## Parallel-bar TEM-type Cavities

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## Parallel Bar Cavity Concept



- Compact design supports low frequencies
- For deflection and crabbing of particle bunches
- Cavity design - Two Fundamental TEM Modes
- 0 mode :- Accelerating mode
- $\pi$ mode :- Deflecting or crabbing mode


## Parallel Bar Cavity Concept



E field on mid plane (Along the beam line)


B field on top plane

Deflection is due to the interaction with the Electric Field

## Parallel Bar Cavity Applications

- Deflecting Cavity - Jefferson Lab 12 GeV Upgrade (499 MHz)
- supported by DOE ARRA to JLab and STTR Phase I to Niowave, (Delayen PI)
- Crab Cavity
- LHC IR Upgrade ( 400 MHz )
- supported by Phase I STTR to Niowave (Delayen PI)
- Jefferson Lab EIC (500 MHz)
- Advantages
- Compact size
- Lower Frequencies
- Fundamental mode with lowest frequency
- Low surface fields
- Higher shunt impedances


## Parallel Bar Cross Sections

Optimizing condition - Obtain a higher deflection with lower surface fields


## Peak Surface Fields

| Design <br> Structure | $\mathbf{E}_{\mathbf{P}} / \mathbf{E}_{\mathbf{T}}{ }^{*}$ | $\mathbf{B}_{\mathbf{P}} / \mathbf{E}_{\mathbf{T}}{ }^{*}$ <br> $(\mathbf{m T} / \mathbf{M V} / \mathbf{m})$ |
| :---: | :---: | :---: |
| (a) | 3.30 | 11.54 |
| (b) | 2.80 | 10.31 |
| (c) | 2.61 | 8.86 |
| (d) | 2.31 | 8.16 |
| At $\mathrm{E}_{\mathrm{T}}{ }^{*}=1 \mathrm{MV} / \mathrm{m}$ |  |  |

- Increasing effective deflecting length along the beam line increases net transverse deflection seen by the particle
- Racetrack shaped structure (d) has better performance with higher deflection for lower surface fields


## Transverse Deflection

$\vec{V}_{T}=\int_{-\infty}^{+\infty}\left[\vec{E}_{x}(z)+\vec{v} \times \vec{B}_{y}(z)\right] e^{j \frac{\omega z}{c}} d z$


Transverse E Field ( $\mathrm{E}_{\mathrm{x}}$ ) (V/m)


Transverse H Field ( $\mathrm{H}_{\mathrm{Y}}$ ) (A/m)


Resultant $\mathrm{V}_{\mathrm{T}}{ }^{*}=0.3 \mathrm{MV}$ At $E_{T}{ }^{*}=1 \mathrm{MV} / \mathrm{m}$

## Transverse Deflection

- Transverse deflecting voltage $\left(\mathrm{V}_{T}\right)$ for a single cell cavity (At $\mathrm{E}_{\mathrm{T}}$ $=1 \mathrm{MV} / \mathrm{m}$ ) is 0.3 MV
- Achievable transverse deflection per cavity at 499 MHz
- For a surface electric field of $\mathrm{E}_{\mathrm{P}}=40 \mathrm{MV} / \mathrm{m}, \mathrm{V}_{\mathrm{T}}=5.84 \mathrm{MV}$
- For a surface magnetic field of $\mathrm{B}_{\mathrm{P}}=100 \mathrm{mT}, \mathrm{V}_{\mathrm{T}}=4.58 \mathrm{MV}$

| Design Parameters | Value <br> (mm) |
| :--- | :---: |
| Cavity reference length | 300.4 |
| Cavity height | 300.4 |
| Cavity width | 400.0 |
| Bar width | 60.0 |
| Bar length | 160.0 |
| Beam aperture | 40.0 |

$\rightarrow$ E Field $\rightarrow$ E and B Field


## Mode Separation by Rounding Edges





Frequency separation due to beam pipe $=1.21 \mathrm{MHz}$


## Design Sensitivities - Rounding Edges

$\rightarrow$ Along $\mathrm{x}-$-Along $\mathrm{y} \rightarrow$ Along z


- Along $x$ - Along y $\Delta$ Along z



Along $\mathbf{x}$


Along y


Along z

## Design Sensitivities - Rounding Edges



- Along $x$ - Alongy $\triangle$ Along z



Along x


Along y

## Optimization of Bar Width - 400 MHz




| Design <br> Parameters | Value <br> (mm) |
| :--- | :---: |
| Cavity reference <br> length | 374.7 |
| Cavity height | 374.7 |
| Cavity width | 400.0 |
| Bar width | 85.0 |
| Bar length | 250.0 |
| Beam aperture | 100.0 |



