

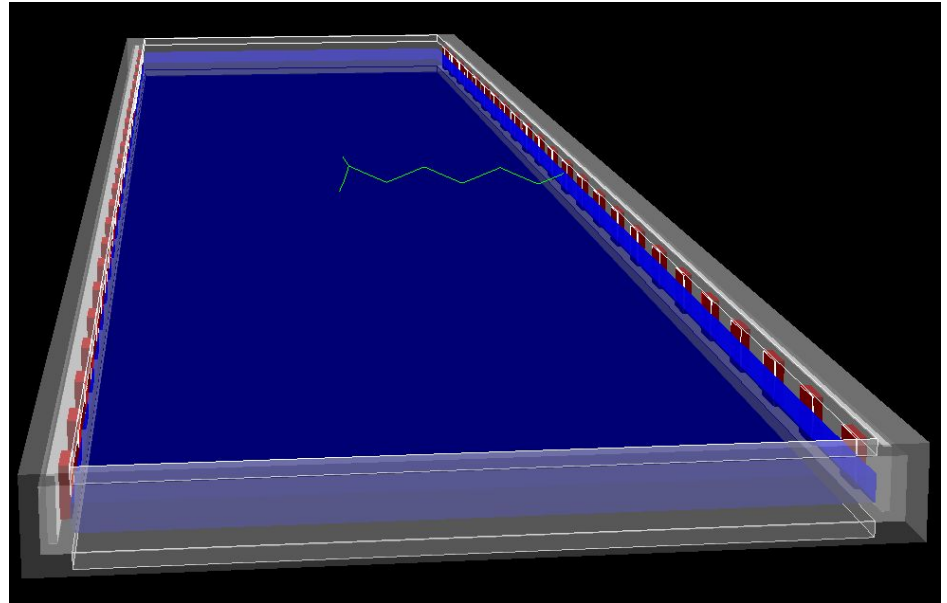
# A Geant4-based simulation of the X-ARAPUCA for the optimization of dichroic filters

