	<b>Lawrence Berkeley National Laboratory</b>	Cat Code <b>SU3322</b>	<b>TECHNICAL NOTE</b>	LBL Technical Note # SU-1011-4084	Rev A	Page 1 of 12
Author(s) Heng Pan			Released By DWCHENG		Released Date Oct 4 2019 2:44:17 PM PDT	
Title LARP QXF LQXF - MAGNET <b>Impact of Class A Inspection on the FAD Calculations of MQXFA-03 and MQXFA-04 Shells</b>						

## I. Introduction

The fracture analyses of MQXFA shells revealed that the critical flaw size for the cutouts is 2 mm [1], which requires a Class AA ultrasonic inspection to detect. In the case of three long (center) shells for each MQXFA-03 and MQXFA-04 structures, the material certs provided by the vendor revealed that they were only inspected to a Class A inspection criteria. Therefore the Fracture Assessment Diagram (FAD) for these shells needs to be updated with this larger critical flaw detectable by a Class A inspection, which is 3 mm.

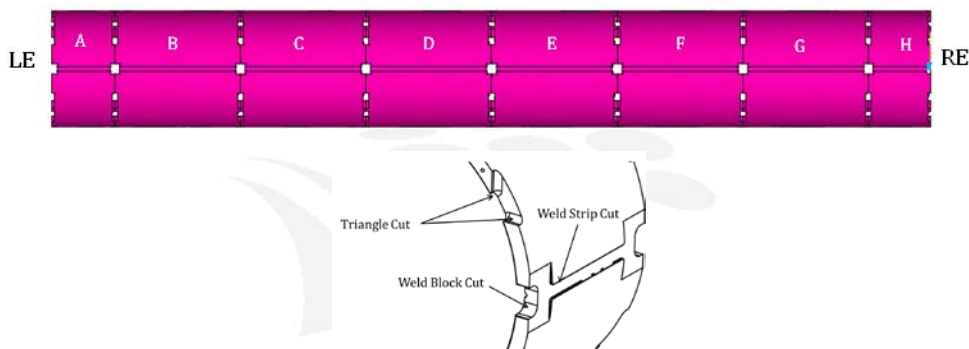


Figure 1 Shells for MQXF magnets and the cutouts on the short shells

The shells for MQXF magnets are shown in Fig. 1. All the raw forged materials of MQXF shells require ultrasonic inspections to detect flaws prior to further machining. Detection limits for ultrasonic methods in wrought aluminum (and most other standards) are described in ASTM B594 [2], and the limits for linear discontinuity is shown in Fig. 2.

Class	Single Discontinuity Response in. (mm) <sup>A,B</sup>	Multiple Discontinuities in. (mm) <sup>C,B</sup>	Linear Discontinuity Length-Response in. (mm) <sup>D</sup>	Loss of Back Reflection (%) <sup>E</sup>	Noise in. (mm) <sup>F</sup>
AAA	$\frac{1}{16}$ (0.40) or 25 % of $\frac{3}{16}$ (1.19) response	10 % of $\frac{3}{16}$ (1.19) response	0.12 (3.0)–10 % of $\frac{3}{16}$ (1.19) response	50	10 % of $\frac{3}{16}$ (1.19) response
AA	$\frac{3}{16}$ (1.19)	$\frac{3}{16}$ (0.79)	0.5 (12.7)– $\frac{3}{16}$ (0.79) response	50	alarm level
A	$\frac{1}{4}$ (1.98)	$\frac{3}{16}$ (1.19)	1.0 (25.4)– $\frac{3}{16}$ (1.19) response	50	alarm level
B	$\frac{3}{8}$ (3.18)	$\frac{3}{16}$ (1.98)	1.0 (25.4)– $\frac{3}{16}$ (1.98)	50	alarm level
C	$\frac{3}{8}$ (3.18)	Not applicable	Not applicable	50	alarm level

Figure 2 Inspection limits specified in ASTM B594-13

However, the standard does not specify the minimal detection limit or resolution explicitly; it is assumed that the calibrated flaw size represents the 95% Confidence Limit of detection.

