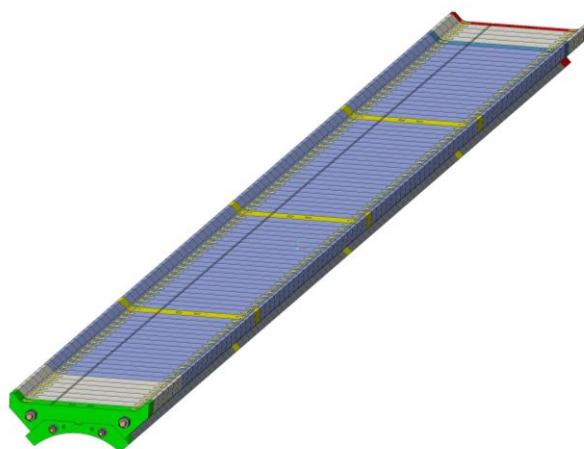


Fig. 6.9. Full-length load pad-collar assembly. The lighter colored ends of the load pads are SST instead of ARMCO Pure Iron.

### 6.3.2.3 Coil Pack Assembly Operations

The bottom pad-collar assembly is placed on the coil pack assembly table, and the two side pad-collar assemblies are assembled on the two pivot tables beside the primary assembly table. See Fig. 6.10. Based on the earlier CMM measurements performed on the coils, the inner curved surface



of the collar stacks are lined with layers of G11 and/or polyimide as radial shims. While the nominal radial shim stack is 0.5 mm, including the coil GPI layer, the actual stack may vary depending on these CMM measurements. The first build also incorporates the use of pressure sensitive film as part of the radial stack up. These layers are eventually replaced by either polyimide or G11 in the final build. See Fig. 6.11.

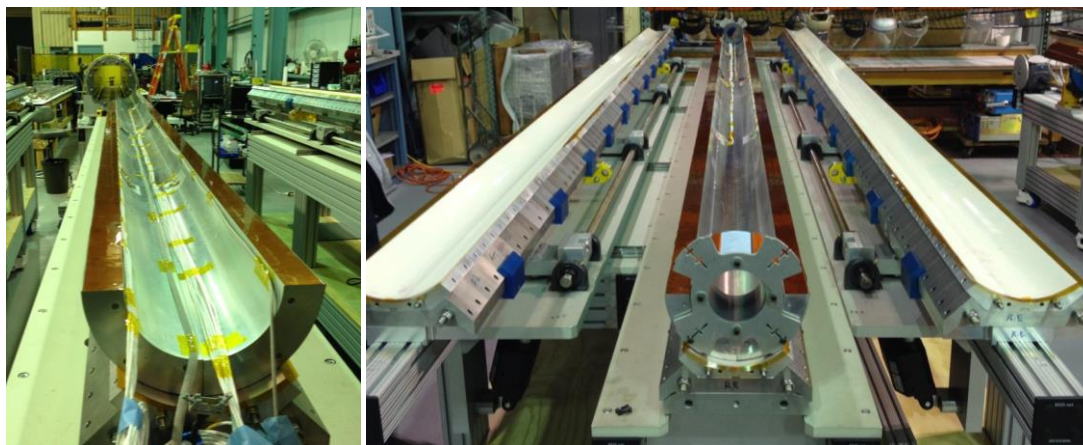


Fig. 6.10. (L) The bottom pair of (dummy) coils placed on the bottom pad-collar assembly. (R) The side pivot tables shown.

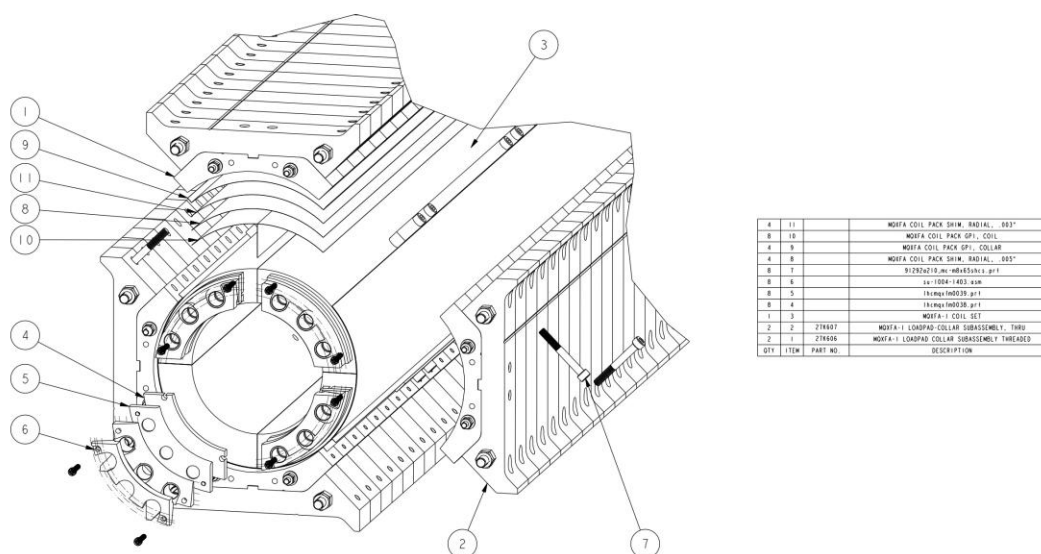


Fig. 6.11. The coil pack assembly shim layers.

