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# Screen current effects, experiencing with quenching REBCO tapes, and implications

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1. Lawrence Berkeley National Lab
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3. KEK

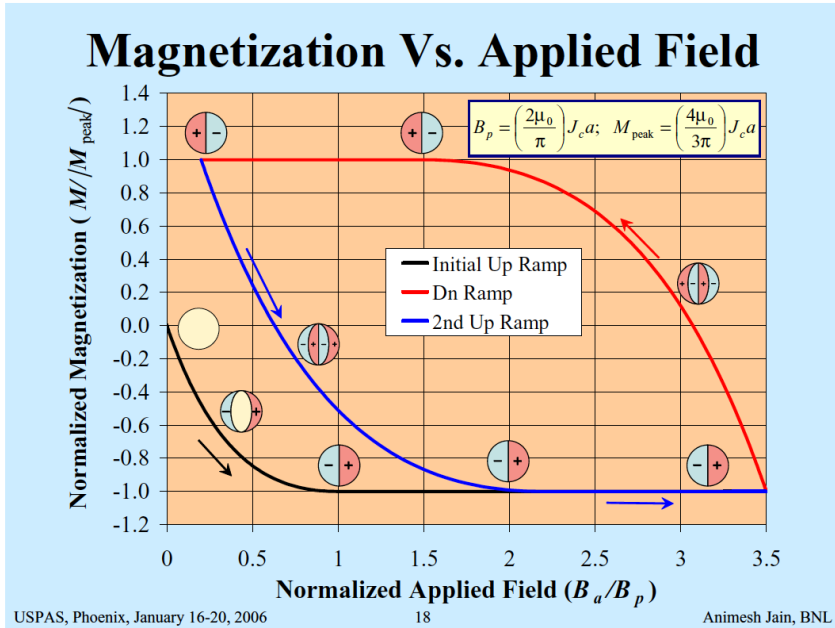
2023/11/02

Presented at the Fermilab REBCO Round Table Meeting

Work financially supported by the U.S. Department of Energy, Office of Science, Office of High Energy Physics through the US - Japan HEP collaboration, U.S. Magnet Development Program, Early Career Program, and benefit from projects supported by the DOE-OHEP SBIR-STTR program.

# Outline and motivations

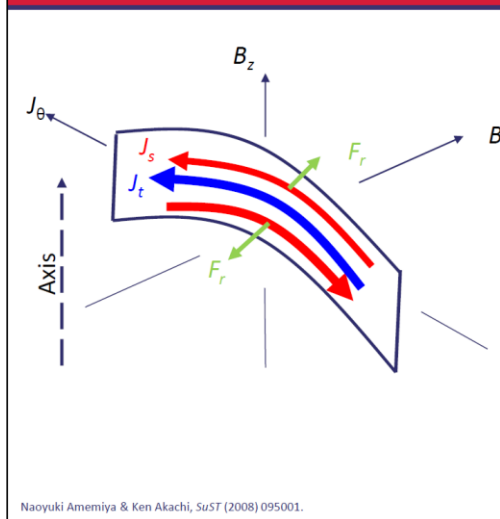
- Superconductor is a nonlinear magnetic material.
- Its magnetization also decays with time.



- $\Delta M \propto J_c \cdot D_{eff}$
- LHC Nb-Ti dipole wire,  $D_{eff} = 6-7 \mu m$ .
- High-Lumi LHC Nb<sub>3</sub>Sn wire,  $D_{eff} \sim 50 \mu m$ .

- Large screen currents affect both field quality and the ability of REBCO magnets to survive high fields.
- Results of FEM models of KEK REBCO coils in a BNL Nb<sub>3</sub>Sn magnet
- Experience with quenching REBCO tapes

## Screening Currents: Tape Conductors



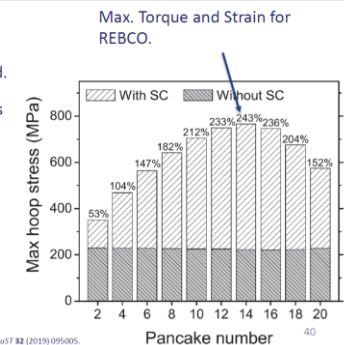
- $J_t$  = transport current in  $\theta$  direction. It creates  $B_z$ . At top of magnet  $B_r$  is positive.
- During charging of the magnet,  $B_r$  creates screening currents,  $J_s$ , in the tape.
- The Screening Current changes the field distribution.

## Screening Currents: Strain

In the 1970s & 1980s, IGC built Nb<sub>3</sub>Sn tape magnets. Rippling of the edge of used tapes was observed.

In 2019 Jing Xia, et al., showed that if a coil was designed for uniform stress due to transport current only, actual stress including screening currents might be 2.4x higher.

Low screening currents at mid-plane due to low radial field.  
High radial field at end of coil limits  $J_c$ .



After Mark Bird, MT26 plenary

# SCIF (screen current induced field) in a hybrid magnet – overall design

## BNL Nb<sub>3</sub>Sn magnet:

Item	Unit	Value
Magnet type	-	2-in-1
Horizontal aperture	mm	31
Vertical aperture	mm	338
Central field	T	8.7
Nominal current	A	8000
Nominal current density	A/mm <sup>2</sup>	425

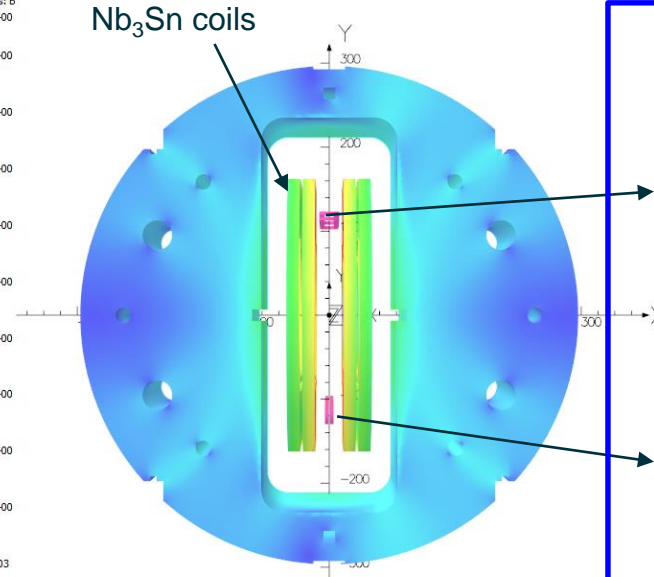
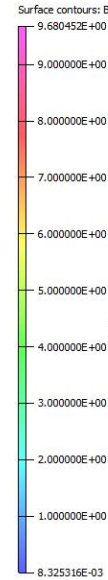
## KEK HTS coils:

Item	Unit	Value
Number of HTS tape	-	20
HTS Tape width	mm	4
Thickness of HTS layer	μm	2.2
Thickness of HTS tape	μm	310
Current of HTS coil	A	500
Center field	T	0.8

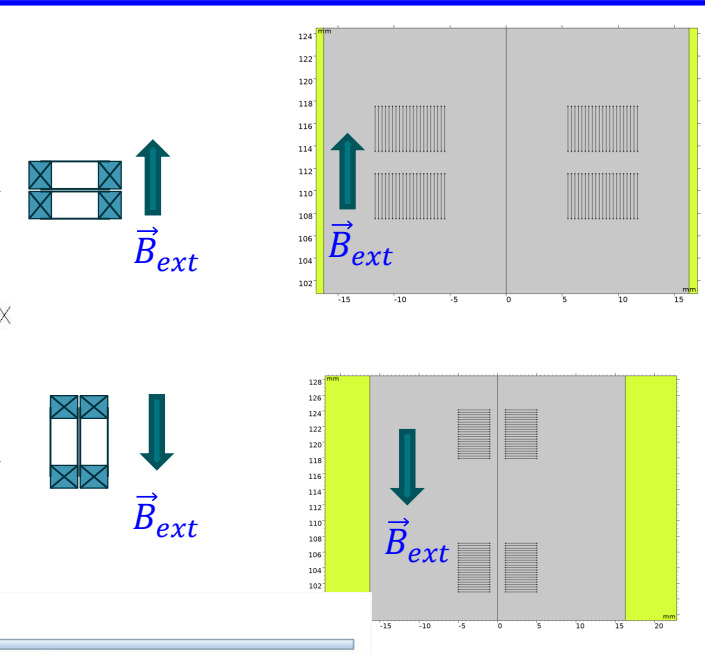
## US Japan HEP collaboration on high temperature superconducting magnets for accelerator facilities

Tengming Shen (US PI), LBNL; Toru Ogitsu (Japan PI), KEK

Xiaorong Wang (US CO-PI), LBNL; Ramesh Gupta, (US CO-PI), BNL; Naoyuki Amemiya (Japan CO-PI, Kyoto University).



## REBCO (flat racetrack) coils

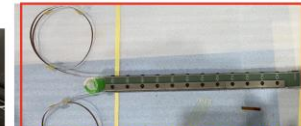
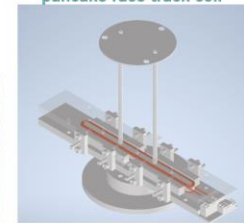
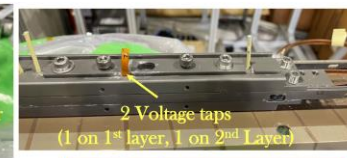
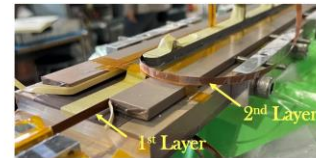


## HTS Coil Fabrication

### Winding : Three coil with Coated ReBCO tape (wet winding)

- The actual conductor thickness: **0.31 mm**  
(EuBCO: 0.16, coating layer: 0.05, adhesive layer: 0.1)
- The number of turns: **20 turns**

Winding setup for double pancake race track coil



HTS coil construction led by Masami Iio, Mukesh DHAKARWAL from KEK and tests led by Febin Kurian, Piyush Joshi from BNL.

