# EM Design Optimization Of The 162.5 MHz - $\beta$ ~ 0.11 - HWR 

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## EM Design Goal

### 1.8 MV at $40 \mathrm{MV} / \mathrm{m}$ and 70 mT

## Choice / Optimization of the cavity $\beta$

- $\beta$ optimization is based on the beta range, design voltage, other cavities ...
- The energy range is $2.1 \mathrm{MeV} / \mathrm{u}$ to $10 \mathrm{MeV} / \mathrm{u} \rightarrow \beta$ : from 0.067 to 0.145
- Using the design voltage of 1.8 MV , we found $\beta$ _opt $\sim 0.11$.

- At this voltage, 5 cavities should be enough to cover the energy range, BUT ...


## EM Design Optimization: Fully Parameterized Geometry



| $\times$ <br>  | Name | Value | Description |
| :---: | :---: | :---: | :---: |
|  | CVAPR | 1.5 | Cavity Aperture Radius |
|  | CVFL | 2.0 | Cavity Flat Length |
|  | $\mathrm{CV} / \mathrm{MH}$ | 7.0 | Cavity Middle Height |
|  | CVMR | 12.0 | Cavity Middle Radius |
|  | CVTBR | [CVTR-ICTR ]/2.0 | Cavity Top Blending Radius |
|  | CVTH | 50.46 | Cavity Top Height |
|  | CVTR | 17.0 | Cavity Top Radius |
|  | DTEBR | 1.5 | Drift Tube Edge Blending Radius |
|  | DTIBR | 0.5 | Drift Tube Inner Blending Radius |
|  | DTIR | 5.0 | Drift Tube Inner Radius |
|  | DTOBR | 3.6 | Drift Tube Blending Radius |
|  | DTOR | 5.0 | Drift Tube Outer Radius |
|  | DTPN | CVMR-(MGD+Gap | Drift Tube Penetration |
|  | Gapw | 4.8 | Gap Width |
|  | ICFL | 2.0 | Inner Conductor Flat Length |
|  | ICRTX | 3.8 | Inner Conductor Rice Track Depth (X) |
|  | ICRTY | 2.0 | Inner Conductor Race Track Height (Y) |
|  | ICRTZ | (MGD-GapW)/2. | Inner Conductor Race Track Width (Z) |
|  | ICTH | CVTH | Inner Conductor Top height |
|  | ICTR | 7.0 | Inner Conductor Top Radius |
|  | MGD | 8.4 | Mid-Gap Distance |
|  | Global |  |  |

- The table shows the list of geometry parameters as seen in MW-Studio
- The geometry parameters are NOT independent


## RF Parameters to Optimize for

- E-peak: Minimize peak surface electric field to limit field emission
- B-peak: Minimize peak magnetic field to maintain superconductivity
- $\mathrm{R} / \mathrm{Q}=\mathrm{V} 2 / \omega \mathrm{U}$ : Maximize $\mathrm{R} / \mathrm{Q}$ to produce more accelerating voltage (V) with less stored energy in the cavity (U)
- G = Rs*Q: Maximize the geometry factor to increase the cavity effectiveness of providing accelerating voltage due to its shape alone


## Geometry Parameters to Choose/Optimize/Fix First

- Choice of Cavity Shape: Cylindrical or Conical based on overall dimensions and RF parameters
- Cavity Outer Dimensions: How big could it be ? Considering
- Overall cavity and cryomodule dimensions
- Mechanical and manufacturing limitations
- Processing and handling limitations
- RF parameters: Bigger is usually better
- ...
- Mid-Gap Distance: Adjusted to get $\beta$ _opt = $\beta$ _design
- $\beta$ _opt may drift during the rest of the optimization but could be adjusted


## EM Design Optimization: Improved Procedure

- The original procedure was manual with ~ 200 k hexagonal meshcells for fast turn-around.
- The new one is semi-automatic where MWS does most of the work: MWS parameter sweeps are used instead of the manual sweeps.
- Smaller geometry parameter variation steps: 1-2 mm instead of 0.5-1 cm
- Higher mesh is used for better accuracy: 1M instead of 200k
- The order of parameter sweeps is important: MGD $\rightarrow$ GapW $\rightarrow$...
- If there are several potential optimum branches, they will be investigated


## 200k versus 1M Results (GapW: Gap Width)

200 k Sweep
1 M Sweep









| Mesh <br> Cells | Freq <br> MHz | $\beta_{\text {_opt }}$ | Leff <br> $(\mathrm{cm})$ | Ep/Ea <br> - | Bp/Ea <br> $\mathrm{Gs} /$. | $\mathrm{R} / \mathrm{Q}$ <br> $\Omega$ | G <br> $\Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 233 k | 162.49 | 0.111 | 20.3 | 4.474 | 64.399 | 224.66 | 46.78 |
| 1.04 M | 162.49 | 0.110 | 20.3 | 4.643 | 63.760 | 225.14 | 47.17 |

$\rightarrow 200 \mathrm{k}$ sweeps show similar parameter dependence as the 1M sweeps BUT have more fluctuations and different absolute values for RF parameters especially E-peak.