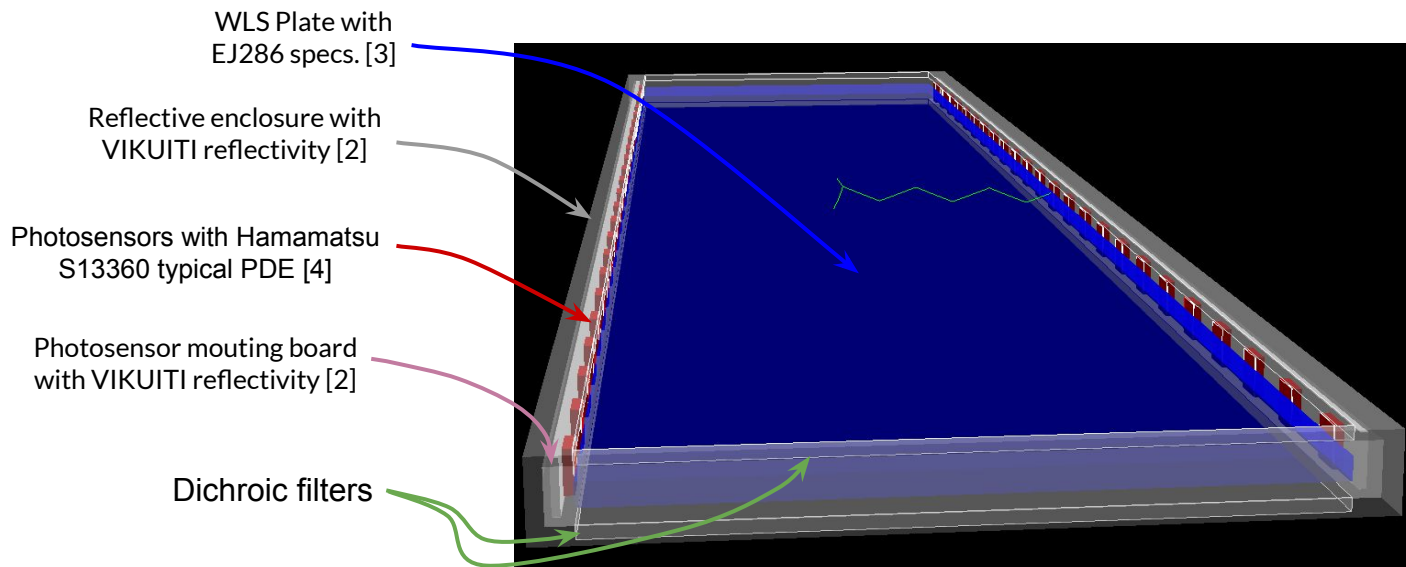
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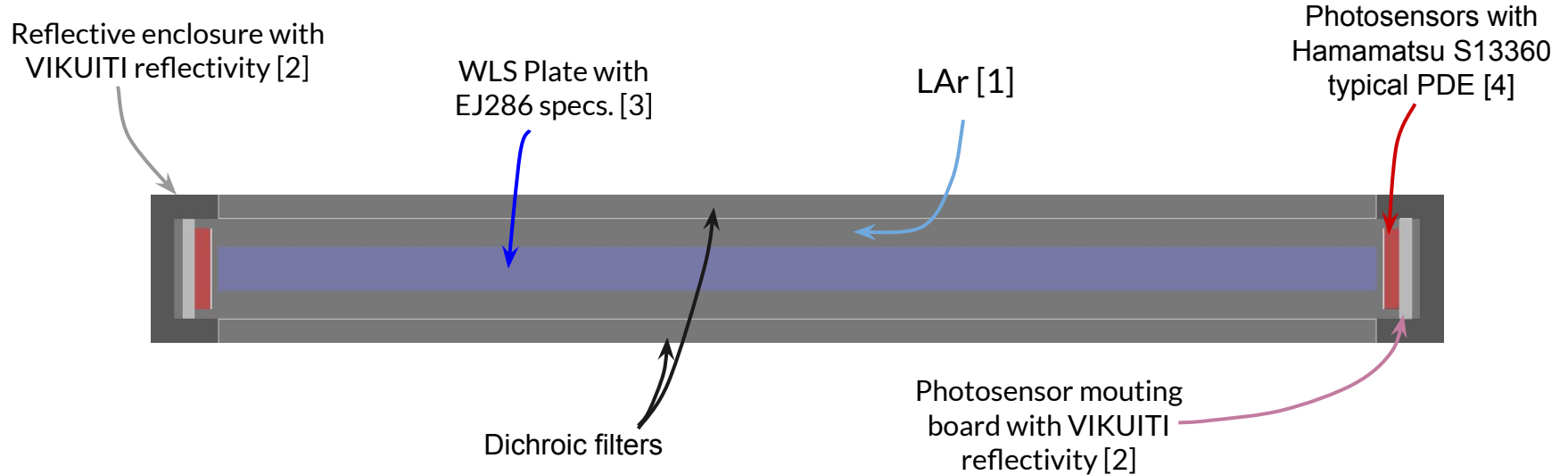
7 July 2022





The used X-ARAPUCA geometry was introduced in previous talks. See:

