

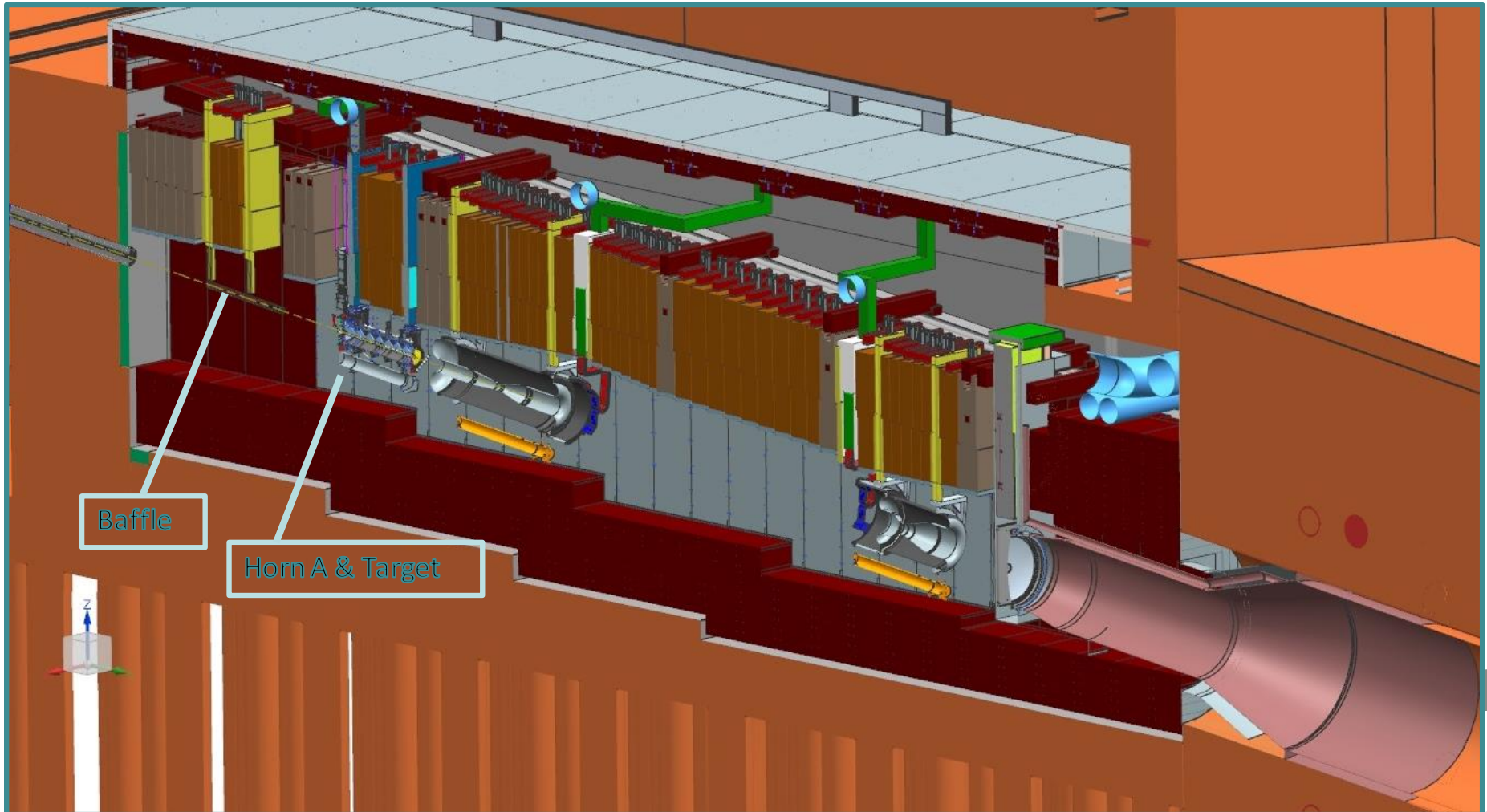
LBNF Target Concept Selection Report to Technical Board

Chris Densham, Peter Loveridge, Mike Fitton, Joe O'Dell, Tristan Davenne,
Dan Wilcox, Eric Harvey-Fishenden, Mike Parkin, Phil Jeffery, Ben Peters
(STFC Rutherford Appleton Laboratory)

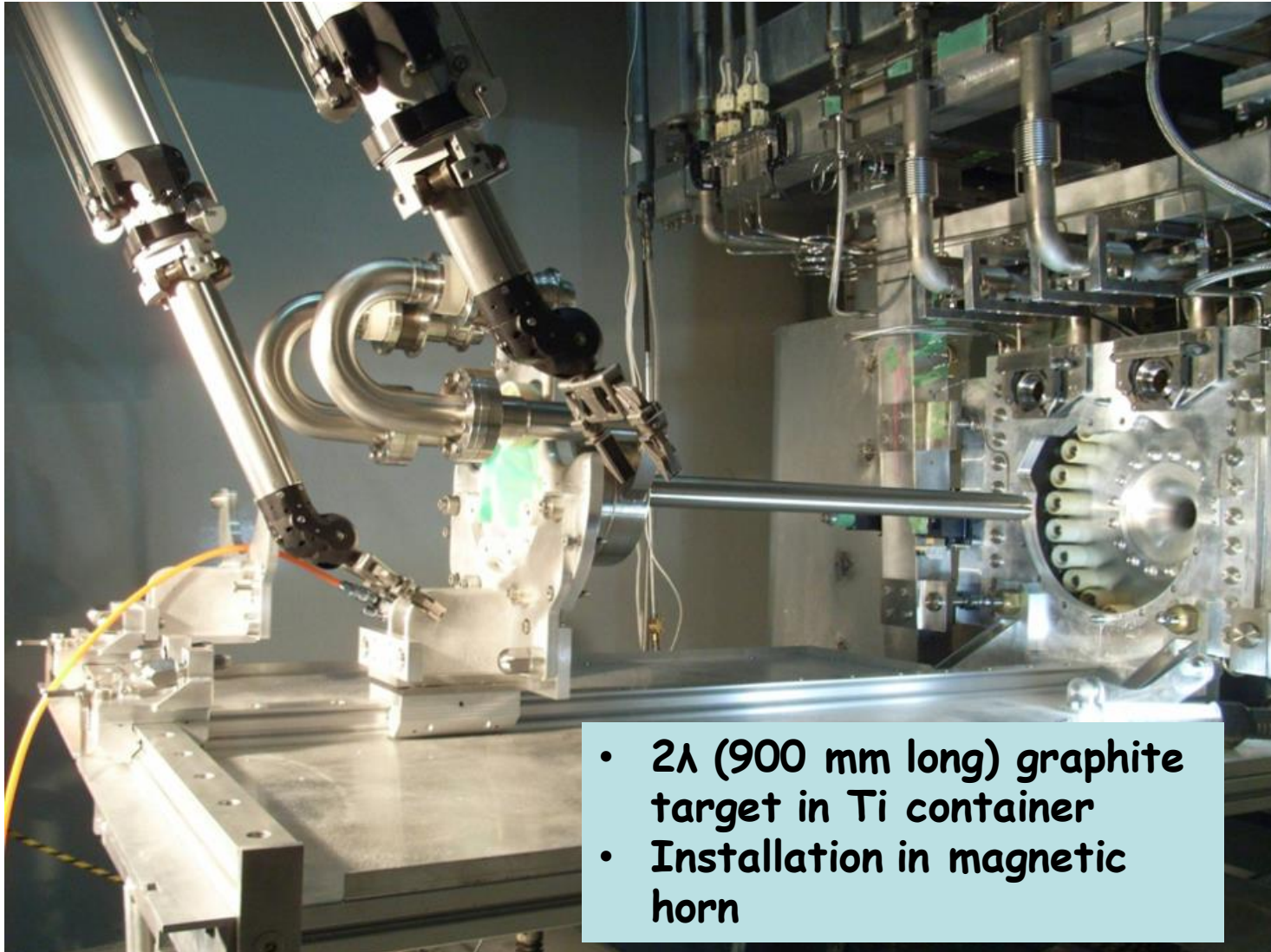
John Back
(University of Warwick)

Pat Hurh, Cory Crowley, Matthew Sawtell, Vladimir Sidorov, Laura Fields,
Andrew Dalesandro, Keith Gollwitzer, Jonathon Lewis
(Fermilab)

LBNF Neutrino Beamline



Our starting point: Helium Cooled T2K Target



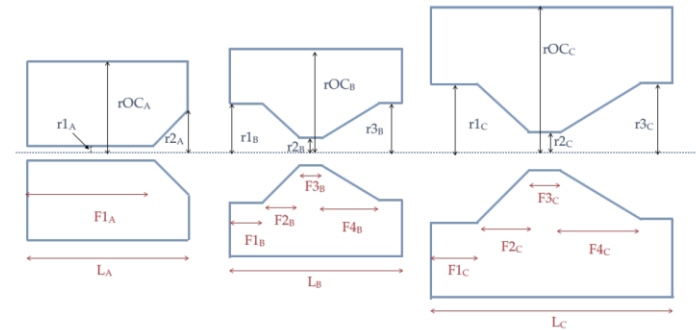
- 2λ (900 mm long) graphite target in Ti container
- Installation in magnetic horn

LBNF/DUNE Requires a *Long* Target

- **BOTF Report (L Fields et al):**

*“We find that it is important that the target be significantly longer than the reference target, and are recommending that the LBNF team design a target that is at least **four interaction lengths**. Other details of the target, including cross sectional area, shape and material, are less critical to physics performance ...*

... At present, both a NuMI-style graphite fin target and a graphite cylindrical target appear to be good options”



$$1\lambda = 46\text{cm of graphite}$$

- **Fermilab LBNF Requirements Documentation “DOORS”:**

*“The target shall have an equivalent length of about **four interaction lengths** ...*


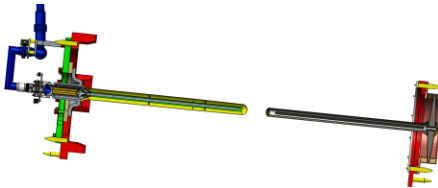
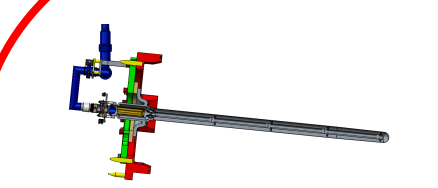
*... The amount of material needed in the target must be enough to maximise secondary particle production, while not absorbing too much. **Four interaction lengths** is an approximately optimal length”*

Target 'Optimum' Design

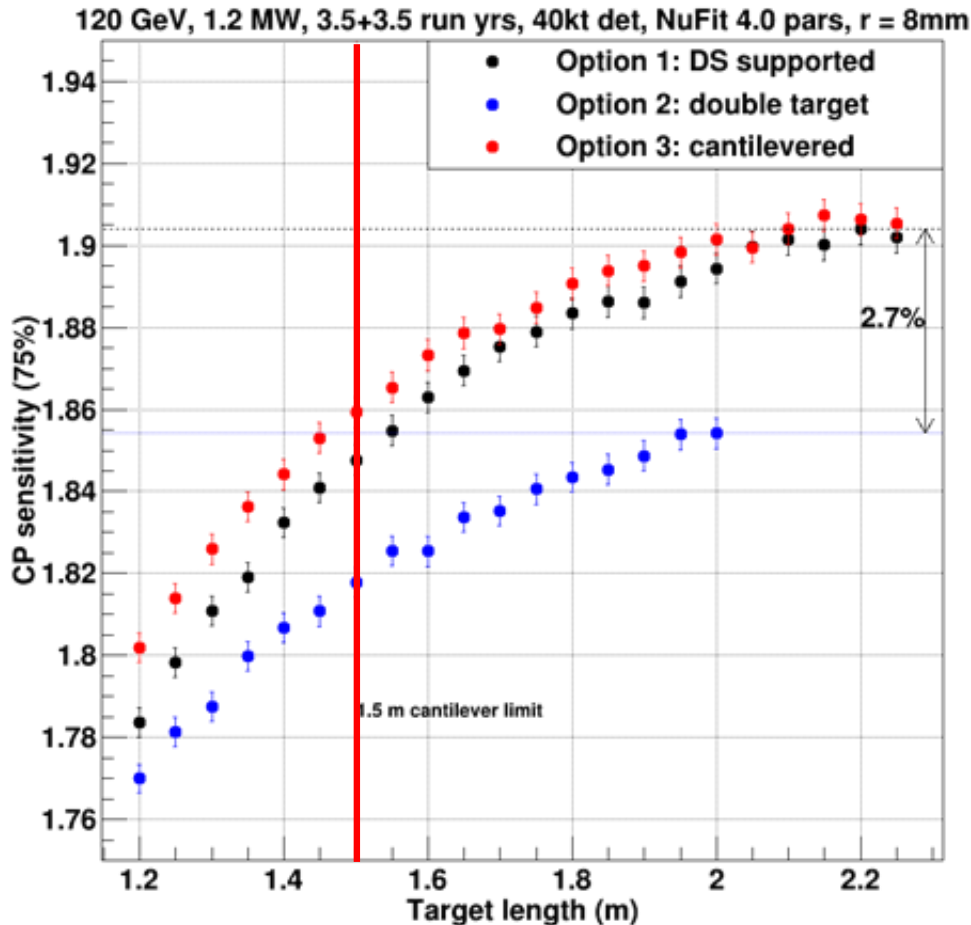
- $\lambda_{overall} = \lambda_{physics} \times \lambda_{reliability}$, where $\lambda_{reliability} = fn(l, \sigma, L \dots)$
- For CP sensitivity – small beam σ is favoured
- For target lifetime – bigger σ is better.
 - Lower power density – lower temperatures, lower stresses
 - Lower radiation damage rate
 - Lower amplitude 'violin' modes (and lower stresses)
- For CP sensitivity – long target (4λ , c.1.8m) is better
- For max lifetime – short and *simple* target is better
- **For integrated optimum performance, need to take both *instantaneous* performance and *reliability* into account**
 - E.g. How to achieve best physics performance possible for a target lifetime of a minimum of 1 year?
 - Answer depends on beam parameters & power, changeout time etc

Target Concept Selection Summary (July 2019)

- consensus achieved!

| |  <p>Option 1: 1x2m long</p> |  <p>Option 2: 2x1m long</p> |  <p>Option 3: intermediate cantilever</p> |
|----------------------------|---|--|---|
| Instantaneous physics | Best instantaneous physics. | Needs an extra 19 days/yr to match option 1. | 1.5m needs an extra 19 days/yr (13 days/yr at 1.6m). |
| Engineering performance | High heat load. Unstable until supported. | High heat load but divided between 2 targets | Pushing at the limits on cantilever length. |
| Manufacturability | Difficult to make long tubes. DS support adds complexity. | 2 nd target low-mass manifold is complex. | Difficult to make long tubes. |
| Ease of remote maintenance | ≈3 weeks exchange time, DS support adds time and risk. | ≈2 weeks exchange time, 2 nd target adds some time and risk. | ≈1 week exchange time, lowest complexity and risk. |
| Cost and schedule impacts | DS support somewhat increases cost and time. | 2 nd target greatly increases cost and time. | Cheapest and fastest to produce. |

CP Sensitivity Comparison

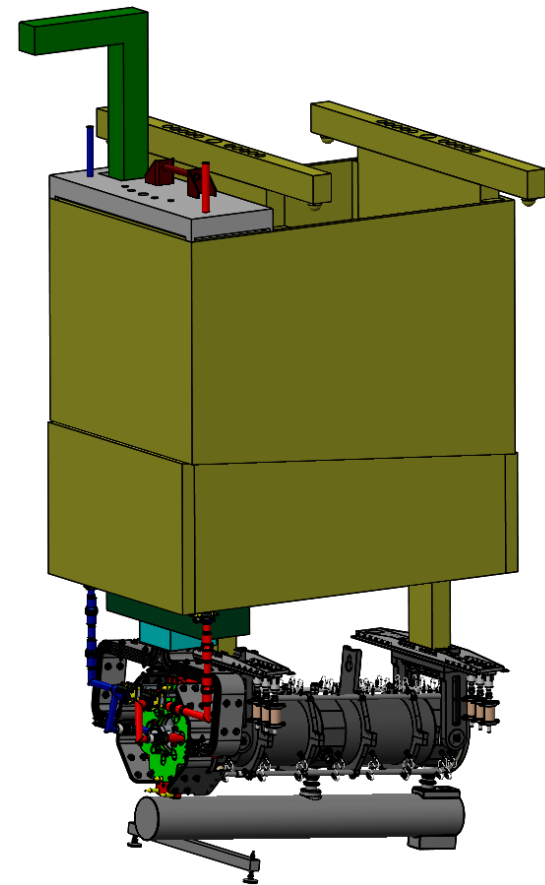


- Simple cantilever gives best performance for a given length (but the achievable length will be limited)
- DS supported target gives best performance for lengths where a simple cantilever is not possible
- Double 1m targets offer similar performance to a single 1.5 m cantilever
- To achieve same instantaneous performance as 2.2 m long target need extra running time:
 - Double Target 9.5% (19 days/run yr)
 - 1.5m Cantilever 9.5% (19 days/run yr)
 - 1.6m Cantilever 6.2% (13 days/run yr)