The analyses according the specification of “MQXFA Structural Design Criteria” [3] assumes that a crack is semi-elliptical, as shown in Fig. 3, and it may grow from a characteristic size, to ratios of either  $a/c = 1$  or  $a/c = 0.8$  upon initial loading, but may still remain sub-critical afterward.

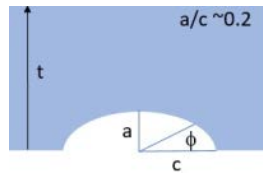


Figure 3 Part-Through crack geometries with definitions of  $a$ ,  $c$ , and  $\phi$

Based on the typical loading conditions that are experienced in MQXF magnets, the critical flaw size of the cutouts of the aluminum shells is determined as 2 mm, where  $K_I$  approaches a “critical” characteristic assessment value e.g.  $K_{Ic}$ . This critical flaw size is used to both determine inspection limits and rejection criteria for components.

In order to make use of the calibrated flaw sizes listed in the standard (Fig. 2) with the assumed geometry in the analyses, one should tie the two by the area of an elliptic flaw. The area of an elliptic flaw is  $A = \pi ac$ ; and the area is  $A = \pi(D/2)^2$  for a circular flaw, where  $D$  is defined as the detection limit for the various inspection grades.

Therefore, for a flaw with  $a/c = 0.2$ , i.e.  $c = 5a$  the area is:

$$A = \pi ac = \pi \left(\frac{D}{2}\right)^2$$

$$a = \frac{D}{2\sqrt{5}}, 2c = D\sqrt{5}$$

A detected flaw with this geometry will start with a characteristic length of  $a$ , with  $2c = 10a$  as showed in Fig. 3. So, the inspection limit for a given grade of inspection should yield a flaw with a width of  $2.24 D$ , as shown in Table 1:

Table 1 Flaw sizes correlated to Inspection Grades for Aluminum Forgings

Inspection Class	Calibration Block	Allowable Critical Flaw Size
AAA	0.40 mm	> 0.90 mm
AA	0.79 mm	> 1.77 mm
A	1.19 mm	> 2.67 mm
B	1.98 mm	> 4.44 mm

According to Table 1, if a critical flaw is 3 mm, a Class "A" inspection is sufficient to detect a critical flaw, whereas critical flaw of 2 mm requires a Class of "AA" inspection for proper detection.

## II. FAD Calculations with Class A Inspection

Since the Class A inspection can only detect a ~3 mm size flaw, the FAD for these shells must be updated with the increased flaw size. Fig. 4 indicates the FAD of different cutouts after cooldown. With larger critical flaw size, the load factor increases for the triangle cutout and weld block cutout; however, the load factor decreases for the weld strip cutout, which reduces the safety margin. A flaw with a load factor of 1.2 is considered acceptable. The load factors of the different cutouts are listed in Table 2, which are applicable to the two shorter end shells.

