



# Conductor and Cable Challenges and Opportunities: Cable Tests for Fusion

Daniel S. Davis

**REBCO Round Table, Fermilab**

November 2, 2023

Coil Group: U.P. Trociewitz, Y. Kim, G. Murphy, C.L. English, C.T. Brady, J. Kvitkovic, G. Miller, W.S. Marshall

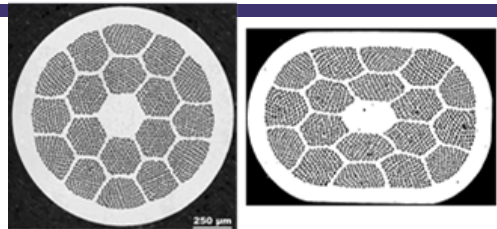
Conductor Group: E.E. Hellstrom, J. Jiang, F. Kametani, J. Lu, J. Levitan, P. Lee

Graduate Students: E. Martin, G. Bradford, S. Barua, A. Oloye

L. Cooley, D.C. Larbalestier

Key Collaborators - LBNL: T. Shen PPPL: Y. Zhai ACT: D.C. van der Laan, J Weiss, Z. Johnson, K Radcliff

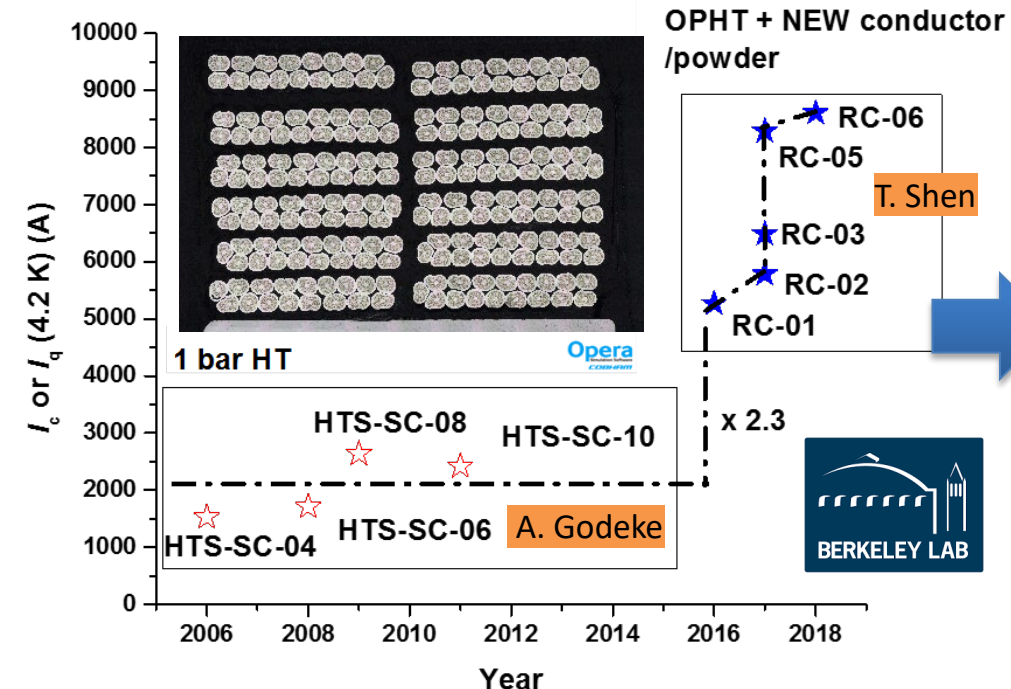
# Magnet Testing is The Bottleneck to Ultra-High Field Applications



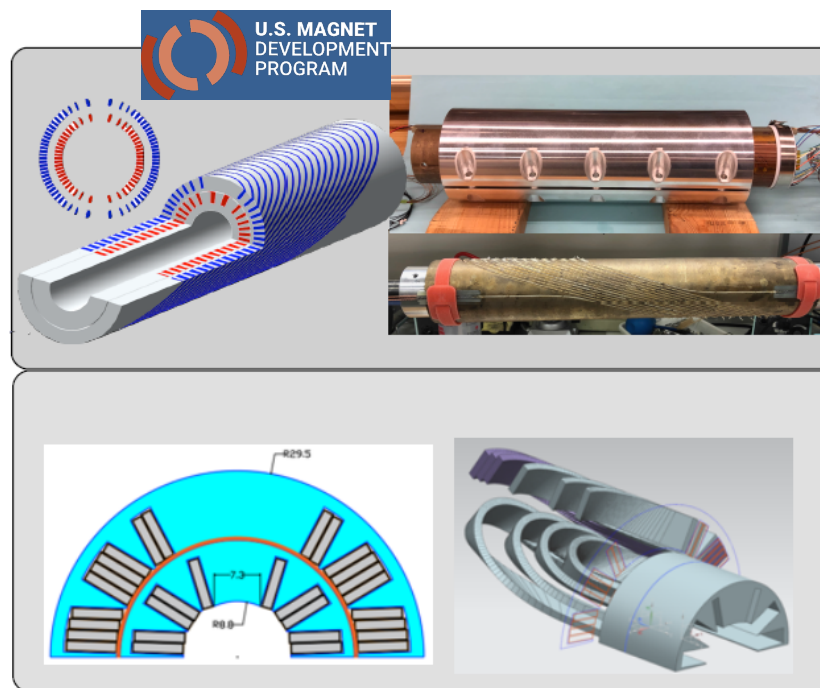
The recent developments of HTS Bi-2212 round wire and cable are clear examples of rapid progress with test coils

T. Shen-LBL

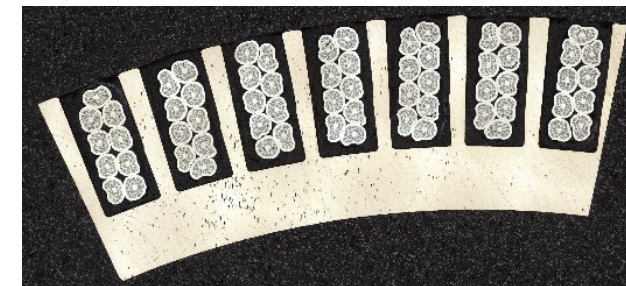
## HTS Racetrack Coils



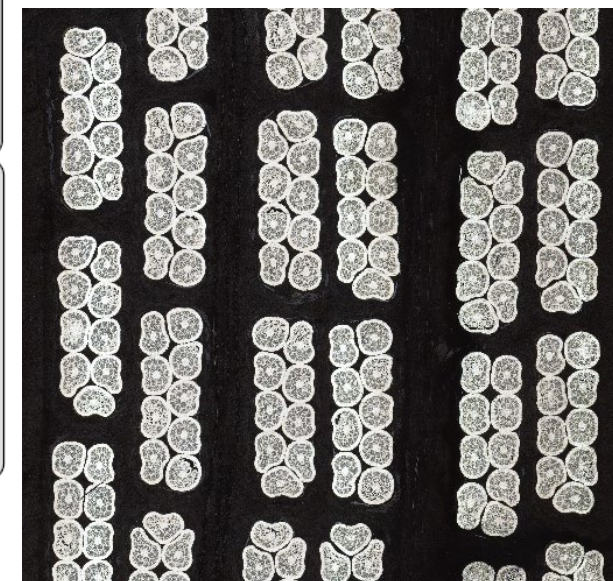
LBL-HTS-RC program: example of a simple-geometry coil series showing progressive performance and developing magnet technologies for 3D dipole geometries



Led to present MDP Bi-2212 program including Bi-2212 cable cosine-theta coils and high field solenoid testing and postmortems