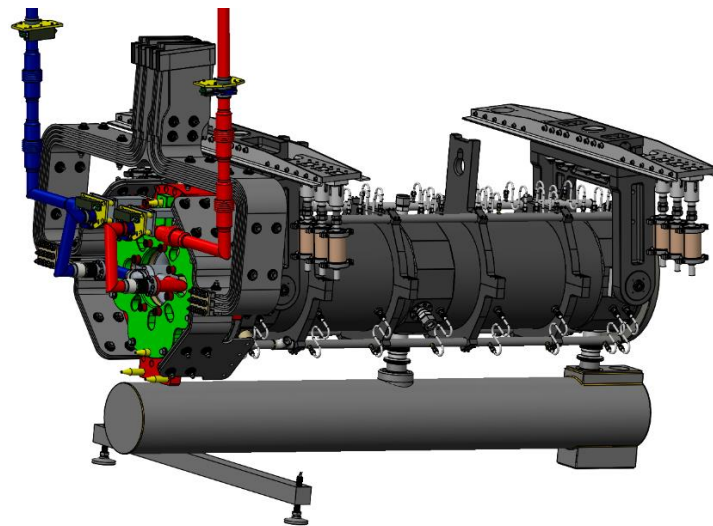
Target Concept Selection Result

Single Intermediate Length Cantilever Target

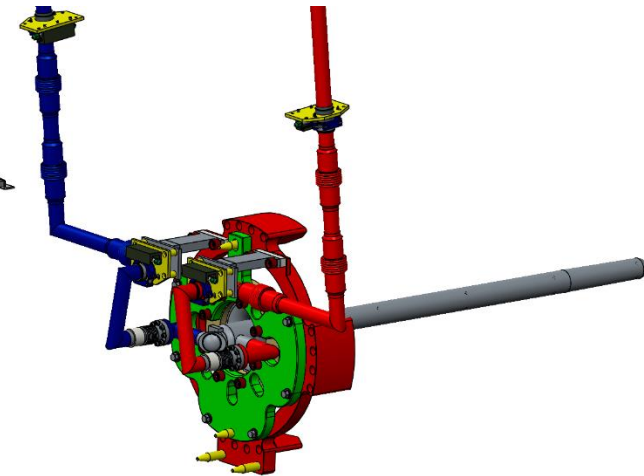
- Manufacturing prototype (operational spare?) to be **1.5m long**
- 1st operational target to be ***“as long as realistically achievable”***



Module Assembly

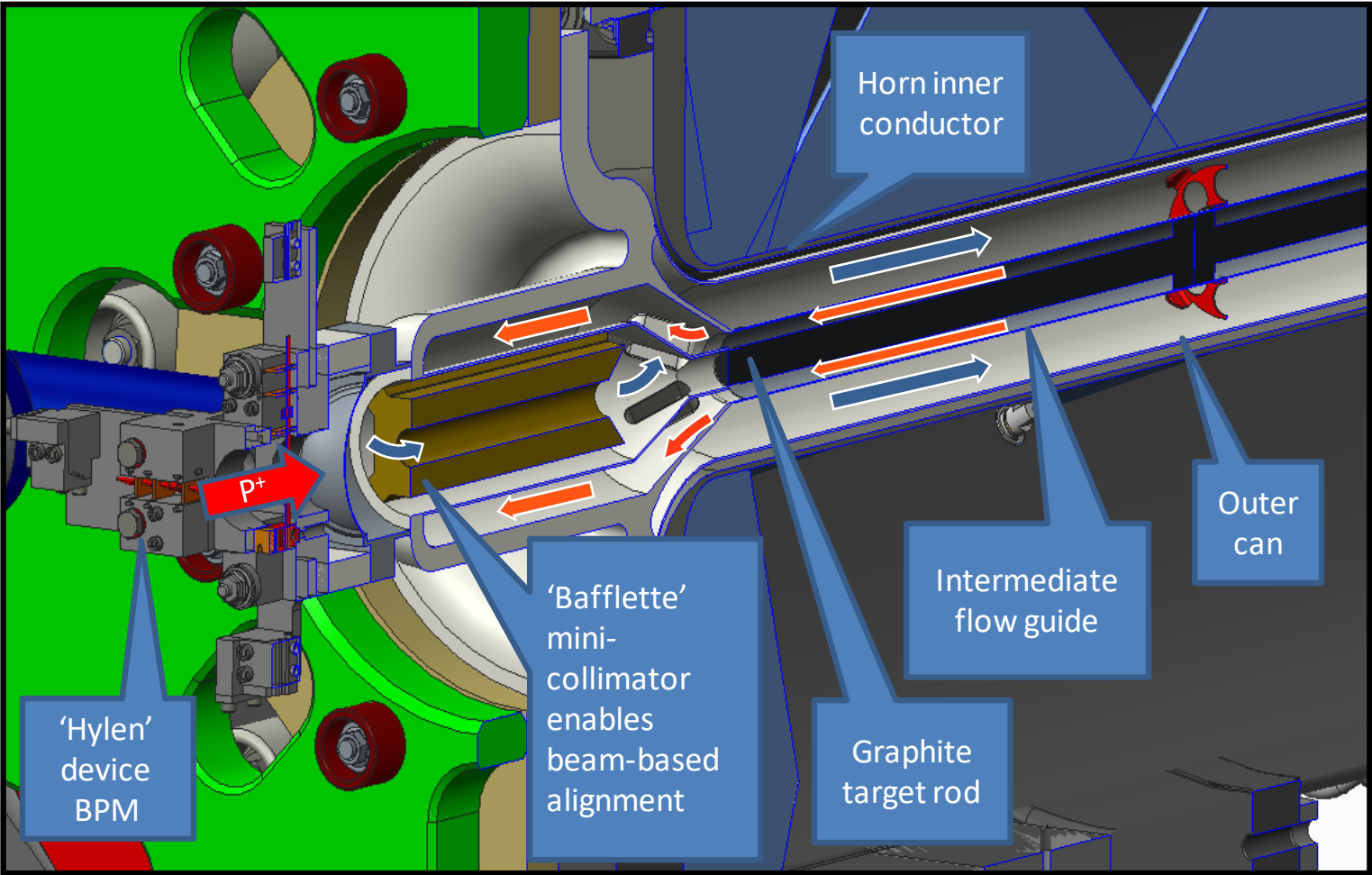


Horn Assembly

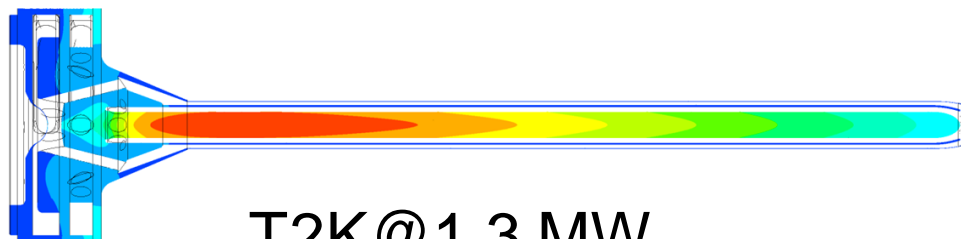


Target

Upstream Target Integration with Horn

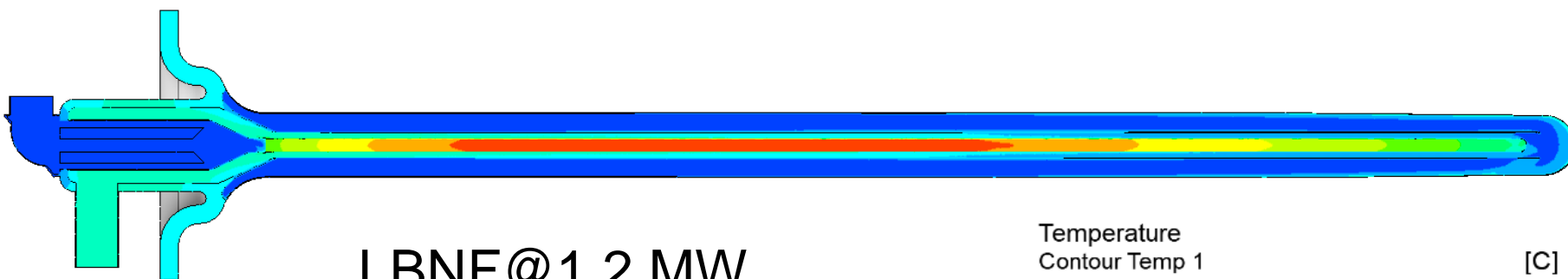
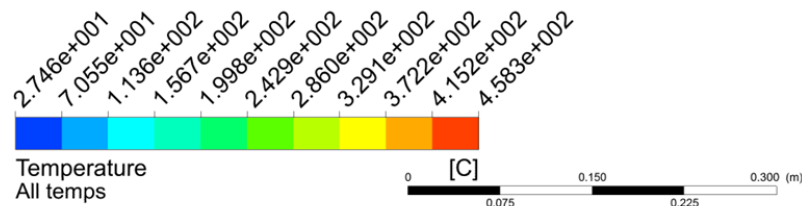


LBNF conceptual design compared with T2K 'state-of-the-art'

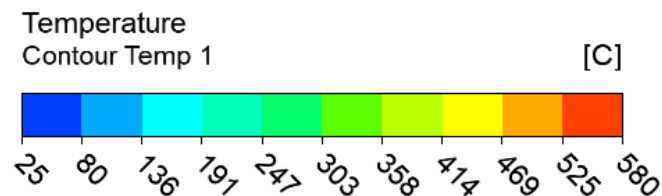


T2K@1.3 MW

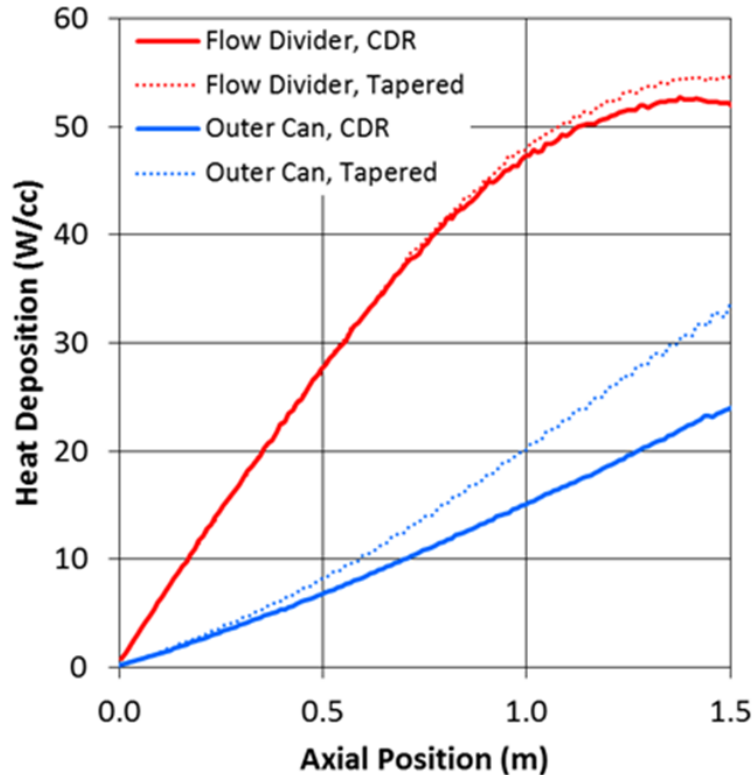
NB current experience up to 500 kW



LBNF@1.2 MW



Thermal management

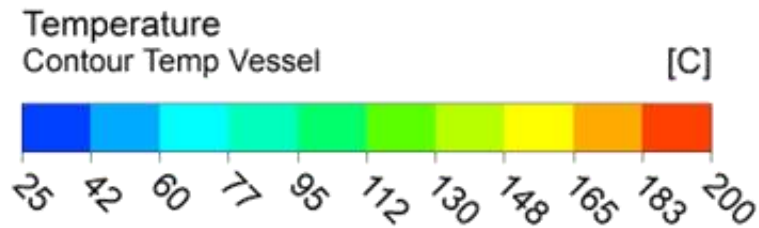


- Heat load in outer can and flow divider increases towards downstream end as particle shower develops
- Need to increase heat transfer along length
- Idea: taper outer tube to accelerate flow along length

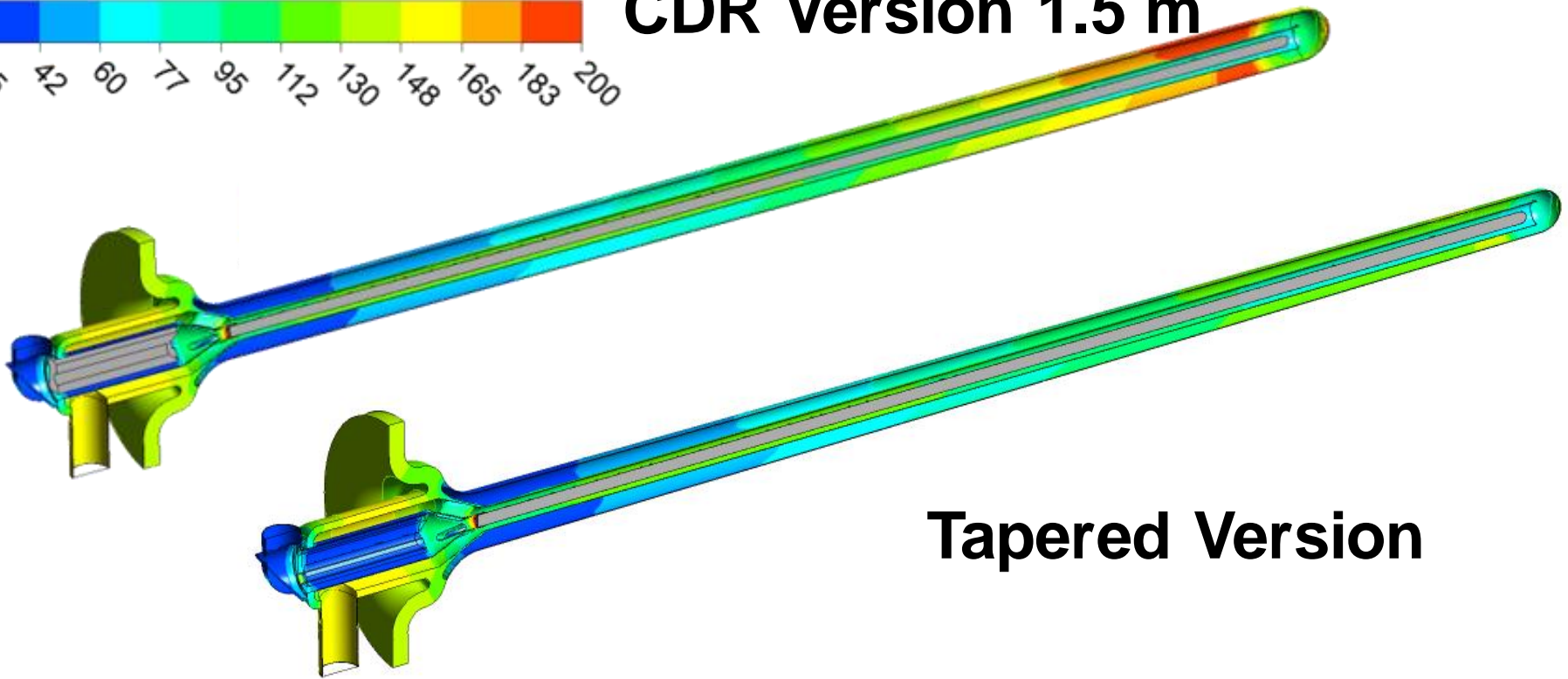
Heat loads in target tubes

Thermal Management, CFD

- CFD studies being carried out in concert with physics and mechanical studies
- Good potential to increase target length beyond 1.5 m



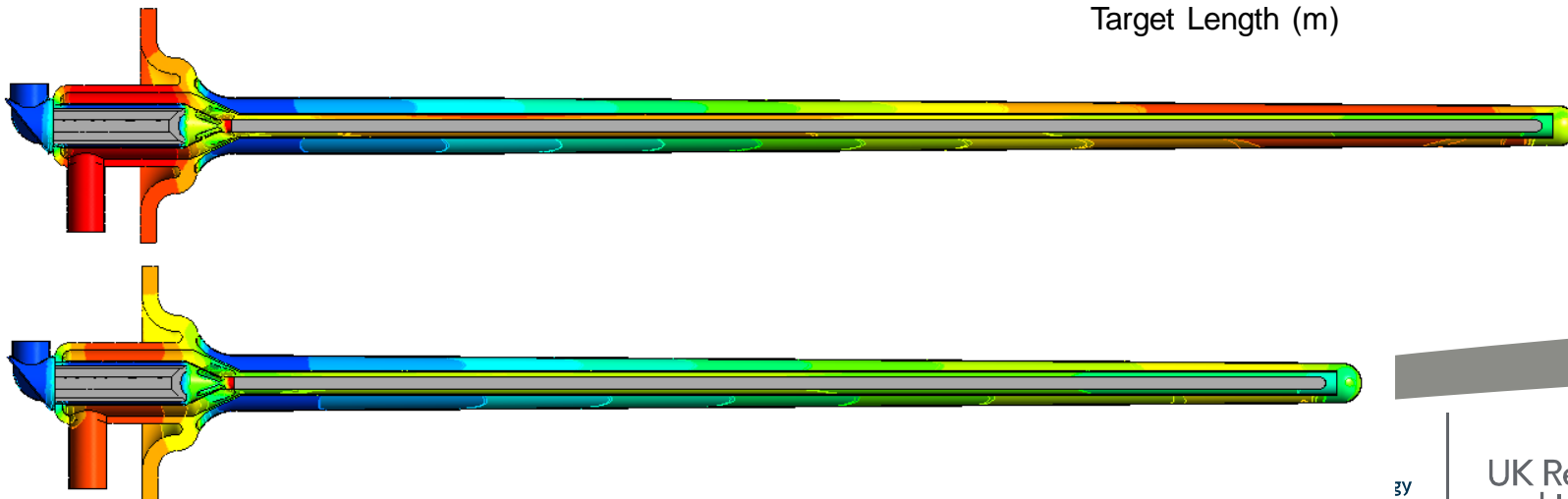
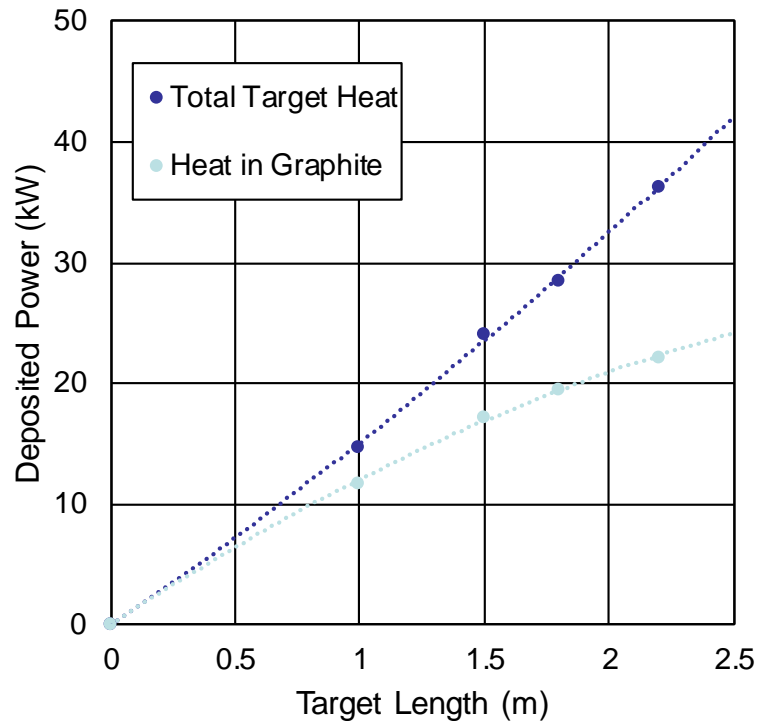
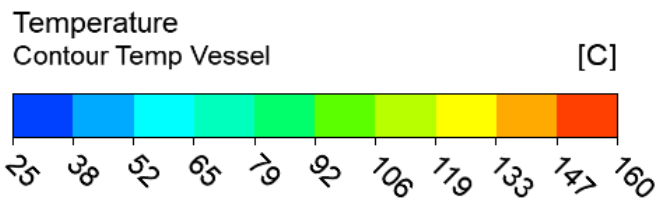
CDR Version 1.5 m