The bottom pair of dressed coils is then moved onto the bottom pad-collar assembly. The upper pair of coils follows this operation, being secured on the assembly before the side pad-collar assemblies are rotated into place. Finally, the upper pad-collar assembly is placed on top, and all the pads are bolted together. At this stage, with unshimmed alignment keys inserted into the coils the gaps between these keys and the collars are measured.

This first assembly with pressure-sensitive paper is disassembled so that the layers can be replaced with the appropriate radial shims, and the alignment keys can be shimmed accordingly to ensure the collar-key contact conditions desired. This will ensure both proper alignment and force

interception from the shell. As of this writing, the design is to leave an average 25  $\mu\text{m}$  gap per side on the alignment keys. The final coil pack is measured; these measurements are used to calculate the initial shim package of the master keys described in the next section. See Fig. 6.12.

A warm magnetic measurement of the coil pack will be performed at this time to ensure that there is nothing grossly out of alignment, and this information will be compared with the later final fiducialization measurement performed after the magnet assembly is complete.

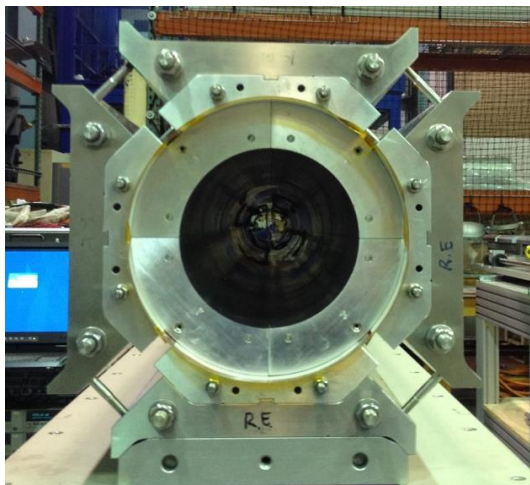
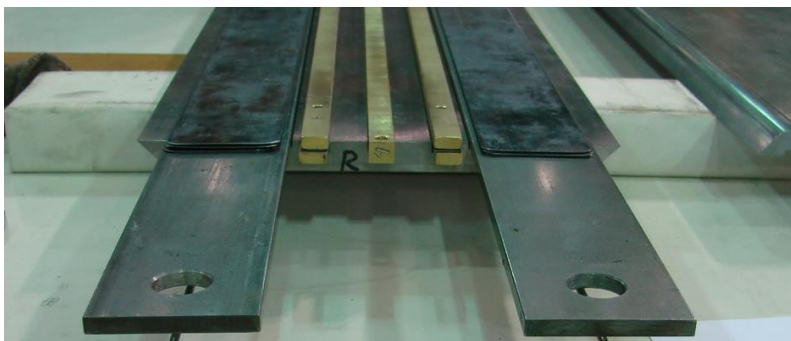


Fig. 6.12. The (dummy) coil pack assembly, with shim layers visible between the coils and collars.

## 6.3.3 Magnet Integration

### 6.3.3.1 Master Key Packages

The mechanical measurements of the yoke opening and the coil pack are used to calculate the initial master key package shims. The master assembly consists of two master key plates, each with slots for bladders, load keys, and an alignment key. The master assemblies will be assembled (“kitted”) with a uniform amount of shims in all the quadrants initially. See Fig 6.13.



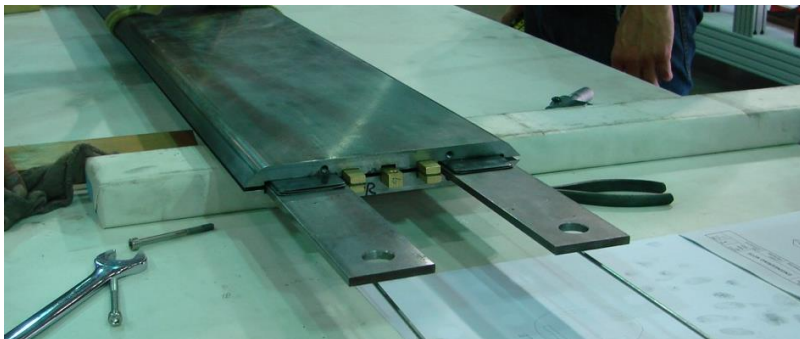


Fig. 6.13. (Top) Kitting the master key packages; (bot) assembled master key package.

The coil pack is inserted into the yoke opening using a set of rollers in the yoke cooling hole slots. Only the bottom quadrant master keys are present in this stage (Fig 6.12). Once the coil pack inserted, however, the rest of the master keys can be inserted into each quadrant.