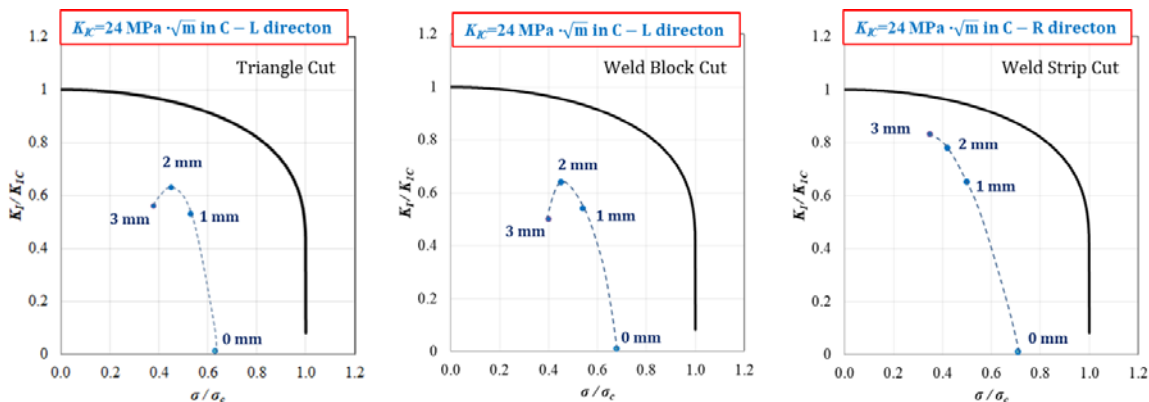


Figure 4 FAD calculations of the three cutouts on the end shell after cooldown

For the six “long” center shells, the trends of load factor vs. crack size are similar, but the margin still seems to be safe because the end effects are smaller on the center shells.

Table 2 Load factors of different cases

	End of the End shell			End of the Center shell
	Triangle Cut	Weld block	Weld strip	Weld strip
2 mm	1.4	1.4	1.24	1.34
3 mm	1.5	1.7	1.16	1.26

The load factors vs. crack sizes for Class A inspection grade are shown in Fig. 5.

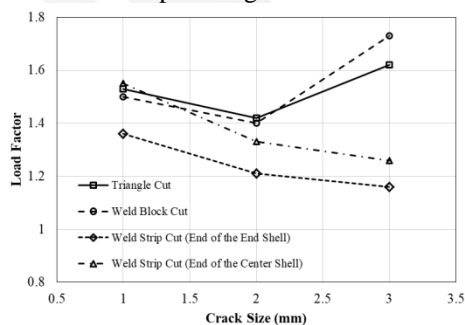
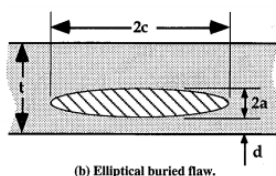


Figure 5 Load factors vs. crack sizes (the least load factor of 1.2 is specified in [3])

### III. FAD Calculations with Class A Inspection for a Buried Flaw

In addition to the UT inspections on the raw forgings, a dye penetrant test is also performed on the shells after machining is complete. The dye penetrant tests performed on these long shells came back negative, meaning no surface flaws were detected (See Appendices). The dye penetration inspection can capture surface flaws as analyzed above; but cannot detect buried flaws. Ultrasonic inspection has no limits on this aspect. Therefore, a similar analysis has been performed for a buried flaw if dye penetration is used for the inspection, shown below.

A buried flaw typically has smaller  $a/c$  value because it tries to grow to be round. A reasonable value of  $a/c$  for an elliptical buried flaw could be 0.2 based on the range given in [4].



(b) Elliptical buried flaw.

Figure 6 Elliptical buried flaw

In the analysis, the formula for a buried flaw is same as that for a surface flaw, but the influence coefficients  $G_j$  of flaw geometry [3] will be changed accordingly.

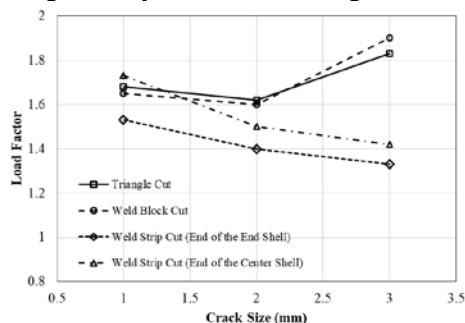


Figure 7 Load factors vs. crack sizes (buried flaw, the least load factor of 1.2 is specified in [3])

The calculated load factor vs. crack size of a buried flaw is shown in Fig. 7. The load factor of a buried flaw is ~20 % higher (safer) compared to the load factor of same size surface flaw.