Bar Width $=50$ mm


Bar Width $=100$

## Optimization of Bar and Cavity Length 400 MHz




# Optimized Cavity Geometry and Field Profiles - 499 MHz 



| Compact Design <br> Dimensions | Value <br> (mm) |
| :--- | :---: |
| Cavity reference length | 388.4 |
| Cavity height | 305.0 |
| Cavity width | 250.0 |
| Bar width | 50.0 |
| Bar length | 278.0 |
| Beam aperture | 40.0 |



E field on mid plane


$B$ field on top plane


B Field

## Optimized Cavity Geometry and Field Profiles - 400 MHz




E field on mid plane


Value (mm)

| Compact Design <br> Dimensions | Value <br> $(\mathbf{m m})$ |
| :--- | :---: |
| Cavity reference length | 456.7 |
| Cavity height | 384.4 |
| Cavity width | 400.0 |
| Bar width | 85.0 |
| Bar length | 332.0 |
| Beam aperture | 100.0 |

U/m .68e6 5.32 e 6 4.61 e6
3.9 Эe6
3.19e6
2.48 e 6
1.77 e 6

55
-

(2)

## Surface Fields

499 MHz

Surface B Field



$$
\begin{aligned}
& \frac{E_{P}}{E_{T}}=2.06 \\
& \frac{B_{P}}{E_{T}}=6.54 \mathrm{mT} /(\mathrm{MV} / \mathrm{m})
\end{aligned}
$$

400 MHz


## Transverse Deflecting Voltage along Beam Line Cross Section - 400 MHz



$$
\frac{V_{T}}{V_{T}(r=0)}=3.0^{\times} 10^{-5} \Delta x^{2}+1.0
$$


$\frac{V_{T}}{V_{T}(r=0)}=-3.0 \times 10^{-5} \Delta y^{2}+1.0$

| Direction | $\Delta \mathrm{V}_{\mathrm{T}} / \mathrm{V}_{\mathrm{T}}$ <br> $(A t \mathrm{R}=50 \mathrm{~mm})$ |
| :---: | :---: |
| x | $1.33 \%$ |
| y | $1.46 \%$ |

## Cavity Properties

| Parameter | $\begin{gathered} 499 \\ \mathrm{MHz}{ }^{(1)} \end{gathered}$ | $\begin{gathered} 499 \\ \mathrm{MHz} \end{gathered}$ | $\begin{aligned} & 400 \\ & \mathrm{MHz} \end{aligned}$ | KEK <br> Cavity | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Frequency of $\pi$ mode | 499.4 | 499.2 | 400.7 | 501.7 | MHz |
| $\lambda / 2$ of $\pi$ mode | 300.4 | 300.4 | 374.7 | 299.8 | mm |
| Frequency of 0 mode | 519.9 | 517.8 | 413.05 | $\sim 700 \mathrm{MHz}$ | MHz |
| Cavity reference length | 388.4 | 394.4 | 456.7 | 299.8 | mm |
| Cavity width | 250.0 | 290.0 | 400.0 | 866.0 | mm |
| Cavity height | 305.0 | 304.8 | 384.4 | 483.0 | mm |
| Bars length | 278.0 | 284 | 332.0 | - | mm |
| Bars width | 50.0 | 67.0 | 85.0 | - | mm |
| Aperture diameter | 40.0 | 40.0 | 100.0 | 130.0 | mm |
| Deflecting voltage ( $V_{T}^{*}$ ) | 0.3 | 0.3 | 0.375 | 0.3 | MV |
| Peak electric field $\left(E_{T}{ }^{*}\right)$ | 2.06 | 1.85 | 2.18 | 4.32 | MV/m |
| Peak magnetic field ( $B_{T}{ }^{*}$ ) | 6.54 | 6.69 | 7.5 | 12.45 | mT |
| Geometrical factor ( $G=Q R_{S}$ ) | 64.7 | 67.96 | 83.9 | 220 | $\Omega$ |
| $[R / Q]_{T}$ | 942.75 | 933.98 | 317.92 | 46.7 | $\Omega$ |
| $R_{T} R_{S}$ | $6.110^{4}$ | $6.310^{4}$ | $2.6710^{4}$ | $1.0310^{4}$ | $\Omega^{2}$ |
| $\text { At } E_{T}^{*}=1 \mathrm{MV} / \mathrm{m}$ |  |  |  |  |  |

* K. Hosoyama et al, "Crab cavity for KEKB", Proc. of the 7th Workshop on RF Superconductivity, p. 547 (1998)