# Modelling the Magnetization in HTS Tapes with FEM tool (COMSOL)

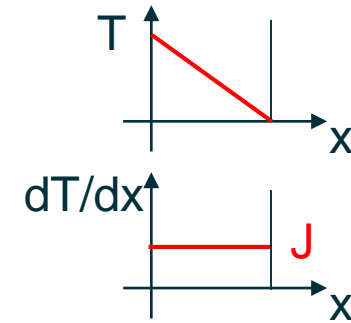
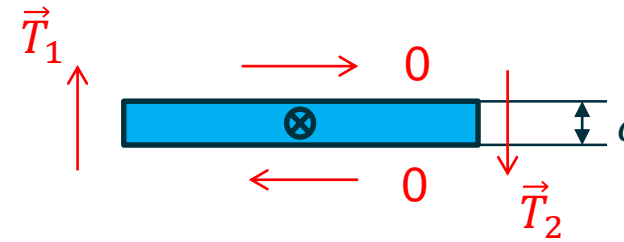
T-A formulation:

$$\begin{cases} \nabla \times (\rho_{HTS} \nabla \times \vec{T}) + \frac{\partial \vec{B}}{\partial t} = 0 & \text{HTS film} \\ \nabla \times \vec{B} - \mu_0 \vec{J} = 0 & \text{Entire domain} \end{cases}$$

$$\begin{aligned} \vec{J} &= \nabla \times \vec{T} && \text{HTS film} \\ \vec{B} &= \nabla \times \vec{A} && \text{Other domains} \end{aligned}$$

Boundary condition:

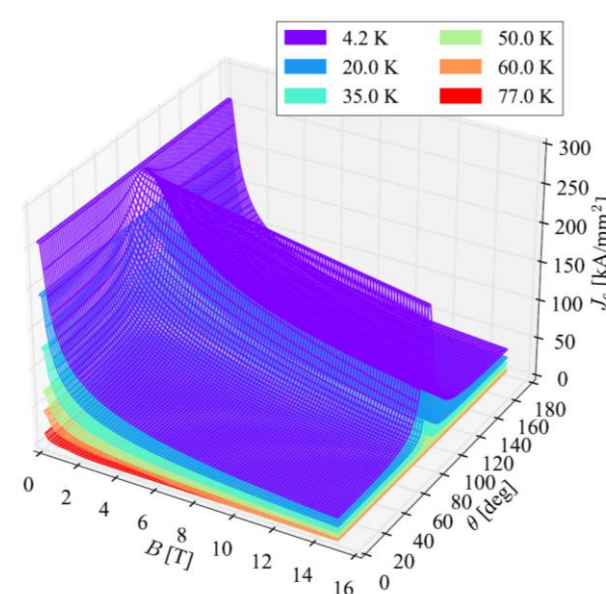
$$I_t = \int \vec{J} dA = \int \nabla \times \vec{T} dA = \oint \vec{T} dl = (\vec{T}_1 - \vec{T}_2) \delta$$



Resistivity of HTS film:

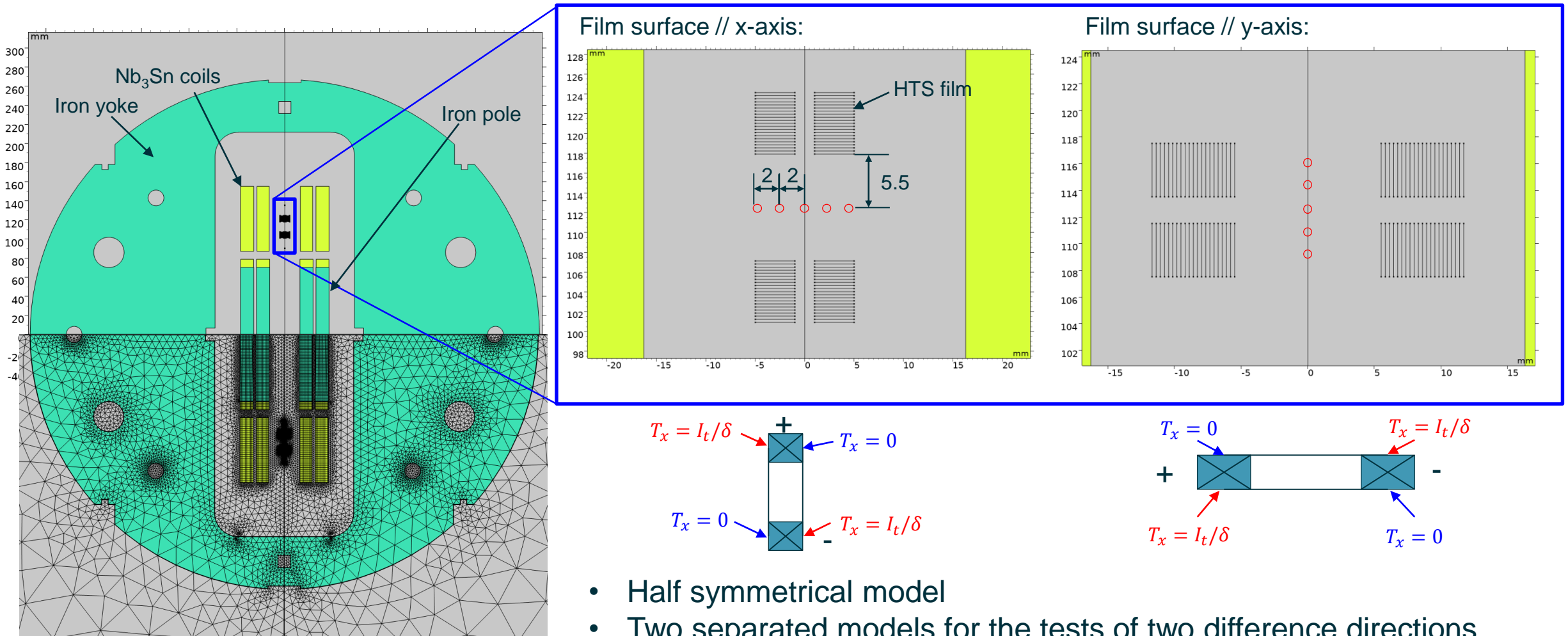
$$\rho_{HTS} = \frac{E_c}{J_c(T, B, \theta)} \left| \frac{\vec{J}}{J_c(T, B, \theta)} \right|^{n-1}$$

N value is fixed at 45



Critical surface for ReBCO tape:

# Numerical Model – 2D infinitive FEM model



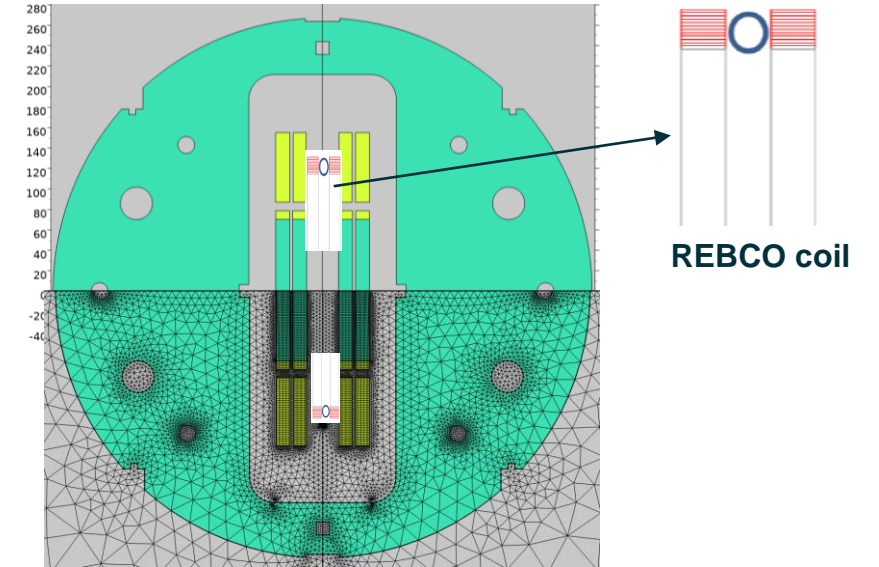
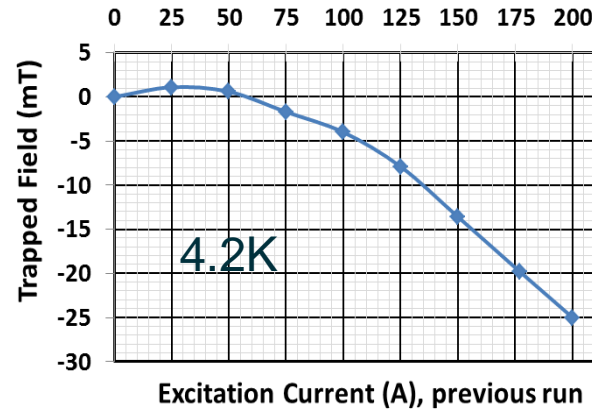
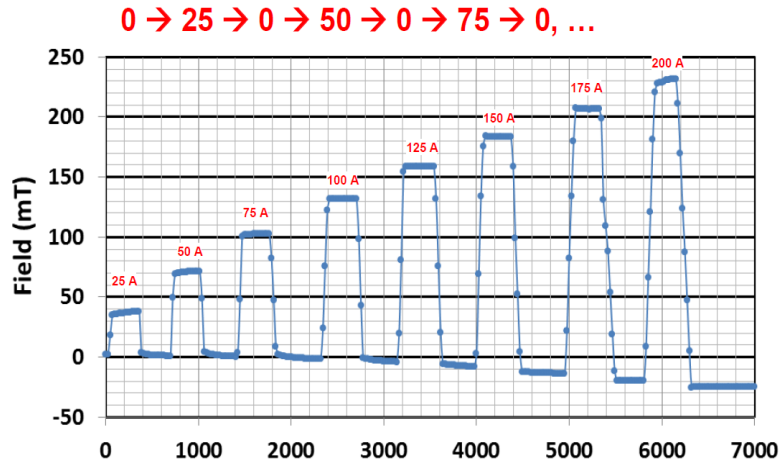
- Half symmetrical model
- Two separated models for the tests of two difference directions
- Hall sensor is set at the center of the HTS coil with the interval of 2mm



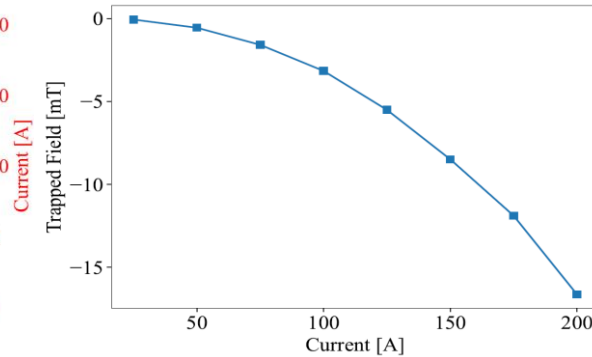
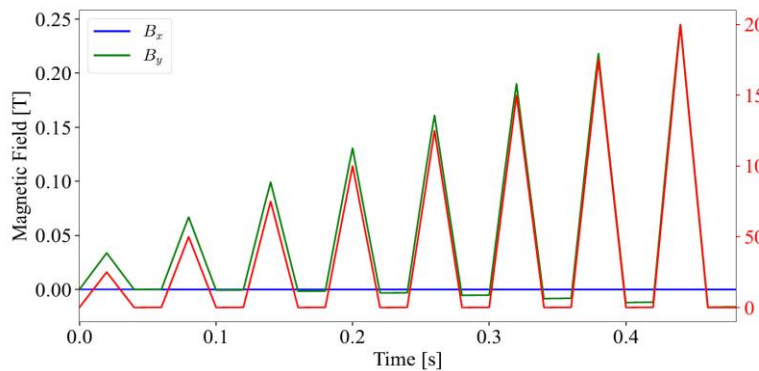
# Validating the modeling technique: The benchmark case

R. Gupta et al, Design, construction, and test of HTS/LTS hybrid dipole, *IEEE Transactions on Applied Superconductivity*, 28(3), 4002305, 2018  
Coil construction and measurement financially supported by a SBIR award from US. DOE OHEP to Particle Beam Lasers, Inc. and BNL.