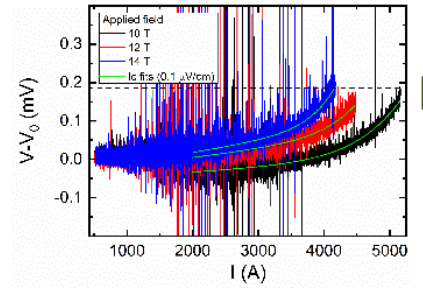
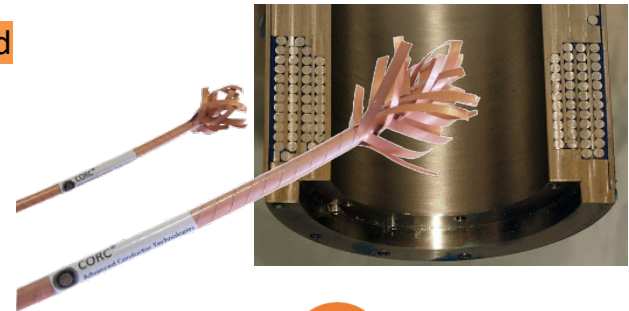
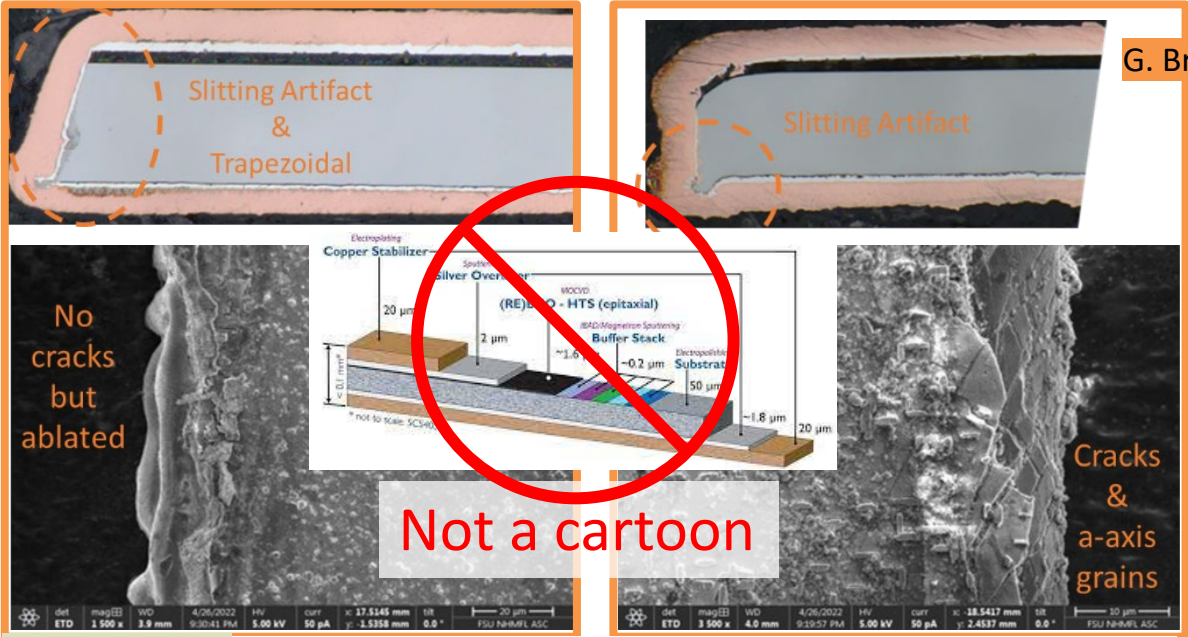


Bi-2212 Canted Cosine Theta Layer Cross Section



Bi-2212 Cable Solenoid Cross Section

# Conductor → UHF → Modelling → Cable/Solenoid → Postmortem Program

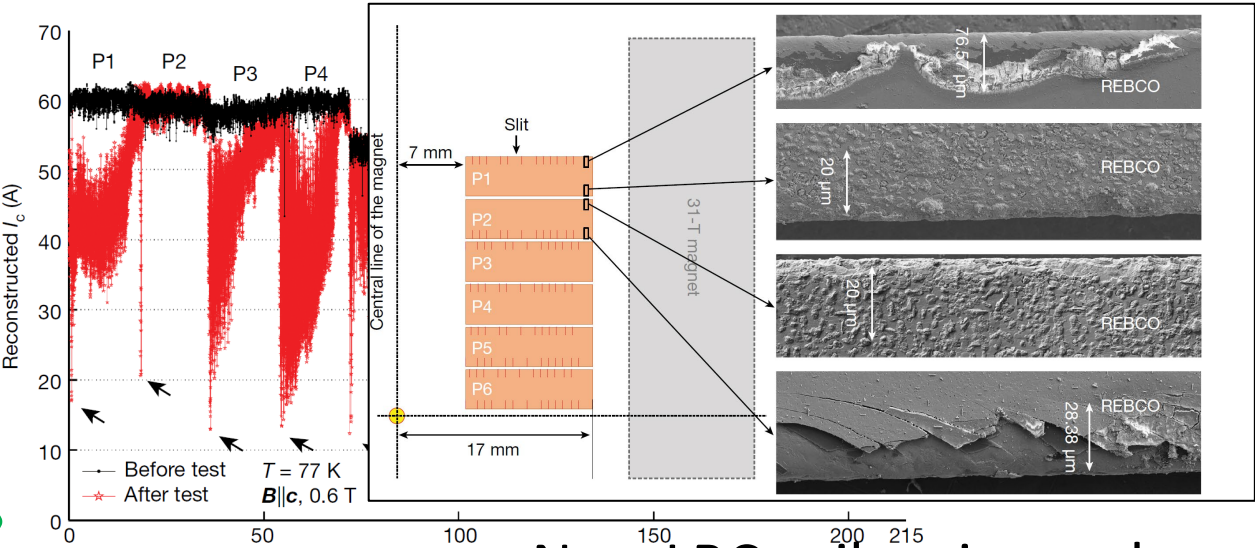
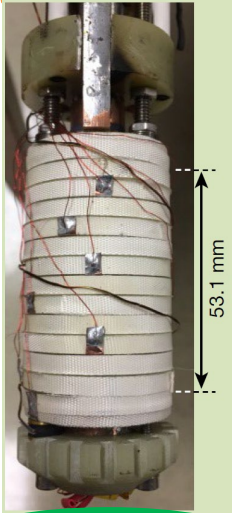
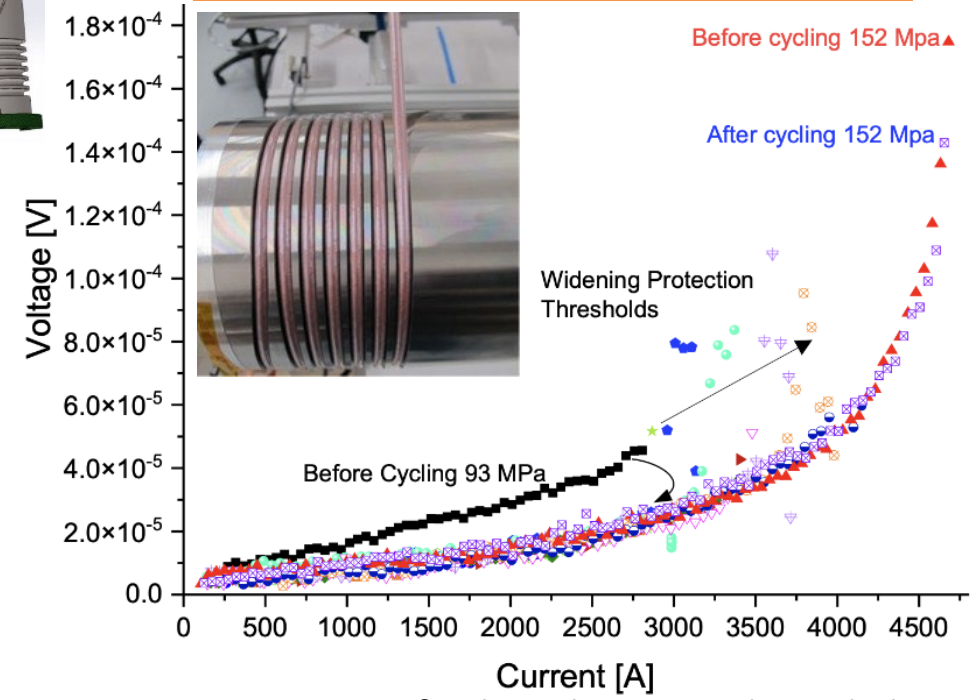


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Y. Zhai, D.C. van der Laan, D. Davis, U.P. Trociewitz

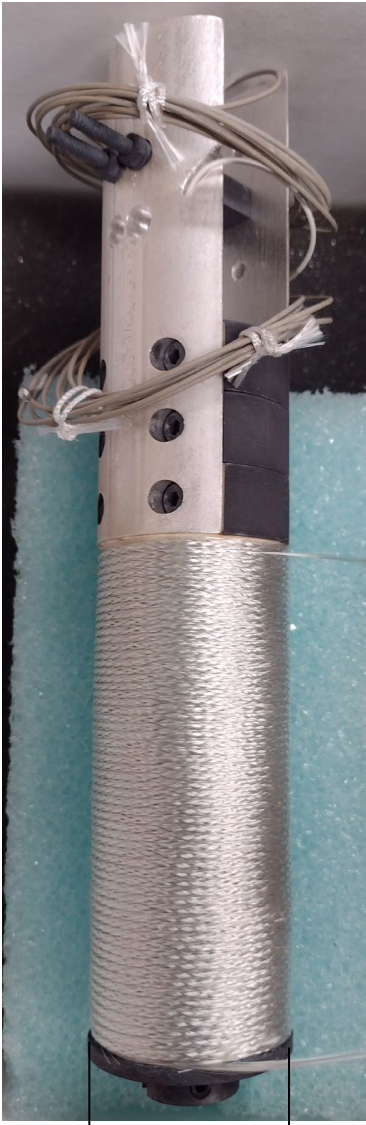


Hahn et al.

New LBC coil series underway!