## Higher Order Modes - 400 MHz

| Mode | Frequency (MHz) | Mode of Operation | Field direction on beam axis |  | [R/Q] ( $\Omega$ ) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | E | B | Direct Integral Method | Using Panofsky Wenzel Theorem |
|  |  |  |  |  |  | ( $\mathrm{r}_{0}=5 \mathrm{~mm}$ ) |
| 1 | 400.60 | Deflecting | x | y | 317.98 | 317.16 |
| 2 | 412.94 | Acclerating | z |  | 81.12 | - |
| 3 | 477.76 | Acclerating | z |  | 10.64 | - |
| 4 | 489.70 | Deflecting | x | y | 2.124 | 2.13 |
| 5 | 524.13 | Deflecting | x | y | 48.24 | 48.42 |
| 6 | 612.03 | Accelerating | z |  | 47.89 | - |
| 7 | 713.89 | Deflecting | x | $y$ | 2.85 | 2.6 |
| 8 | 737.67 | Deflecting | x | y | 4.2 | 3.5 |
| 9 | 793.85 |  |  | z | 0.0 | 0.0 |
| 10 | 796.26 | Acclerating | z |  | 49.3 | - |
| 11 | 810.72 | Deflecting | y | x | 0.0199 | 0.0043 |
| 12 | 836.70 | Deflecting | y | x | 65.04 | 62.51 |
| 13 | 855.67 |  |  | z | 0.0 | 0.0 |
| 14 | 868.28 |  |  | z | 0.0 | 0.0 |
| 15 | 924.27 | Deflecting | y | x | 6.29 | 6.87 |
| 16 | 941.54 | Deflecting | x | y | 19.53 | 16.87 |
| 17 | 999.08 |  |  | z | 0.0 | 0.0 |
| 18 | 1013.13 | Deflecting | x | y | 0.0144 | 0.00761 |
| 19 | 1018.24 |  |  | z | 0.0 | 0.0 |
| - 20 | 1032.98 | Accelerating | z |  | 15.0 | - |



Fundamental Mode Separation $=12.3 \mathrm{MHz}$


FISA

## Modes of Interest - 400 MHz



## Asymmetry Study - 499 MHz

- Study of mixing in transverse and longitudinal voltage along the beam line at the fundamental mode, due to asymmetry in
- Cavity Width
- Cavity Edge Radius
- Bar Width
- Bar Length
- Bar Separation


## Asymmetry in Cavity Width





## Asymmetry in Cavity Edge Radius



## Asymmetry in Bar Width





## Jefferson Lab

## Asymmetry in Bar Length




Asymmetry in Bar Length (mm)

$\frac{\text { sivp }}{\mathrm{O}_{\mathrm{LD}}}$
DOMINION UNIVERSITY

## Asymmetry in Bar Separation



## Emittance Growth



## Preliminary Stress Analysis

## Material Properties of $\mathrm{Nb}^{*}$

| Property | SI Units | English Units |
| :--- | :---: | :---: |
| Modulus - <br> Room Temp | $1.03 \mathrm{E}+11 \mathrm{~Pa}$ | $1.49 \mathrm{E}+07 \mathrm{psi}$ |
| Modulus - <br> Cryo Temp | $1.23 \mathrm{E}+11 \mathrm{~Pa}$ | $1.79 \mathrm{E}+07 \mathrm{psi}$ |
| Poisson's <br> Ratio | 0.38 |  |
| Density | $8.58 \mathrm{E}-03$ <br> $\mathrm{~g} / \mathrm{mm}^{3}$ | 0.31 <br> $1 \mathrm{lb} / \mathrm{in}^{3}$ |
| Yield - RT | $4.83 \mathrm{E}+07 \mathrm{~Pa}$ | 7.0 ksi |
| Yield - Cryo | $5.77 \mathrm{E}+08 \mathrm{~Pa}$ | 83.7 ksi |

- Analysis using properties at room temperature
- Cavity wall thickness $=3 \mathrm{~mm}$
- Mechanical model
- Standard gravity $=9.806 \mathrm{~ms}^{-2}$
- Pressure normal to the cavity outer surface $=0.20265 \mathrm{Mpa}(29.392 \mathrm{psi})$
Stress $=432 \mathrm{MPa}>$ Yield Strength $=48 \mathrm{MPa}$



## Cavity Deformations



Directional Deformations

- x axis $\rightarrow 9 \mathrm{~mm}$
- y axis $\rightarrow 0.8 \mathrm{~mm}$
- z axis $\rightarrow 0.3 \mathrm{~mm}$


## Test Cryostat Concept



## Test Cryostat Concept