## Measurement:



## Simulation:



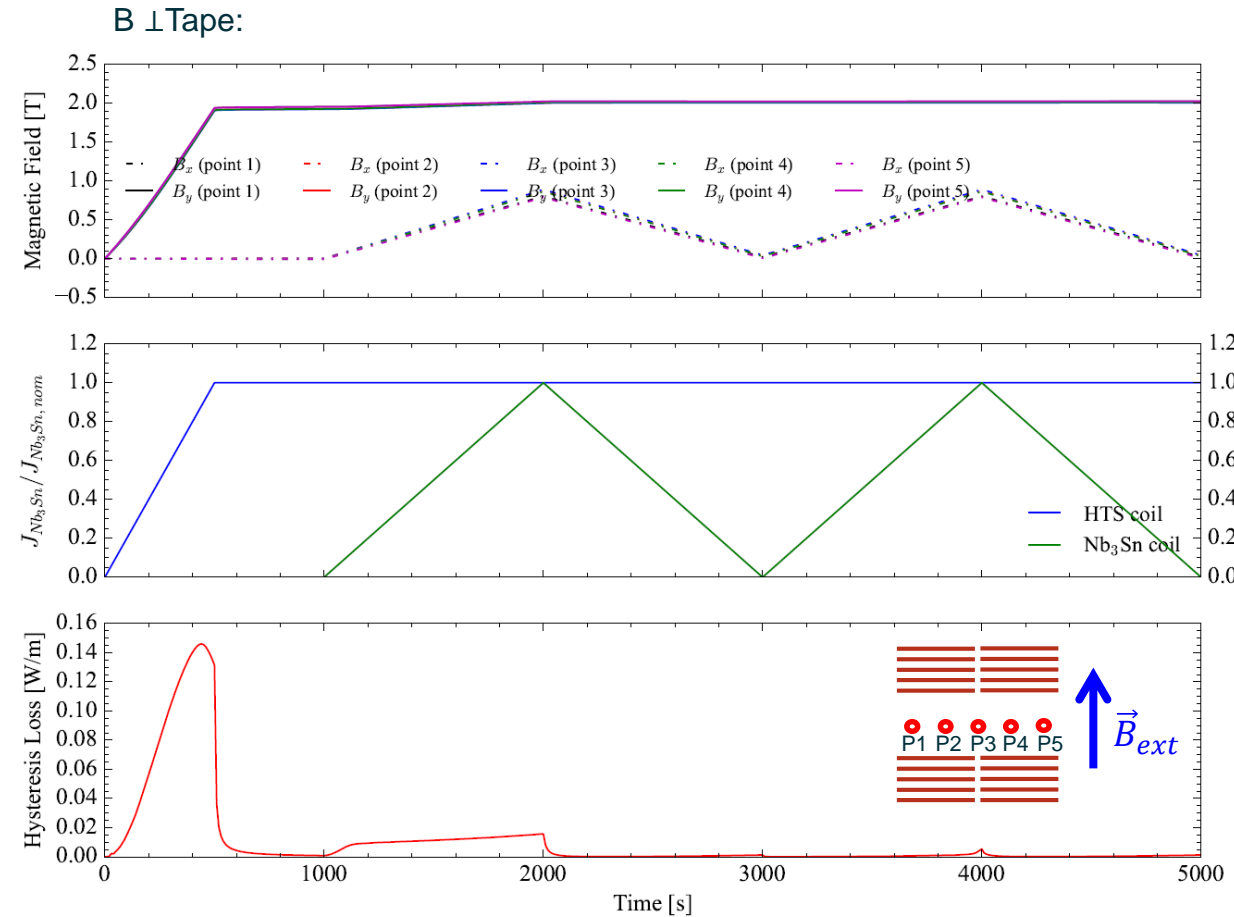
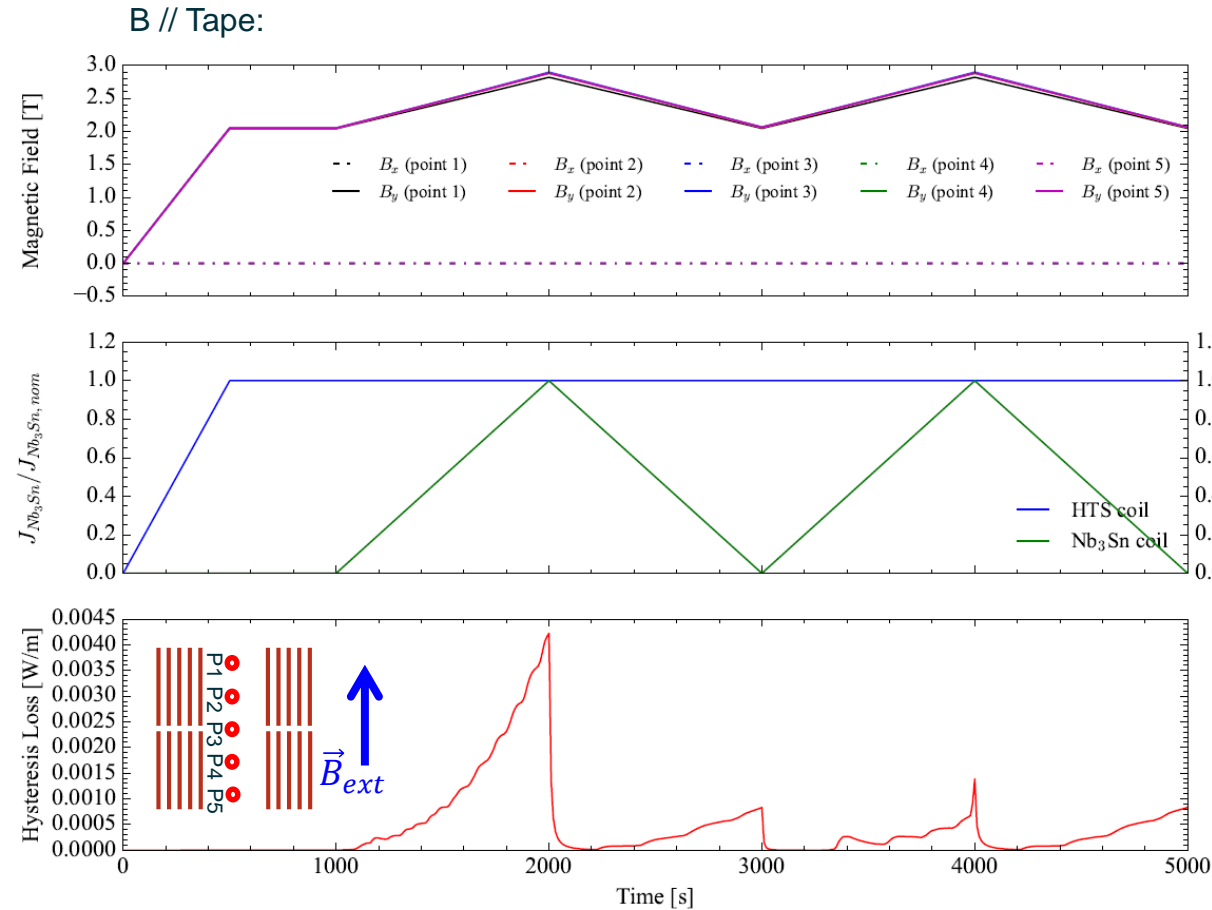
## HTS Tape:

<b>Manufacturer:</b> AMSC	0.20 x 12.1 mm Tape
<b>YBCO</b>	YBCO layer is 10 mm x 1.2 μm
<b>Description :</b> 3R-174-1-37-38	<b>Area (mm2):</b> 2.420 <b>Length:</b> 30 mm
<b>SAMPLE #</b> 1	<b>SC_Area (mm2):</b> 0.012
<b>FIELD Dir.</b> PERP-H	

Thanks Ramesh for the information!

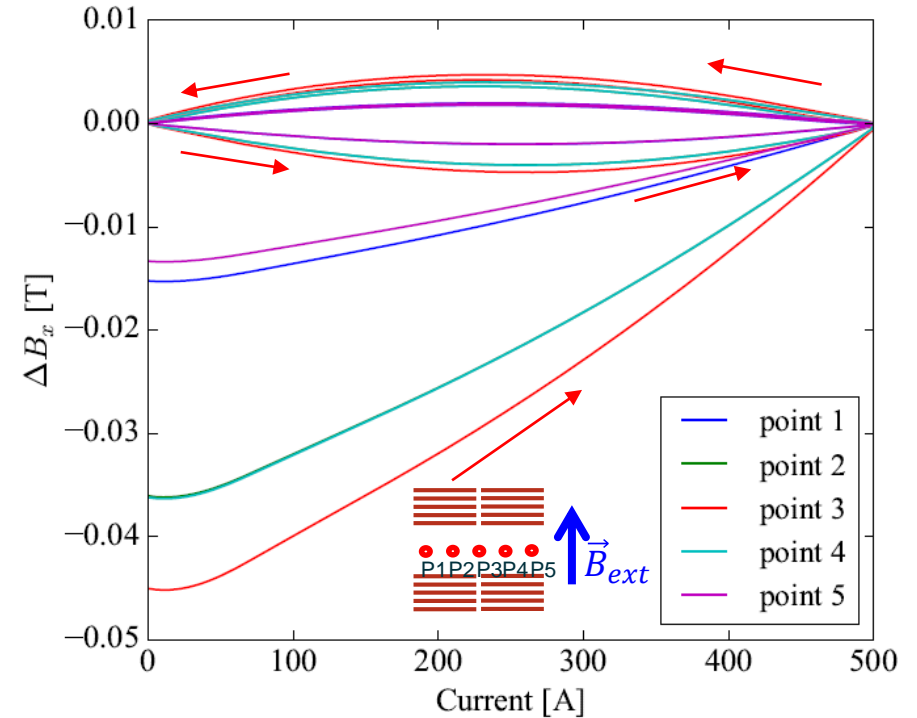
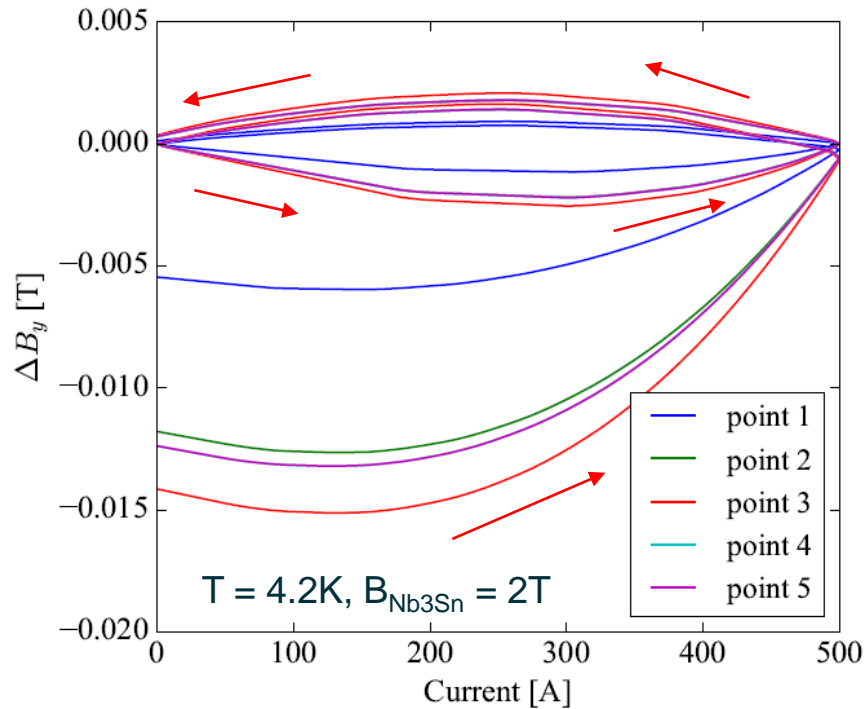
# Return to the US-Japan case:

## Field and AC loss during energization of the Nb<sub>3</sub>Sn Magnet and HTS coils



- Energized Nb<sub>3</sub>Sn magnet first, then powered up the HTS coil with two cycles
- B<sub>x</sub> and B<sub>y</sub> are generated by the cases B//Tape and B⊥tape, respectively