Tapered Version

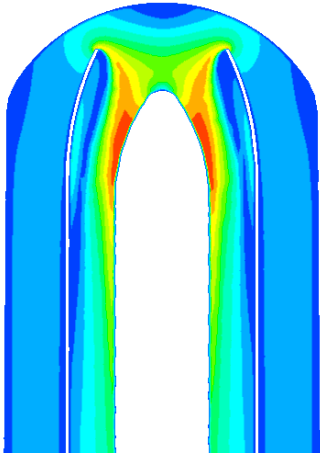
1.8m vs 1.5m Target – Thermal Issues

- Harder to keep vessel cool in longer (1.8m) target
- Solution → compensate by increasing helium flow from 35 to 46 g/s

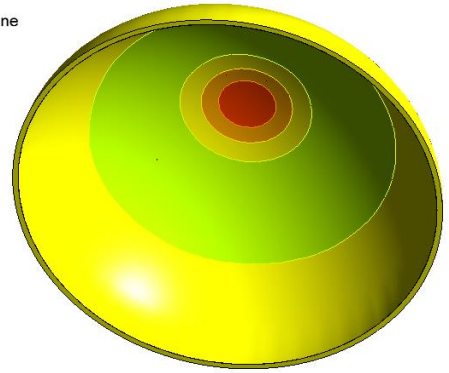


Downstream window temperature/ stress/ pressure drop optimization

Velocity Contour Vel
441
397
353
309
265
221
176
132
88
44
0
[m s⁻¹]

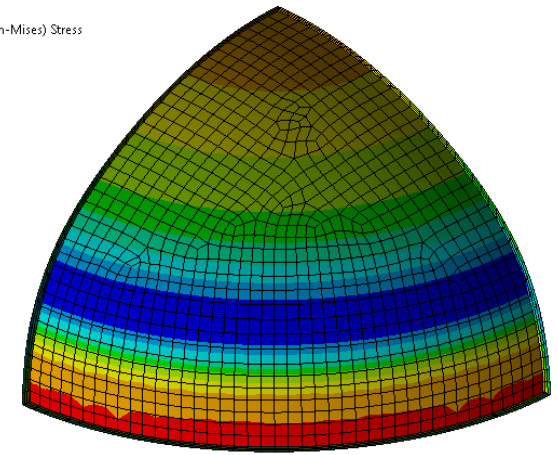


Temperature Contour Temp Plane
76
71
66
60
55
50
45
40
35
30
25
[C]



Temperatures

C: Static Structural
Equivalent Stress
Type: Equivalent (von-Mises) Stress
Unit: MPa
Time: 1
21.093 Max
19.415
17.737
16.058
14.38
12.702
11.024
9.3458
7.6677
5.9896 Min

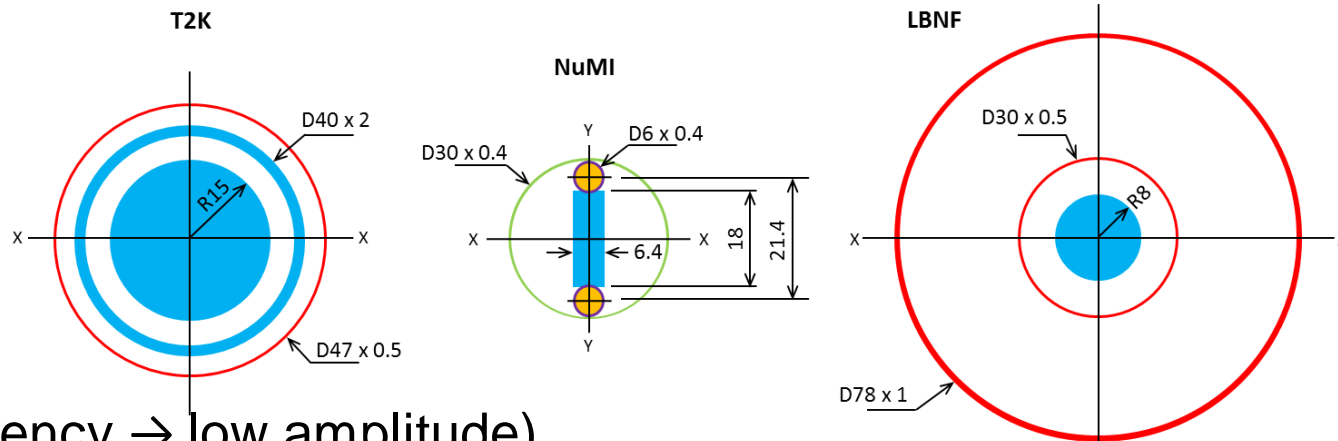


Combined thermal and mechanical stresses with 5 bar internal pressure

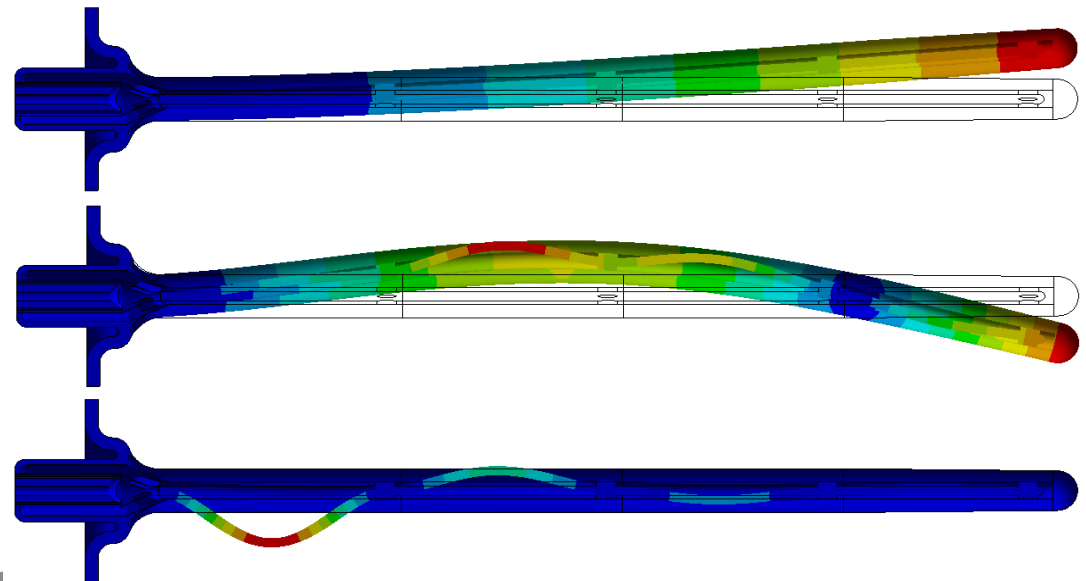
Velocity contours

| Parameter | LBNF | T2K |
|----------------------|------|-----|
| Mass flow (g/s) | 35 | 60 |
| Inlet pressure (bar) | 2 | 5.3 |
| V_{max} (m/s) | 441 | 250 |
| T_{max} (C) | 136 | 102 |
| σ_{max} (MPa) | 21 | 41 |

Dynamic stability as an indicator of 'robustness'



First 3 natural frequency modes:



(high frequency → low amplitude)

| | LBNF (1.5 m) | NuMI | T2K (0.9 m) |
|-------------------------------|-----------------|--------------------|----------------|
| Deflection under gravity (mm) | 0.79 | ≈0.9 | ≈0.5 |
| Natural Freq (Hz) for mode: | | | |
| 1 | 22 | 14 (Horizontal) | 28 |
| 2 | 135 | | |
| 3 | 228 | | |

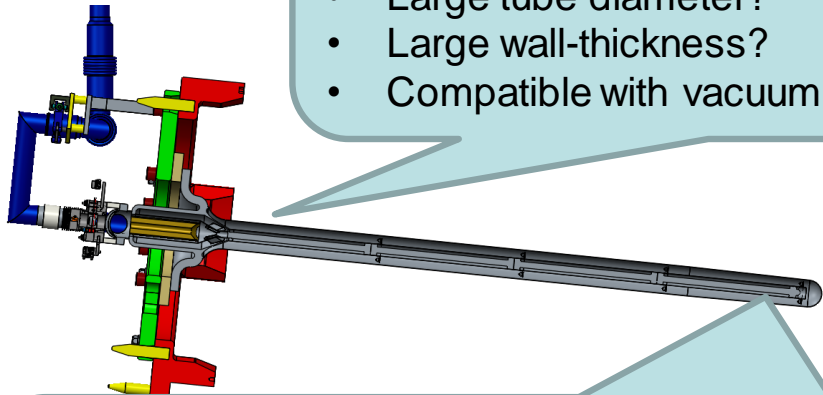
How can we maximise target length?

- Factors point towards a tapered (cone shaped) outer container
 - potentially good for mechanics, thermal management, and physics!
- Currently working to optimise present design

Upstream part of Cantilever

Bending moment → High, Volumetric heating → Low

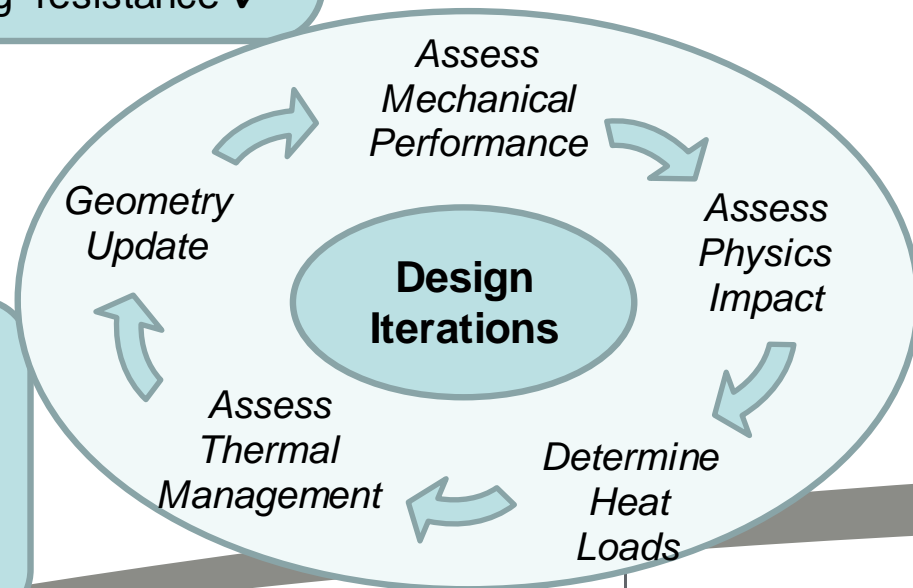
- Large tube diameter?
- Large wall-thickness?
- Compatible with vacuum buckling resistance ✓



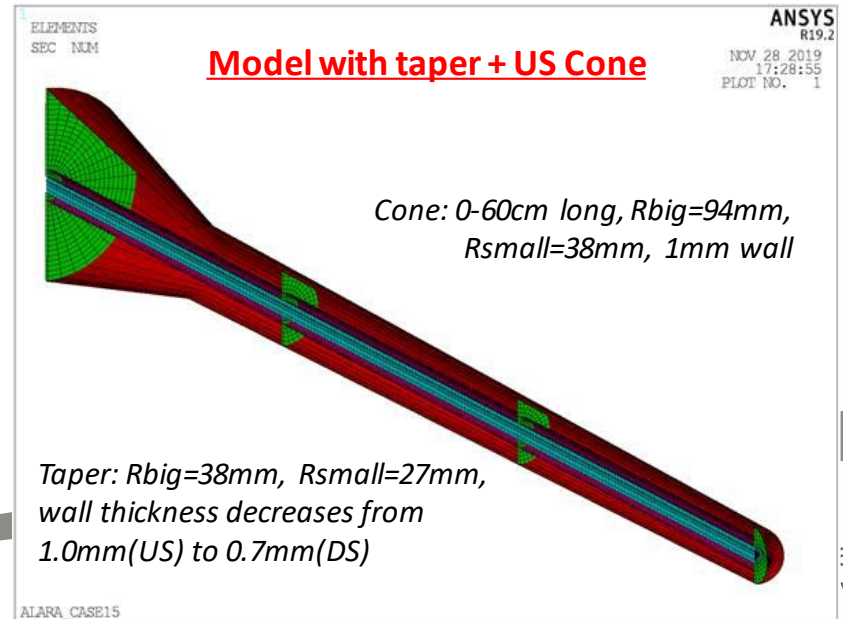
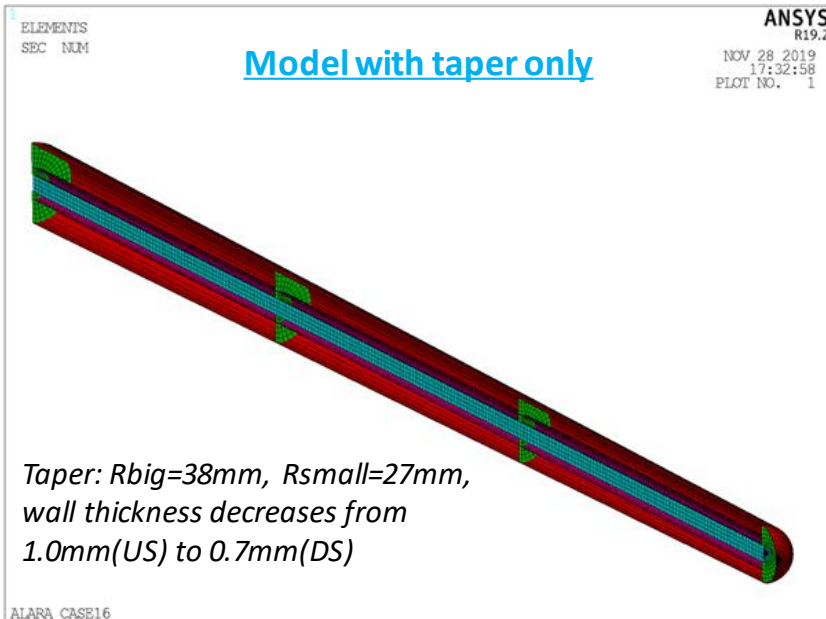
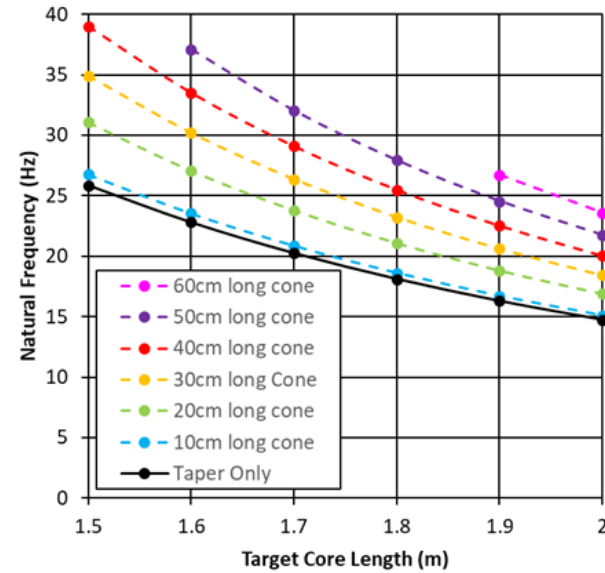
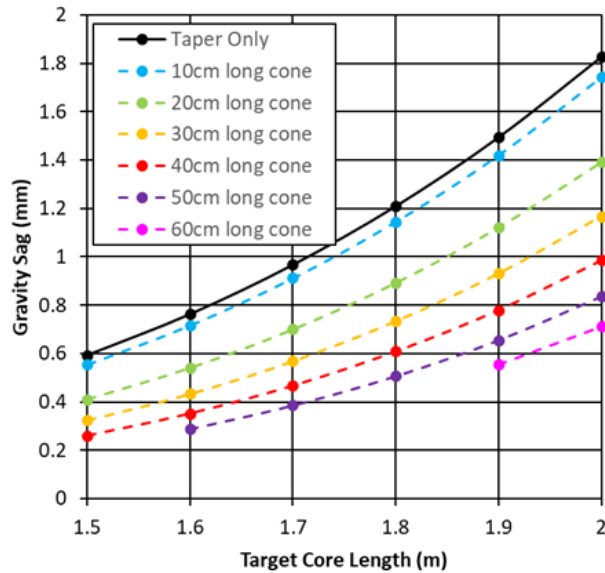
Downstream part of Cantilever