#### IV. Conclusion

In summary, the above analyses show that the detectable flaw size of the Class A UT inspection limits does not impact the safety margin significantly in the FAD for long MQXFA shells under the same loading conditions. Note this result, however, does not apply to the shorter end shells, but these were, in fact, inspected to Class AA UT. Additionally, dye penetrant tests performed on all shells passed; therefore, a worst-case scenario that a buried flaw of Class A size may exist. Fortunately, however, such a condition does not detrimentally affect the FAD of either the long or short shells. These results indicate that the long (center) shells of MQXFA-03 and MQXFA-04 inspected to Class A standard still meet the structure design criteria guidelines.

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Document Control Center

## V. Appendices

**STEEL INDUSTRIES INC.**  
an **AFGlobal** Company

**Quality Certification**  
Heat Code: 376102

Steel Industries Inc.  
An AFGlobal Company  
12600 Beech Daly Rd. Redford, MI 48239-2455  
Phone: (313) 535-8505 Fax: (313) 534-2165

METALEX MANUFACTURER ME5500		PO: 27344-BL-2623 <i>Item#</i>		Sales Order: 159609		Line: 1	
5750 CORNELL RD		Item Code: <i>213</i>		Qty Shipped: 6			
CINCINNATI, OH 45242-2010		Item Desc: Rings				Supplier Heat: 376102	
Spec: AMS 4126C, Grade 7075, Condition T6 ✓							

Element	(%wt)	Ladle	Product	EPCRA	CAS#	Element	(%wt)	Ladle	Product	EPCRA	CAS#
Mn	Manganese	0.01		✓	7439-96-5	Al	Aluminum				
Si	Silicon	0.06				Fe	Iron	0.015			
Cu	Copper	1.6		✓	7440-50-8	Zn	Zinc	5.8			
Cr	Chromium	0.20		✓	7440-47-3	Mg	Magnesium	2.5			
Ti	Titanium	0.03		✓	7440-02-0						

Mechanical Testing		Other
Tensile - Longitudinal (KSI)	79.0 ✓	Stock used
Yield Strength - Longitudinal (KSI)	67.0 ✓	15" Ingot.
Elongation <sub>t</sub> - Longitudinal	11 ✓	
ROA <sub>t</sub> - Longitudinal	21 ✓	
Tensile - Long trans (KSI)	73.5 ✓	
Yield Strength - Long trans (KSI)	61.5 ✓	
Elongation <sub>t</sub> - Long trans	9.7 ✓	
ROA <sub>t</sub> - Long trans (KSI)	18 ✓	
Tensile - Short trans (KSI)	75.0 ✓	
Yield Strength - Short trans (KSI)	62.5 ✓	
Elongation <sub>t</sub> - Short trans	7.6 ✓	
ROA <sub>t</sub> - Short trans	14 ✓	

*Job # 2623*  
*PART# SU-1010-1073*  
*P.O# 27344-BL*  
*S/N: 001, 002, 003,*  
*004, 005, 006*  
*6 PCS TOTAL*

**LBL Job#18-2623**  
P/N SU-1010-1073  
S/N 001 thru 006  
PO#27344 Item#2/3

METALEX  
Q.A. DEPT  
ACCEPTED  
DATE 11/26/18  
BY KKS

The recording of false, fictitious, or fraudulent statements or entries on this document may be punishable as a felony under Federal statute.

EPCRA Supplier Notification: This product may contain one or more toxic chemicals subject to the reporting requirements of Section 313 of the Emergency Planning and Community Right-to-Know Act (Title III of the Superfund Amendments and Reauthorization Act of 1990) and 40 C.F.R. Part 372. Potentially reportable chemicals are indicated with a checkmark in the "EPCRA" column and a Chemical Abstract Service (CAS) registry number is provided for each such chemical in addition to the percent by weight of the chemical present in this product. It is your responsibility alone to determine whether your facility is required to submit a Toxic Release Inventory Report under EPCRA Section 313.

Certification No.: 1344682  
 Certification Date: 9/28/2018  
 Issued By: Nick Kraft  
This report is issued in compliance with the requirements of EN10204 3.1

### Quality Certification

Heat Code: 376102

Steel Industries Inc.