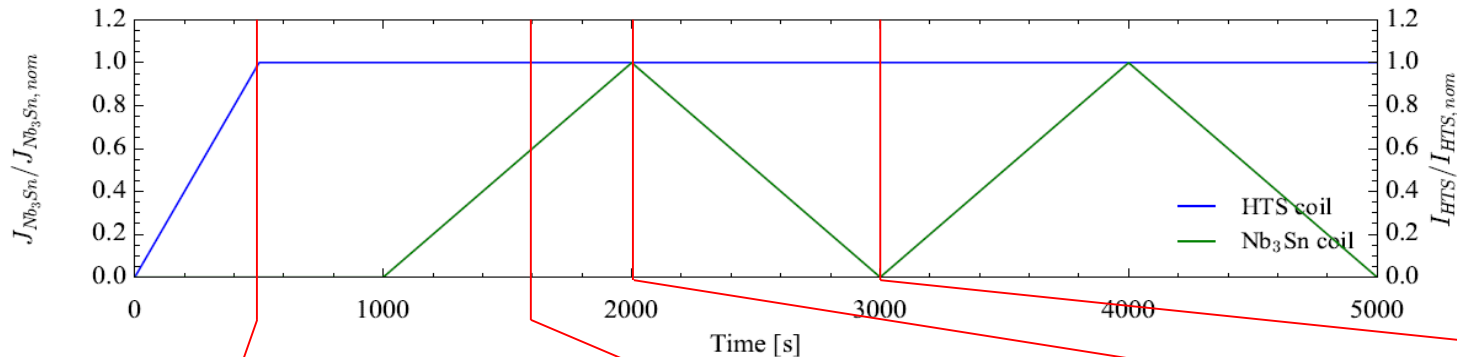
# SCIF by HTS coils during energization with LTS magnet field removed



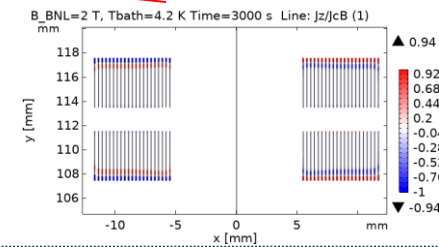
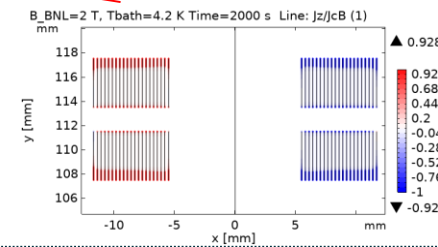
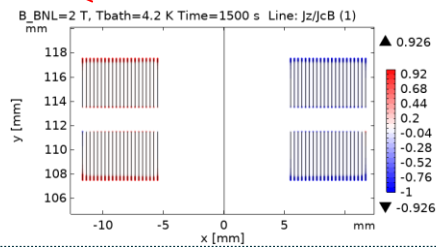
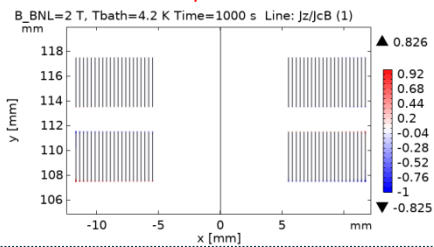
- Case of  $B \parallel c$  has a large loop about  $\Delta B_x \sim 10 \text{ mT}$
- The loop for the case  $B \parallel ab$  only has  $\Delta B_y \sim 5 \text{ mT}$



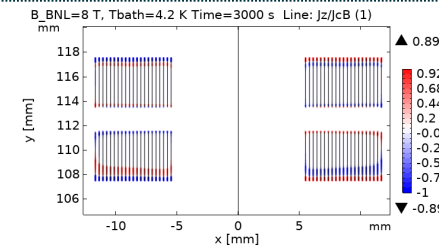
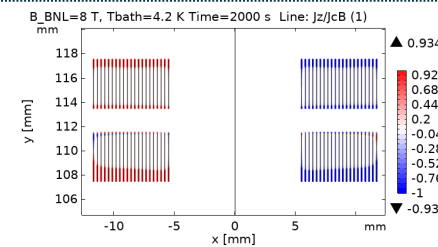
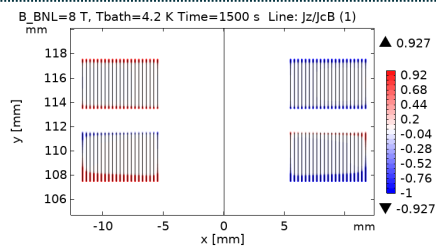
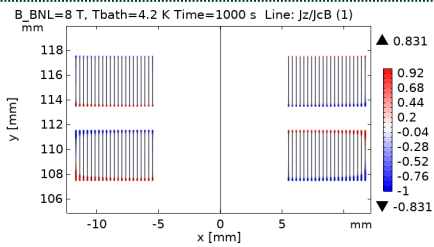
# Screening Current distribution (B // Tape case)



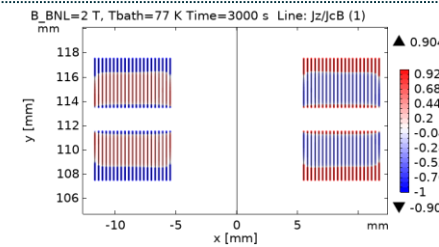
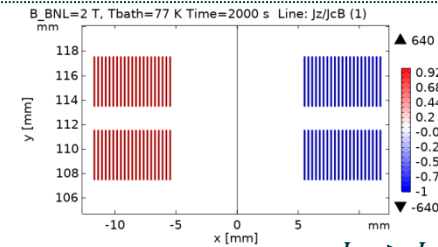
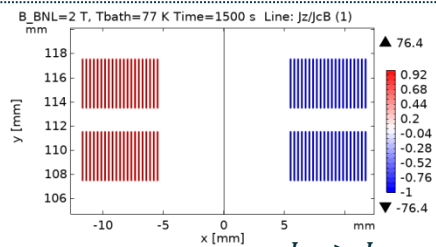
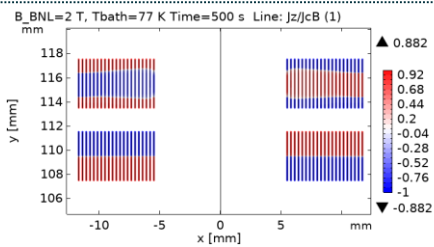
- Field is not fully penetrated into the HTS tape at 4.2K due to the high critical current
- Current flows uniformly at 77K because  $I_{op} > I_{SSL}$



B = 2T, T = 4.2K



B = 8T, T = 4.2K

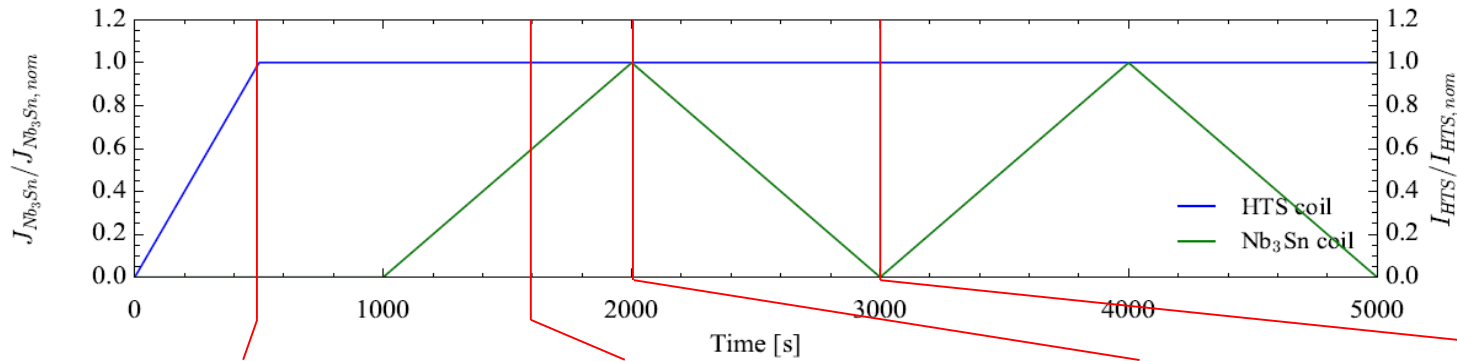


B = 2T, T = 77K

$I_{op} > I_{SSL}$

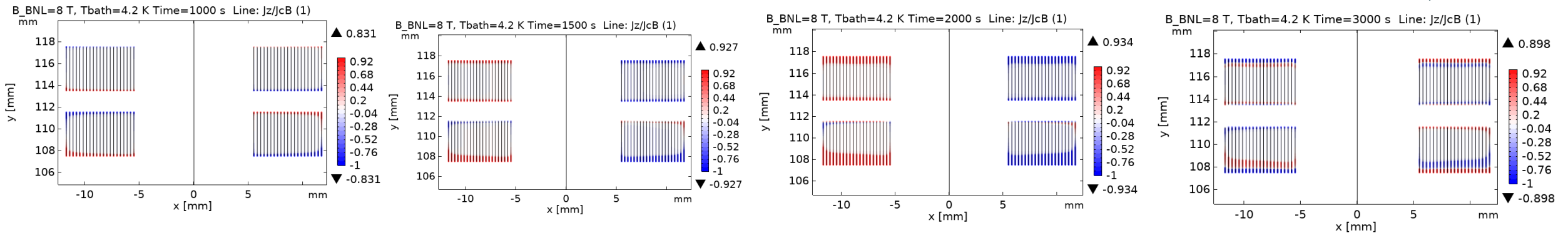
$I_{op} > I_{SSL}$

# Screening Current distribution (B // Tape case)

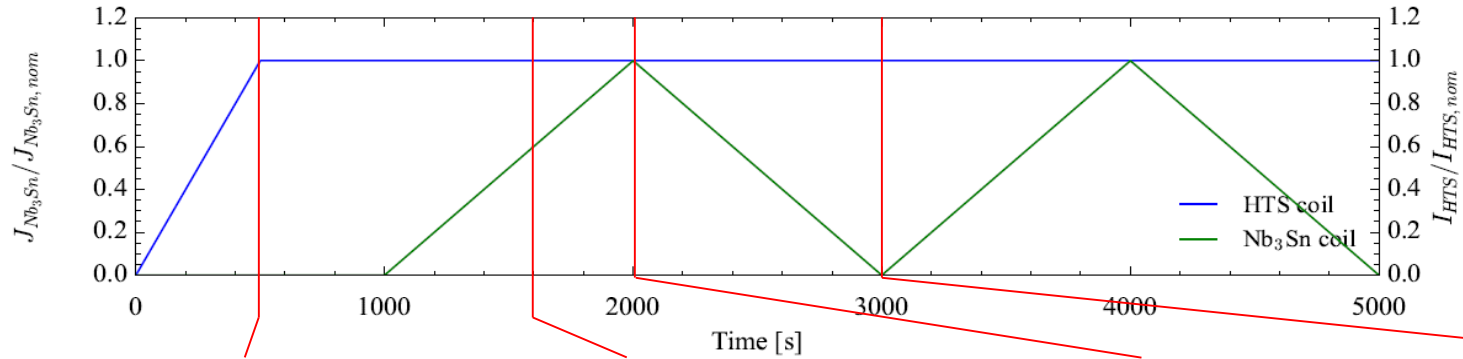


- Field is not fully penetrated into the HTS tape at 4.2K due to the high critical current
- Current flows uniformly at 77K because  $l_{op} > ISSL$