2-Layer CORC® solenoid in grooved mandrel 12 T background field at 4 K

# Ultra-High-Field Solenoid Testing in the 31 T Resistive Magnet Demonstrates Conductor Capabilities and Magnet Technology



38 mm

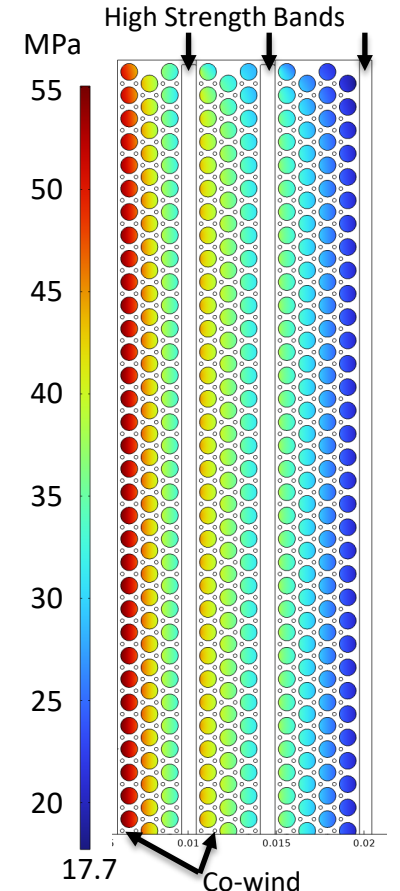


Over-banding

Like the LBCs, TEO-type coils are a cost-efficient vehicle to test materials and processes

Coil Specs:

Coil Name		TEO 1	TEO 2	TEO 3
Wire	PMM No.	PMM180928 ( $\Phi$ 1.0 mm)		
	Insulation	TiO2 coat – Mullite Braid ( $\Phi$ 1.3 mm)		
ID; OD; Height [mm]		12.0; 34.2; 80.9	12.0; 37.5; 80.4	12.0; 37.4; 88.6
Turn ; Layer (Total)		60.3 ; 8 (482)	59.2 ; 10 (592)	59.1 ; 10 (591)
Innerbands		2 (Band)	2 (Band)	2 (Wind)
Overband		Hastelloy C276	Hastelloy C276	Inconel X750
Conductor		35 m	45 m	45 m
Field Const.		7.2 mT/A	8.8 mT/A	8.1 mT/A
Inductance		1.0 mH	1.7 mH	1.5 mH
Ic Test at 12 T		> 500 A	> 500 A	270 A



Stress with Reinforcement

peak source hoop stress ( $J_E * B * R$ ) between **237 - 273 MPa**

# Ultra-High-Field Solenoid Testing in the 31 T Resistive Magnet Demonstrates Conductor Capabilities and Magnet Technology

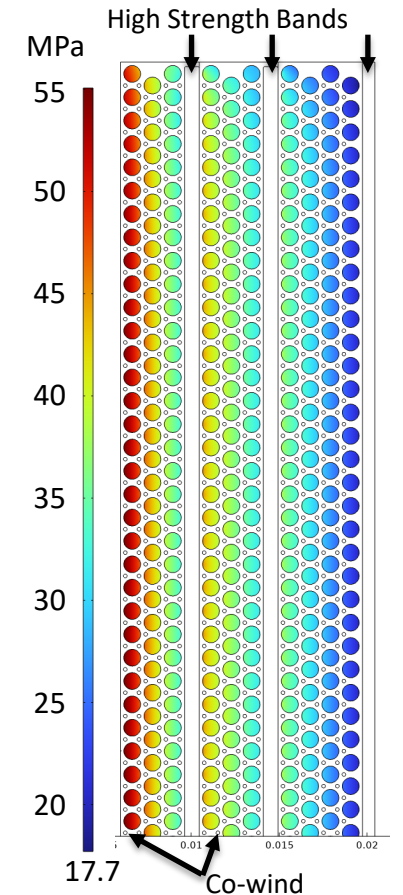


Next generation scientist, Teo Kim with "Teo-2"

Like the LBCs, TEO-type coils are a cost-efficient vehicle to test materials and processes

Coil Specs:

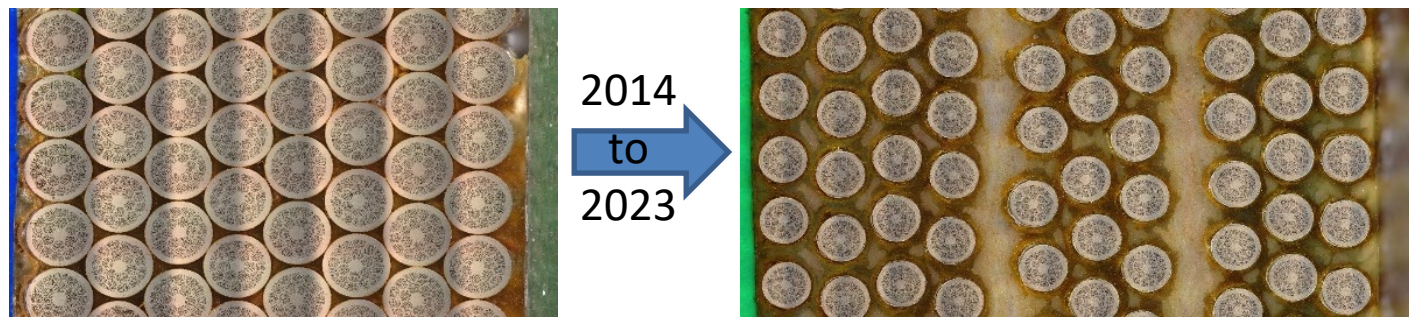
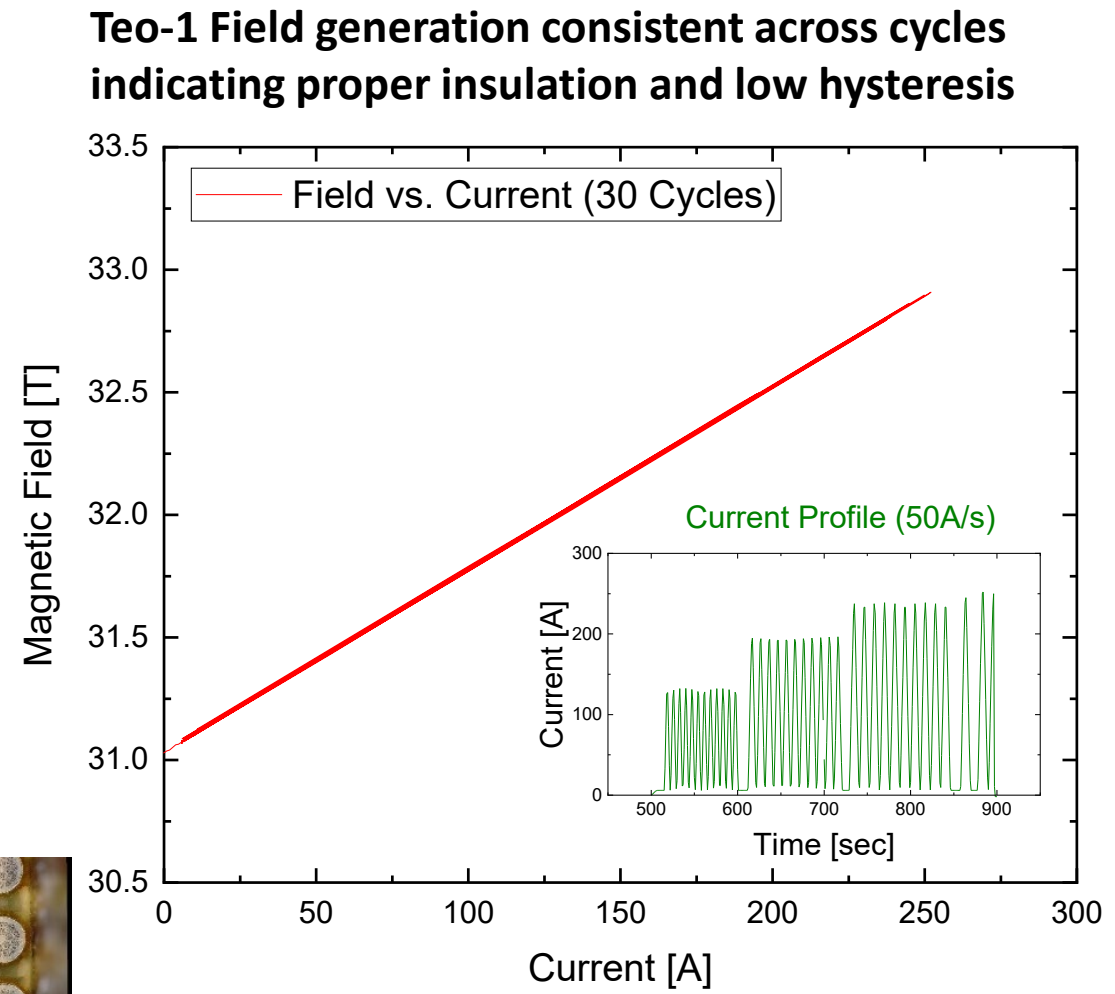
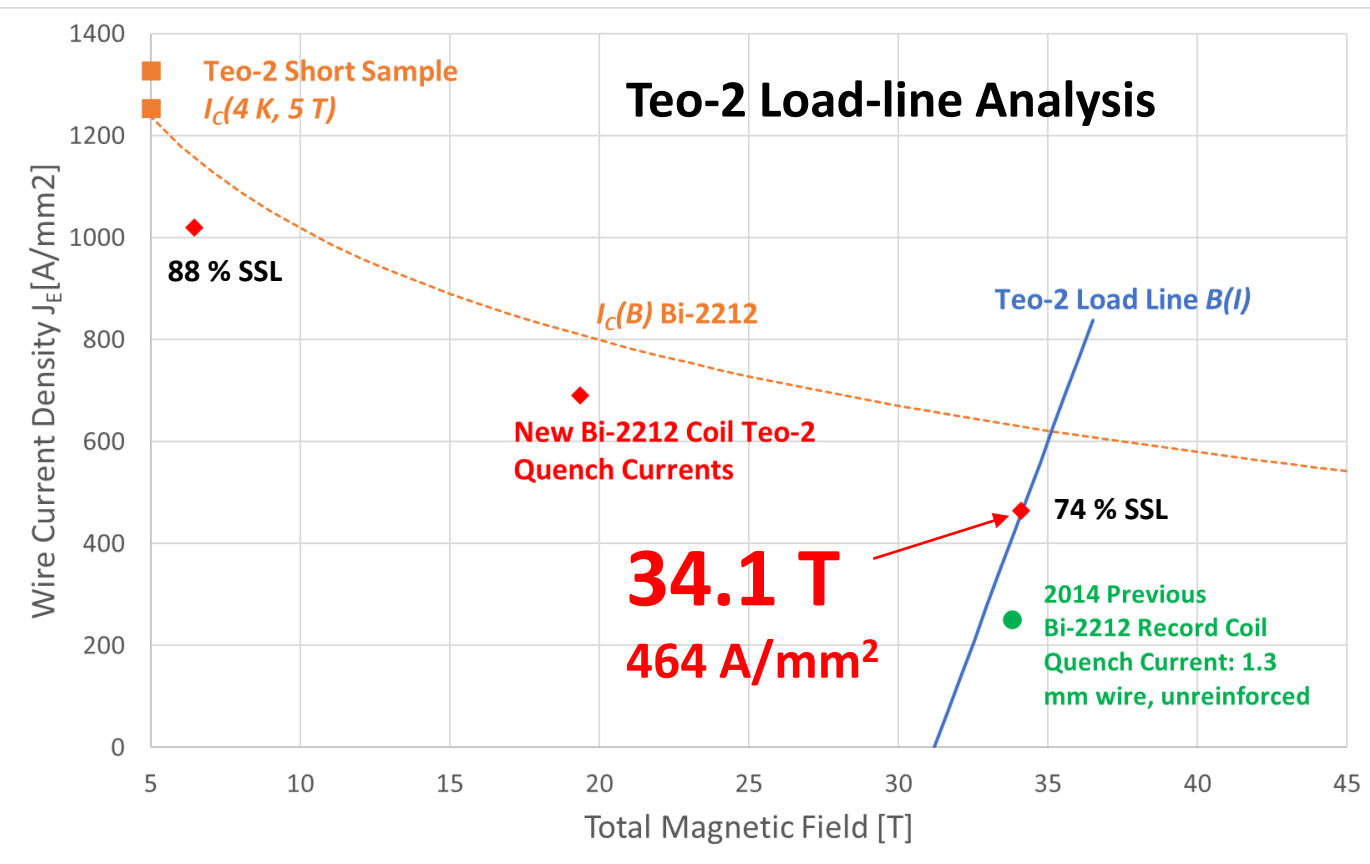
Coil Name		TEO 1	TEO 2	TEO 3
Wire	PMM No.	PMM180928 (Φ1.0 mm)		
	Insulation	TiO2 coat – Mullite Braid (Φ1.3 mm)		
ID; OD; Height [mm]		12.0; 34.2; 80.9	12.0; 37.5; 80.4	12.0; 37.4; 88.6
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Stress with Reinforcement