### 6.3.3.2 Magnet Preload Operations

The high-pressure pump is attached to the bladders on both ends of the magnet (keys and bladders are half-length). The load keys will be shimmed to obtain the target strain on the shells and coils, as measured by the strain gauges, determined by the FEA model. A final magnet (mechanical and magnetic) fiducial survey will be performed at this stage.

When the azimuthal preload is completed, the axial loading rig is attached to the axial rods to perform the axial preload operations (Fig 6.14). This completes the magnet preload operations. Electrical QC measurements are taken at this stage to ensure that none of these operations have damage coils, or insulation layers.

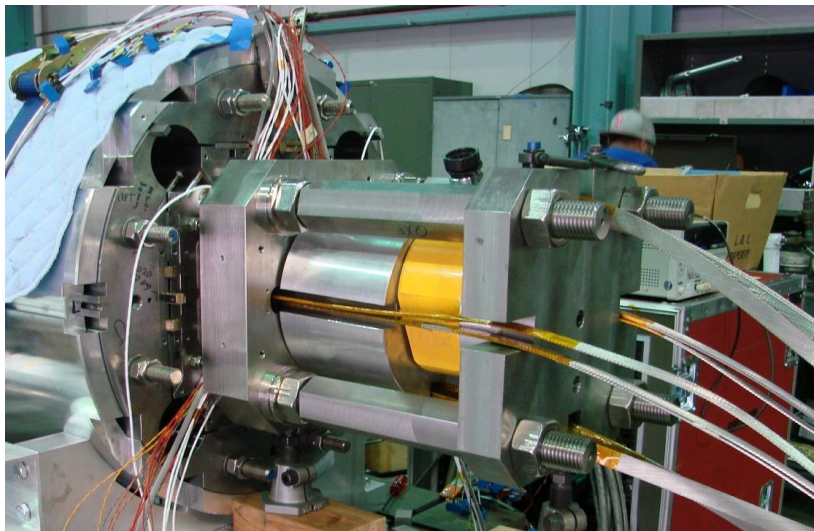


Fig. 6.14. Axial preloading operation with the axial loading rig.



## 6.3.4 Magnet Finishing Operations

### 6.3.4.1 Splice Connections

The magnet splice connections are made after the magnet preload operations are complete. Fig. 6.15 shows the physical layout of the magnet splice connections box, which is made up of two layers due to space constraints and the bend radius of the cables [1].

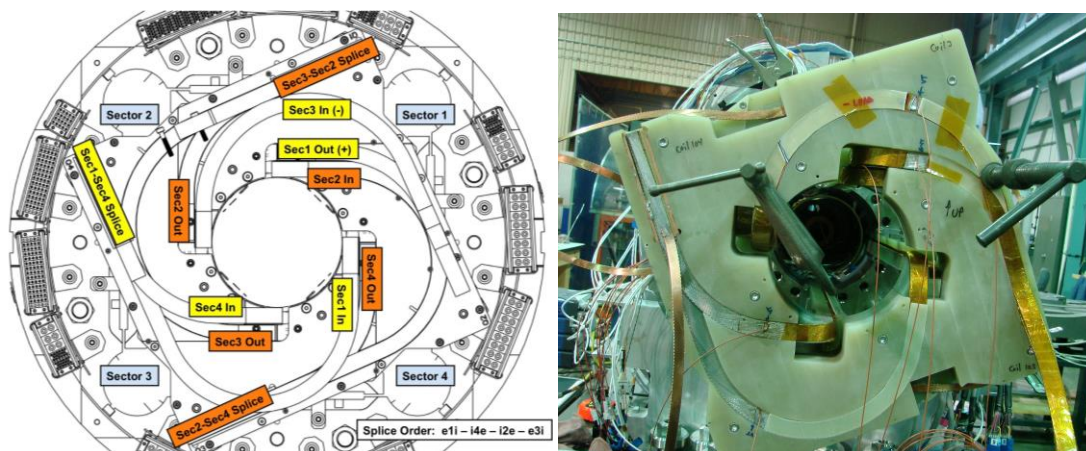


Fig. 6.15. Splice connections for the MQXFA.

The “A” and “B” magnet leads are uncut leads from two separate coils in the magnet: outer layer (OL) leads correspond to the “A” magnet lead, and inner layer (IL) leads correspond to the “B” magnet lead. The “A” lead requires 455 mm of length from the end of the coil to the exit of the splice connection box. The “B” lead requires 670 mm from the end of the coil to the exit of the splice connection box (see Fig. 6.16).