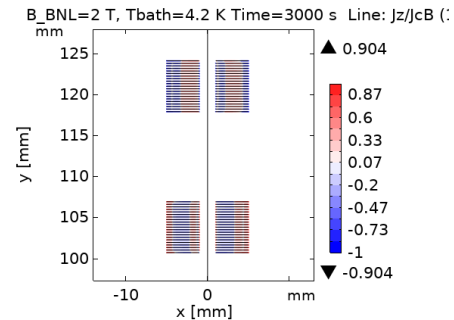
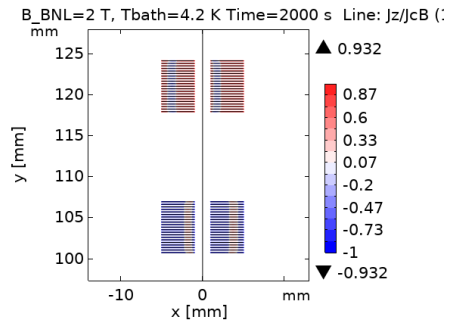
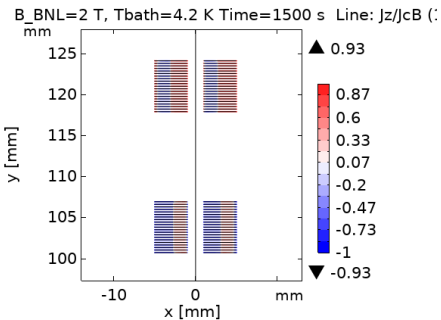
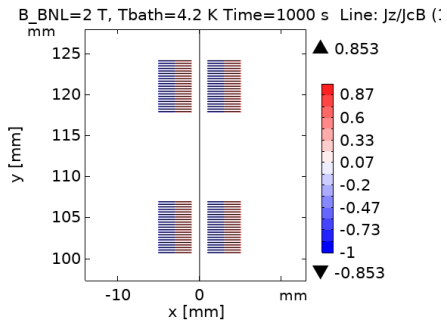
B = 8T, T = 4.2K



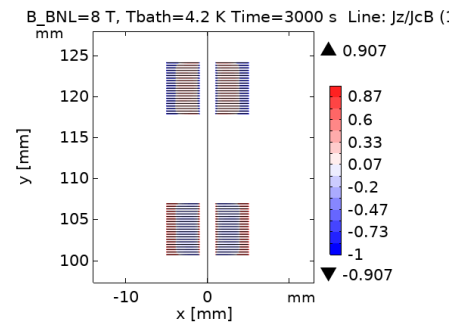
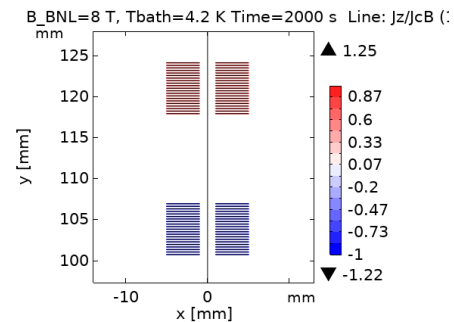
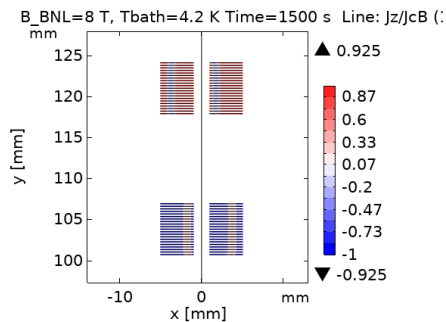
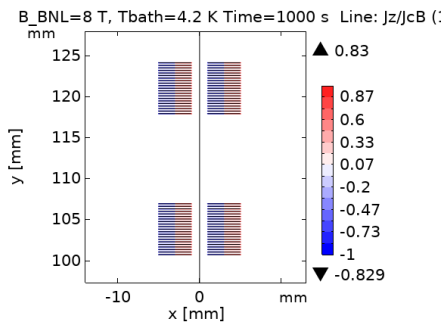
# Screening Current (B $\perp$ Tape case)



- Field is fully penetrated into the tape at the beginning of the energization of the HTS coil.



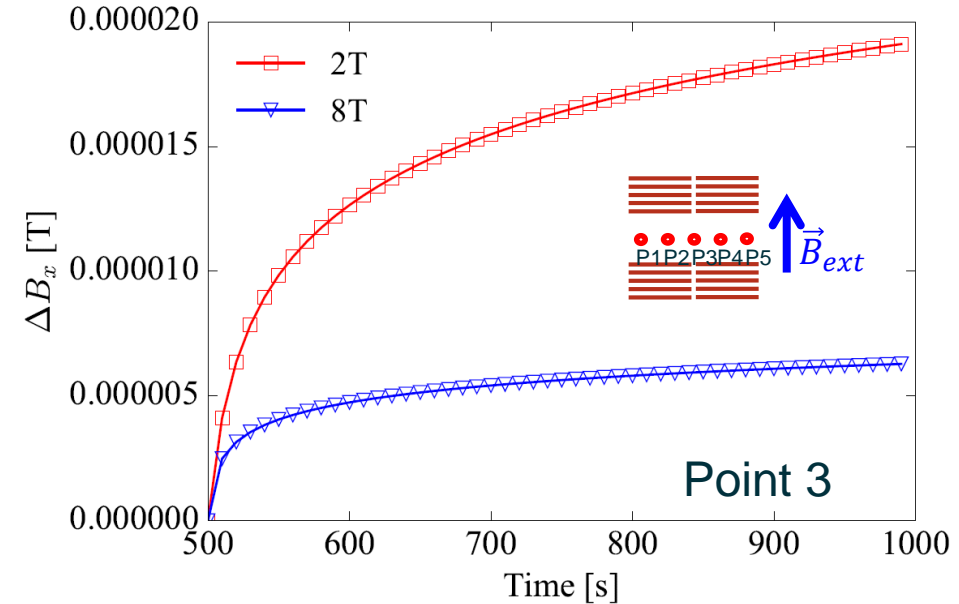
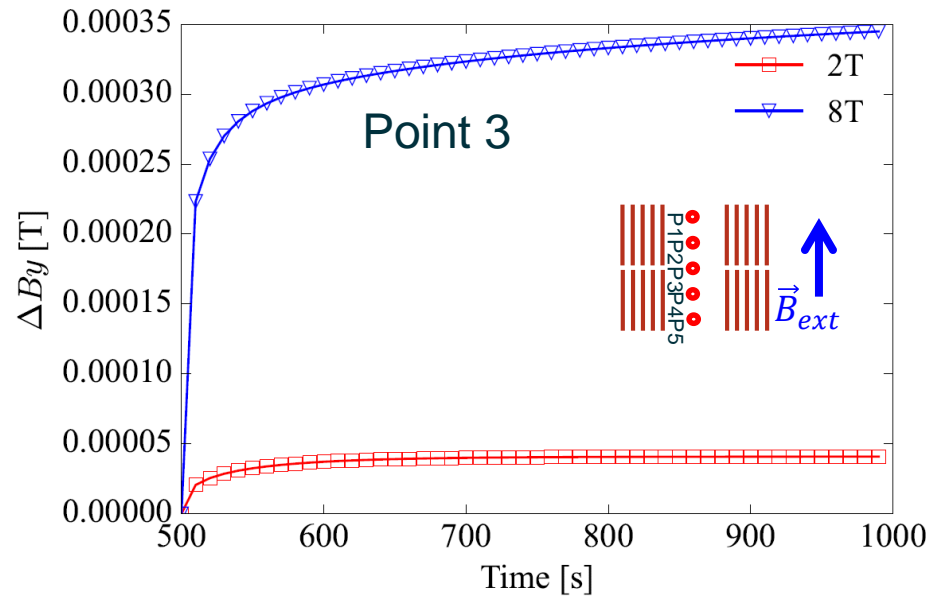
B = 2T, T = 4.2K



B = 8T, T = 4.2K

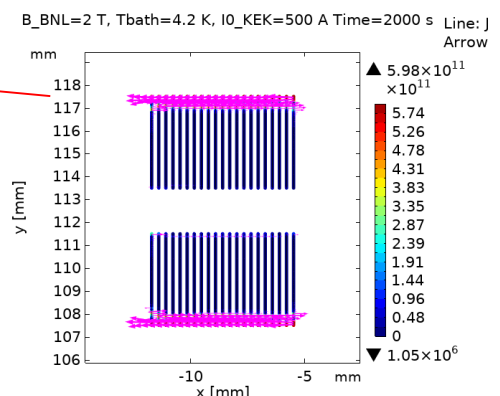
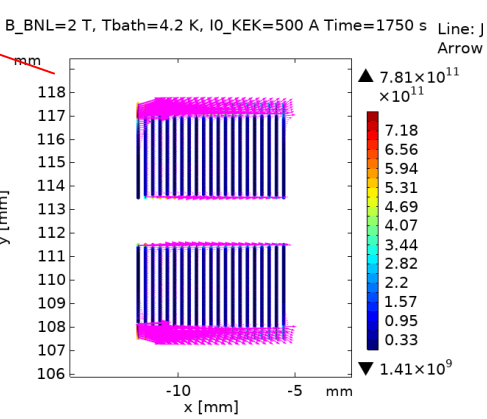
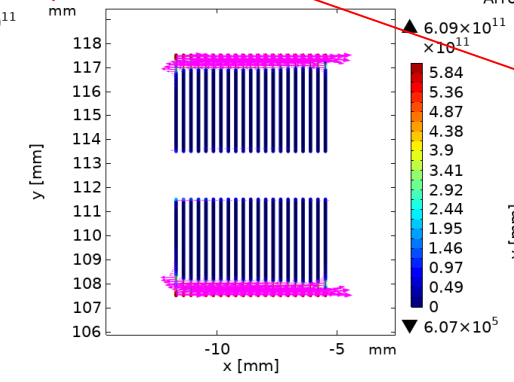
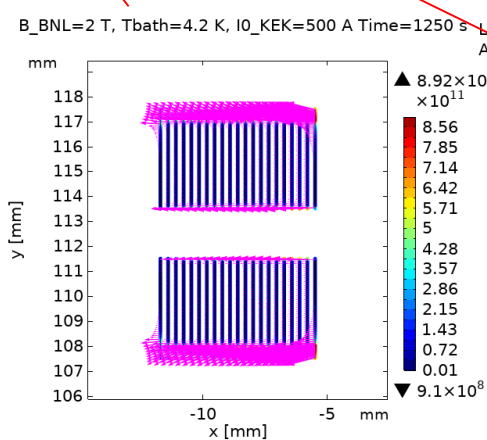
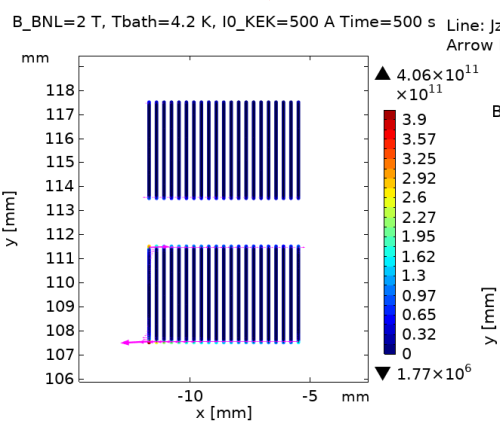
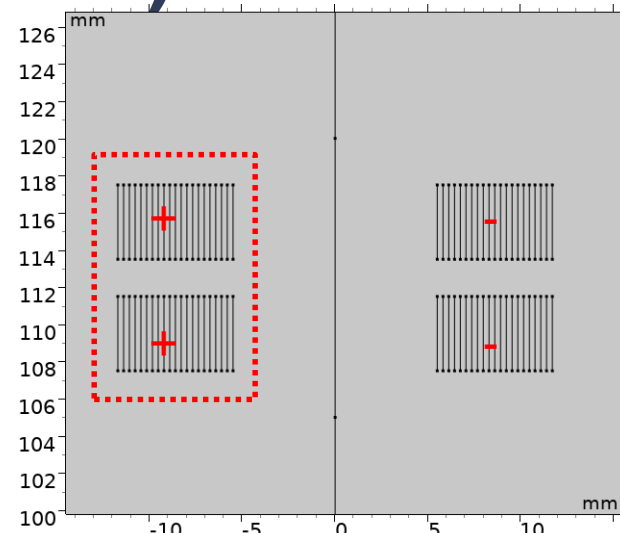
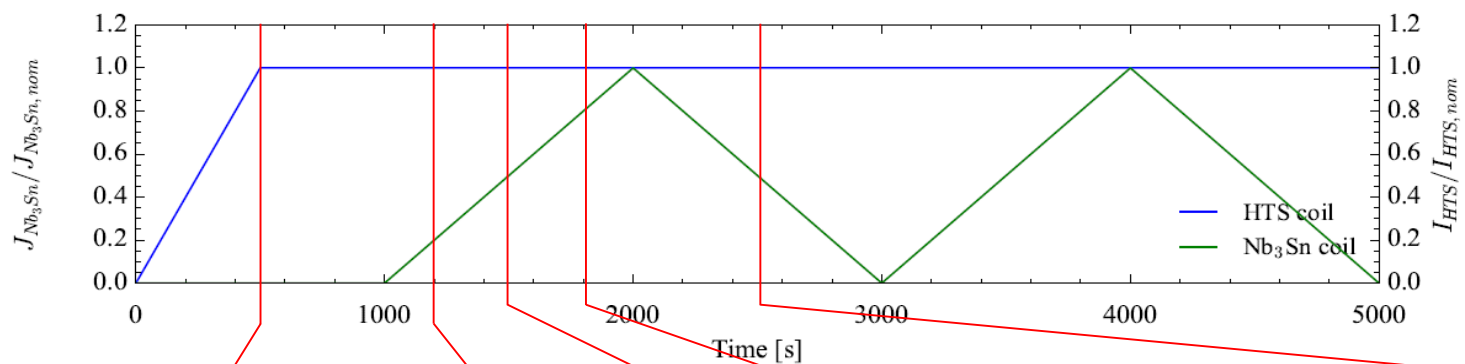
$$I_{op} > I_{SSL}$$