peak source hoop stress ( $J_E * B * R$ ) between **237 - 273 MPa**

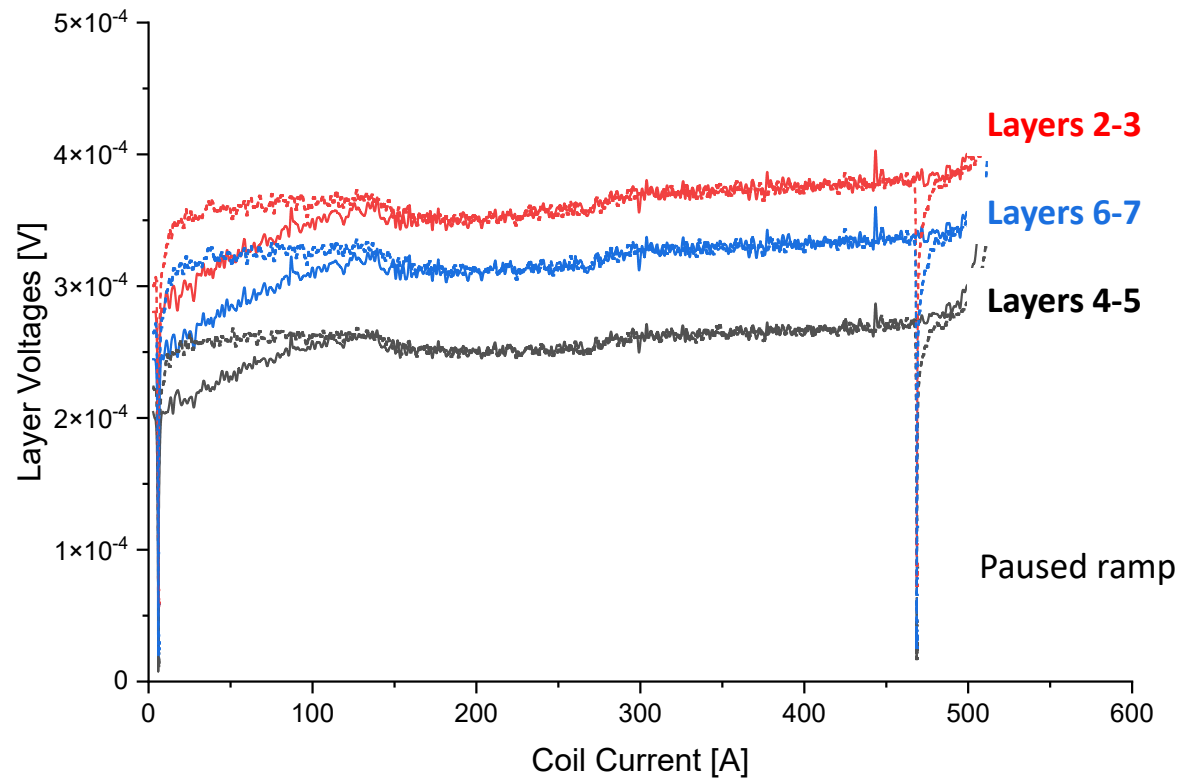
# Robust Operation of High Temperature Superconducting Bi-2212 Magnets at 34 T and Ramp Rates Over 23 T/s !



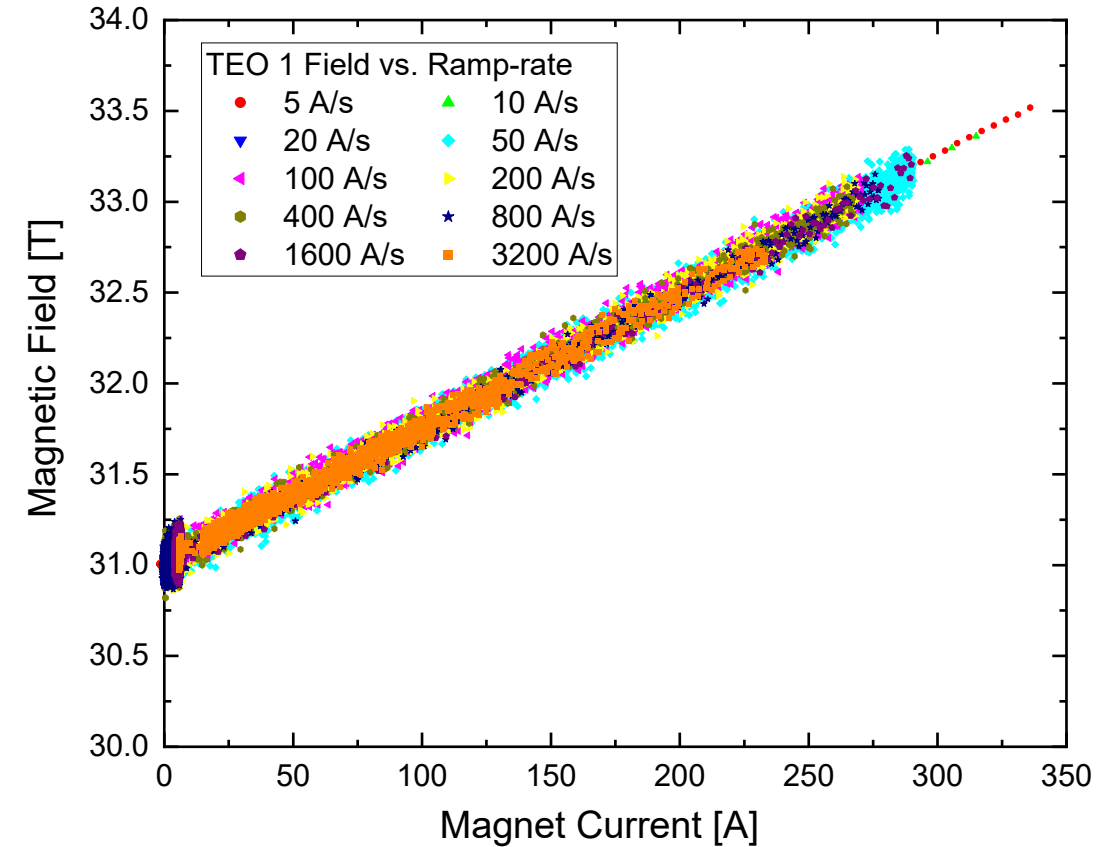
# Robust Operation of High Temperature Superconducting Bi-2212 Magnets at 34 T and ramp rates over 23 T/s