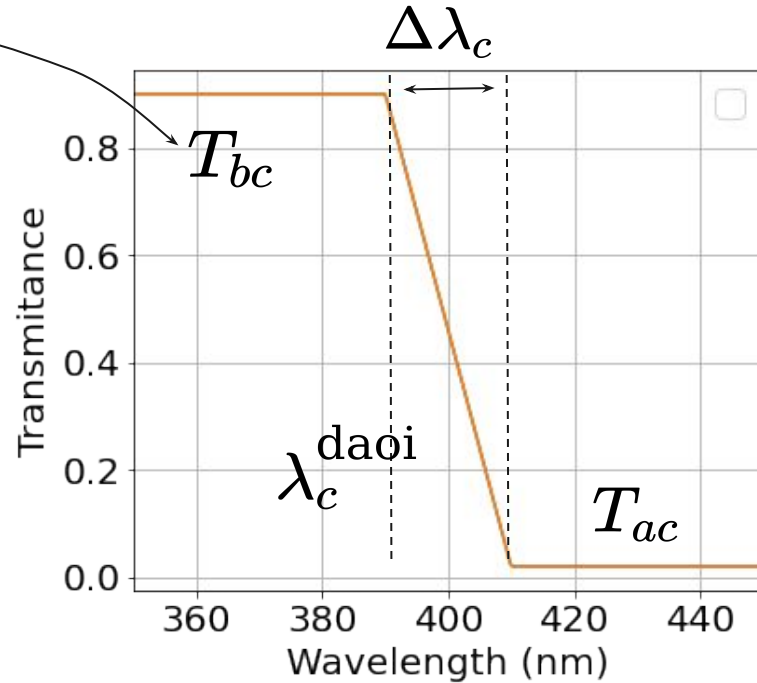
- [indico.fnal.gov/event/50217/contributions/241738/attachments/155327/202219/IFIC\\_x-arapuca\\_sim\\_17042022.pdf](https://indico.fnal.gov/event/50217/contributions/241738/attachments/155327/202219/IFIC_x-arapuca_sim_17042022.pdf)
- [indico.fnal.gov/event/54798/contributions/242876/attachments/155944/203305/df\\_simulation\\_07\\_06\\_2022.pdf](https://indico.fnal.gov/event/54798/contributions/242876/attachments/155944/203305/df_simulation_07_06_2022.pdf)



Dimensions were taken from [5] (TDR vol. IX)



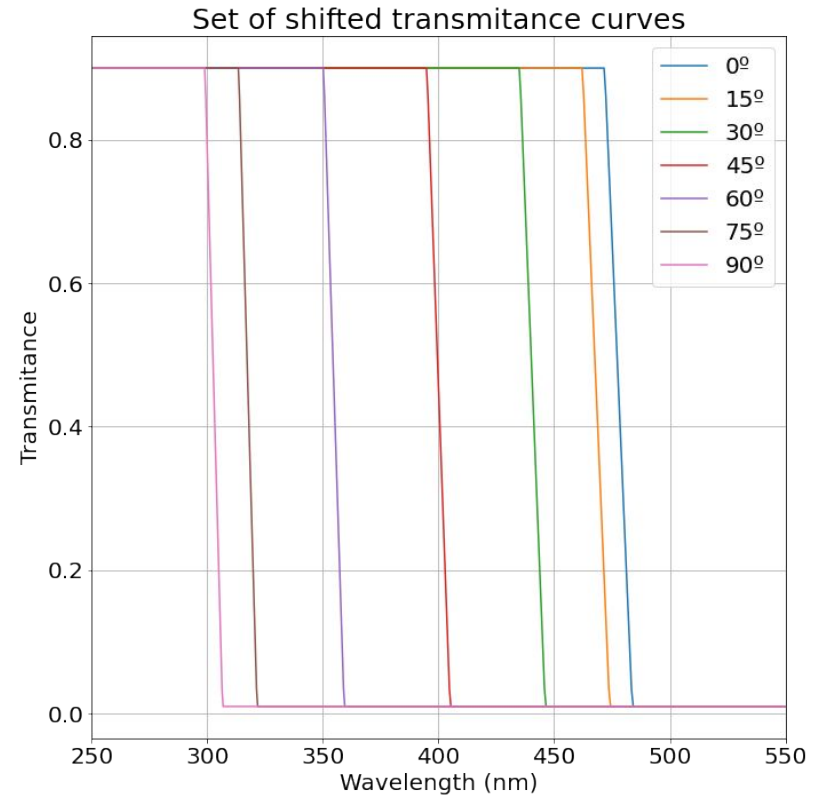
Our first study fixes  $T_{bc}$ , since it should just scale the amount of light that enters the X-ARAPUCA. This would leave three parameters to iterate over.