# Decay of SCIF after Ramping Nb<sub>3</sub>Sn Magnet



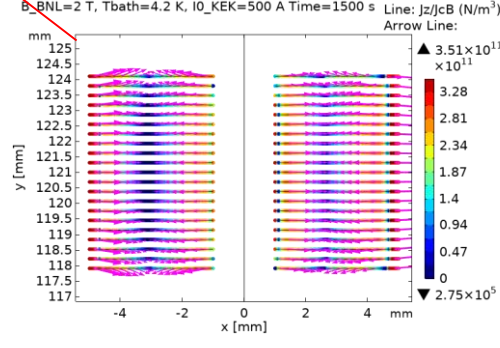
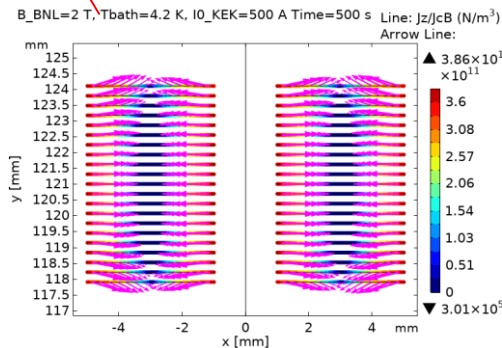
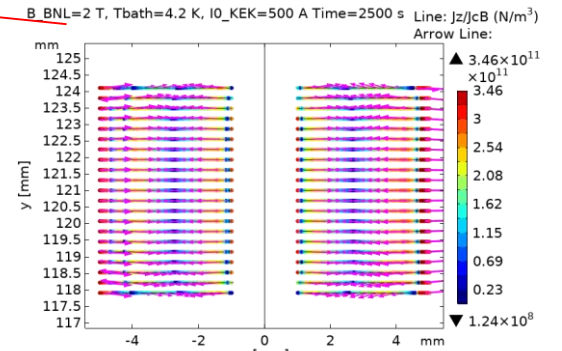
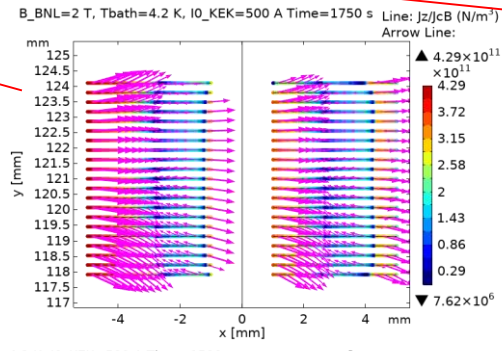
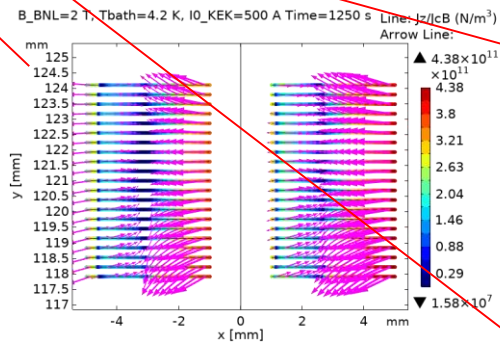
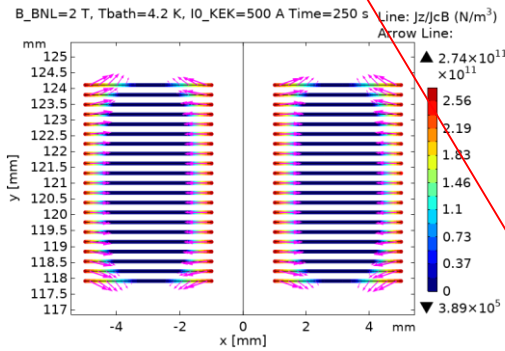
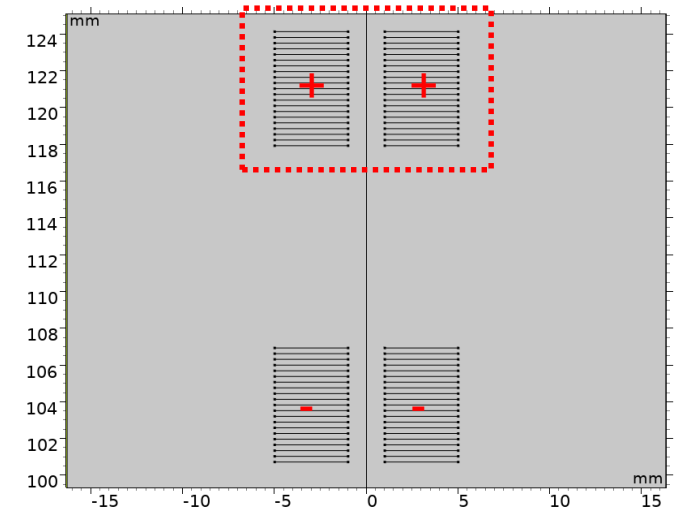
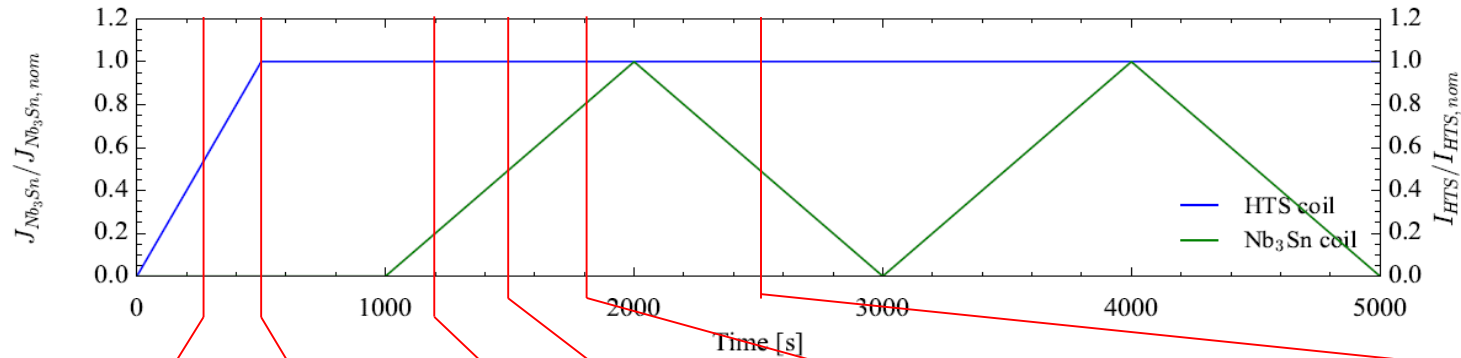
- Field decays as a function of time due to the resistivity of flux flowing
- Field increases because the shielding field is decreased
- Field decay at 2T background field for the case  $B // c$  seems faster than at 8T
- For the case  $B // ab$ , the field decay is faster at 8T