Teo-1 V-I curves (4 K, 15 T)  
before(dotted) & after(solid) high-rate tests at 31 T

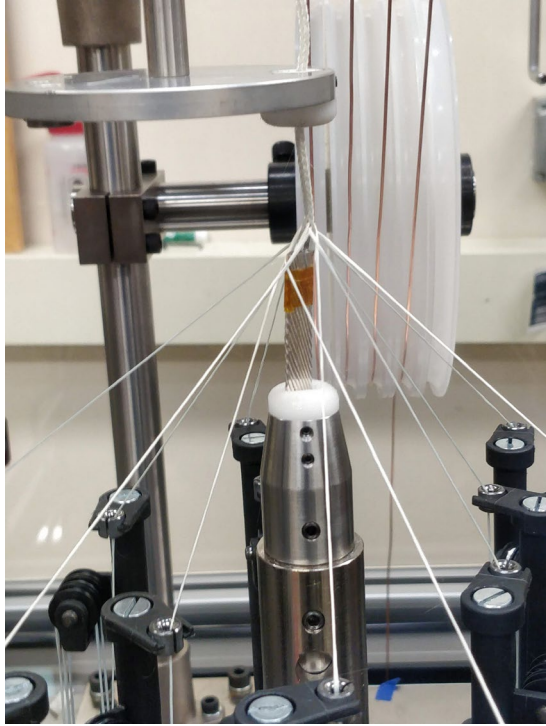


Teo-1 Field generation consistent across ramp rates indicating proper insulation



This robust operation of multiple coils in fields >30 T is an important demonstration to our collaborators including commercial partners Cryomagnetics Inc. and Oxford Instruments (OI) developing compact 25 T class research magnets, the US-DOE Magnet Development Program developing hybrid HTS/LTS 16 T dipoles, and Princeton Plasma Physics Laboratory (PPPL) pursuing fusion ohmic heating solenoids, as well as our own efforts at ASC towards >1.2 GHz NMR with an NIH-R01 submission.

# Implementing New Insulation in Rutherford Cables Magnets



**First 17 strand cable length insulated with pure alumina**

**9-strand Bi-2212 Rutherford cable is a surprisingly flexible and easy to work with conductor**

Specs.:

9 strand (4 x 1.44 mm bare)

1500 denier

12-thread, 16 ppi

0.15 mm thick on flat side

0.2 mm thick on edges



Pure alumina braid

Inconel compression blocks

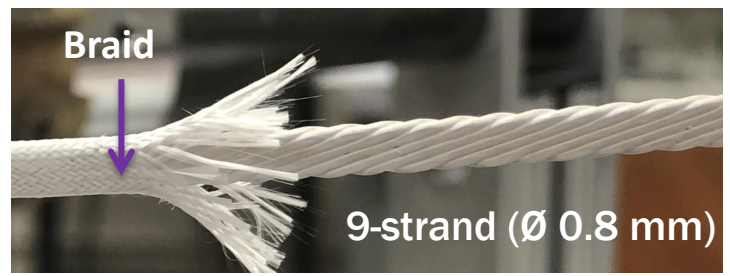
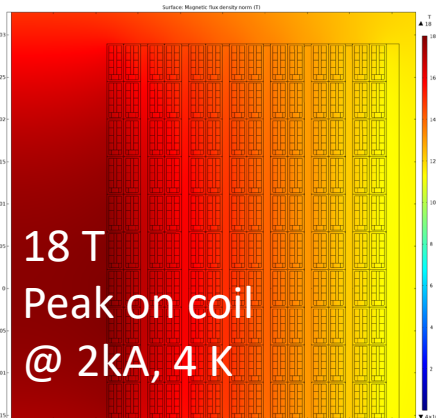
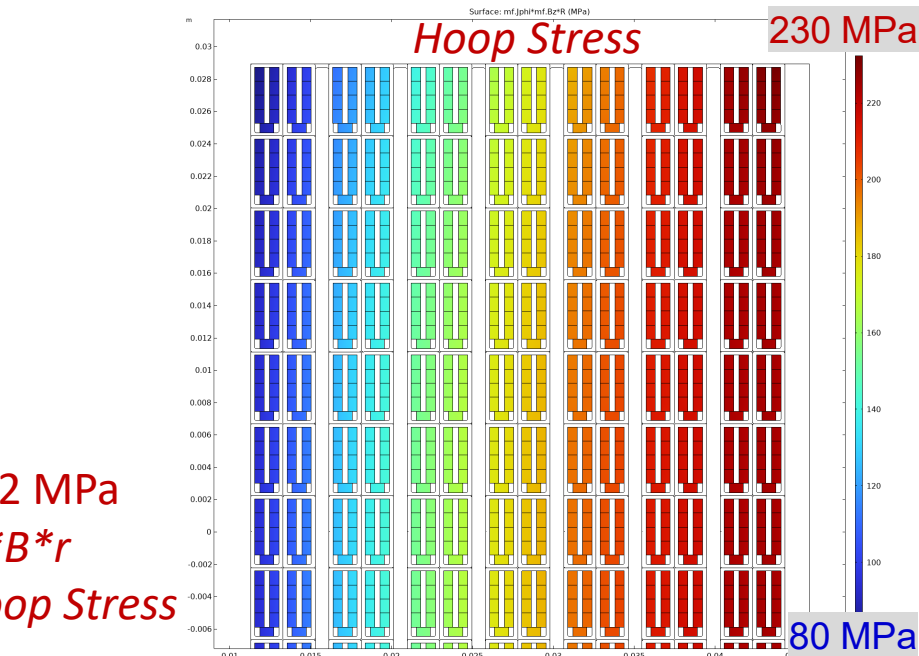
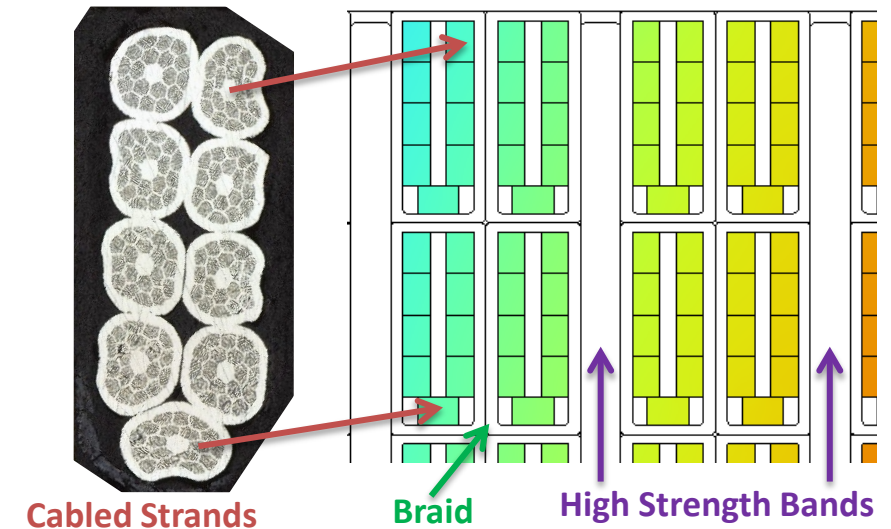
- **No leakage in fully OPHT'ed Rutherford cable sample with pure alumina braid**
- **Very little to no embedding of fiber in Ag-matrix**



# ~5 T Rutherford Cable Solenoid to Validate Alumina Braid Insulation



Bi-2212 Rutherford (BR) Cable Solenoids			
		BR-1	BR-2
Wire	Product No.	PMM170725	PMM130723-1
	Powder	nGimat (85 x 18)	Nexans (37 x 18)
	Insulation	In-house coating(no top-coat)+mullite braid	Pure Alumina (Nextel) Braid
	Diameter [mm]	Φ 0.8 (bare)	Φ 0.8 (bare)
Cable	ID	LBNL-1093	LBNL-1075
	Size, uses (length)	9-Strand, CCT leftover (8.5 m)	9-strand, winding/insulation tests (31 m)
	Geometry	4.0 x 1.44 mm (bare) / 4.38 x 1.82 mm (ins.)	4.0 x 1.44 mm (bare) / 4.4 x 1.74 mm (ins.)
ID ; OD ; Height [mm]		44.45 ; 69.67 ; 26.29	24.0 ; 84.5 ; 55.0
Turn ; Layer (Total)		6 ; 6 (36)	12.5 ; 14 (175)
Magnet constant [mT/A]		0.708	2.876
Inductance [mH]		0.064	0.7
Conductor length [m]		6.5	30
Status		Tested	Final Design and Test Winding