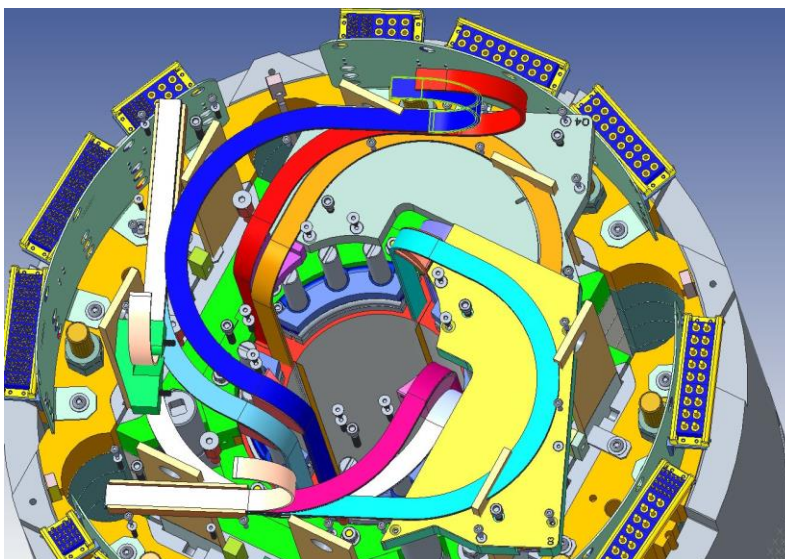


Fig. 6.16. MQXFA coil leads: The red lead is the OL lead (A) and the blue one is the IL lead (B),



## 6.3.4.2 Voltage taps for quench detection

The quench detection instrumentation includes three redundant (3x2) quench detection voltage taps located on each magnet lead and at the electrical midpoint of the magnet circuit, two (2) voltage taps for each internal MQXFA Nb<sub>3</sub>Sn-NbTi splice, OL heater current leads.

## 6.3.4.3 Connector Skirts

After the splice connections are completed, the final operation is to mount the all the instrumentation connectors. This includes protection heaters, voltage taps, strain gauges, etc. for the entire magnet (see Fig 6.17). After a final QC check of all these connections the magnet will be ready to be packaged for shipment.

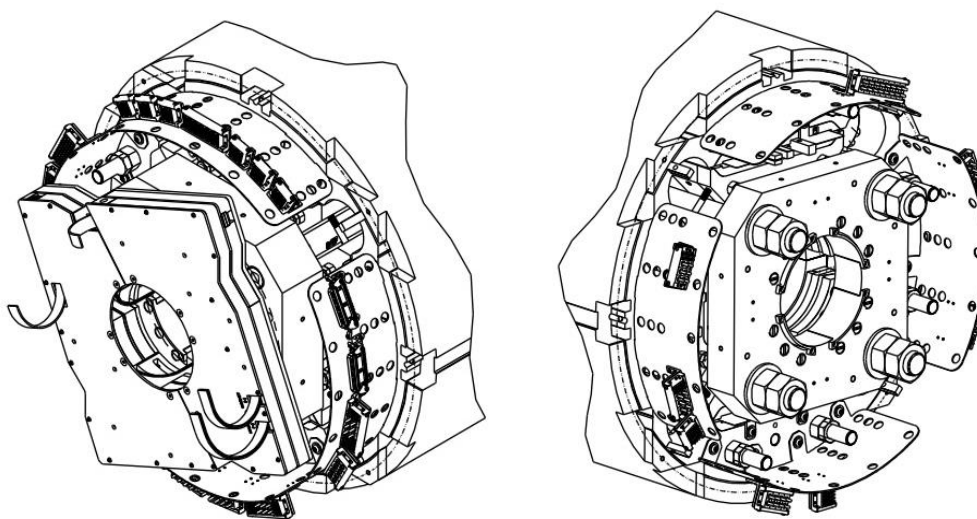


Fig. 6.17. Location of the connector skirts for the LE (L), and RE (R).

## 6.3.4.4 Magnet handling and shipment

MQXFA magnets handling and shipping requirement are specified in ref. [2].

MQXFA magnets have four coils made of strain sensitive Nb<sub>3</sub>Sn conductor. To prevent conductor degradation, handling and shipping operations shall meet the following requirement for each MQXFA magnet:

**MQXFA H&S Requirement #1: The conductor strain shall never exceed 500 microstrain in any part of the coils during any MQXFA handling (for instance lifting, lowering, rotation and up-righting) and shipping operation.**

The following requirement preserves MQXFA longitudinal rigidity, and prevents structure damage:

**MQXFA H&S Requirement #2: Where the tie-rods go through the iron laminations, the laminations shall always remain in contact during any MQXFA handling and shipping operation.**

MQXFA magnets will be shipped from LBNL (assembly site) to BNL (vertical test site), and then to FNAL (cold-mass assembly site) or back to LBNL (repair site) using a shipping fixture designed to minimize shocks during transportation, and truck loading/unloading. Two accelerometers will be placed on the fixture and a dedicated truck equipped with air-raide suspension will be used for transportation.

If there are no shock above 4.5 g, the standard QC for magnet reception can be performed

A more detailed description of those requirements together with the shipping procedure and plans are report in ref. [2,3]

## 6.4 Magnet Fabrication Infrastructure at LBNL

### 6.4.1 Yoke-Shell Subassembly Tooling

A single assembly pad is designed to assemble the half-length shell-yoke assemblies vertically. This can be seen in both Fig 6.6, and Fig 6.18. Originally designed to use the same bladder configuration as in a real magnet (eight bladders, two per quadrant), it has since been configured to employ bladders inserted into the cooling holes instead. This configuration improves efficiency by reducing the required amount of bladders (eight => four), and the forces are more directly applied to the gap.