# Lorentz Force at the HTS Film (B // Tape case)



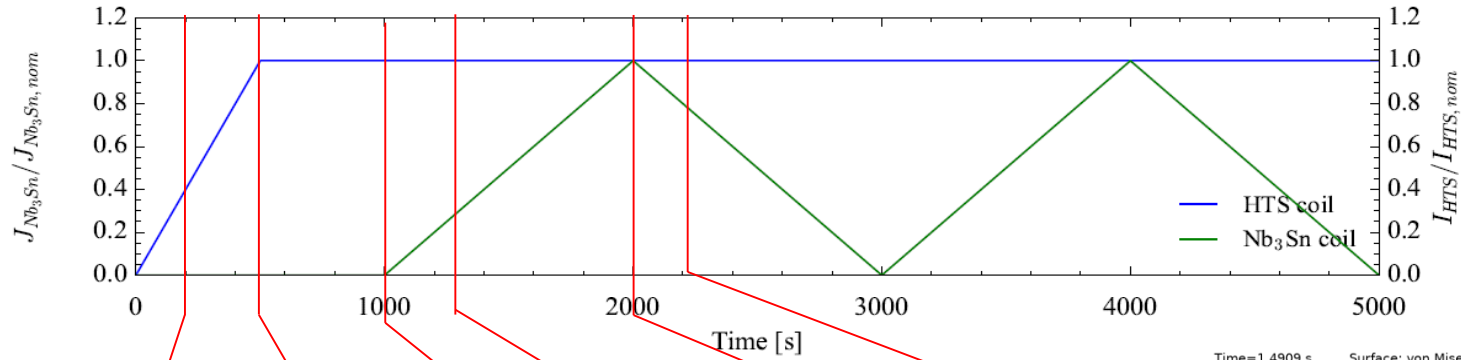


# Lorentz Force at the HTS Film ( $B \perp$ Tape case)

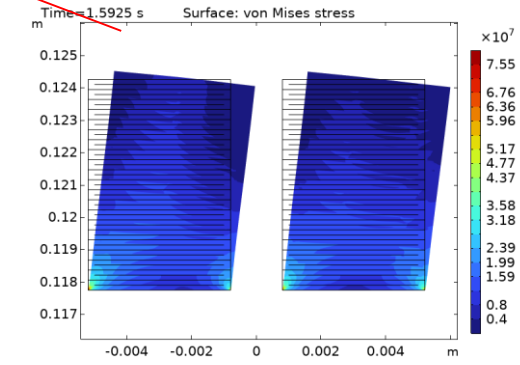
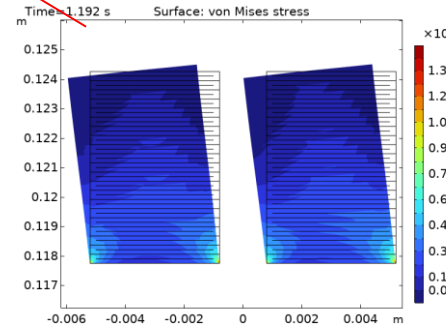
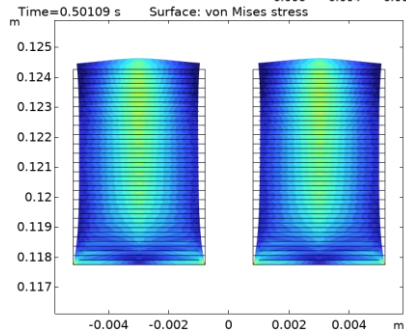
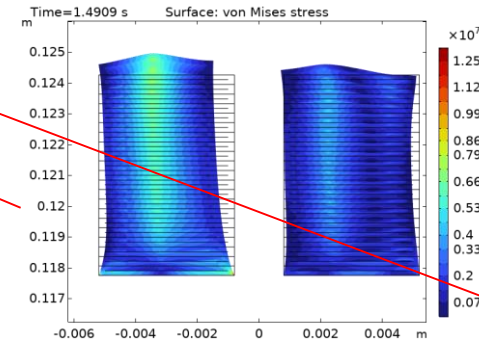
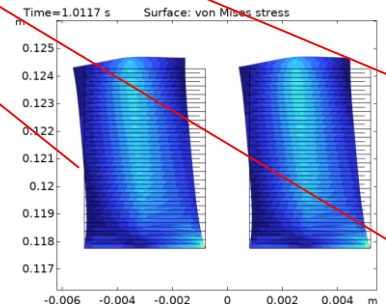
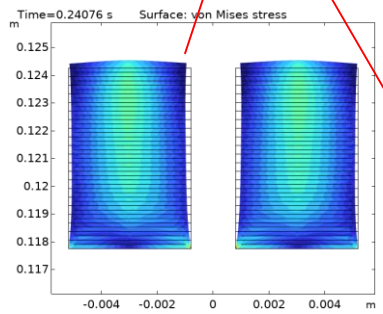
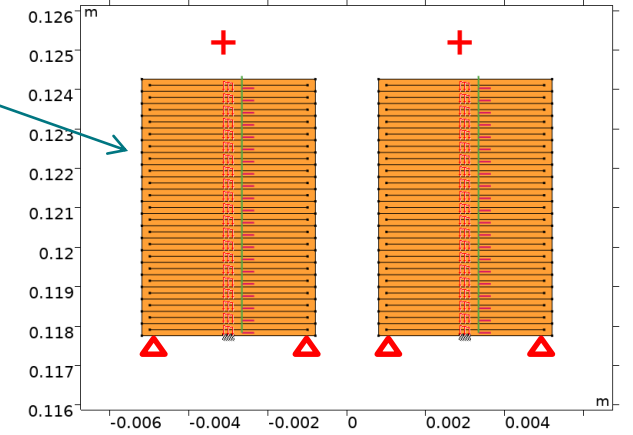


- Once the transport current is applied, the Lorentz force distribution is not balanced

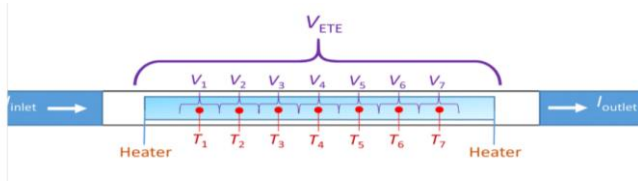
# Deformation during the energization (B $\perp$ Tape case)



Cu tape



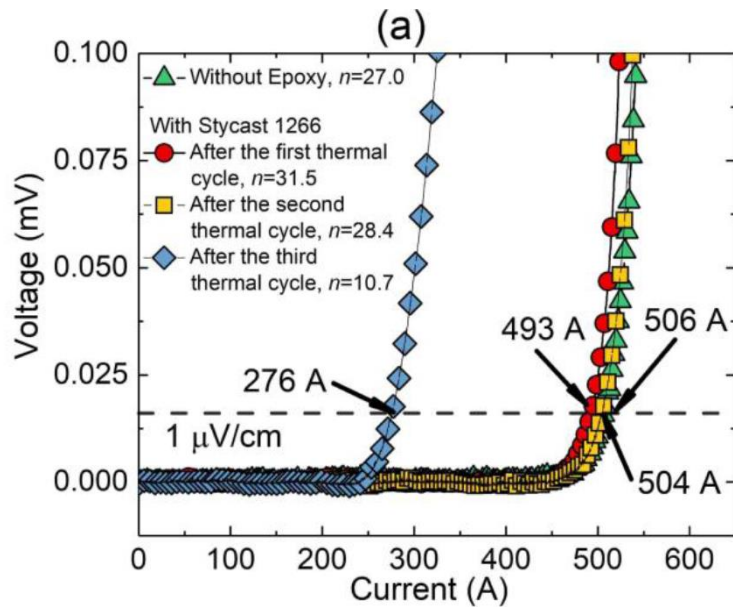
# Experience with impregnating and quenching REBCO tapes



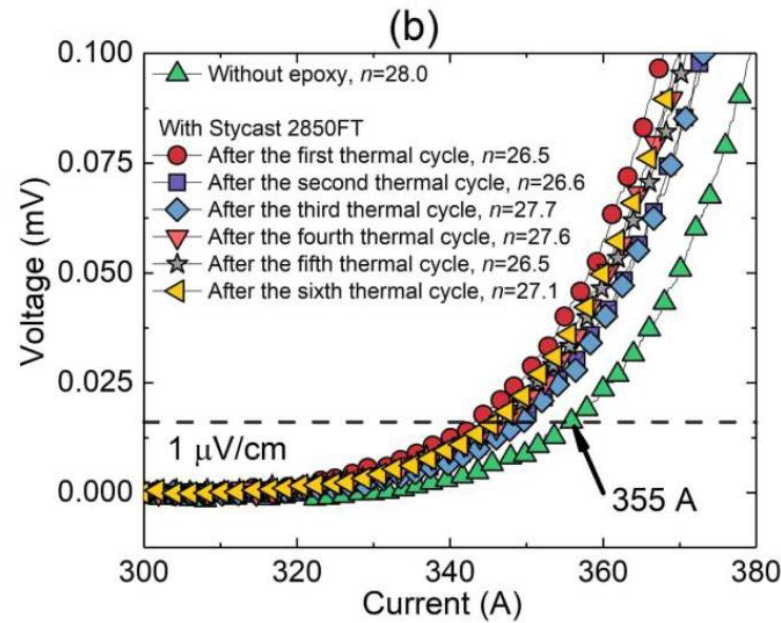
S. Yin et al., Degradation of REBCO coated conductors due to a combination of epoxy impregnation, thermal cycles, and quench: Characteristics and a method of alleviation, J. Appl. Phys. 128, 173903 (2020)

Uncertainty with maximum allowable temperature during a quench

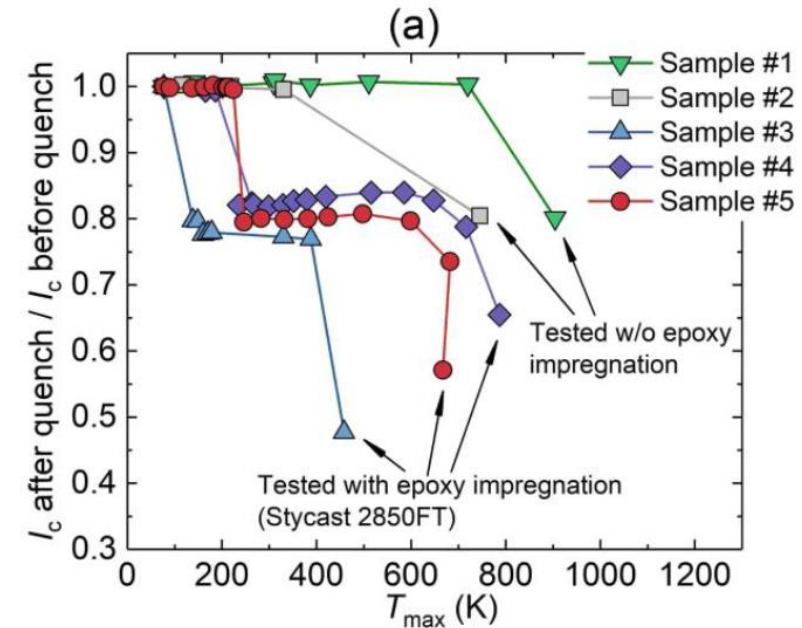
## REBCO tape + Stycast1266



## REBCO tape + Stycast2850 (filled resin)



## REBCO tape + Stycast2850 + quench

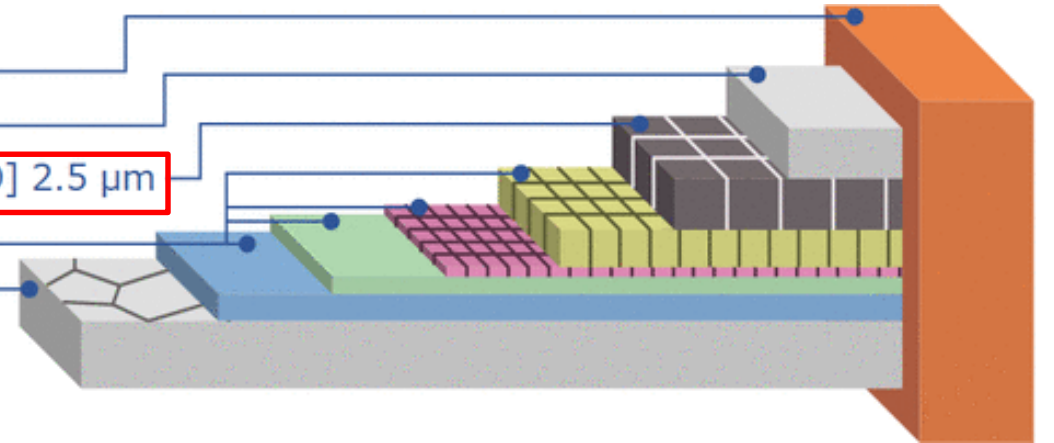


# Concluding remarks

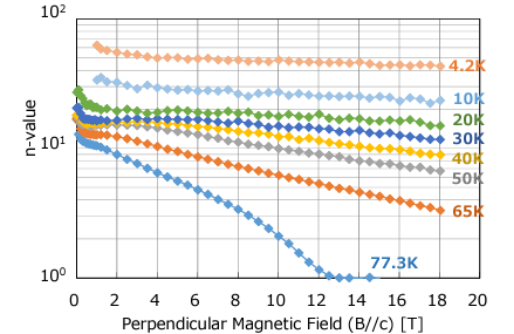
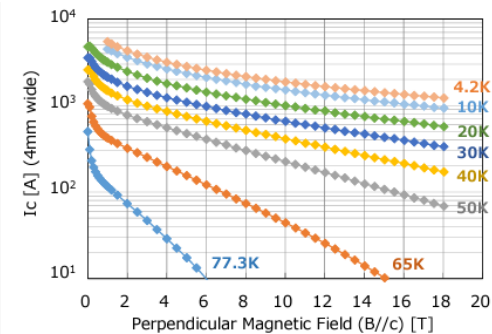
- **A tool developed for predicting SCIF for the upcoming US-Japan collaboration's test of KEK HTS coils at BNL.**
  - **Screening currents in HTS coils calculated by solving the T-A formulation.**
  - **The model was benchmarked with earlier measurement data at BNL.**
  - **Strong mechanical consequences.**
- **Experience with impregnating and quenching REBCO tapes**
  - **Further work needed to access the conductor limits.**