# Unique HTS Test-bed : 161 mm, 12 T LTS, 10 kA



## 12 T HTS Coil Test Bed

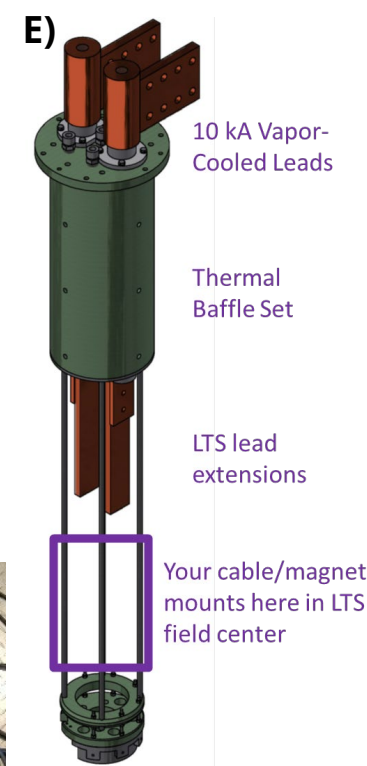
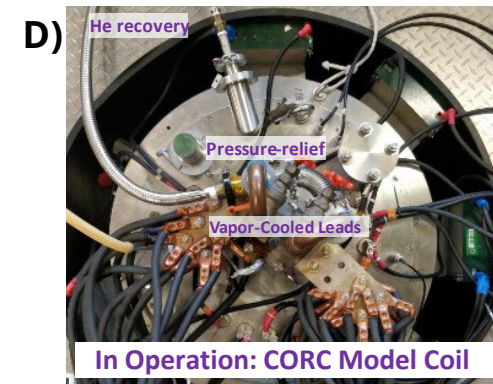
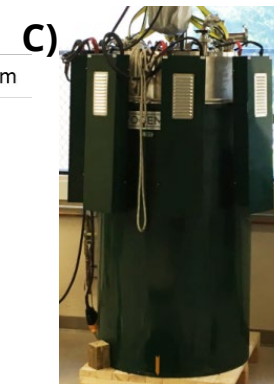
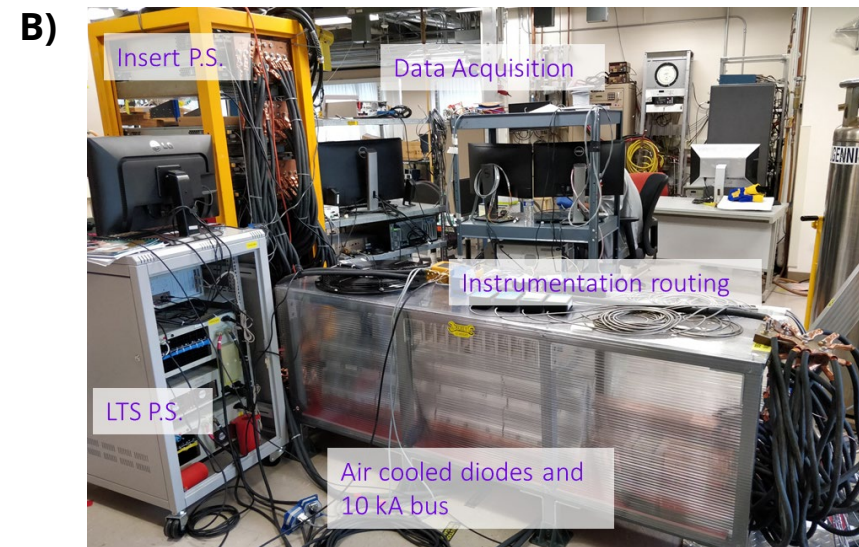
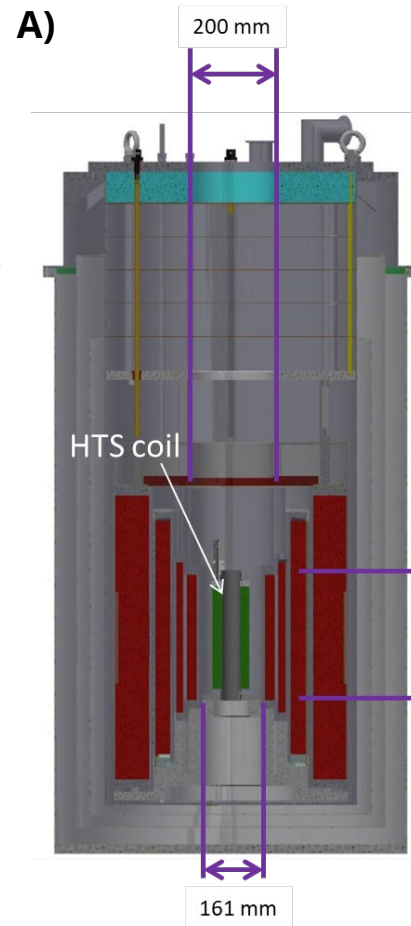
- 10 kA bus, 8 x 1.2 kA power supplies
  - Enables individual cable and cable magnet testing
- Magnet bore 161 mm, 200 mm access bore for leads, 128 ppm uncorrected homogeneity (1 cm DSV)

Large bore enables insert magnets:

- To explore field generation and mechanical limits in strand-wound and cable wound coils
- To add additional means to improve field homogeneity (e.g., compensation coils, shims etc.)
- Implement novel HTS quench management

Features

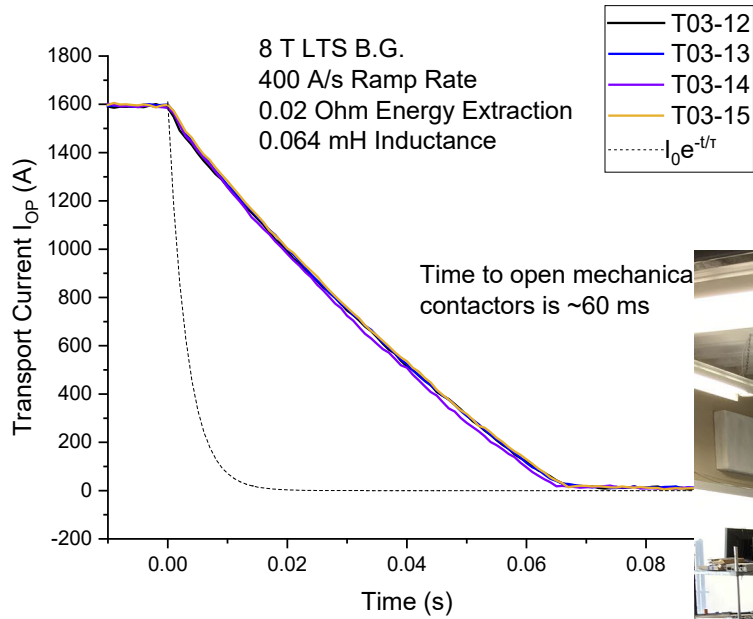
- 1 kA, 7.5 kA, and 10 kA VCL probes
- FPGA control and IGBT quench management
- Variable dump resistors and varistors