Fig. 6.18. Half shell-yoke assembly stand.

The integration table is where the majority of the magnet assembly activities take place. It consists of two support plates on Thompson linear rails so that each half-length shell-yoke assembly can be independent handled, then joined (see Fig 6.19). This table is also where the final magnet integration takes place, and all the finishing and magnetic measurements take place.



Fig. 6.19. “Panoramic” view of magnet integration table, shown with two half-length shell-yoke assemblies prior to joining.

## 6.4.2 Coil Pack Assembly Tooling

The coil pack assembly table incorporates a platen that a pad-collar assembly would be resting on. The platen can be raised via hydraulic pressure for when an assembled coil pack is ready to have its insertion rails attached. It is mounted on wheels so that the coil pack can be moved to the integration table when ready, however it would be moved to location where clear access to the ends is available during coil pack assembly steps. Two auxiliary tables are also part of this table, which facilitate the handling and assembly of the full length pad-collar assemblies. These tables are visible in Fig 6.10. This set of coil pack assembly tooling tables will be duplicated during the production run in order to allow for two technician teams to work on parallel activities of magnet assembly.

## 6.4.3 Coil Rollover Tooling

Tooling for safely handling coil rotation operations are shown in Fig 6.20. During coil preparations it is required that access to a coil’s inner bore and outer surfaces be maintained. Coils are captured in “wheels” are driven by a gear assembly to rotates single coils or coil pairs. A second rollover tooling table will be procured for the project, allowing for coils in varying stages of processing to be handled at once when magnet production ramps up.



Fig. 6.20. Coil rollover tooling table.

## References

- [1] MQXFA Magnet Interface Specification, US\_HiLumi-Doc-1674
- [2] MQXFA Magnet Handling and Shipping Requirements. US-HiLumi-Doc-838, January 26, 2018. <http://us-hilumi-docdb.fnal.gov/cgi-bin/ShowDocument?docid=838>
- [3] MQXFA Coils and magnets Shipping Plans US-HiLumi-Doc-1686 [https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=1686&filename=MQXFA-Coils\\_and%20magnets%20shipping%20plan.docx&version=3](https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=1686&filename=MQXFA-Coils_and%20magnets%20shipping%20plan.docx&version=3)

## 7 MQXFA Vertical Test

The MQXFA test requirements are specified in the Functional Test Requirements document for MQXFA magnets [1]. Summary information is provided here for information only.

All prototype and production MQXFA magnets will be fully trained and tested in the vertical test facility (Figure 7.1) at Brookhaven National Laboratory (BNL), and on acceptance will be shipped to FNAL for assembly into LQXFA cold masses to be tested there. Comprehensive magnetic field measurements will also be performed at BNL. There will be 4 prototype tests and 23 production models of MQXFA, so there will be a total of 27 tests at the BNL vertical test facility. The cold masses at FNAL will be assembled into the cryo-assemblies that will become the Q1 and Q3 elements of the HL-LHC inner triplets.

Vertical test stand 3 (Figure 7.2), to be used for the MQXFA testing, is one of the vertical test cryostats previously used for over 30 years to test a wide variety of superconducting magnets, including RHIC and SSC arc dipole and quadrupole short prototypes, all the RHIC corrector magnets, and many others. This particular test stand has been upgraded to accommodate the size



of the MQXFA magnets and also to provide testing at 1.9 K, and less, and at a pressure of 1 bar, or more, and to also provide powering up to 24 kA with fast switching capabilities for quench protection. In parallel with this, the cryogenics facility has also seen extensive upgrades in 2016, most of which have been funded by BNL. In the fall of 2016, the new facility was successfully commissioned, and in late 2016 and Jan of 2017, the first ever long coil of MQXFA design was tested in a mirror configuration (MQXFPM1) and it reached the LHC ultimate operating point of 17.890 kA in 11 quenches, and after 19 quenches, reached 8% above ultimate (Figure 7.3). Along with this, quench protection heater tests and other R&D type measurements were done.

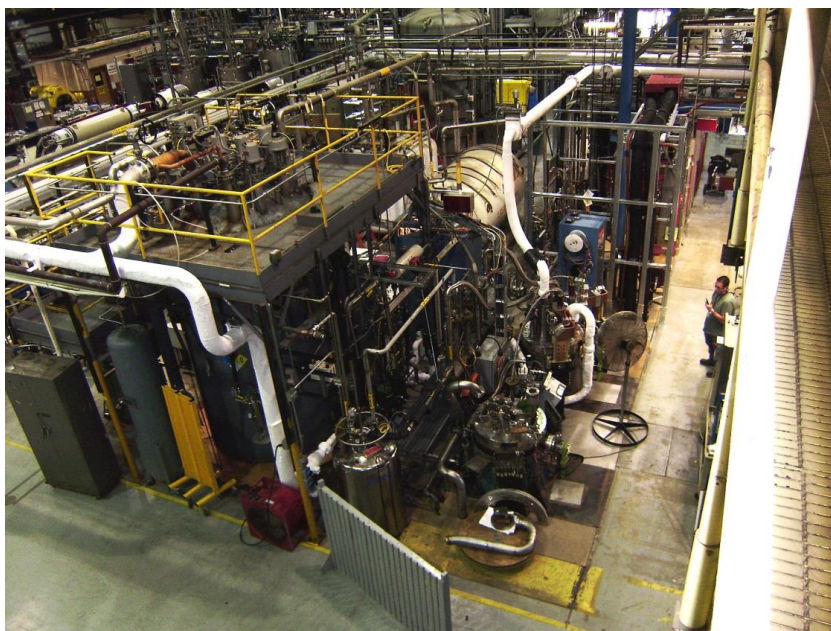


Figure 7.1: Vertical Test Facility at BNL, showing two of the five test cryostats and the backup refrigerator.