The curve that is generated for the design AOI (DAOI), is transformed for every AOI using

$$\lambda_{\theta} = \lambda_0 \sqrt{1 - \left( \frac{n_0 \sin(\theta)}{n_{\text{eff}}} \right)^2} \quad [7]$$



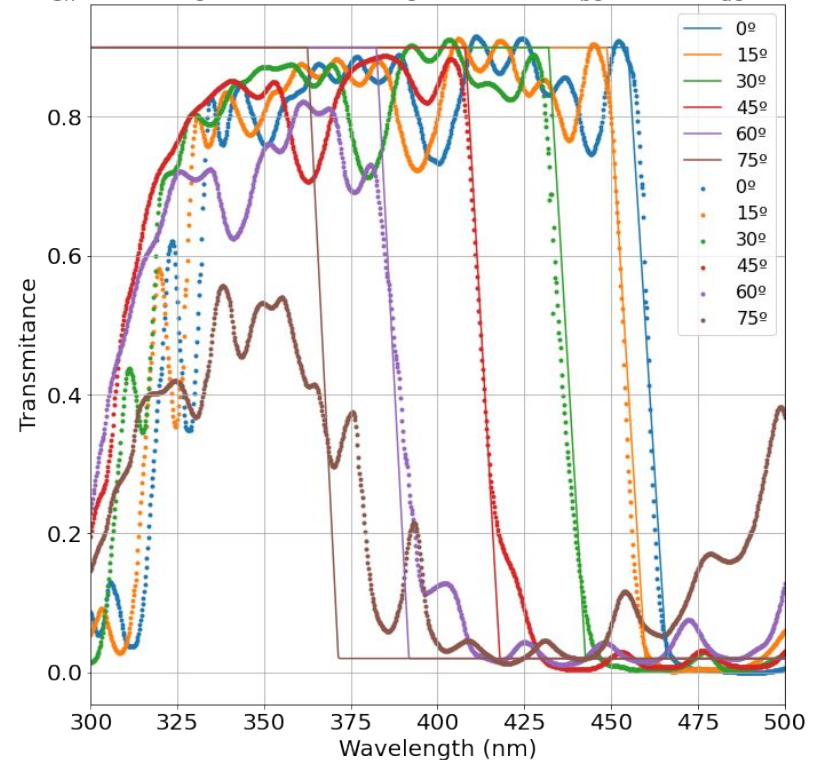


$$\lambda_{\theta} = \lambda_0 \sqrt{1 - \left( \frac{n_0 \sin(\theta)}{n_{\text{eff}}} \right)^2} \quad [7]$$

In order to make a reasonable estimate of the effective refractive index, we fitted a particular case of our model to the **OPTO** data measured at UNICAMP [8]

This fit gave  $n_{\text{eff}}=1.6$ , which is a plausible value given the refractive index (1.52) of the OPTO filters substrate (SCHOTT B270).

$n_{\text{eff}} = 1.6$ ,  $\lambda_c = 413 \text{ nm}$ ,  $\Delta\lambda_c = 15 \text{ nm}$ ,  $T_{bc} = 0.9$ ,  $T_{ac} = 0.0$