An AFGlobal Company

12600 Beech Daly Rd. Redford, MI 48239-2455

Phone: (313) 535-8505 Fax: (313) 534-2185

METALEX MANUFACTUR ME5500 5750 CORNELL RD CINCINNATI, OH 45242-2010	PO: 27344-BL-2623 Item Code: Item Desc: Rings	Sales Order: 159609 Line: 1 Qty Shipped: 6 Supplier Heat: 376102
Spec: AMS 4126C, Grade 7075, Condition T6		

Job 2623

24.17 x 21.89 ID x 25.64 (finish sizes)  
 P.O. Item 2 (5 pcs)  
 24.60 x 21.39 ID x 26.14 (approx. supplied sizes)  
 P.O. Item 3 (1 pc)  
 24.60 x 21.39 ID x 28.14 (approx. supplied sizes)  
 Forged  
 Heat treated in accordance with AMS 2772G to the T6 temper  
 Solution treated 890F, 4:06 hours, cold water quenched  
 Aged 250F, 24:08 hours, air cooled  
 Hardness achieved (10mm/500kg): 158/158/158/158/158/158 HBW  
 Rough machined  
 Ultrasonic inspected per ASTM B594-13, Class A: No indications detected ✓

Other Elements, each: 0.05  
 Other Elements, total: 0.15

P.O. Lines 2 & 3

No welding was performed on this material.  
 Material is free from mercury contamination.

We hereby certify that the above item(s) has been inspected and tested in accordance with the listed specifications and is in conformance with all requirements as modified by the Purchase Order and/or Steel Industries, Inc. Quote.

Steel Industries, Inc. operates a quality management system in accordance with Quality Manual, Issue 2, Revision 2 dated June 14, 2018, which conforms to the following quality programs and directives for the manufacture of open die forgings and seamless rolled rings:

- 1) ISO 9001:2015 and AS9100D - certified by Performance Review Institute (PRI)
- 2) NADCAP (National Aerospace Accreditation Program) for heat treating - certified by Performance Review Institute (PRI)
- 3) PED (Pressure Equipment Directive) 2014/68/EU Annex 1 Para 4.3 - certified by Bureau Veritas
- 4) CFR Part 21 - Unauthorized Shipment of Defective Material applies

LBL Job#18-2623  
 P/N SU-1010-1073  
 S/N 001 thru 006  
 PO#27344 Item#2/3

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Certification No.: 1344682  
 Certification Date: 9/28/2018  
 Issued By: Nick Kraft

  
 Nicholas Kraft - Q.C. Certification Specialist

This report is issued in compliance with the requirements of EN10204 3.1

Page 2 of 2



Certified Inspection Report

Order Number	1001016192	Customer P/O	27329-001
Lot	L1	Item Description	SCALPRED ALUMINUM INGOT
Lot No.	11	Item No.	7175 W/F 361,982
Lot No.	11	Item No.	7175 W/F 361,982
Lot No.	11	Item No.	7175 W/F 361,982

Quantity Shipped	Item Description	Date Shipped	Item No.
4572	19.5 IN DIA	06-JUL-18	7175 W/F 361,982
237944	AM45-A-2271 REV C	06-JUL-18	AM45-A-2271 REV C
11793318	AM45-QQ-A-387 REV E	06-JUL-18	AM45-QQ-A-387 REV E
	AM45-149 REV E	06-JUL-18	AM45-149 REV E
	AM45-179 REV D	06-JUL-18	AM45-179 REV D
	AM45-186 REV M	06-JUL-18	AM45-186 REV M
	AM45-214 REV U	06-JUL-18	AM45-214 REV U
	AM45-148 REV E	06-JUL-18	AM45-148 REV E
	AM45-126 REV C	06-JUL-18	AM45-126 REV C
	AM45-131 REV D	06-JUL-18	AM45-131 REV D
	AM45-147 REV D	06-JUL-18	AM45-147 REV D
	AM45-4310 REV E	06-JUL-18	AM45-4310 REV E
	AM45-4311 REV E	06-JUL-18	AM45-4311 REV E
	AM45-4323 REV C	06-JUL-18	AM45-4323 REV C
	P7-A11 REV 4	06-JUL-18	P7-A11 REV 4