Bending moment → Low, Volumetric heating → High

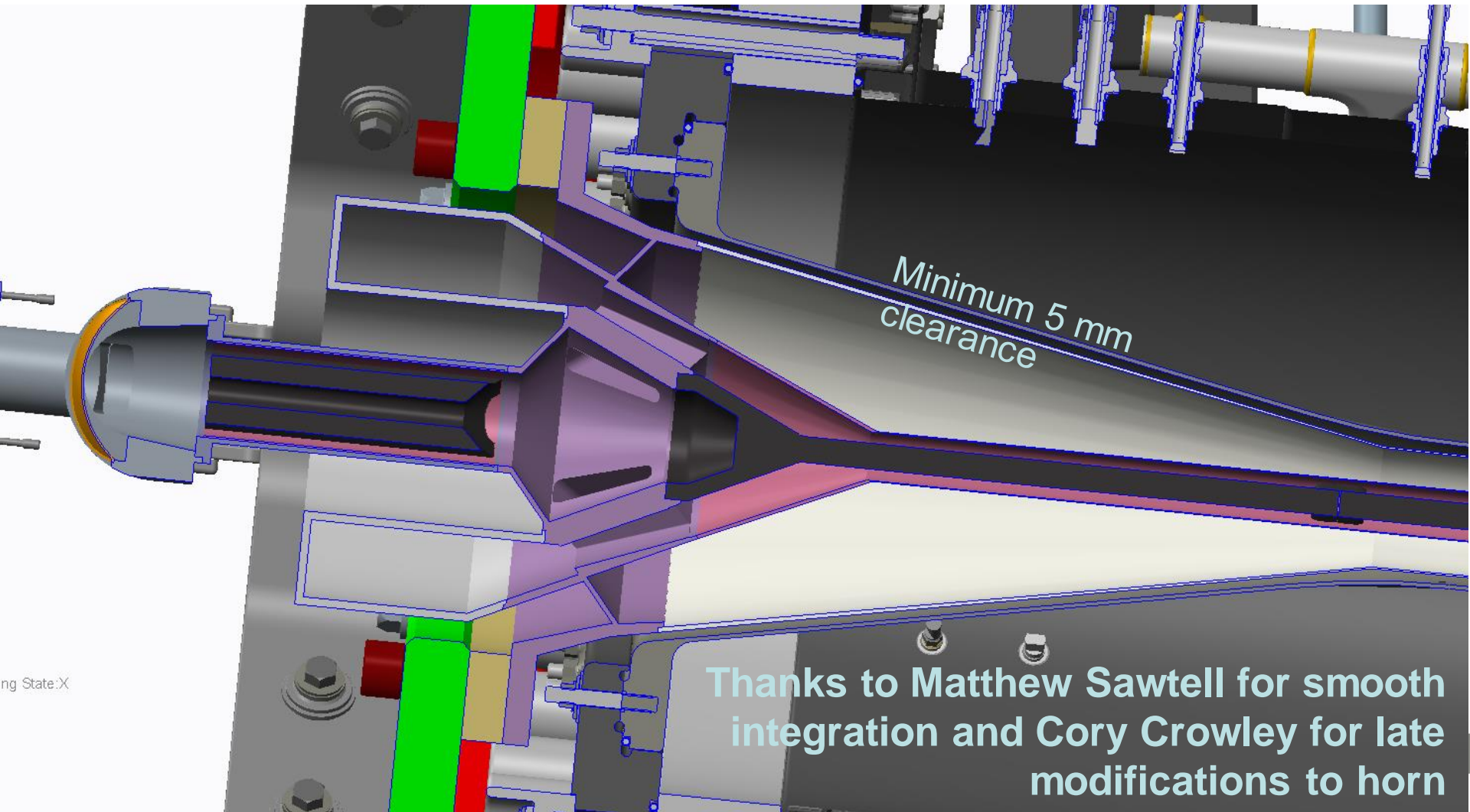
- Small tube diameter?
- Small wall-thickness?
- Compatible with vacuum buckling resistance ✓



US cone potentially “buys” us some extra target length

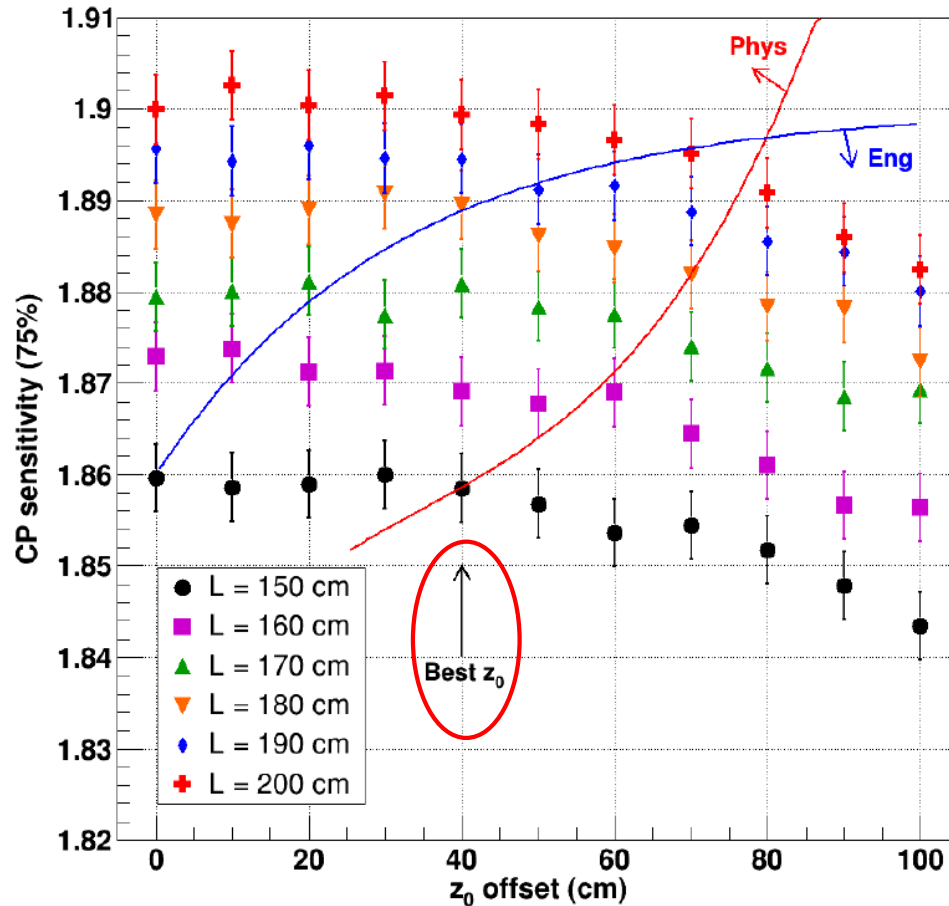


Tapered Target & Horn Integration



Thanks to Matthew Sawtell for smooth integration and Cory Crowley for late modifications to horn

Physics/engineering optimization



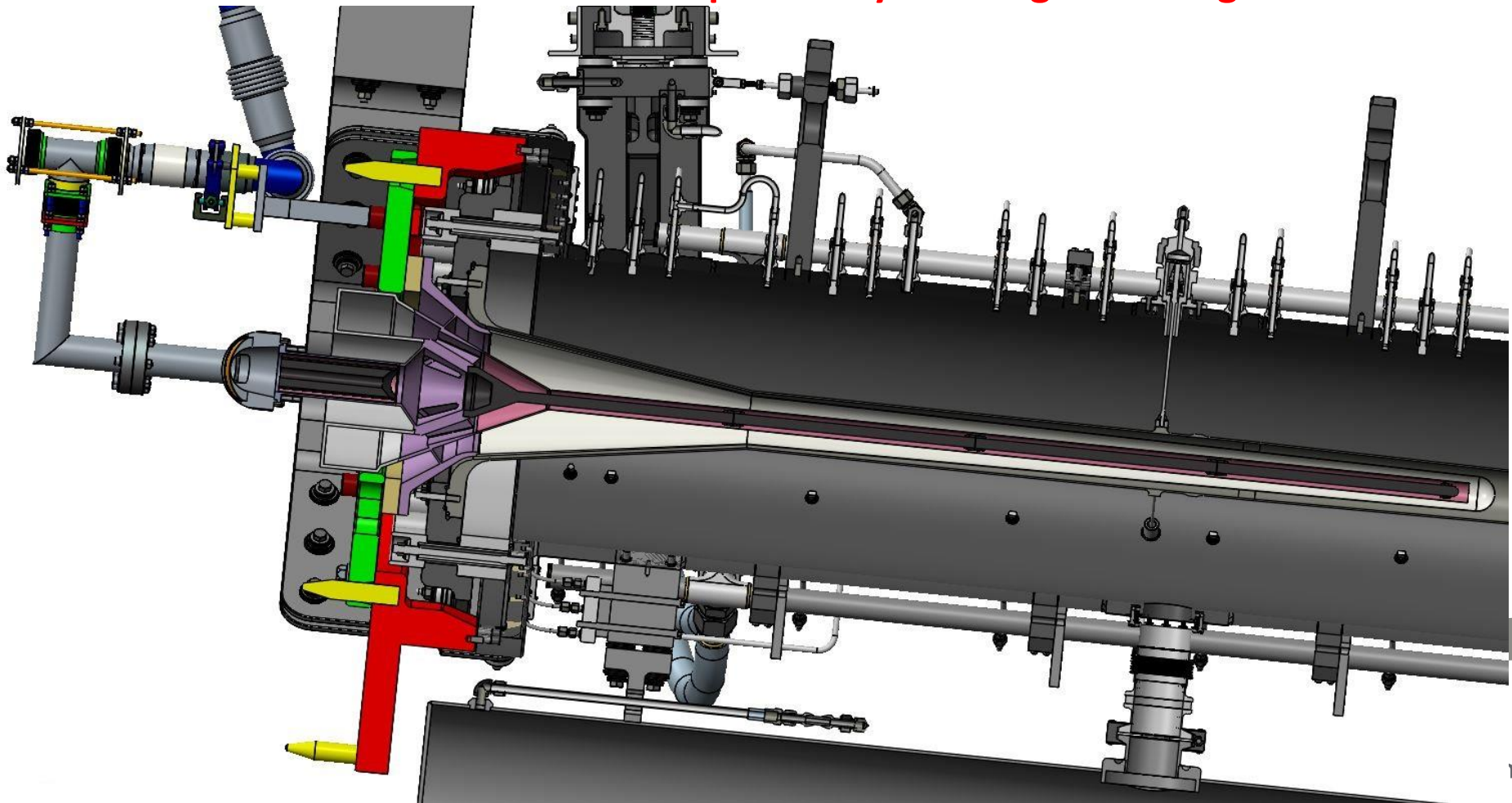
Upstream cone length

| Target core length L (cm) | Vessel cone min length z_0 (cm) | Extra time needed per run year (days) |
|---------------------------|-----------------------------------|---------------------------------------|
| 150 | 0 | 19 |
| 160 | 17 | 13 |
| 170 | 28 | 11 |
| 180 | 42 | 6 |
| 190 | 56 | 5 |
| 200 | 73 | 4 |

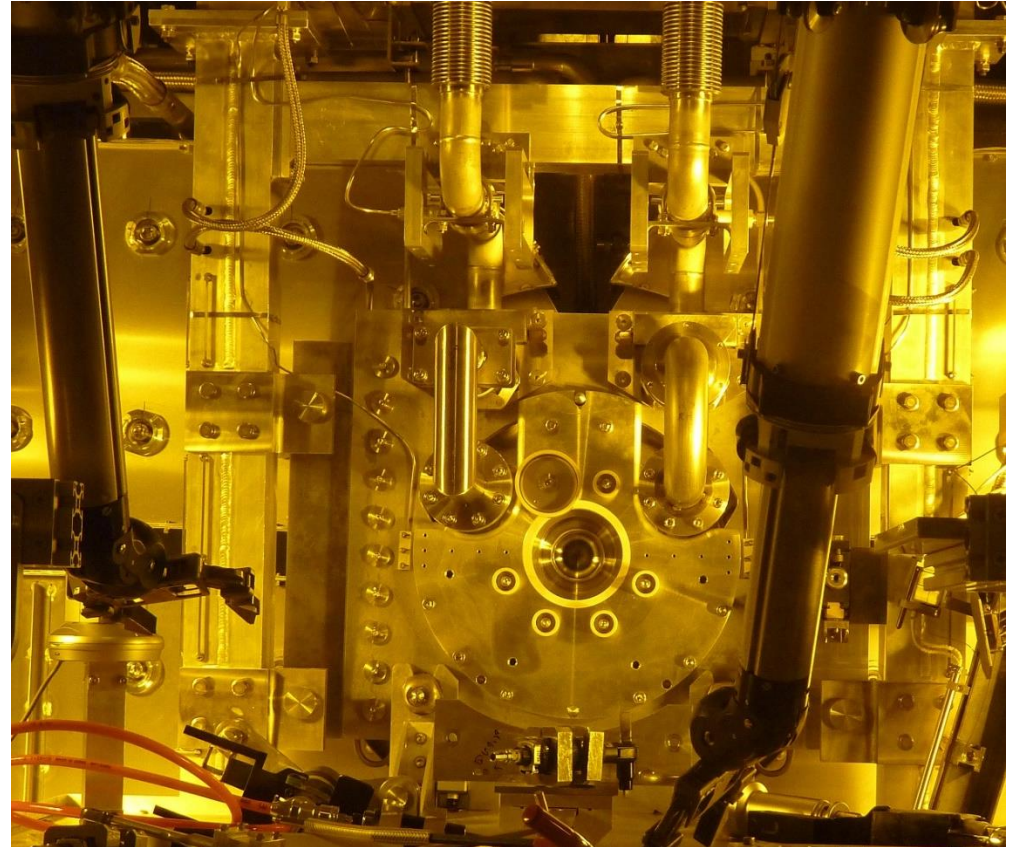
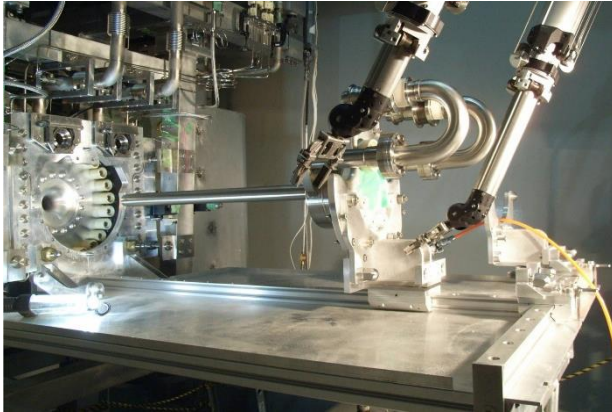
Target/horn integration and remote handling

- Expect targets to fail
- Horns are inherently complex, costly and take a long time to produce
- Target cost $\approx 1/10^{\text{th}}$ horn cost, and spares can be produced more readily

→ Hence the need for an independently exchangeable target

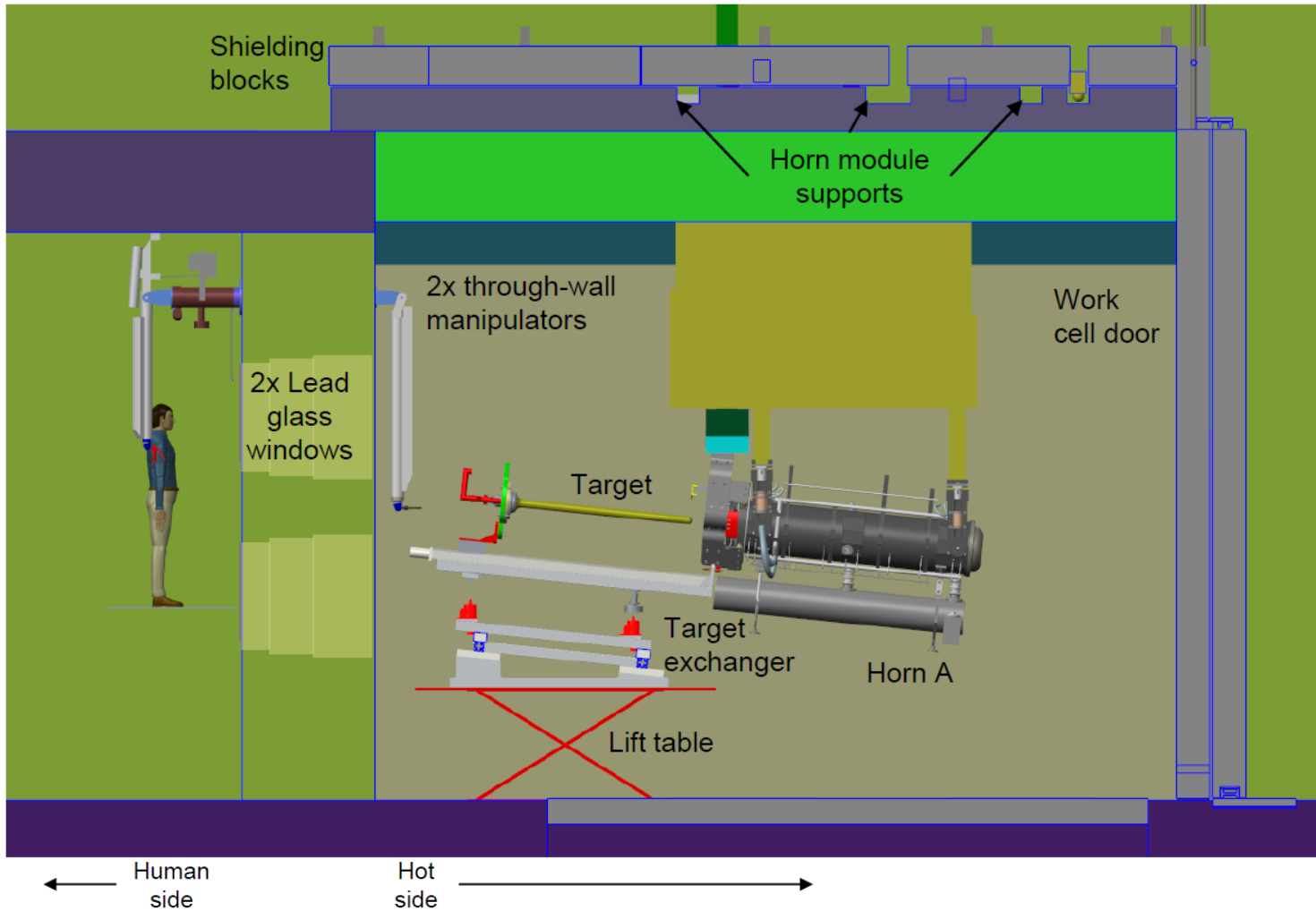


Current Experience – T2K



- Experience from T2K will feed into LBNF exchanger design
- NB Never needed to replace a failed T2K target