# Transmission curve model

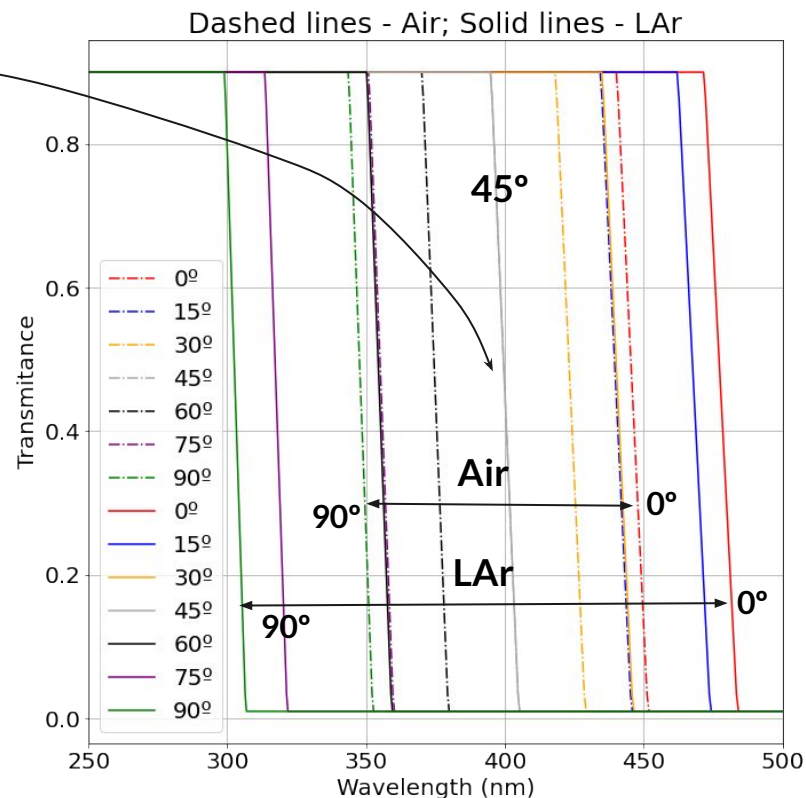


Given certain parameters, a curve is generated for DAOI=45°. The shift is applied afterwards.

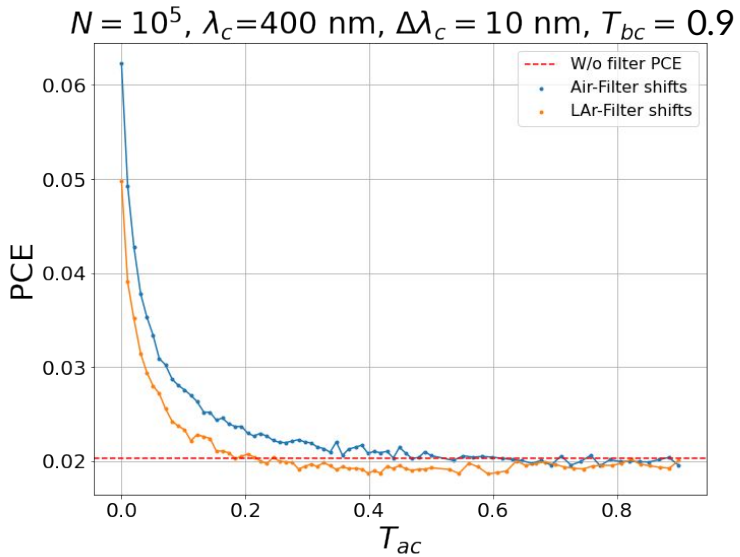
$$\lambda_{\theta} = \lambda_0 \sqrt{1 - \left( \frac{n_0}{n_{\text{eff}}} \sin(\theta) \right)^2} \quad [7]$$

The bigger  $n_0$ , the greater the shift. For this range of wavelengths, we considered constant refractive indices of  $n_{\text{air}}=1.0003$  and  $n_{\text{LAR}}=1.2375$ .

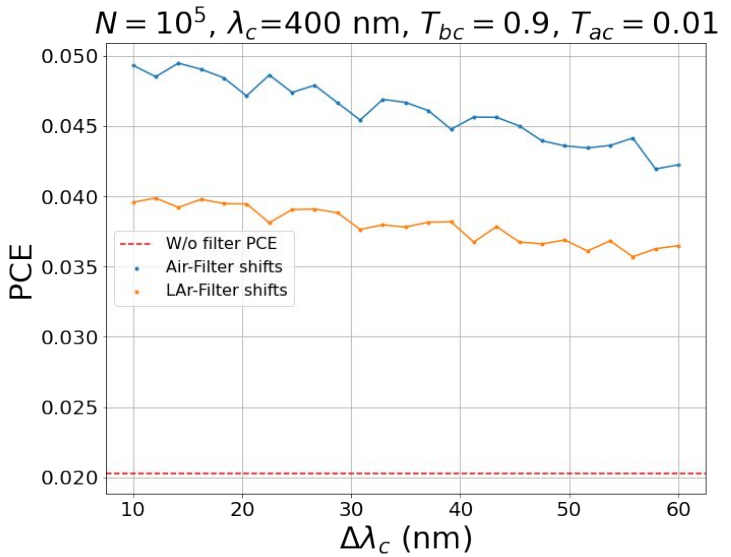
$n_0$  is fixed by LAR, but  $n_{\text{eff}}$  depends on the filter