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ACCEPTED  
DATE 11/26/18  
BY KKS

LBL Job#18-2623  
P/N SU-1010-1073  
S/N 001 thru 006  
PO#27344 Item#2/3

**Notes**

Cart # Log Length Width 376100 5.163 250.4920 376100 1.163 250.4922 376101 5.157 209.4334 376101 3.152 375.4616 376100 4.161 625.4900 376100 2.151 100.4374 376101 2.159 750.4614 376699 5.151 125.4576 376102 3.150 875.4566 376102 5.150 079.4572

**CERT NOTE: METS TEST CHEMISTRY REQUIREMENTS OF BOTH 7175 AND 2075 ALLOY.**  
Current version of ABE Quality Manual is June 15, 2012. This material was not welded while being processed. The material is free of radioactive contamination. Homogenization Practice: 800-890 for 20 hrs. Heat and cast using Inducton and Alcoa B205 procedure only.

**CAUTION:** When forged, removed or rolled mill products, produced from Accore Ingot by Accore customers, are ultrasonically inspected before being placed into service and Inducton will sign found which record the applicable USI limits. Accore will provide replacement ingot. Accore will accept no incidental or consequential damage claims arising from the backaction or use of product from such ingots, the customer's exclusive remedy being the above stated replacement ingot. Unless the product fabricated from Accore Ingot is ultrasonically inspected prior to being placed into service, Accore does not make the warranty stated herein.

**COMPOSITION NOTE:** The values for 'Others Total' and 'Others Total' have met the limits as shown on this certified inspection report. Remainder is Aluminum.  
CASTING NUMBER: 3760982592107 37610025562107 37610125562107 37610225562107

**Legal Statement**

We hereby certify that, unless otherwise indicated, the material covered by this report has been manufactured, inspected, and tested in accordance with, and that tests found to meet, the applicable requirements described herein, including any specifications forming a part of the description and that samples representative of the material met the composition. Also, note that accuracy is not a normal component in aluminum alloys and neither is the accuracy of its compounds are used in the manufacture of our product. This certification is not to be reproduced in partial form without prior written approval of our Quality Assurance Dept.

**Signature and Title**

Genia Watson  
Quality Assurance Manager  
06-JUL-18

**Quantities per Lot / Packages**

Package Number	Lot Number	Quantity	UOM	Gross Weight	Net Weight
G16-PKG669377	25562107	1	PCS	4602	4572



ARCONIC FORGING AND EXTRUSIONS  
Firmco Inc  
6833 West Wills Road  
Chandler, AZ  
85226

**Certified Inspection Report**  
Sales Order Number: 1001016192  
Line No. 1.1  
Customer P/O: 27328-001

Cert Number: ABR716164  
Page: 2/2  
Cert Print Date: 06-JUL-18

Alloy	Composition Results		Si		Fe		Cu		Mn		Mg		Cr		Zn		Ti
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	
7175	0.15	0.15	0.20	0.20	1.2	2.0	0.10	0.10	2.1	2.9	0.18	0.28	5.1	6.1	0.10	0.10	

Alloy	Composition Results		Si		Fe		Cu		Mn		Mg		Cr		Zn		Ti
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	
7175	0.05	0.05	0.06	0.06	0.15	0.15	1.6	1.6	0.01	0.01	2.5	2.5	0.20	0.20	5.8	5.8	0.03