LBNF Work Cell During Target Exchange



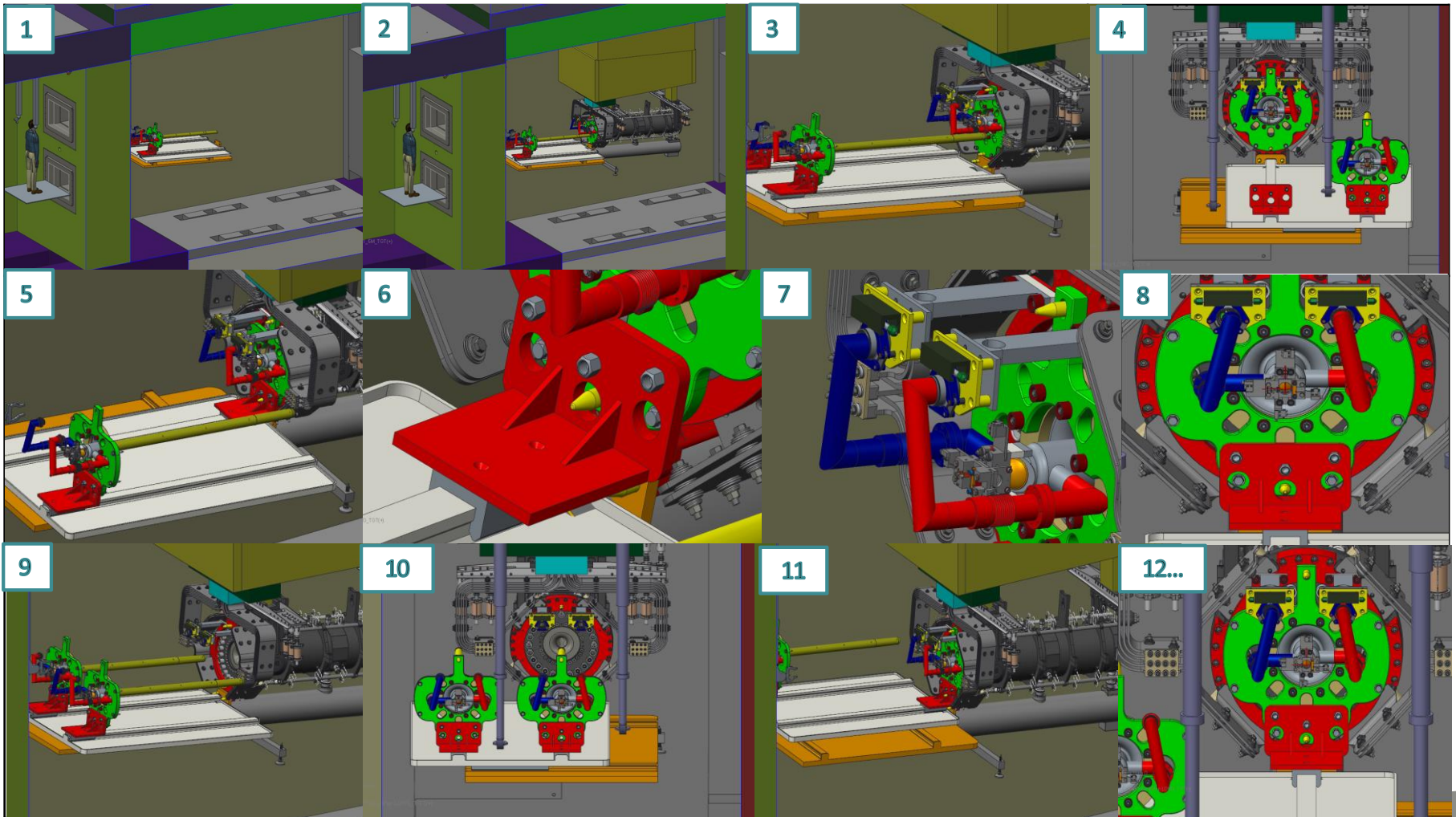
Horn module supported from the top of the work cell

Target exchanger located on lift table on work cell floor

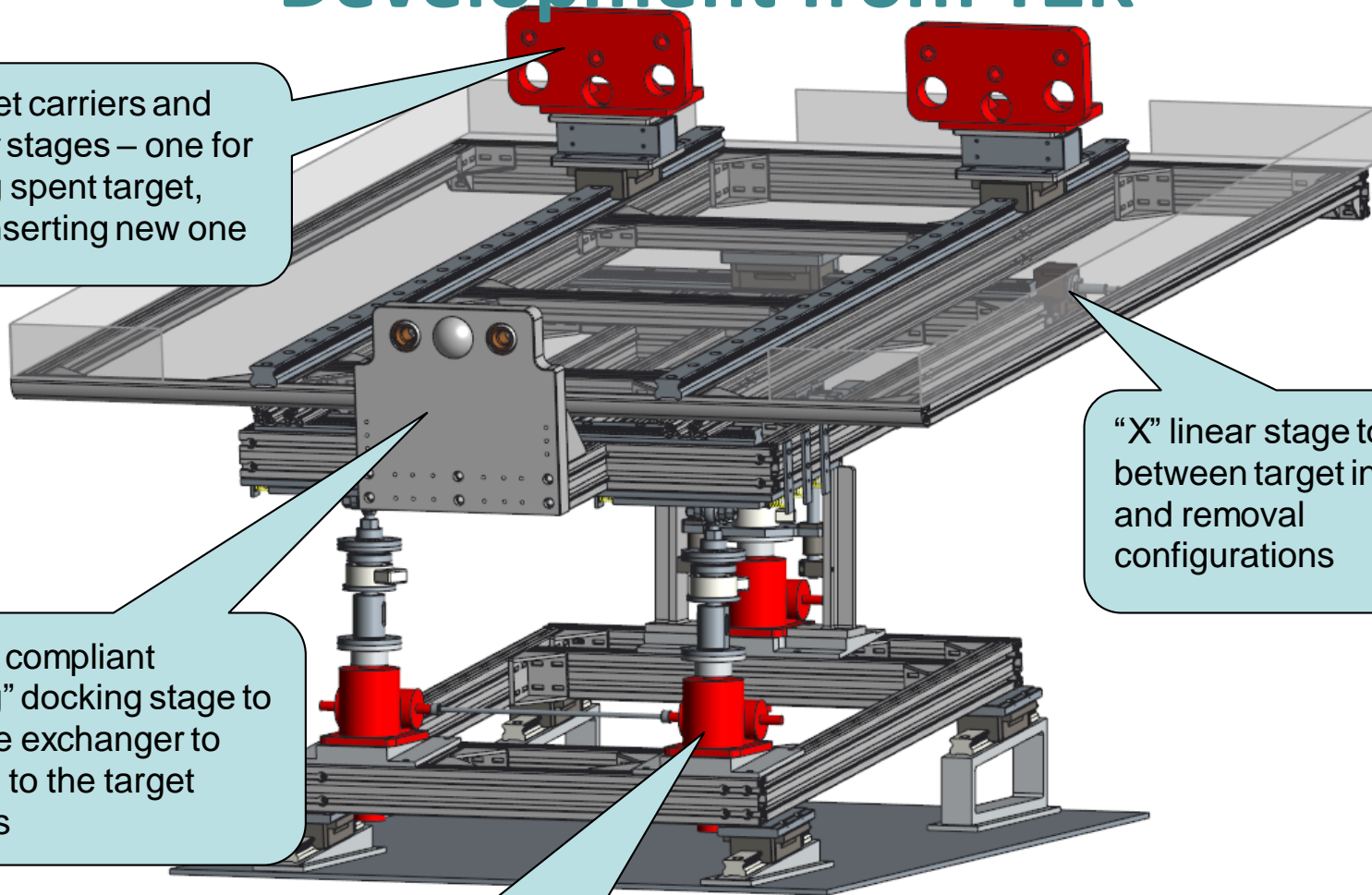
Persons using through-wall manipulators are approximately 4m away from the front face of the horn

Market survey has been carried out of suitable manipulators

Outline Procedures for Target Exchange



Target Exchanger Concept – Development from T2K



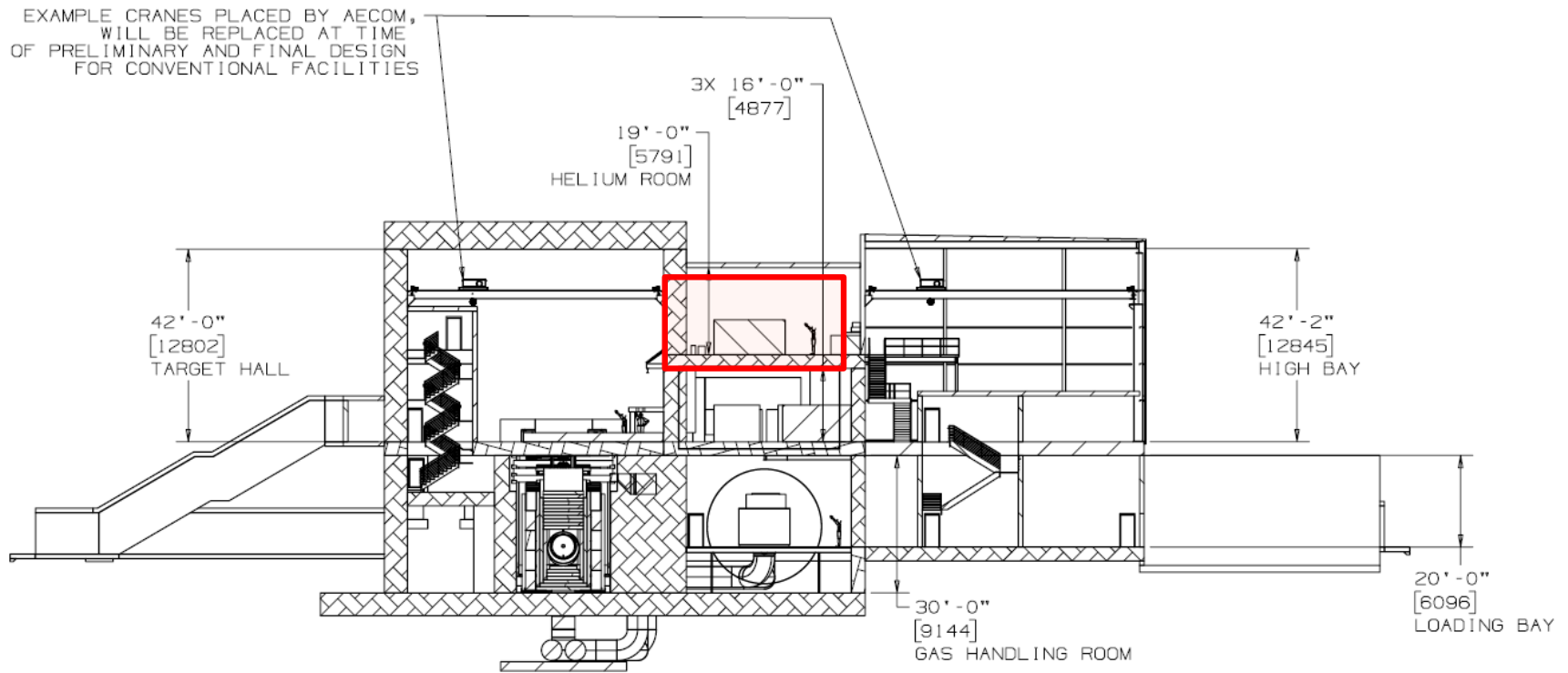
Two target carriers and “Z” linear stages – one for removing spent target, one for inserting new one

“X” linear stage to transfer between target insertion and removal configurations

Sprung, compliant “floating” docking stage to allow the exchanger to mate up to the target supports

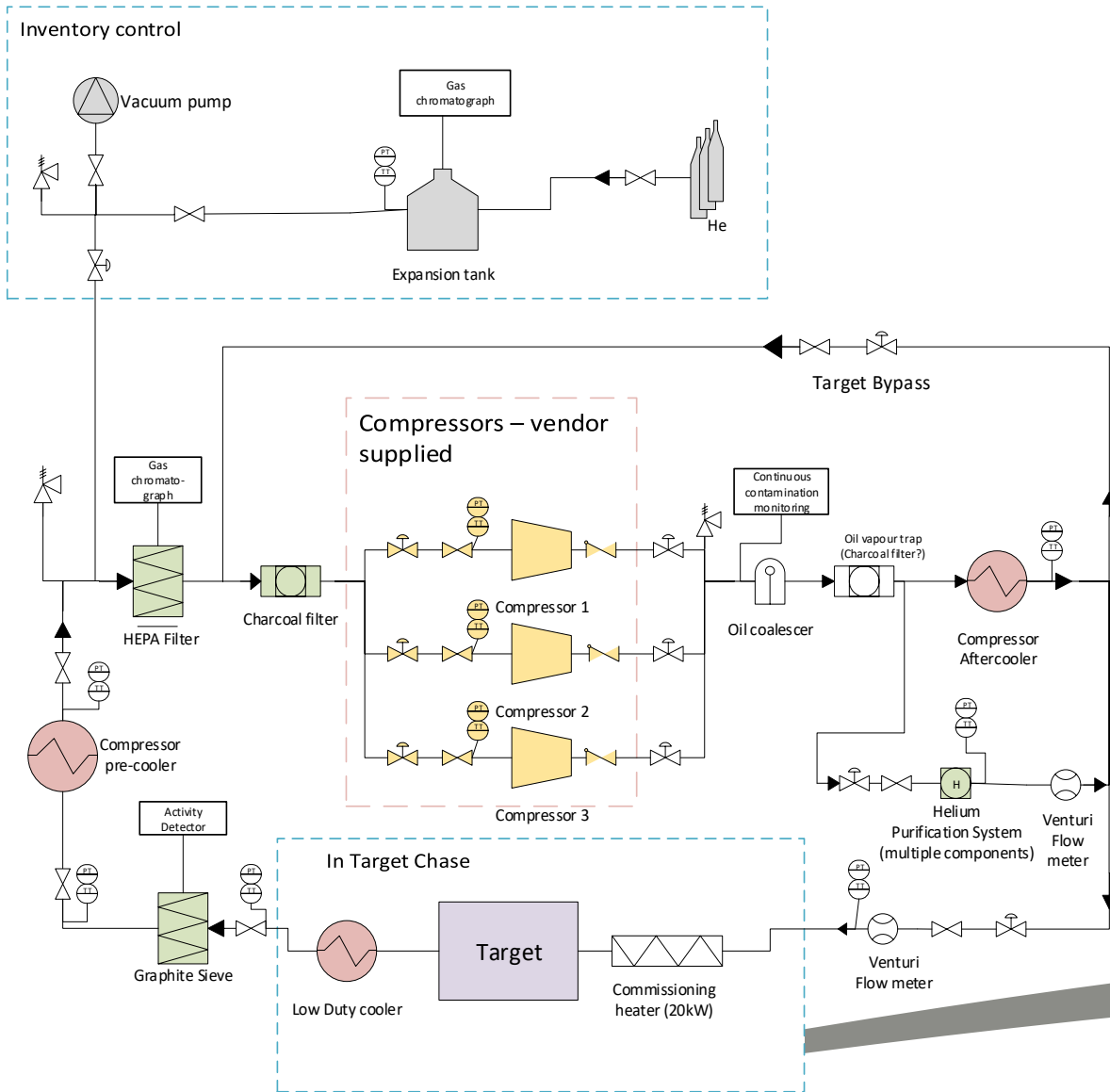
Screw jacks and linear stages to position and align the exchanger during docking procedure

LBNF-20 Target Hall – Helium Room Location



[Drawn by: Matthew Sawtell,](#)
[Fermilab](#)

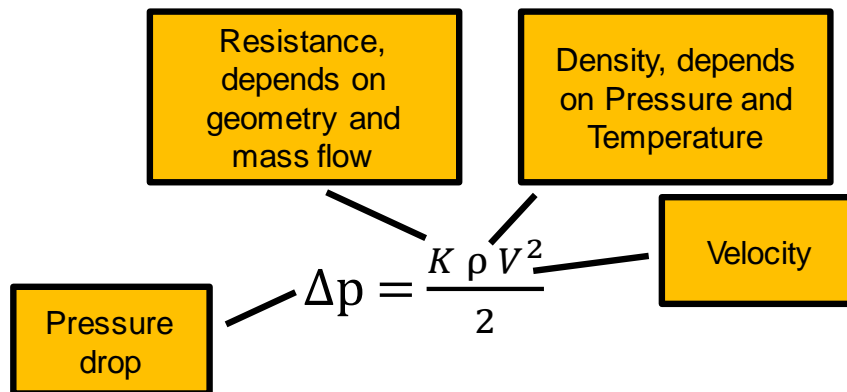
Target Helium Circuit



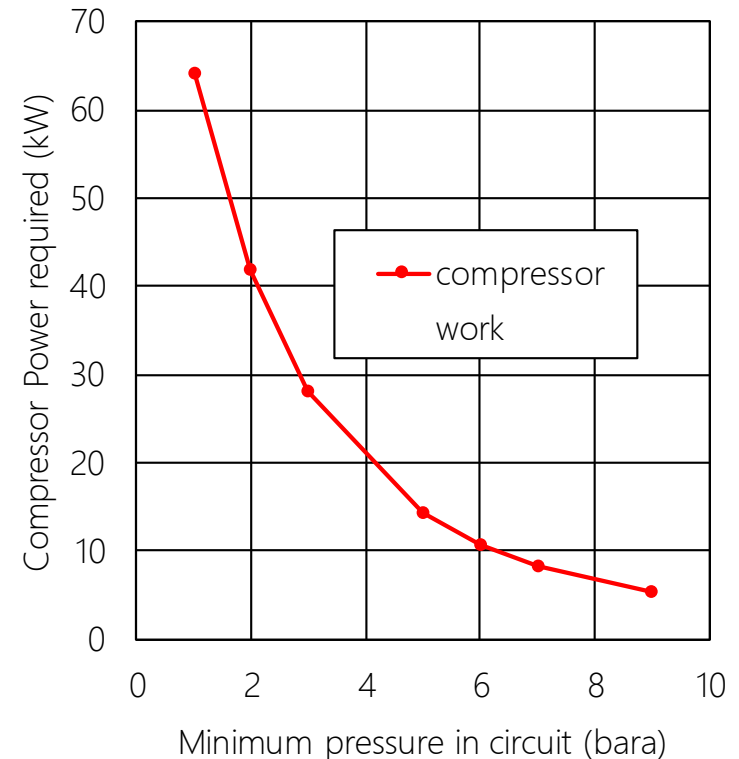
- Potential compressor and heat exchangers identified as future UK In-Kind Contributions
- Possibility to prototype flow control/ monitoring on T2K helium plant