# 1D scans



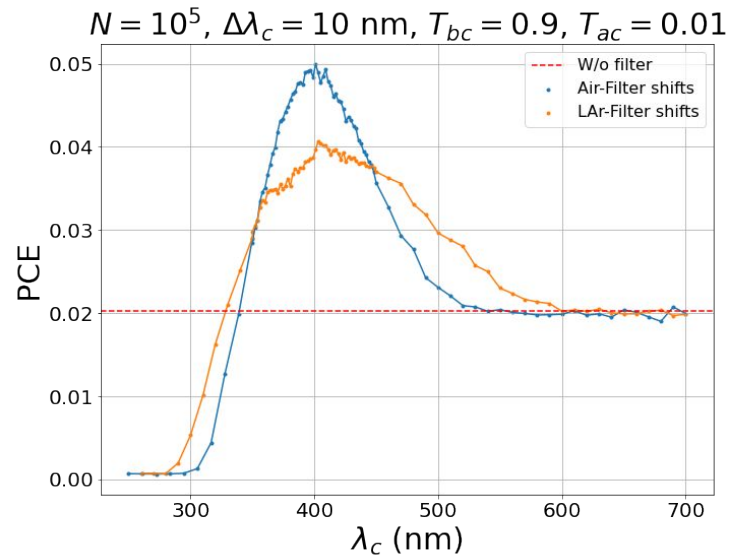
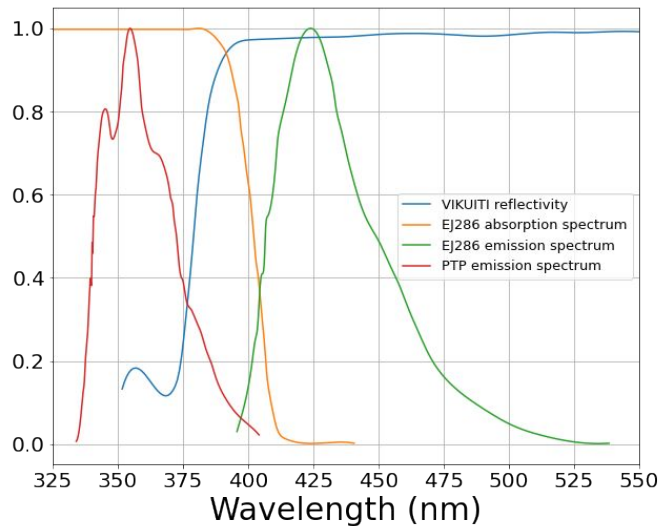
Transmission above cut-off



Cut-off width

The reflectance above the cut-off has a greater impact on photon collection than other parameters such as the cut-off width.