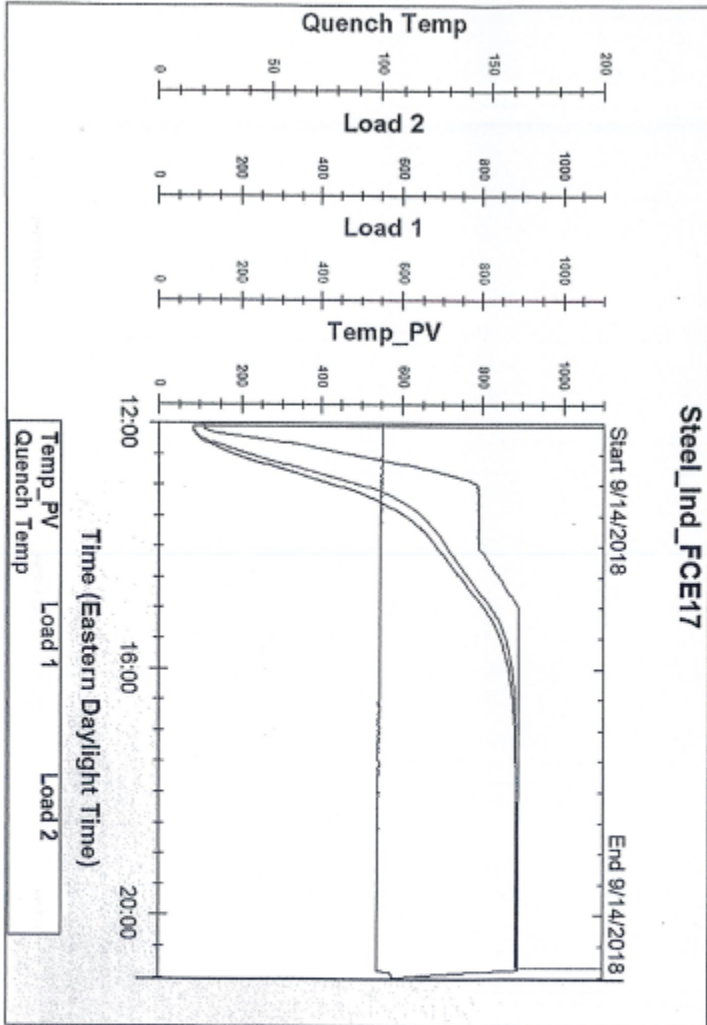
Heat / Cast / Lot Number	Composition Results		Si		Fe		Cu		Mn		Mg		Cr		Zn		Ti
	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	Min	Max	
376099	0.07	0.07	0.16	0.16	1.6	1.6	0.02	0.02	2.5	2.5	0.21	0.21	5.8	5.8	0.02	0.02	
376100	0.05	0.05	0.15	0.15	1.6	1.6	0.01	0.01	2.6	2.6	0.21	0.21	5.8	5.8	0.02	0.02	
376101	0.05	0.05	0.15	0.15	1.6	1.6	0.01	0.01	2.5	2.5	0.20	0.20	5.7	5.7	0.03	0.03	
376102	0.06	0.06	0.15	0.15	1.6	1.6	0.01	0.01	2.5	2.5	0.20	0.20	5.8	5.8	0.03	0.03	

Cert Notes:  
Anodic - Primaco Inc. manufactured the item described above in a plant whose quality management system is certified/registered as being in conformity with ISO9001:2008 & AS9100 Rev C by BSI Management Systems under Certificate # PA72752.  
Made in USA  
The test report shall not be reproduced except in full, without the written approval of the Quality Department. No alteration, addition or other change is authorized to be made to this certificate.  
The recording of false, fictitious, or otherwise fraudulent statements or entries on this certificate may be punished as a felony under applicable law.