## Starting Geometry: Scaled from an optimized design




## Sweep GapW (Gap Width)



E-peak U, B-peak $\uparrow, R / Q \downarrow$ and $G \uparrow \rightarrow$ GapW $=5.2 \mathrm{~cm}$ E-peak minimum is around 5.2 cm , but B-peak is minimum around 4 cm

## Sweep ICRTX (Inner Conductor Race Track Width)



E-peak $\uparrow, B-$ peak $\uparrow, R / Q \downarrow$ and $G \downarrow \rightarrow$ ICRTX $=3.6 \mathrm{~cm}$

## Sweep ICRTY (Inner Conductor Race Track Height)



E-peak $\rightarrow$, B-peak ~, R/Q and G $\uparrow \rightarrow$ ICRTY $=5.0 \mathrm{~cm}$

## Sweep DTOR (Drift Tube Outer Radius)



E-peak U, B-peak $\uparrow, R / Q \cap$ and $G \downarrow \rightarrow$ DTOR $=5.0 \mathrm{~cm}$

## Sweep DTOBR (Drift Tube Outer Blending Radius)






$$
\text { E-peak U, B-peak } \rightarrow, \text { R/Q and } G \rightarrow \rightarrow \text { DTOBR }=4.0 \mathrm{~cm}
$$

## Sweep DTIBR (Drift Tube Inner Blending Radius)



## Optimum Geometry



## Optimization Results

| Geometry | Mesh <br> Cells | Freq <br> MHz | $\beta$ _opt | Leff <br> $(\mathrm{cm})$ | Ep/Ea <br> - | $\mathrm{Bp} / \mathrm{Ea}$ <br> $\mathrm{Gs} /$. | $\mathrm{R} / \mathrm{Q}$ <br> $\Omega$ | G <br> $\Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 1.04 M | 162.50 | 0.110 | 20.3 | 4.642 | 63.76 | 225.14 | 47.17 |
| End | 1.04 M | 162.50 | 0.113 | 20.85 | 4.351 | 67.69 | 228.75 | 47.69 |

- The end cavity has better E-peak and R/Q but worse B-peak
- The start cavity is capable of delivering 1.75 MV at $40.0 \mathrm{MV} / \mathrm{m}$ and 54.9 mT and 2.23 MV at 51.0 MV/m and 70.0 mT
- The end cavity is capable of delivering 1.92 MV at $40.0 \mathrm{MV} / \mathrm{m}$ and 62.2 mT and 2.16 MV at $45.0 \mathrm{MV} / \mathrm{m}$ and 70.0 mT
- The end cavity meets the 1.8 MV design goal at $40 \mathrm{MV} / \mathrm{m}$ and 70 mT


### 162.5 MHz - $\beta$ ~ 0.11 - HWR: Field Distributions (X cut)

Type
Monitor
Component
Maximum-3D
Frequency
Phase

Type
Monitor
Component
Maximum-3D
Frequency
Phase

## H-Field (peak)

Mode 1
Abs
$12483.4 \mathrm{~A} / \mathrm{m}$ at $5.34202 / 27.7441 /-2.6819 \mathrm{e}-815$
162.502

95 degrees
B. Mustapha

### 162.5 MHz - $\beta$ ~ 0.11 - HWR: Field Distributions (Z cut)



## Larger Aperture Effect on the RF Parameters

| Aperture | Mesh <br> Cells | Freq <br> MHz | $\beta_{\text {_opt }}$ | Leff <br> $(\mathrm{cm})$ | Ep/Ea <br> - | Bp/Ea <br> $\mathrm{Gs} /$. | R/Q <br> $\Omega$ | G <br> $\Omega$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 30 mm | 1.04 M | 162.50 | 0.113 | 20.85 | 4.351 | 67.69 | 228.75 | 47.69 |
| 40 mm | 1.07 M | 162.51 | 0.108 | 19.93 | 5.110 | 76.17 | 200.24 | 47.36 |

- The cavity was re-optimized with a 40 mm aperture instead of 30 mm .
- The outer cavity dimensions are kept unchanged $\rightarrow$ same G factor.
- We notice a significant effect on E-peak, B-peak and R/Q but it should be less significant for the final aperture choice of 33 mm .
- The 40 mm cavity is capable of delivering 1.56 MV at $40.0 \mathrm{MV} / \mathrm{m}$ and 59.6 mT and 1.83 MV at 47.0 MV/m and 70.0 mT
- The 40 mm cavity meets the 1.8 MV design goal at $47 \mathrm{MV} / \mathrm{m}$ and 70 mT


## Summary

- We have established a finer EM design optimization procedure.
- We have developed an optimized EM design for the 162.5 MHz $-\beta \sim 0.11$ - HWR exceeding the design goal of 1.8 MV with a 30 mm aperture.
- The design was re-optimized with a 40 mm aperture where significant effect on the RF parameters was observed.
- The aperture effect should be less important for the final aperture choice of 33 mm

