

Recent Progress of Nb₃Sn Thin Film SRF Cavity Coated by Vapor Diffusion Method at IMP

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Background



3 Conclusion

Background

- Amongst the research activities conducted since the 1970s, only Cornell University, JLab, and FNAL have managed to successfully coat highperformance Nb₃Sn SRF cavities by the vapor diffusion method
- Further investigations and optimizing the coating process of highperformance Nb₃Sn SRF cavities using the vapor diffusion method remains an essential research problem for further studies







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Research approach



Differences and optimizations of the subsequent 7 coating processes

Coating process	Sn source Temperature/°C	Growth stage time / Minute	Exploration of methods for adsorbing residual Sn va				
		Sn power ¹	Valves ²	Mo belt ³	Ceramics ⁴		
1	1310	180	On	Closed	On	Without	
2	1200	180	On	Closed	On	Without	
3	1200	180	Off	Closed	On	Without	
4	1200	180	On	Opened	On	Without	
5	1200	180	On	Closed	Bottom On	Without	
6	1200	180	On	Closed	On	With	
7	1233	120	Off	Closed	Bottom On	With	

¹The condition of the Sn source power supply immediately after the film growth stage.

²The condition of the valves between the Nb coating chamber and the vacuum pump.

³The condition of the Mo heating belts surrounding the Nb coating chamber throughout the coating process.

⁴Whether or not to hang high-purity absorbent ceramic bricks above the cavity.

The deposition system



Initial design: C contamination from absence of Nb chamber, non-uniform growth of Nb₃Sn films from the distance of Sn and cavity Upgradation: Nb chamber to prevent contamination, heat transfer along the chamber wall to reduce the distance of Sn and cavity

Coating Process (1)





Nanometer-scale white spots on the surface

Coating conditions of process (1)

ICP-OES test results of the Sn content in the HNO₃ solution

Reagents	Sn (ppm)	Conditions		
1#	0.26	Background		
2#	0.47	Immersed with Nb ₃ Sn sample		

XPS surface analysis results of the $\rm Nb_3Sn$ sample before and after immersion in $\rm HNO_3$ solution

Samples	Nb Atomic %	Sn Atomic %	Sn/Nb
Original	45.22	54.78	1.21
HNO ₃ rinse	71.03	28.97	0.41

Surface Sn content of samples measured by AES before and after immersion in ${\rm HNO}_3$ solution

Samples	Nb Atomic %	Sn Atomic %	Sn/Nb
Original	54.39	45.61	0.84
HNO ₃ rinse	67.90	32.10	0.47

The nanometer-scale white spots are Sn droplets that are formed by condensation of the residual Sn vapor on the film surface during the natural cooling process

Sn source Temperature/°C	Growth stage	Exploration of methods for adsorbing residual Sn vapor				
	time / Minute	Sn power	Valves	Mo belt	Ceramics	
1310	180	On	Closed	On	Without	



the quench field of $E_{acc,max}$ =16.11 MV/m.

□ The Sn source temperature of 1310°C is rather excessive for our deposition system

26.40

Average Sn content

Coating Process (2)



The Sn source temperature was lowered to 1200°C to decrease the Sn vapor pressure and the Sn evaporation rate. This is to reduce or avoid the formation of Sn droplets and spots from the residual Sn vapor.

Coating conditions of process (2)

Sn source Temperature/°C	Growth stage	Exploration of methods for adsorbing residual Sn vapor			
	time / Minute	Sn power	Valves	Mo belt	Ceramics
1200	180	On	Closed	On	Without



Despite the reduced gradient, the nanometer-scale Sn droplets still indicates tin vapor is in excess?

Coating Process (3)



Temperature profiles of coating process (3): the temperature of the Sn source heater drops rapidly to about $570^{\circ}C$ after the film growth stage

The conditions of the Coating Process (3) at the film growth stage were the same as those of the Coating Process (2). However, the Sn source of the Coating Process (3) was powered off immediately after the film growth stage to prevent additional Sn evaporation in the annealing stage. It is also expected that the lower temperature Sn source region adsorbs some Sn vapor during the annealing stage, hence reducing the Sn droplet density during the cooling stage.

Coating conditions of process (3)

Sn source Temperature/°C	Growth stage	Exploration of methods for adsorbing residual Sn vapor			
	time / Minute	Sn power	Valves	Mo belt	Ceramics
1200	180	Off	Closed	On	Without







Nanometer-scale Sn droplets with **significantly reduced** density (left) and patchy areas (right) on the Nb3Sn film surface coated by the Coating Process (3). This confirms the **effectiveness** of the **adsorption** in reducing the formation of Sn droplets

EDS composition of the Nb₃Sn films by Coating Process (3)

Position	1	2	3
Sn content(at. %)	26.23	26.50	25.96
Average Sn content		26.23	



The Q₀ of the Nb₃Sn SRF cavity by Process (3) reaches 1.8×10^{10} at 4.2 K in the low field region. The cavity quenches at E_{acc,max} = 10.46 MV/m because of the patchy areas found on the surface.