LBL Job#18-2623  
P/N SU-1010-1073  
S/N 001 thru 006  
PO#27344 Item#2/3

METALEX  
Q.A. DEPT  
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LBL Job#18-2623  
 P/N SU-1010-1073  
 S/N 001 thru 006  
 PO#27344 Item#2/3

METALLEX  
 Q.A. DEPT  
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 DATE 11/26/18  
 BY KKS

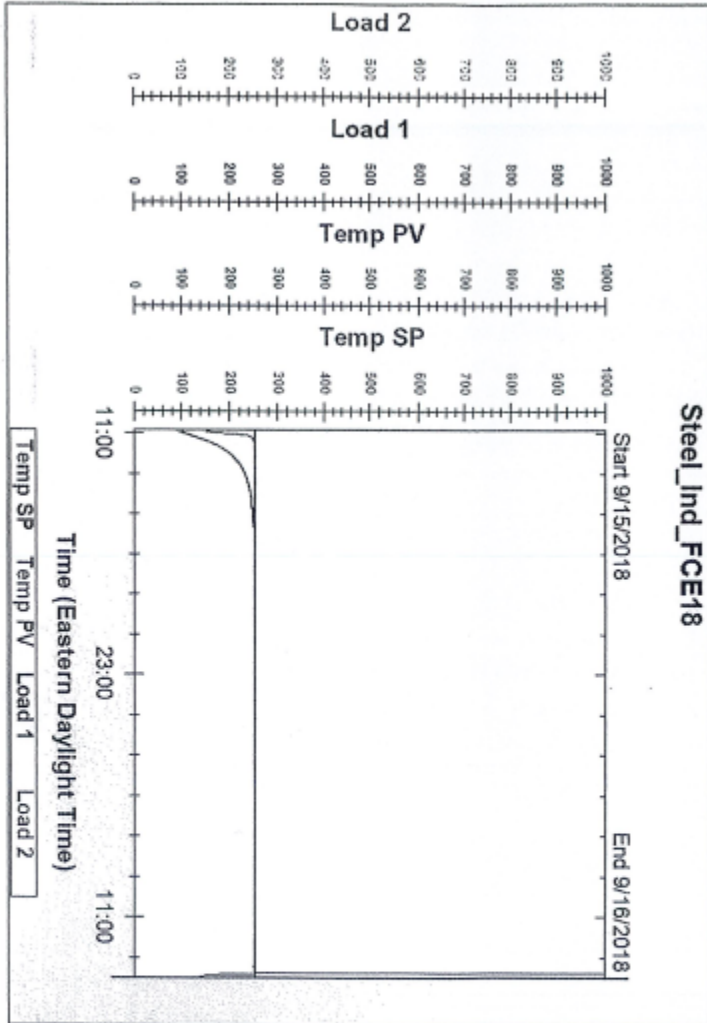
**STEEL INDUSTRIES INC.**  
 SERVING AMERICAN INDUSTRY SINCE 1913

SO# 159609  
 GRADE 7075-T6  
 HEAT# 376102  
 CUSTOMER METALLEX  
 PO# 27344-86-2623  
 P/N

THERMAL TREATMENT:  
 SOLUTION ANNEAL 890F  
 4 Hr. 6 mi.  
 WATER QUENCH

Leo  
 Beverley

0751A 0751A



LBL Job#18-2623  
 P/N SU-1010-1073  
 S/N 001 thru 006  
 PO#27344 Item#Z/3

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 BY KKS

**STEEL INDUSTRIES INC.**

SO# 159609  
 GRADE 7025-76  
 HEAT# 376102  
 CUSTOMER METALEX  
 PO# 27344-BL-2623  
 P/N \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

THERMAL TREATMENT:  
Age 250 F  
24 Hrs. 8 axis  
Min. cool  
Leo  
Beverley

RT.S14 05/04



 Lawrence Berkeley National Laboratory	Cat Code <b>SU3322</b>	<b>TECHNICAL NOTE</b>	LBNL Technical Note # SU-1011-4084	Rev A	Page 12 of 12
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- [3] E. Anderssen, S. Prestemon. "US HL-LHC Accelerator Upgrade Project Structural Design Criteria", 2018
- [4] T. Anderson, "Fracture Mechanics", Second Edition, 1994.