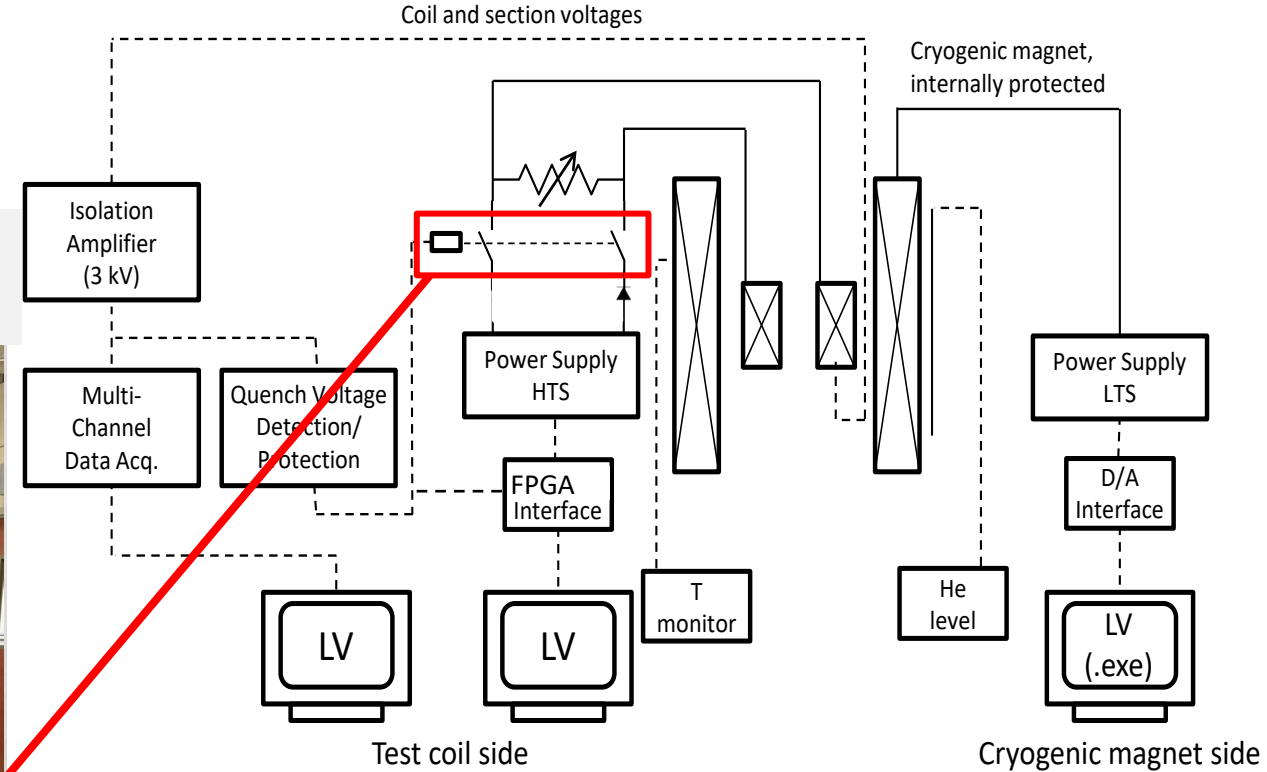
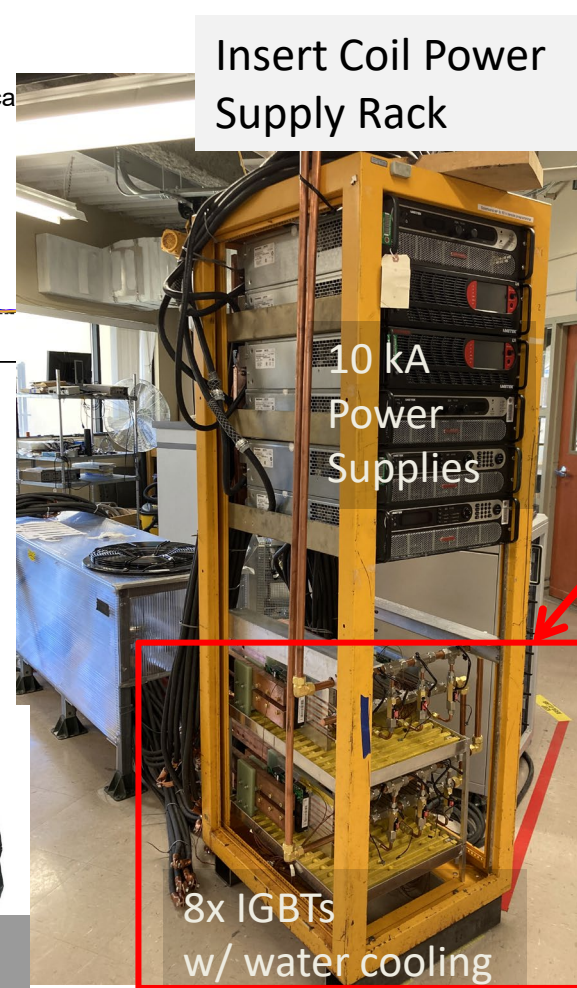
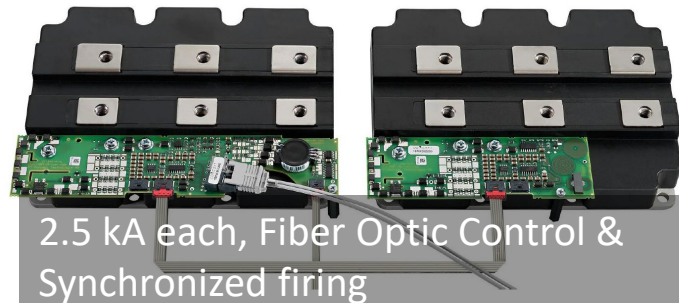
**A)** Schematic of the 12 T LTS (red) magnet with a 200 mm probe access and a 161 mm cold bore for HTS insert (green); **B)** Picture of the LTS & HTS support systems; **C)** Picture of the 12 T magnet cryostat with external protection elements; **D)** Picture of the top plate of the 12 T magnet during a recent test of an HTS Bi-2212 Rutherford cable solenoid; **E)** Schematic of the 10-kA vapor-cooled-lead probe being prepared



# IGBT Quench Circuit Upgrade



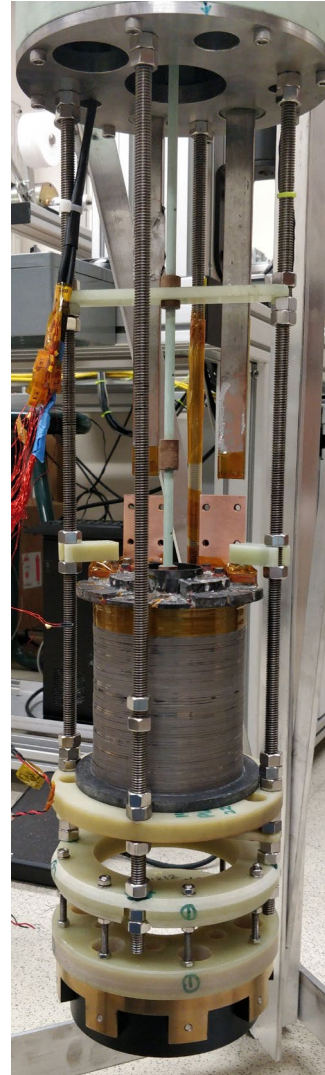
Cable solenoid protection speeds were limited by hardware limits of mechanical contactors rather than the coil inductance or peak voltage.



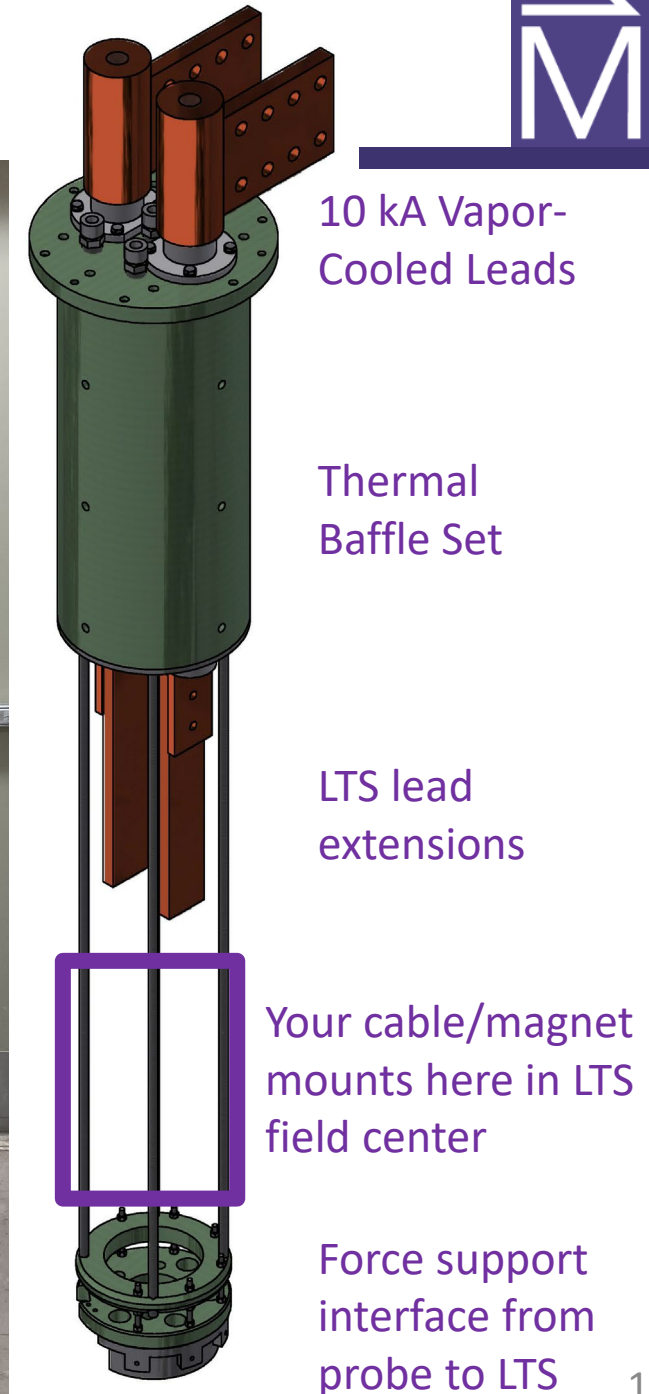
# Cable-Coil/Sample Test Platforms



- A probe with 10 kA helium vapor cooled leads is ready to operate inside our 14 T, 161 mm large bore magnet
- Will accommodate Bi-2212 as well as ReBCO cable coils/samples
- We have existing 7.5 kA and 1 kA probes for lower current cables and wires with reduced heat load on the system.