Figure 7.2: Vertical Test Stand 3, upgraded to provide 1.9 K at 1 bar (nom) and 24 kA, for testing of the 4.2 m-long MQXFA quadrupoles. The picture shows the test stand with the mirror MQXFPM1 under test.

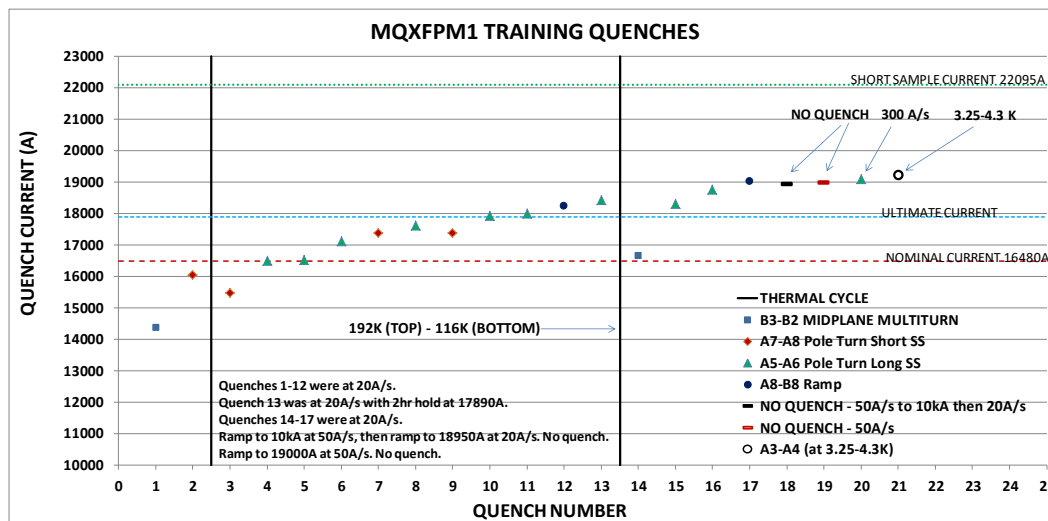


Figure 7.3: Plot of training quenches for the MQXFPM1 mirror at the BNL Vertical Test Facility.

In late 2017 and early 2018, until 20-Feb, the first long prototype quadrupole MQXFAP1 was tested. A total of 18 training quenches were performed with the magnet reaching 17.426 A, or 97%

of ultimate at Quench 18. Due to the development of a coil short to ground, testing was stopped to disassemble the magnet to investigate the short and re-assemble with a spare coil for later retest. During the training of MQXFAP1, the quench protection heaters satisfied the LHC requirement or better, and CLIQ was used successfully for the first time on long magnet. Quench history is shown in Fig. 7.4 below

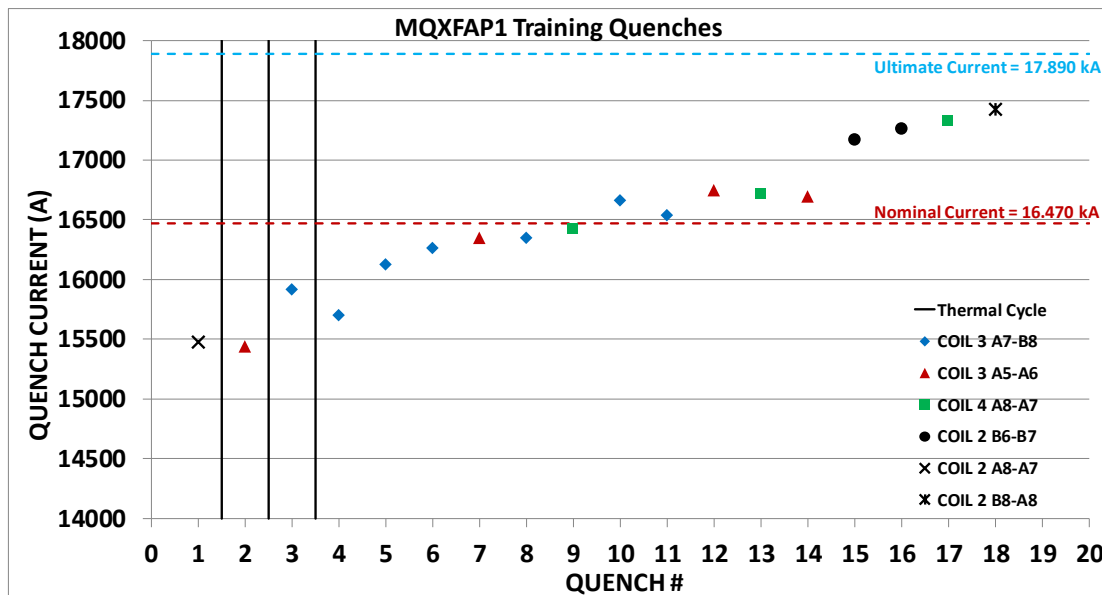


Fig. 7.4: Plot of training quenches for the MQXFAP1 prototype at the BNL Test Facility.