System Pressure Considerations

- For a given helium mass flow, can increase system back pressure “Pmin” to reduce component pressure drops



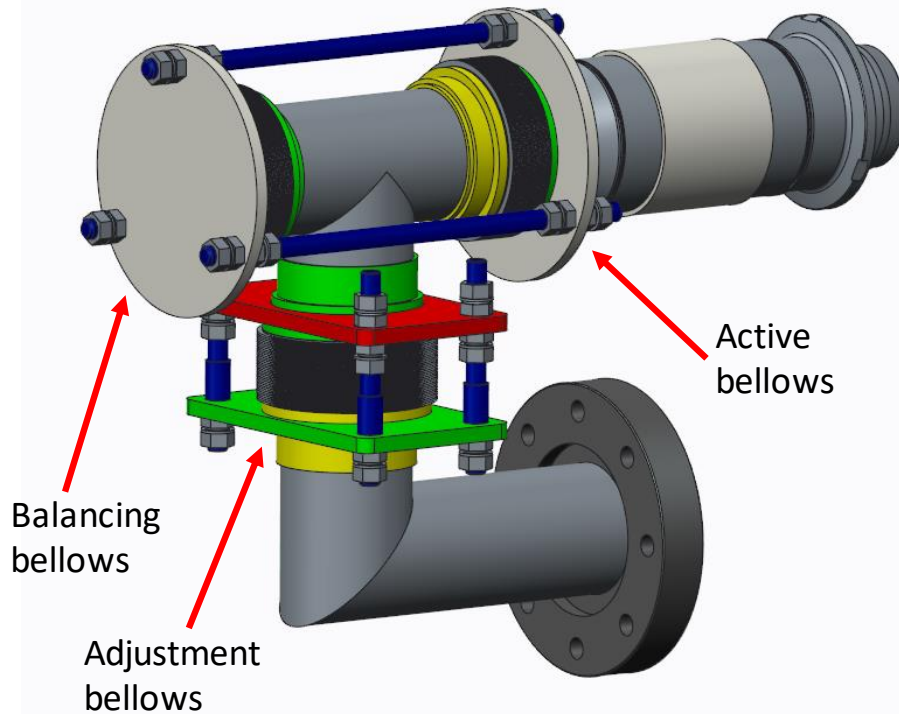
- Aim to reduce pressure ratio: $\frac{\text{Pressure out}}{\text{Pressure in}}$
- Leads to a reduction in compressor work (re: system cost, running cost, etc...)
- Win-win for heat-exchanger pressure drop due to reduced heating of fluid



T2K: Pressure-balanced Bellows Arrangement

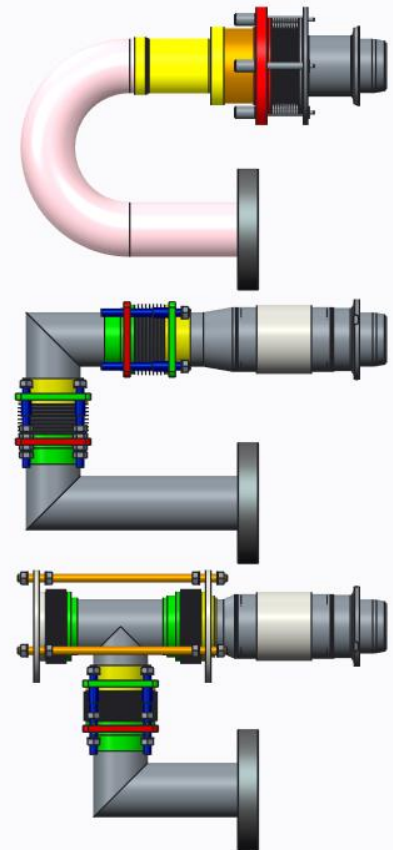
- Intend to profit from ongoing T2K target pipe R&D, enabling high pressure (5 bar) operation

Potential pressure balanced pipe design: Prototype under construction



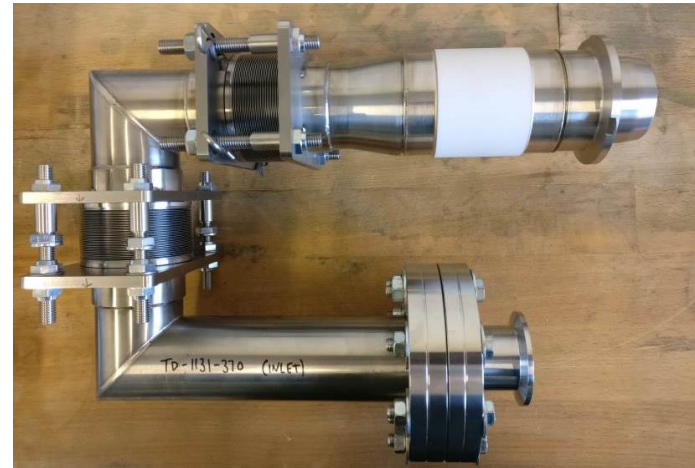
T2K Target Pipe Evolution:

Time→



T2K: Ceramic Isolator Development

- Ceramic breaks are a necessity for electrical isolation in all Neutrino facilities (used in target, horn, striplines etc.)
- They are brittle, fragile and easily broken if loaded in any manner except axial compression
- Intend to profit from historical testing of various types of isolator for T2K with varying degrees of success
 - Diffusion bonded
 - Bolted
 - Brazed
- A test-bed has been used at RAL to address the issue of thermal shock/fatigue on target ceramics



Target helium pipes with brazed alumina isolator for 750kW operation



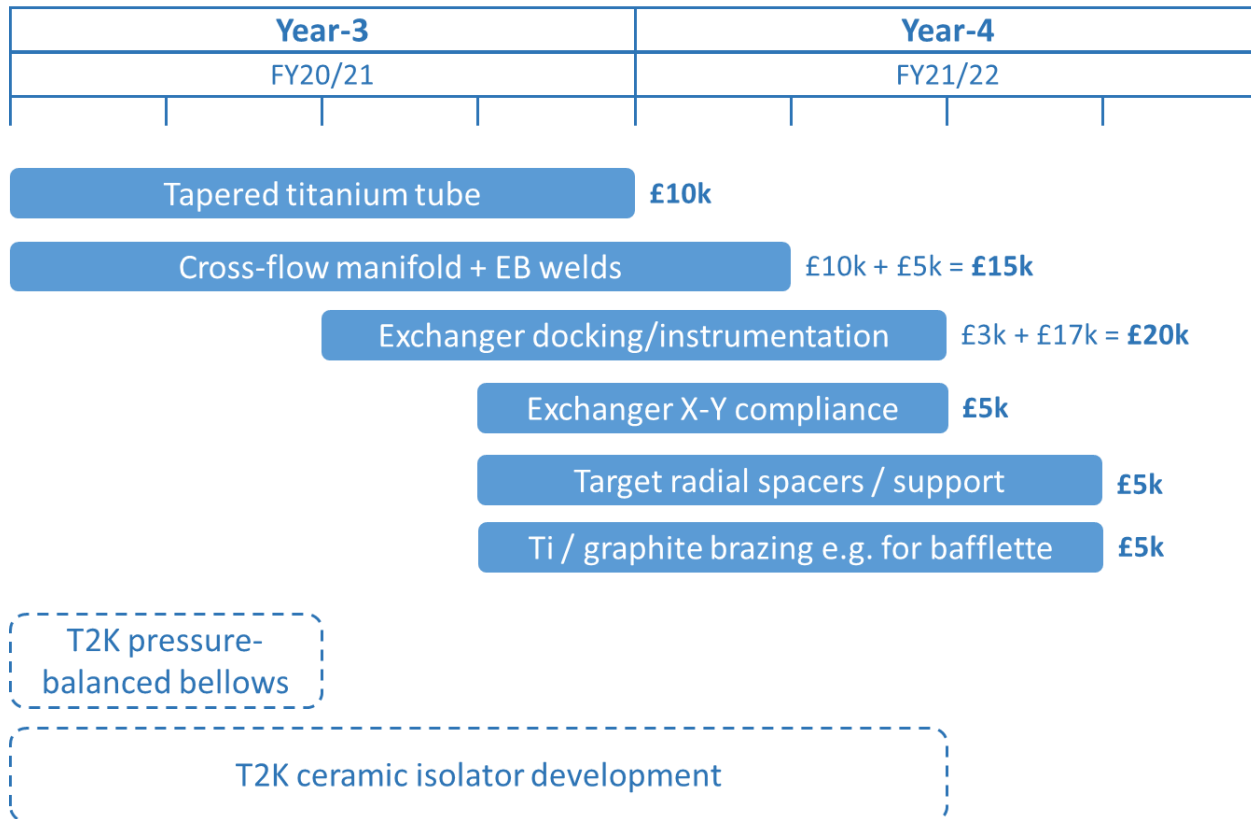
Acoustic enclosure (air inlet) Centrifugal blower (600 m³/hr)

Ceramic test section

Acoustic enclosure (air exhaust)

Phase-1 Prototyping Plan

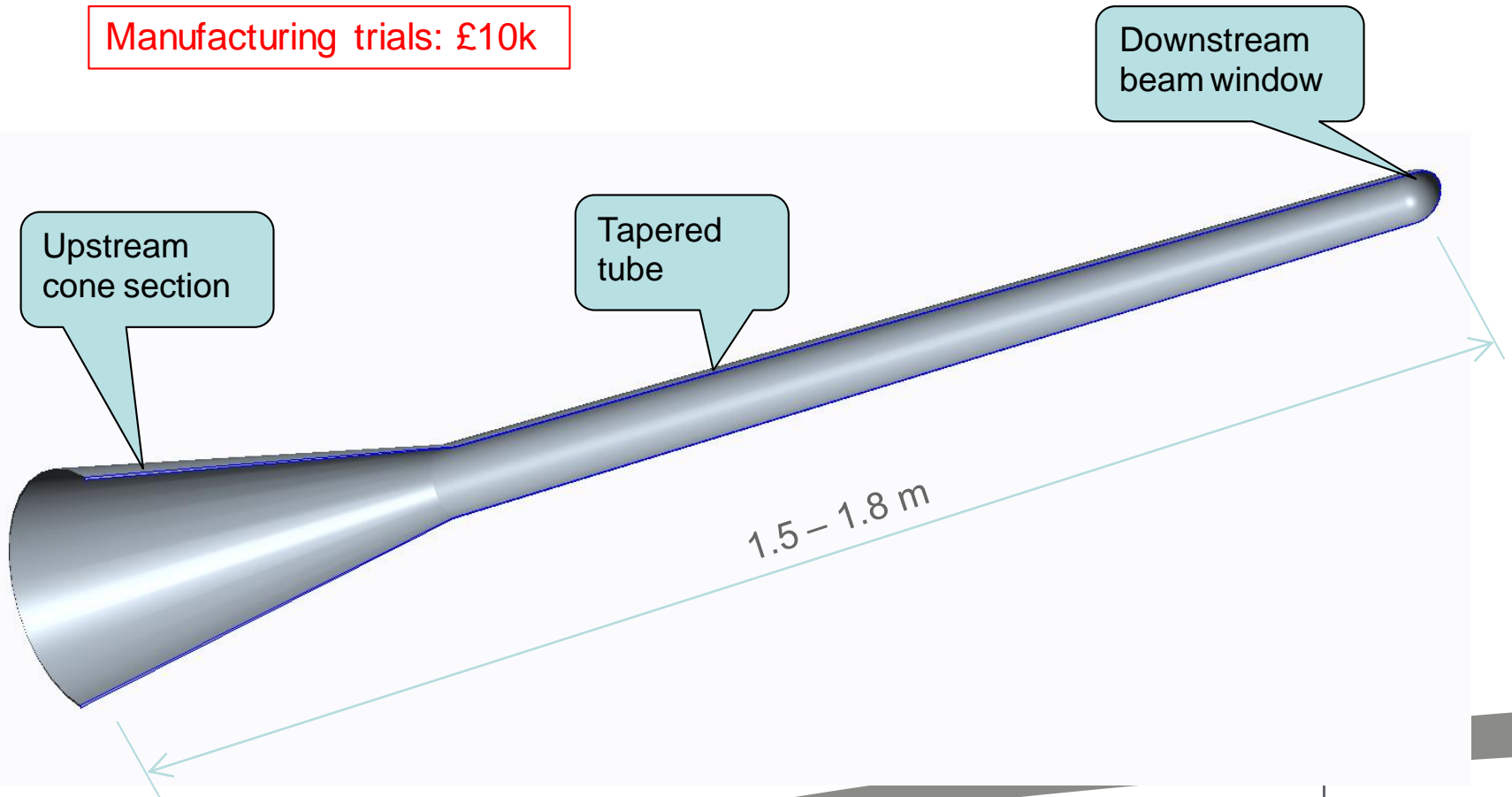
- Feature-prototyping required to inform preliminary-design, identify manufacturing routes / make technology choices and improve cost estimates for LBNF single cantilever target option
- Intend to spend LBNF prototyping budget in FY20/21 and FY21/22
- Will also profit from T2K prototyping activities



Prototyping Plan: Tapered Titanium Tube

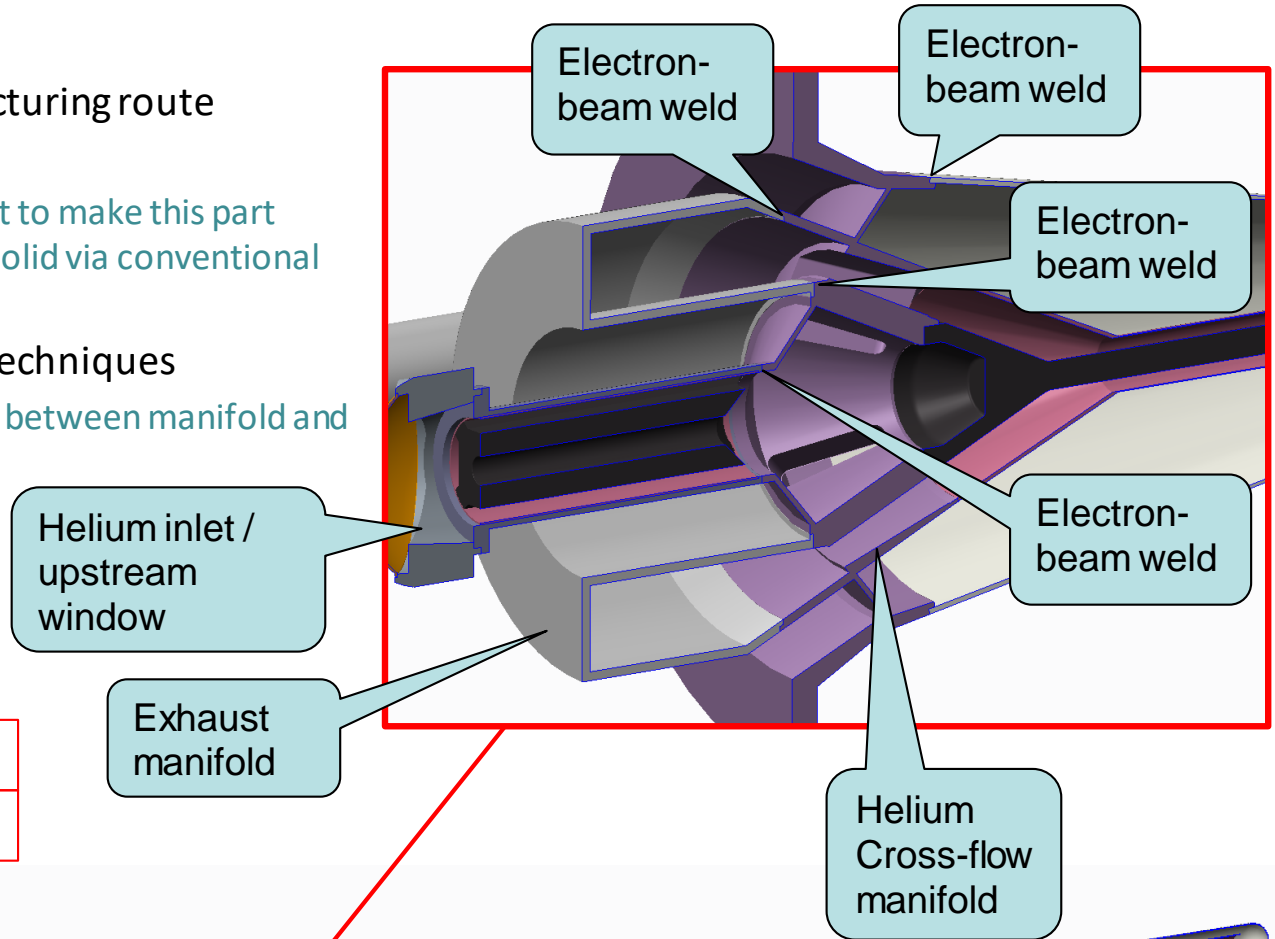
- Demonstrate manufacturing route for outer container (we expect this to be more challenging than for T2k)
 - Longer, Variable wall thickness, Tapered, Precision achievable?