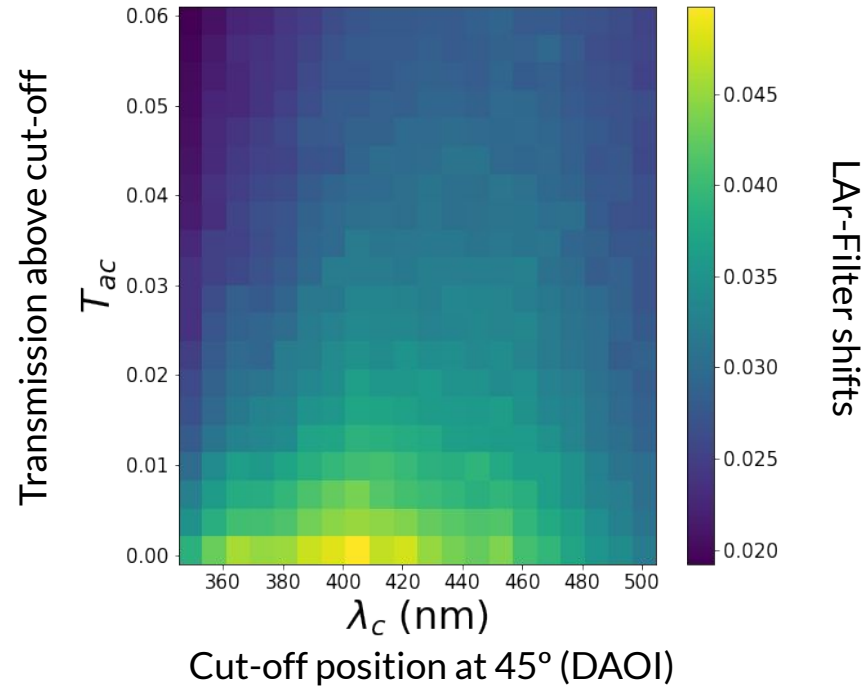


Cut-off position at  $45^\circ$  (DAOI)

As expected, the optimal position for the cut-off at  $\text{DAOI}=45^\circ$  seems to be 400 nm. For peak efficiency, switching from Air shifts to LAr shifts entails a 20% decrease in PCE. This is only due to larger shifts as a function of the angle.



PCE ( $N = 10^5$ ,  $\Delta\lambda_c = 10$  nm,  $T_{bc} = 0.9$ )

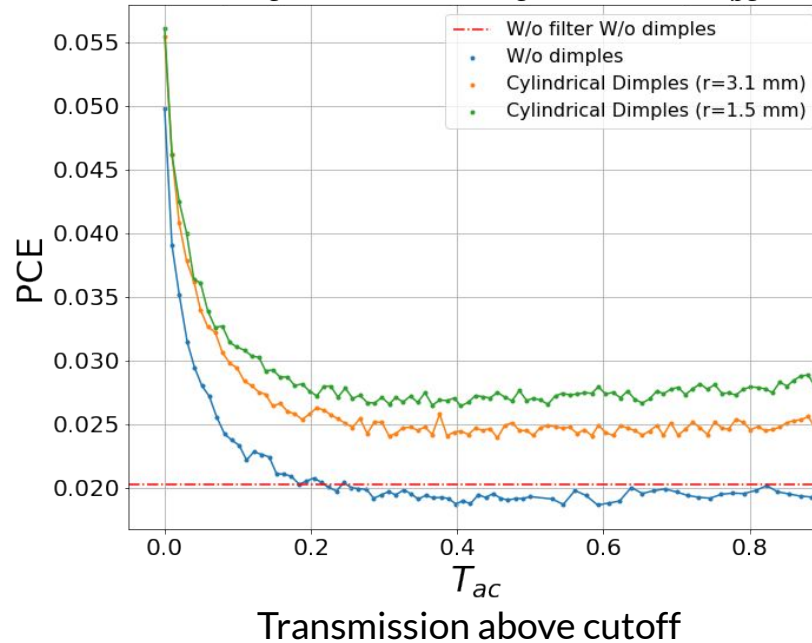


Optimal cut-off position seems to get slightly bigger as  $T_{ac}$  increases.



## LAr-Filter shifts

$N = 10^4$ ,  $\lambda_c = 400$  nm,  $\Delta\lambda_c = 10$  nm,  $T_{bc} = 0.9$



We have also investigated the PCE vs.  $T_{ac}$  dependence for some dimple geometries. [9]



- A simulation study iterating over the model-curve parameters has been performed.
- Both in air and LAr, the filter is optimal when its cut-off is positioned at 400 nm (at DAOI=45°).  
**The peak efficiency loss when switching from air-shifts to LAr-shifts is roughly 20%.**  
A way to recover this 20% would involve increasing the effective refractive index of the filter, most likely using a different substrate. This is currently under investigation with PhotonExport.
- The most critical parameter is the transmission above cut-off. **Rising it from 1% to 5% entails a 50% loss in PCE.**
- The parameter with the lowest impact on PCE is the cut-off width. Increasing it from 10 nm to 50 nm entails a 9% loss in PCE. As a matter of fact, **narrower cut-offs can be sacrificed in favour of a larger reflectance above cutoff.**

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