As a result of He gas recovery issues during the early training quenches of MQXFAP1, additional upgrades were made to the cryogenics facility He gas recovery system in order to mitigate the loss of He gas after a quench caused by the opening of relief valves. This was due to fast and large increases in boiloff pressure after a quench. Stored energies in the magnet can be as high as 6 MJ).



## 7.1 Vertical Test Scope and Objectives - Prototypes

There will be two more MQXFA prototype models MQXFAP2 and MQXFAP3, which unlike the first prototype meets the requirements for use in the LHC. The primary objective of the prototype testing is to provide information to magnet designers to validate design choices, verify performance, and reduce risk of MQXFA production. Another objective is acceptance before delivery to FNAL for possible assembly into a cold mass and a spare LQXFA cryo-assembly. The scope of these tests includes quench performance and training of magnets, room temperature (warm) and 1.9 K (cold) magnetic field quality and integral field measurements, and tests designed to determine the characteristics and parameters of the quench protection systems, among others.

MQXFA prototype magnets will be quench-tested to train to the maximum required test current of 19.8 kA, to verify stable mechanical and electrical operation. Magnet protection during training will make use of energy extraction to an external dump resistor as well as copper clad stainless steel quench protection heater strips and CLIQ. In addition, quench protection studies with protection heaters and CLIQ units, but without external energy extraction, will be performed. As already mentioned training and other spontaneous quench tests will be done with the external energy extraction system included, in order to save liquid helium and reduce the quench recovery time during training.

NbTi-NbTi splices between the magnet leads and the power bus-bars will be inspected at room temperature and monitored after cool down and during testing.

Major checkouts and measurements to be conducted for the two prototypes at the vertical test stand include:

At room temperature before cool down

- Electrical checkouts and tests ensuring the integrity of the insulation (high voltage, or hipot)
- Magnetic measurements: integral field strength and field harmonics (rotating probe)
- Strain Gauge measurements

Measurements during cooldown and warmup

- Temperature sensor (RTD) measurements
- Strain Gauge measurements
- Residual Resistivity Ratio (RRR) Measurements

After cool down to 1.9 K

- Hipot Measurements
- Magnetic Measurements
  - **Rotating probe measurements**
- Quench Training up to 19.8 kA

- Quench Characterization
  - **Voltage taps measurements**
  - **Quench Antenna measurements**
- Strain Gauge measurements while cold and during powering
- Ramp Rate Dependence Measurements
- Holding ultimate operation current (2-8 hours)
- Quench Protection Studies with heaters and/or CLIQ
- Measurement of the magnet inductance versus current
- Quench Propagation Studies
- Voltage Spikes Measurements
- Energy Loss Measurements
- Splice Measurements (at 1.9 or 4.5 K)

#### Measurements at 4.5 K

- Assess short sample limit percentage at 4.5 K after 1.9 K training
- Ramp Rate Dependence at 4.5 K in case of issues at 1.9 K

#### At room temperature after warm-up

- Electrical checkouts and tests ensuring the integrity of the insulation (high voltage, or hipot)
- Magnetic measurements: integral field strength and field harmonics (rotating probe)

A thermal cycle will be included to verify that the magnet retains its training.

For planning purpose, we may assume 50 training quenches.

A magnet re-test after pre-stress adjustment or coil exchange may be needed and should be planned for all prototypes. The test plan for prototype re-tests should be shorter than the plan for a new magnet, aiming at assessing quench performance improvements/changes and completing the test plan. For planning purpose, we may assume 30 training quenches and ½ effort for protection and other studies. A thermal cycle should be planned also for MQXFA re-tests.

## 7.2 Vertical Test Scope and Objectives – Production Magnets

The primary objective of the production testing is quench training, magnet qualification and quality assurance. Each magnet will be tested and trained prior to cold mass (LMQXFA) assembly, in order to check its quality and verify that it meets all requirements. Production magnets will not be tested above 18 kA (ultimate operating current with margin).

The test cycle of production magnets is expected to be shorter: production magnets will not have prototype instrumentation (for instance only voltage taps for splice measurement and quench detection and not for quench localization). Presently, the following numbers of quenches are suggested for planning purpose: 25 quenches at 1.9 K and, 2 quenches at 1.9 K after the thermal cycle (if needed).

NbTi-NbTi splices between the magnet leads and the power bus-bars will be inspected at room temperature and monitored after cool down and during testing.