Manufacturing trials: £10k

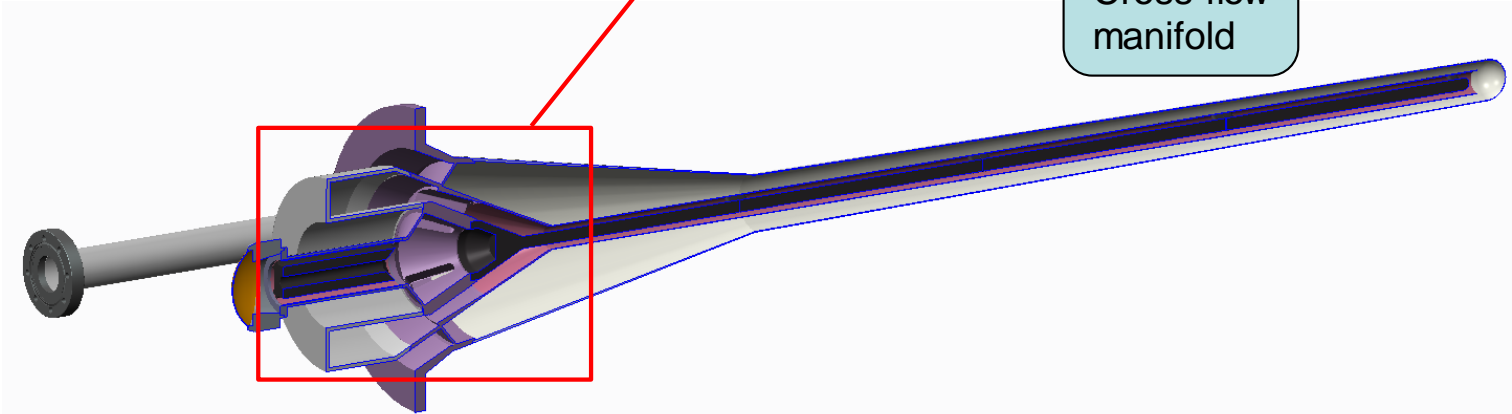


Prototyping Plan: Cross-flow manifold + EB welds

- Demonstrate manufacturing route
 - Complex geometry
 - Recent design effort to make this part machineable from solid via conventional methods
- Demonstrate joining techniques
 - EB welding of joints between manifold and vessel wall



Machining trials: £10k
Welding trials: £5k

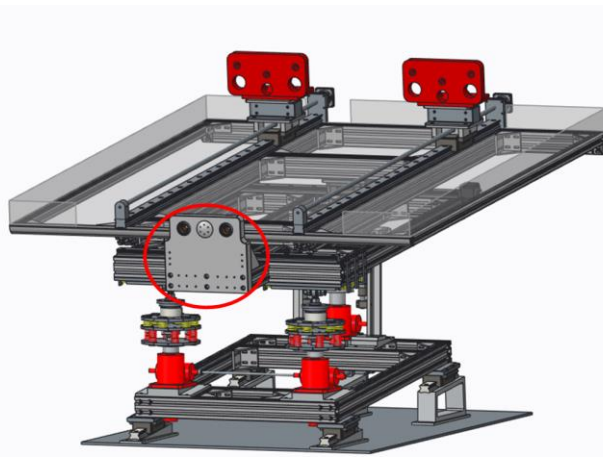
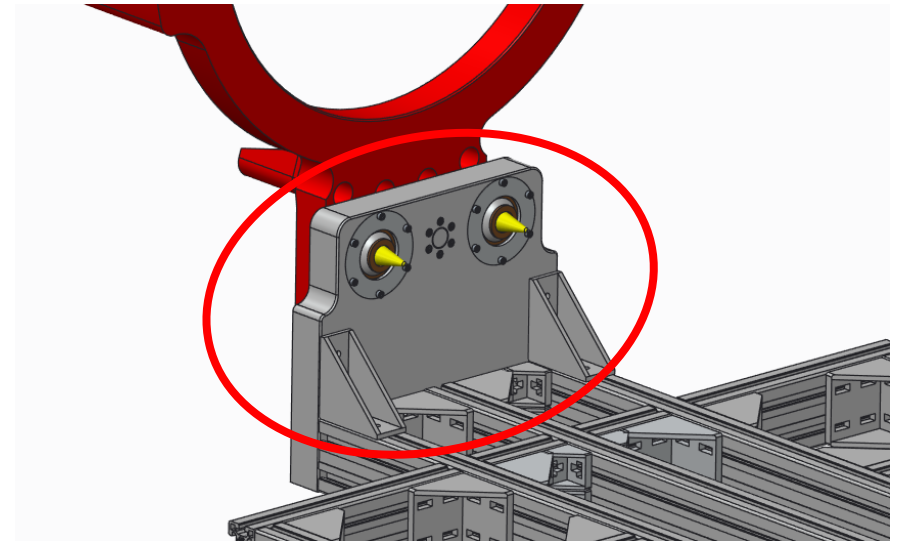


Prototyping Plan: Exchanger Docking / Instrumentation

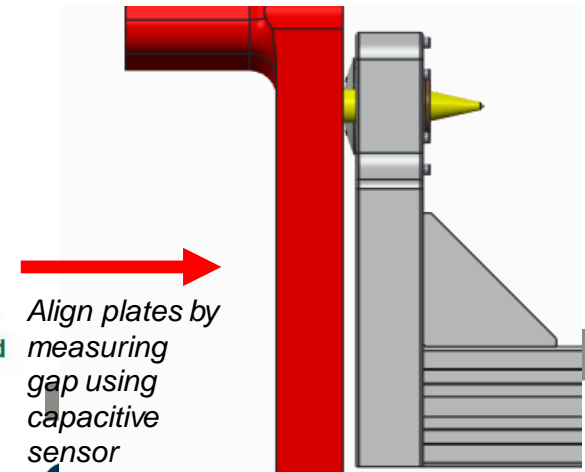
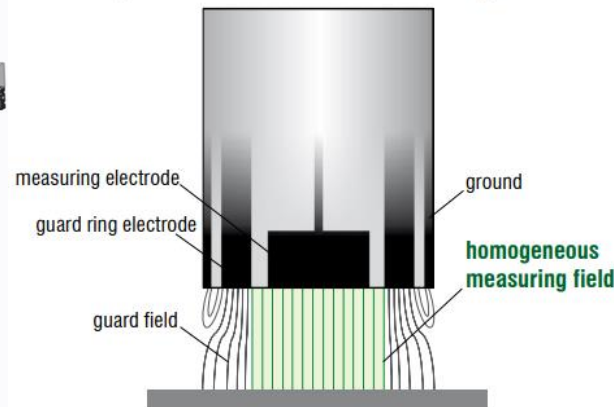
- Prototype the proposed exchanger remote docking interface and remote alignment instrumentation
- Select non-contact instrumentation technology
- Instrumentation could be re-used in production exchanger if successful

Instrumentation: £17k

Hardware interface: £3k



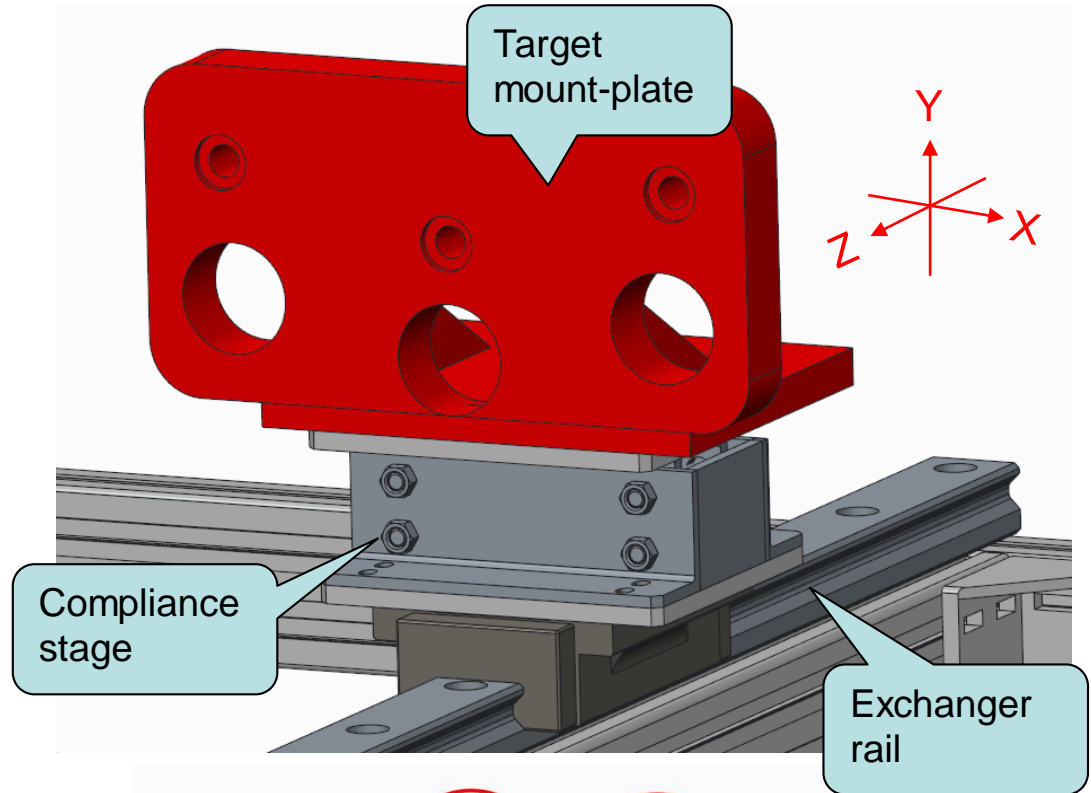
capaNCDT sensor with triaxial design



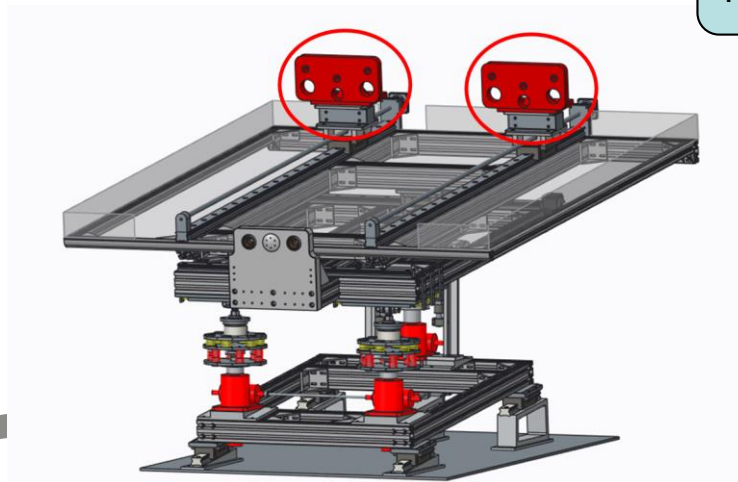
Align plates by measuring gap using capacitive sensor

Prototyping Plan: Exchanger X-Y Compliance

- Need **rigid** mounting system to attach target to exchanger tooling that is also **compliant** in X-Y to permit docking onto precision remote alignment pins
- May be integrated with remote docking/ instrumentation prototype (see previous slide)



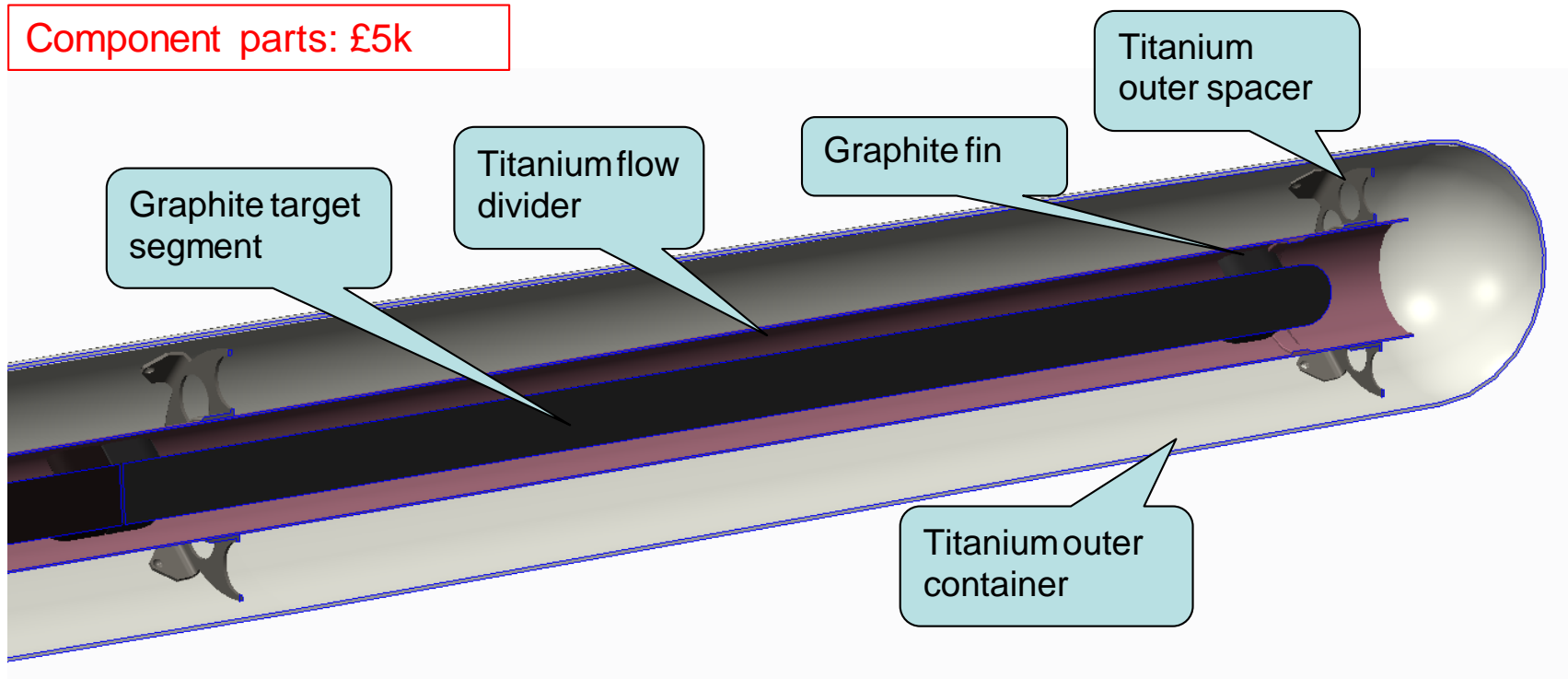
Manufacturing trials: £5k



Prototyping Plan: Radial Spacers / Support

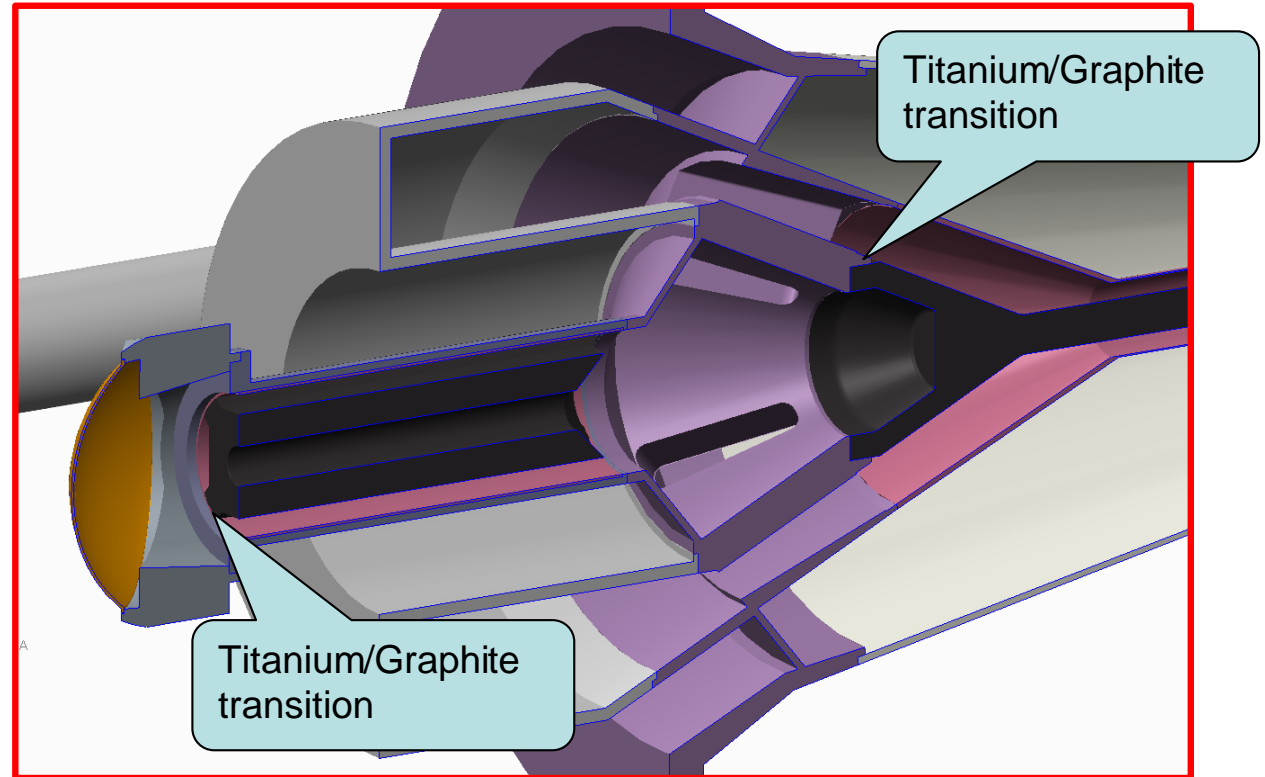
- Graphite target is arranged in segments, which are supported by the outer container using radial spacers
- Different radial support scheme to T2k
 - Titanium outer spacer in particular needs to be prototyped and tested
 - Plan to make a short section demonstrator (e.g. 1 segment long)
 - Identify build sequence