# HTS Tape

Stabilizer [Cu plating] 20 $\mu$ m  
 Protection layer [Ag] 2 $\mu$ m  
 Superconducting Layer [GdBCO] 2  $\mu$ m / **[EuBCO+BHO] 2.5  $\mu$ m**  
 Buffer layer [MgO, etc.] 0.7 $\mu$ m  
 Substrate [Hastelloy®] 75 / 50  $\mu$ m



Products	Width [mm]	Thickness [mm]	Substrate [ $\mu$ m]	Stabilizer [ $\mu$ m] *5	Critical Current [A] @77K, Self-field	Critical Current [A] @20K, 5T <sup>1/4</sup>	Remarks
FYSC-SCH04	4	0.13	75	20	$\geq 165$	368	Non-AP <sup>3</sup>
FYSC-SCH12	12	0.13	75	20	$\geq 550$	1,104	Non-AP <sup>3</sup>
FYSC-S12 *1	12	0.08	75	-	$\geq 550$	-	Non-AP <sup>3</sup>
FESC-SCH02	2	0.11	50	20	$\geq 30$	257	AP <sup>3</sup>
FESC-SCH03	3	0.11	50	20	$\geq 63$	497	AP <sup>3</sup>
FESC-SCH04	4	0.11	50	20	$\geq 85$	663	AP <sup>3</sup>
FESC-SCH04(05)	4	0.07	50	5	$\geq 85$	663	AP <sup>3</sup>
FESC-SCH12	12	0.11	50	20	$\geq 250$	1,990	AP <sup>3</sup>
FESC-S12 *1	12	0.06	50	-	$\geq 250$	-	AP <sup>3</sup>

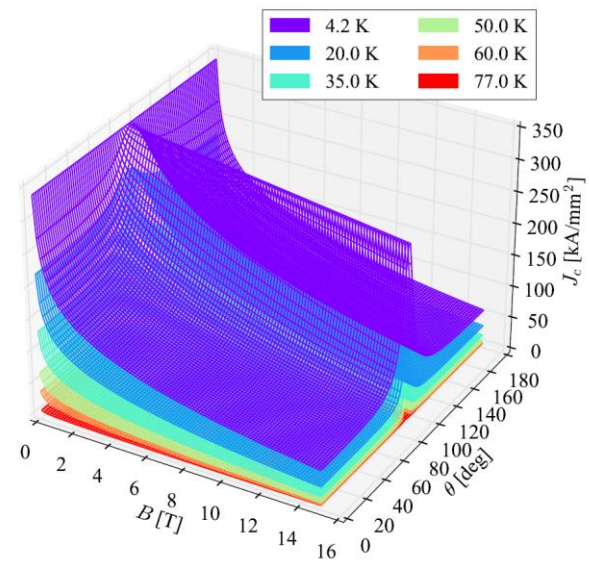
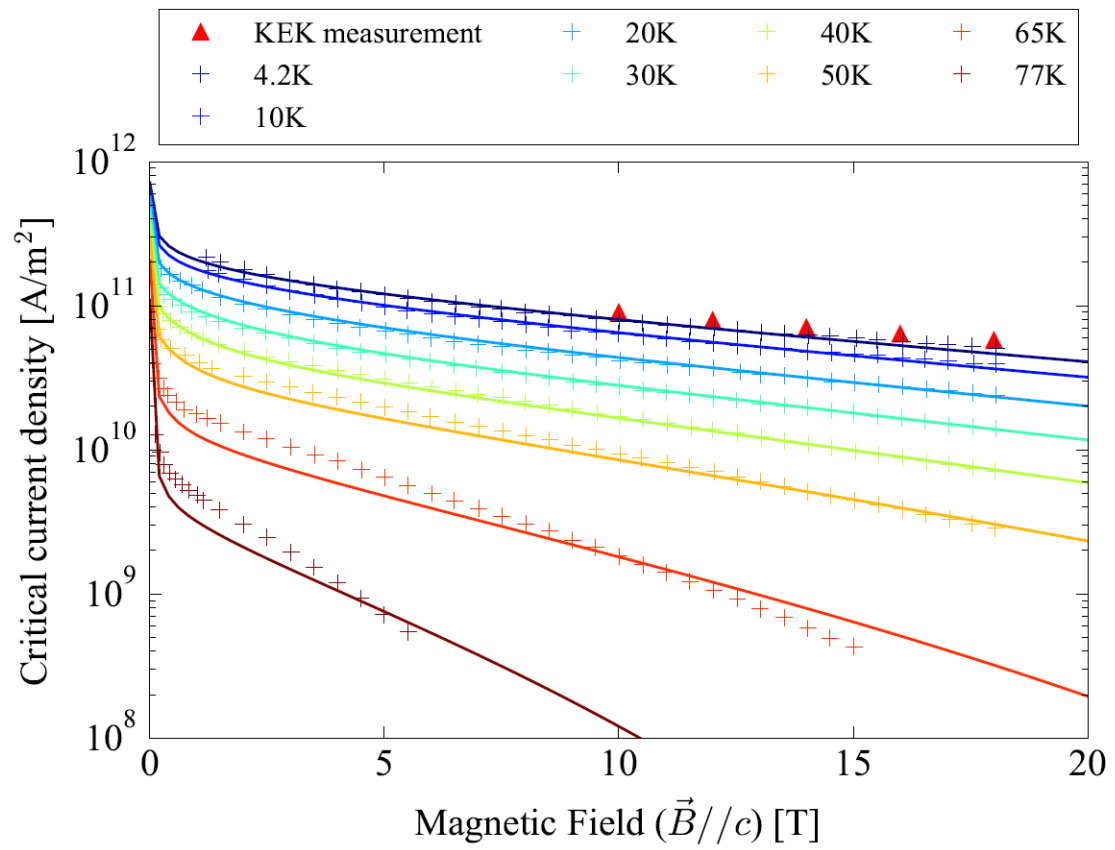


Sample:

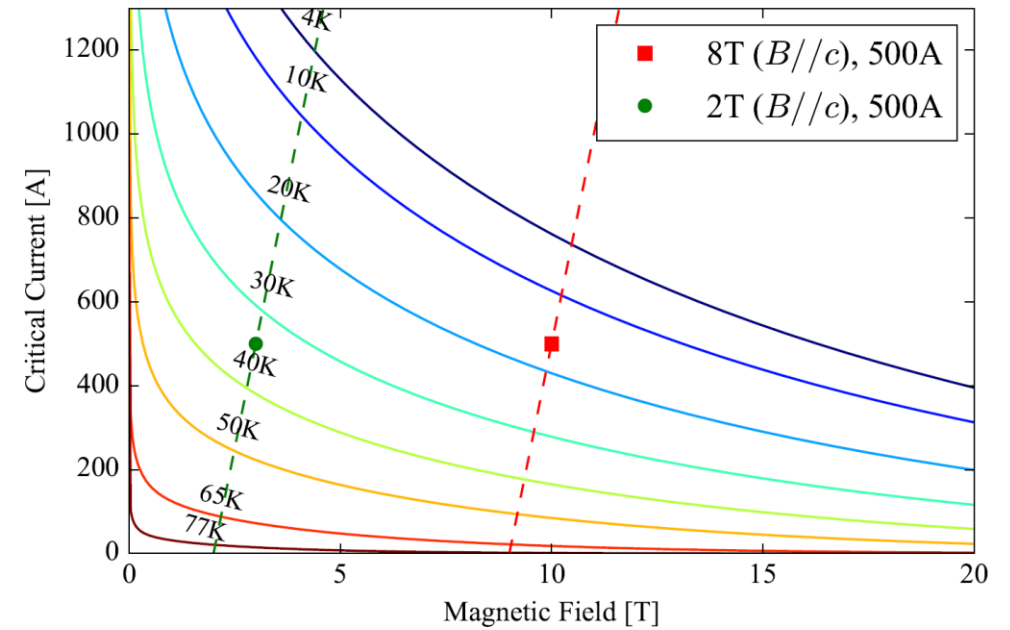
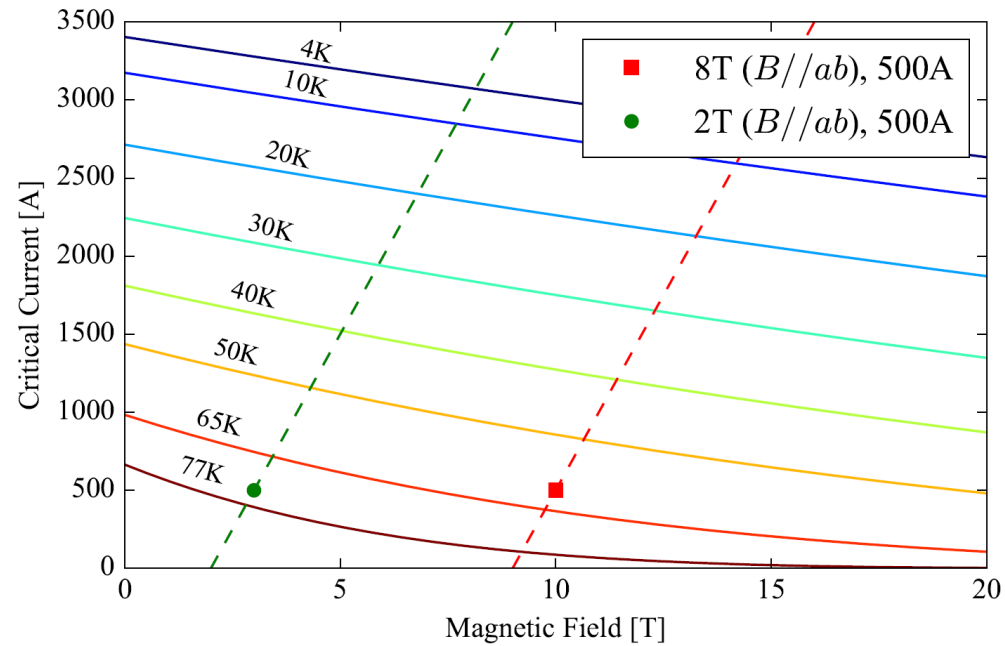
- Width: 10 mm, thickness: 2.4  $\mu$ m



### Fujikura measurements



# Short Sample Limit



- Still can test the HTS coil in the background field of 2T at 77K with 200A ( $B//ab$ )

# Thank You