Major checkouts and measurements to be conducted for the 22 production models at the vertical test stand include:

At room temperature before cool down

- Electrical checkouts and tests ensuring the integrity of the insulation (high voltage, or hipot)
- Magnetic measurements: integral field strength and field harmonics

After cool down to 1.9 K

- Electrical checkouts (including high voltage)
- Quench test training – to 18 kA (ultimate operating current with margin)
- Magnetic measurements: integral field strength and field harmonics
- Holding the ultimate current for an extended period of time
- Quench Protection Heater tests to verify nominal operation
- Splice measurements

At room temperature after warm-up

- Magnetic measurements: integral field strength and field harmonics
- Electrical checkouts before shipping to FNAL

## 7.3 Field Quality Measurements

Magnetic field measurements are performed at room temperature before and after the cool down, and at 1.9 K. The field harmonics are measured with a rotating probe based on the multi-layer printed circuit board design [2]. Integral field strength is determined with z-scans using the rotating probe.

At room temperature, field harmonics will be measured at low currents.

Field measurements will be done after cool down to 1.9 K. Integral field strength and field harmonics will be measured at a series of currents including injection (960 A) and collision (16480 A) currents.

A standard list of magnetic measurements with rotating probe for prototype magnets developed jointly with CERN include and already being performed on short models are:

- Z-scan
- Integral field measurements (as much as possible within test facility constraints)
- Loops (14, 20 and 40 A/s)
- Stair steps (with large steps)
- Accelerator cycle

## 7.4 Acceptance Tests

Requirements for qualification (acceptance) of the MQXFA magnets must be met before shipment to FNAL and assembly into LQXFA cold masses. The magnets will be accepted for shipment if all requirements, including quench performance at 1.9 K and specified tolerances for field quality for the integral magnetic field and the field harmonics before and after and during testing at 1.9 K.

## 7.5 High-Voltage Withstand Levels (Hipot Tests)

The MQXFA electrical design requirements and test values are specified in [3, 4]. We provide here a summary table for information only. The official documents can be accessed through the links provided below

During operation the MQXFA magnets may experience high voltages in case of magnet quench. An extensive study of peak voltages during operation of the HL-LHC Inner Triplet magnets has been performed taking into account the possible impact of different conductor/coil parameters, different quench-start locations, and in case of heater failure scenarios. The results are summarized in [2] for three possible quench protection systems: (i) only Outer Layer Quench Heaters (O-QH), (ii) Outer and Inner Layer Quench Heaters (O-QH + I-QH), and (iii) Outer Layer Quench Heaters and Coupling-Loss Induced Quench system (O-QH + CLIQ). The third option is the baseline quench protection system for the Inner Triplet of HL-LHC.

Based on these studies, electrical test criteria have been defined to qualify the magnets for machine operation. Two different voltage levels are defined for: (1) Nominal Operating Conditions



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(NOC); and (2) tests at warm (room temperature in dry air with  $T = 20 \pm 3$  °C and humidity lower than 60%).

The MQXFA electrical test values are summarized in Table 7.1. Once again this table is provided for information only while the official reference is provided in [3,4,5]. It should also be noted that once the components have been exposed in a previous stage to helium, reception values cannot be longer applied as the presence of helium may weaken insulations by creating creepage paths.

Table 7.1 MQXFA required hi-pot test voltages and leakages current [5].

Circuit Element	Expected Vmax [V]	V hi-pot	I hi-pot [ $\mu$ A]***	Minimum time duration [s]
Coil to Ground at RT before helium exposure *	n.a.	3.68 kV	10	30
Coil to Quench Heater at RT before helium exposure *	n.a.	3.68 kV	10	30
Coil to Ground at cold **	670	1.84 kV	10	30
Coil to Quench Heater at cold **	900	2.3 kV	10	30
Coil to Ground at RT after helium exposure *	n.a.	368 V	10	30
Coil to Quench Heater at RT after helium exposure *	n.a.	460 V	10	30

## References

- [1] MQXFA Magnets Functional Test Requirements, US-HiLumi-doc-137
- [2] J. DiMarco et al., “Application of PCB and FDM Technologies to Magnetic Measurement Probe System Development”, IEEE Trans. Appl. Supercond., vol. 23, no. 3, 9000505, 2013
- [3] MQXFA Electrical Design Criteria, US-HiLumi-Doc-826, <http://us-hilumi-docdb.fnal.gov/cgi-bin/ShowDocument?docid=826&version=1>
- [4] Electrical Design Criteria for the HL-LHC Inner Triplet Magnets, US-HiLumi-Doc-879, EDMS 1963398
- [5] Acceptance Criteria part A: MQXFA magnets, US-HiLumi-Doc-1103, [https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=1103&filename=HL\\_Acceptance\\_criteria\\_part-A\\_MQXFA\\_v1.0.pdf&version=6](https://us-hilumi-docdbcert.fnal.gov/cgi-bin/cert/RetrieveFile?docid=1103&filename=HL_Acceptance_criteria_part-A_MQXFA_v1.0.pdf&version=6)