Component parts: £5k

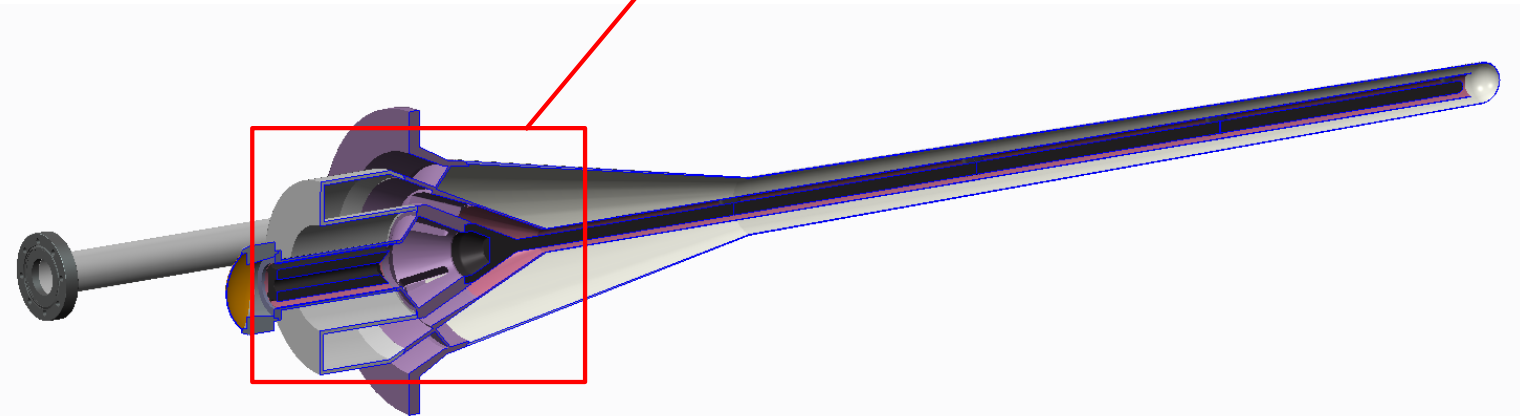


Prototyping Plan: Titanium / Graphite Brazing

- Demonstrate joining technique for titanium/graphite transitions
- Have identified promising vacuum brazing route
 - Trials using in-house facilities (vacuum furnace)
 - This is on a larger scale to anything we have demonstrated previously



Component parts: £5k



CDR Recommendation #1:

Formal Performance & Specification requirement

| Parameter/Specification | Include in Summary | Value for CD4 1.2 MW | Ultimate Value LBNF Final Phase - 2.4 MW | Units |
|--|--------------------|---|---|--------|
| PROTOTYPE TARGET / OPERATIONAL SPARE | | | | |
| Construction: | | | | |
| Core Material | | Graphite | | |
| Core Geometry | | Cylindrical | | |
| Core Length | | 1.5 | | m |
| Core Diameter | | 16 | | mm |
| No. Core Segments | | 2 to 5 | | |
| Vessel Material | | Titanium Alloy | | |
| Support Plate Material | | Aluminium Alloy | | |
| Weight of Target Assembly | | ?? | | kg |
| Beam Operating Limits: | | | | |
| Beam Energy (nominal) | | 120 | | GeV |
| Beam Power (max) | | 1.2 | | MW |
| Protons per Pulse (max) | | 7.5E+13 | | PPP |
| Max. protons on target / year | | ?? | | POT/yr |
| Beam Sigma (nominal) | | 2.667 | | mm |
| Beam Sigma (max) | | ?? | | mm |
| Beam Sigma (min) | | ?? | | mm |
| Beam Offset (max) | | ?? | | mm |
| Thermal Management: | | | | |
| Heat deposited in target assembly | | ?? | | kW |
| Cooling Medium | | Helium gas | | |
| Colant flowrate | | ?? | | g/s |
| Helium Inlet Temperature (nominal) | | 30 | | °C |
| Helium Exhaust Temperature (max) | | 180 | | °C |
| Maximum Graphite Temperature | | 700 | | °C |
| Maximum Titanium Temperature | | 200 | | °C |
| Maximum Aluminium Temperature | | 100 | | °C |
| Pressure drop across target | | ?? | | mbar |
| Electrical Isolation: | | | | |
| Grounding Scheme | | connected to horn conductor via resistor | | |
| Resistor Size | | ?? | | Ohms |
| Min. nominal clearance to Horn-A Inner Conductor | | 5 | | mm |

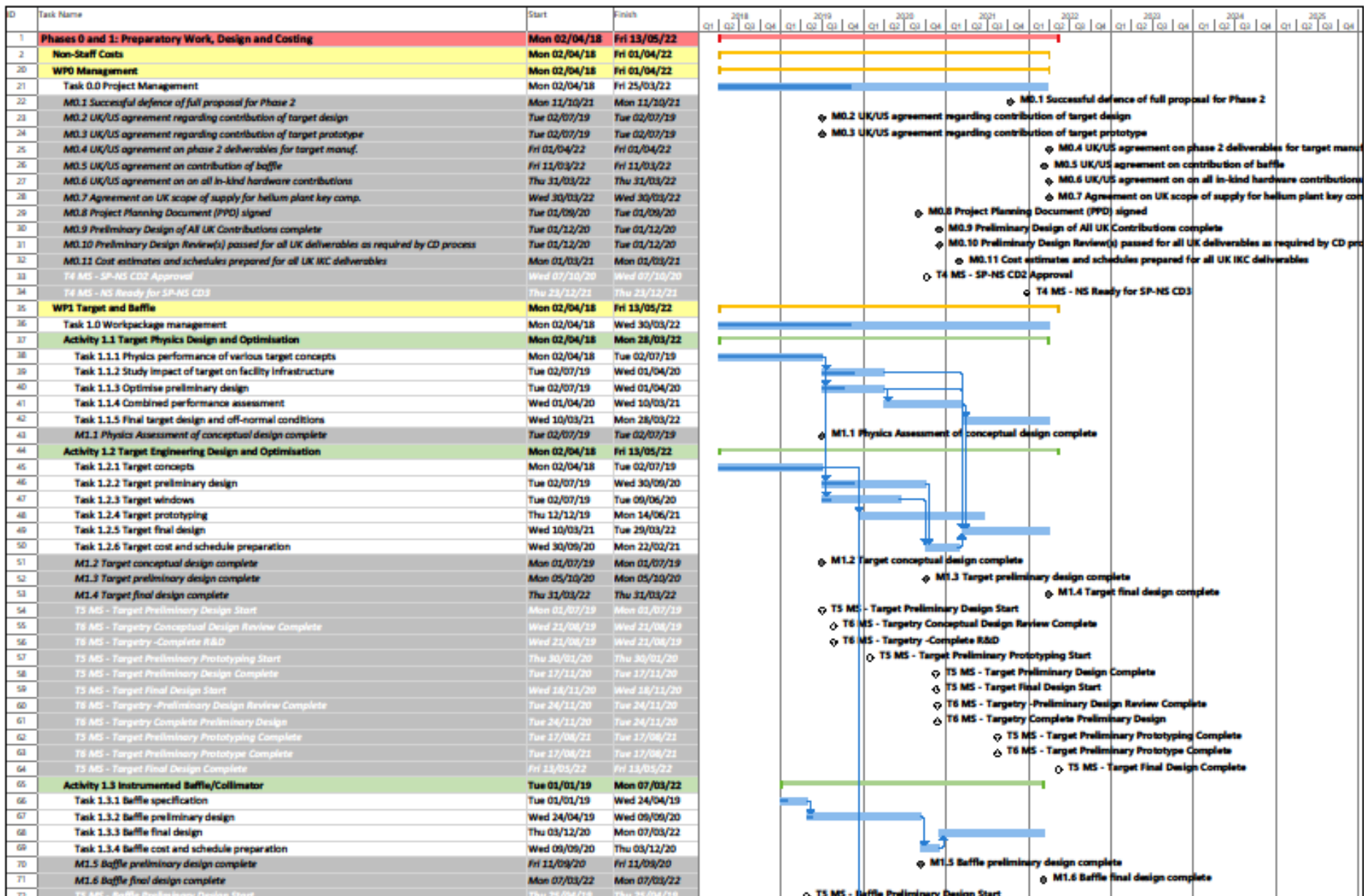
Outline LBNF
beamline design
parameters
spreadsheet

- Work just starting
- Proceeding in parallel to horn parameters spreadsheet

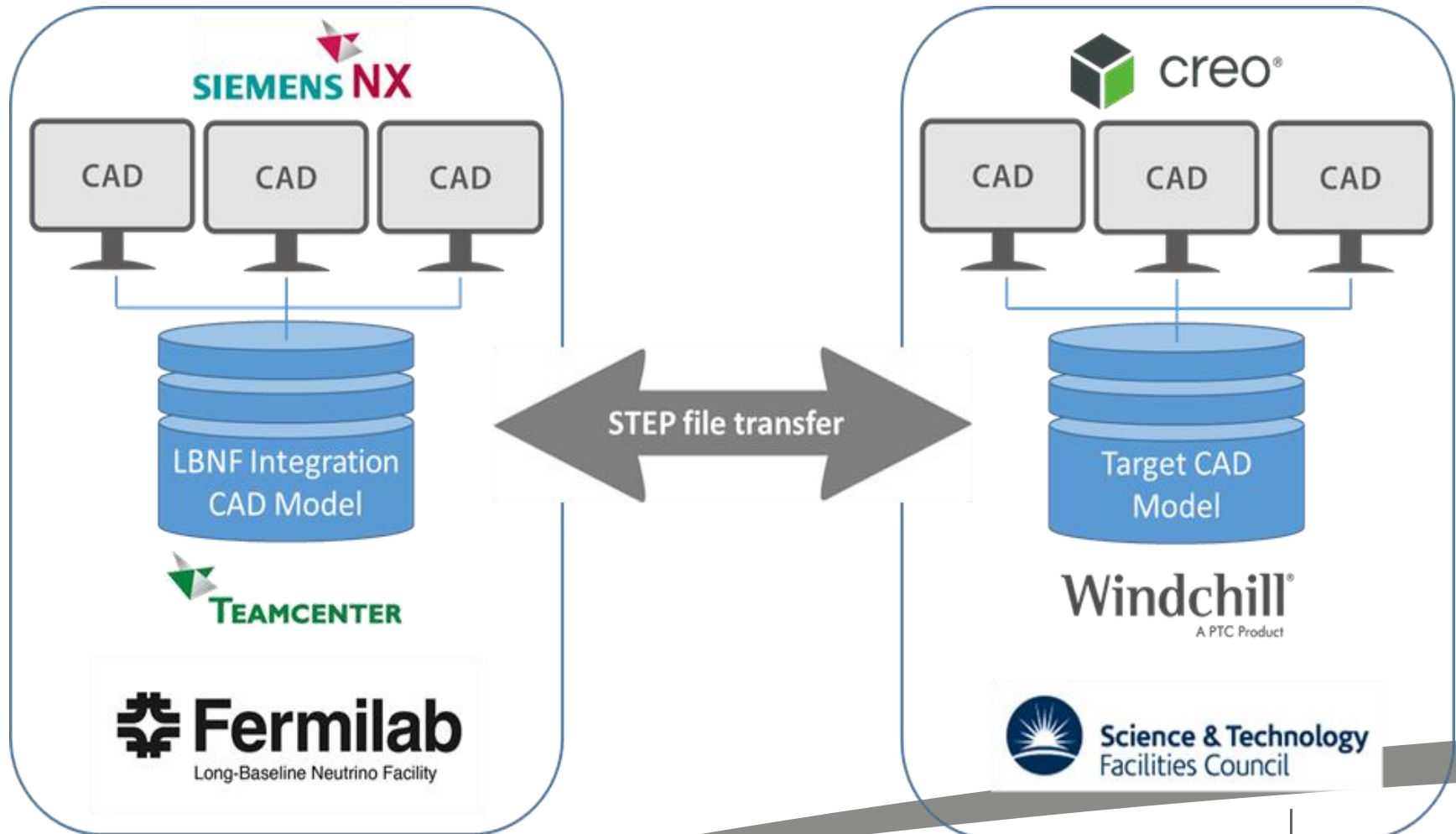
CDR Recommendation #2: Milestones (from draft PPD)

| Completion Milestones | Planned/ Baseline date | Location | Comments |
|---|---------------------------|-----------|--|
| Phase 1: Preliminary Design Phase | | | |
| Preliminary design of target and baffle complete | 17 Nov 2020 | RAL | |
| Preliminary design of target exchange system and remote handling equipment complete | 02 Dec 2020 | RAL | |
| Preliminary design of He gas cooling system complete | 13 Oct 2020 | RAL | Includes shielded He penetrations |
| Preliminary Design Review(s) of all UK contributions complete | 10 Dec 2020 | Fermilab? | May be one or several preliminary design reviews |
| Feature Prototyping Results Report complete | 17 Aug 2021 | RAL | |

Phase 1: Target Schedule


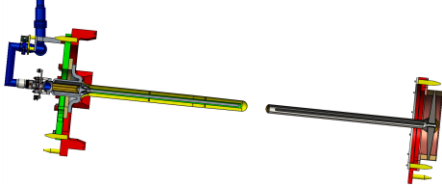
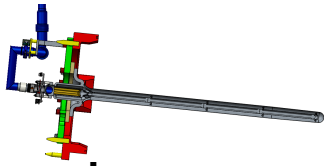


CDR Recommendation #3: CAD Integration & version control


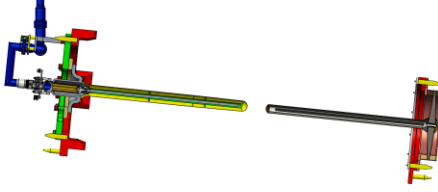
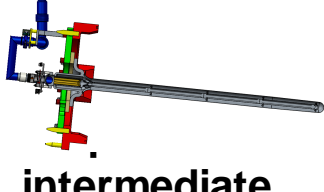


Backup Slides


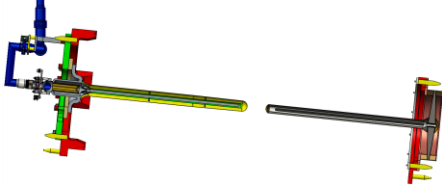
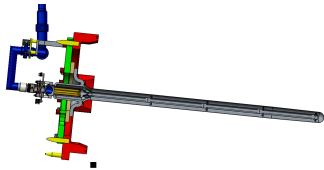
Key Design and Manufacturing Issues

| |  <p>Option 1: 1x2m long</p> |  <p>Option 2: 2x1m long</p> |  <p>intermediate cantilever</p> |
|----------------------------------|---|--|---|
| Complexity of horn Interface | Interfaces at both US and DS of horn, plus self interface! Needs Helium services routing to DS end. | Interfaces at both US and DS of horn. Needs Helium services routing to DS end. | Interface to horn US end only |
| Departure from Proven Technology | Departure from T2K in terms of length / segmentation and Self docking interface. | Closest to two-interaction length T2K target | Departure from T2K in terms of length / segmentation |
| Design Challenges | DS support design for radial stiffness + longitudinal compliance, requires prototyping. | DS support/manifold design w.r.t. pressure stress and thermal distortion. | Pushing for longest feasible length (re: deflection, violin modes) |
| Manufacturing Challenges | DS support manufacture is complex. Manufacture of long thin-walled titanium tube to tight dimensional tolerances. | US target most similar to T2K. DS low-mass manifold manufacture is complex. | Manufacture of long thin-walled titanium tube to tight dimensional tolerances. |
| Cost | Relatively high cost of manufacture and outstanding design tasks | Relatively high cost of manufacture and outstanding design tasks | Relatively low cost of manufacture and outstanding design tasks |

Key Operation Issues

| |  <p>Option 1: 1x2m long</p> |  <p>Option 2: 2x1m long</p> |  <p>intermediate cantilever</p> |
|---------------------------------------|---|--|---|
| Spare Production | Intermediate cost Build two in parallel? | Highest cost Build four (2 US + 2 DS) in parallel? | Lowest cost Build two in parallel? |
| Thermal Management | Highest heat load, single target cooling loop. Also need to cool DS support. | High heat load but divided between two cooling loops | Lowest total heat load |
| Mechanical loads | DS prop required to keep self-weight deflection and natural frequency in check | Most “robust” structure as measured by natural frequency and self-weight deflection | Inherently pushing at the limits on cantilever length |
| Complexity / number of failure points | High complexity due to cooled downstream mount | High complexity due to additional downstream target system | Low Complexity / number of components |
| Alignment Issues | Relies on DS support for target placement precision | Perceived difficulties with beam based alignment | Single object to align but largest self-weight deflection |

Key Remote Maintenance Issues

| |  <p>Option 1: 1x2m long</p> |  <p>Option 2: 2x1m long</p> |  <p>intermediate cantilever</p> |
|---|---|--|---|
| Time estimate for planned target exchange | 3 weeks | 2 weeks | 1 week |
| Risk / complexity | High (number of operations) | High (number of operations) | Medium (number of operations) |
| Work Cell Interfaces | Two sets of exchange tooling with mechanical/services interface | Two sets of exchange tooling with mechanical/services interface | One exchanger tool |
| Manipulator operations | Ergonomics compromised when module rotated. Long-reach manipulators. | Ergonomics compromised when module rotated | Can optimise reach/view for the single required configuration |
| Crane operations | Two module rotations, including re-configuration of supports etc | One module rotation, including re-configuration of supports etc | All work achieved with single module configuration |