- **Q**-slope of process 3 is more gentle than process 2 at $E_{acc} < \sim 5$ MV/m, but at $E_{acc} > 5$ MV/m Q-slope of process 2 becomes more precipitous and the Q₀ drops to the same level of process 3.
- Nanometer-scale Sn droplets mainly affect the RF performance in the low-field region. patchy areas have a more pronounced impact on the RF performance in the higher-field region, leading to a precipitous Q-slope and early quench.

> Adsorption effect confirmation : *Coating Process (4),(5) and (6)*

Sn source Temperatu	Growth stage time	Exploration of methods for adsorbing residual Sn vapor [*]				
re/°C	/ Minute	Sn power	Valves	Mo belt	Ceramics	
1200	180	On	Open	On	Without	
		On	Closed	Bottom On	Without	
		On	Closed	On	With	

Coating conditions of process (4), (5) and (6)





Process (5): Manufacture of cold trap of ~27°C by keeping the middle and upper Mo heating belts powered off all the process ($\sqrt{}$)

1E+01E-1 1000 1E-2 emperatur 600 1E-3 1E-4 2 400 1E-5 50 Time (Hour) - Cavity-T1 ---- Cavity-T2 ---- Cavity-T3 -----Sn-T Signal A = InLens Mag = 50.00 K X Vacuum of Process (2) — Vacuum of Process (4)

Process (4): Attempt at vacuum pumping by opening the valves between the coating chamber and the vacuum pump immediately after the film growth stage to pump away the residual Sn vapor(\times)



Process (6): High-purity ceramic bricks are suspended above the cavity to increase the adsorption of residual Sn vapor ($\sqrt{}$)

By creating lower-temperature cold traps and suspending high-purity ceramic bricks, the adsorption of Sn vapor can be effectively enhanced to prevent the condensation of Sn droplets on the film surface.

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Coating Process (7)



Cavity-T1 Cavity-T2 Cavity-T3 Sn-T

Recipe of the Coating Process (7) with the Nb cavity at 1100°C and the Sn source at 1233°C

Optimization idea: under the premise of effectively inhibiting the condensation of Sn droplets, the Sn source temperature can be safely increased.

Targeted modifications to the Coating conditions:

- 1. During the film growth stage, the temperature of the Sn source was kept at 1233°C, but the duration was shortened to 2 hours.
- 2. Keeping the bottom Mo heating belts powered on while turning off the middle and upper Mo heating belts during the whole coating process.
- 3. The Sn source heater was turned off immediately after the film growth stage.
- 4. Two pieces of high-purity ceramic bricks were suspended above the cavity to further increase the adsorption of residual Sn vapor.

Coating conditions of process (7)

Sn source Temperature/°C	Growth stage	Exploration of methods for adsorbing residual Sn vapo			
	time / Minute	Sn power	Valves	Mo belt	Ceramics
1233	120	Off	Closed	Bottom On	With

➤ Coating Process (7)



SEM images of the Nb₃Sn film coated by the Coating Process (7): no patchy areas are found in the 125 μ m by 125 μ m area (left) and nanometer-scale Sn droplets on the surface of the Nb₃Sn film (right)

EDS composition of the Nb₃Sn films by Coating Process (7)

Position	1	2	3
Sn content(at. %)	25.60	25.86	25.75
Average Sn content		25.74	



The Q₀ of the Nb₃Sn SRF cavity by Process (7) at 4.2 K in the low field region is about 1.4×10^{10} and the $E_{acc,max}$ reaches 18.03 MV/m. Moreover, despite the condensed Sn droplets, the Q-slope is relieved with the Q₀ larger than 1×10^{10} at $E_{acc} = 12$ MV/m and 4.2 K.



1

3



Background



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Film characterization and RF performance comparison

Coating process	Sn droplets	Sn spots	Patchy aera	Q₀ at low field	E _{acc,max}	Onset of precipitou s Q-slope
1	Yes	Yes	No	8.8E9	16.11MV/m	~12MV/m
2	Yes	No	Doubtful	1.9E10	13.39MV/m	~7MV/m
3	Yes	No	Yes	1.8E10	10.46MV/m	~5MV/m
4	Yes	No	Doubtful	No test	No test	No test
5	No	No	Doubtful	No test	No test	No test
6	No	No	Doubtful	No test	No test	No test
7	Yes	No	No	1.4E10	18.03MV/m	~12MV/m

- □ The composition and causes of nanometer-scale Sn droplets, millimeter-scale Sn spots, and locally extremely thin patchy areas on the surface of Nb₃Sn films were confirmed.
- □ The impact of nanometer-scale Sn droplets, millimeter-scale Sn spots, and patchy areas on the RF performance of Nb₃Sn SRF cavities, such as Q₀, E_{acc,max}, and Q-slope, were also distinguished and clarified.
- □ The method of achieving high-quality Nb₃Sn films by increasing the adsorption of residual Sn vapor to suppress the generation of nanometer-scale Sn droplets was explored under the premise of ensuring uniform film growth by increasing the Sn vapor flux.

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