Recent Bi-2212 strand solenoid test



# High-field insert solenoid wound from CORC<sup>®</sup> cables

## Addresses main challenges of low-inductance HTS magnets

- Operate CORC<sup>®</sup> insert solenoid in **14 T background field**
- CORC<sup>®</sup> insert should have meaningful bore: 100 mm diameter
- High operating current: **4,000 – 5,000 A**
- $J_e > 200 \text{ A/mm}^2$
- Operate at **JBr source stress >250 MPa**

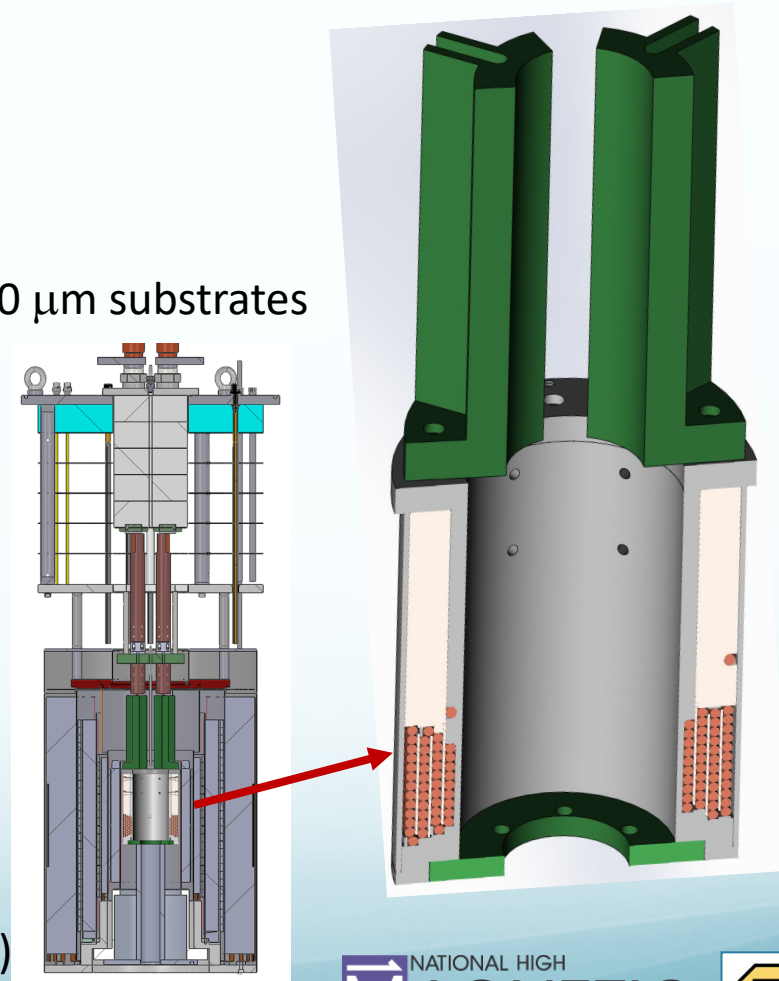
## CORC<sup>®</sup> cable layout

- 28 REBCO tapes of 3 mm width containing 30  $\mu\text{m}$  substrates
- 4.56 mm CORC<sup>®</sup> cable outer diameter

## CORC<sup>®</sup> insert layout

- 100 mm inner diameter, 143 mm OD
- 4 layers, 45 turns
- 18.5 m of CORC<sup>®</sup> cable
- Wet-wound with Stycast 2850
- Stainless steel overbanding between layers

14 T LTS  
(161 mm bore)



Danko van der  
Laan et al.,  
CCA21, October  
14th, 2021

This work was in part supported by the US Department of Energy under agreement numbers DE-SC0009545, DE-SC0014009 and DE-SC0021710.



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# CORC<sup>®</sup> insert solenoid test: summary

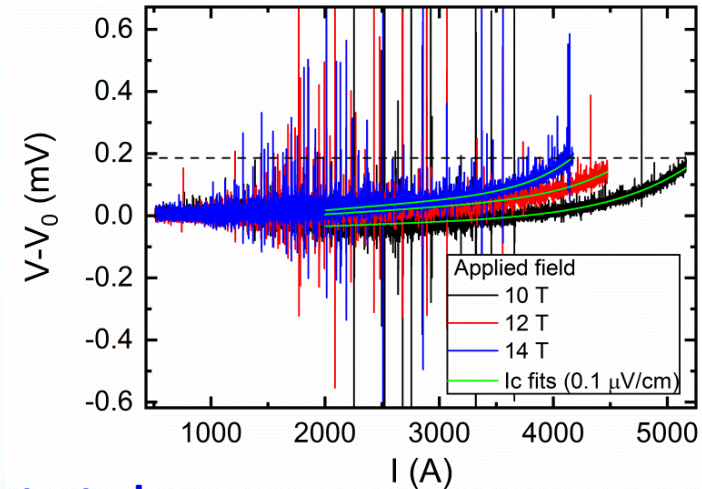
## CORC<sup>®</sup> insert impact

- First HTS insert magnet tested at high current (>1 kA) in a background field
- Stable operation likely due to current sharing between tapes in the CORC<sup>®</sup> cable
- Combination of high  $I$ ,  $J_w$  and JBr demonstrated at 16.8 T peak field

Applied field [T]	Central field at $I_c$ [T]	Peak field at $I_c$ [T]	$I_c$ (0.1 $\mu$ V/cm) [A]	$n$ -value [-]	$J_w$ [A/mm <sup>2</sup> ]	$J_e$ [A/mm <sup>2</sup> ]
10	12.25	13.35	5,315	7.9	203.9	340.3
12	14.08	15.09	4,908	9.1	188.3	314.2
14	15.86	16.77	4,404	10.5	168.9	281.9

D. C. van der Laan, et al.,  
Supercond. Sci. Technol. (2020)

<https://doi.org/10.1088/1361-6668/ab7fbe>



## First high-current CORC<sup>®</sup> insert solenoid successfully tested

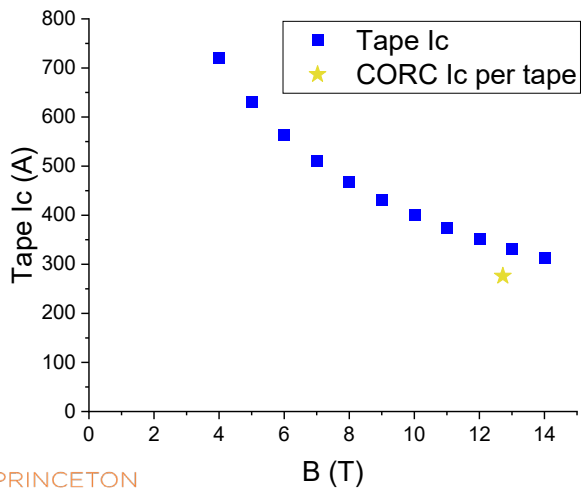
- Operation at over 4.4 kA in 14 T background field, generating a peak field of 16.77 T
- Operated at 282 A/mm<sup>2</sup> and 275 MPa JBr source stress at 14 T background field

## Conductor challenges when going to higher field and larger coil diameters

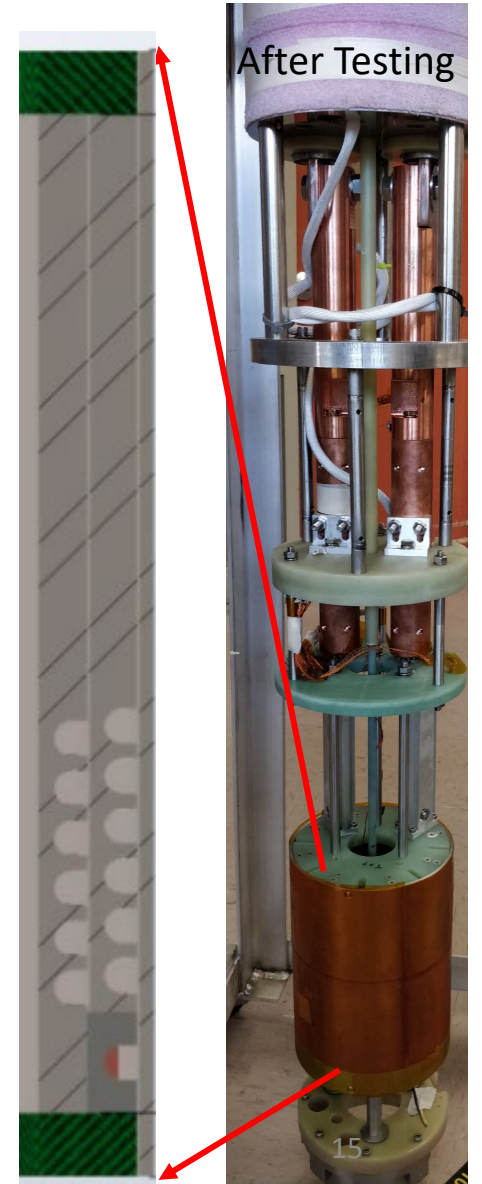
- A Central Solenoid in a future compact fusion reactor may have a JBr of 200 A/mm<sup>2</sup> x 20 T x 0.2 m = 800 MPa (source stress)
- How to further optimize the CORC<sup>®</sup> conductor to allow higher hoop stress, but also a higher irreversible strain limit?

# Fatigue testing a Prototype Ohmic Heating (OH) CORC Cable Solenoid

Prototype Ohmic Heating CORC Cable Solenoid		
Cable	Product No.	ACT- CORC, 20191113-3
	Tape	SP M4-534-105 0508
	Insulation	Heat Shrink + Kapton between Cu tape and cable
	Diameter [mm]	5.86
ID ; OD ; Height [mm]		119; 152; 60
Turn ; Layer (Total)		6; 2 (12)
Magnet constant [mT/A]		0.102
Inductance [mH]		~ 0.019
Conductor length [m]		5.1
Status		Tested

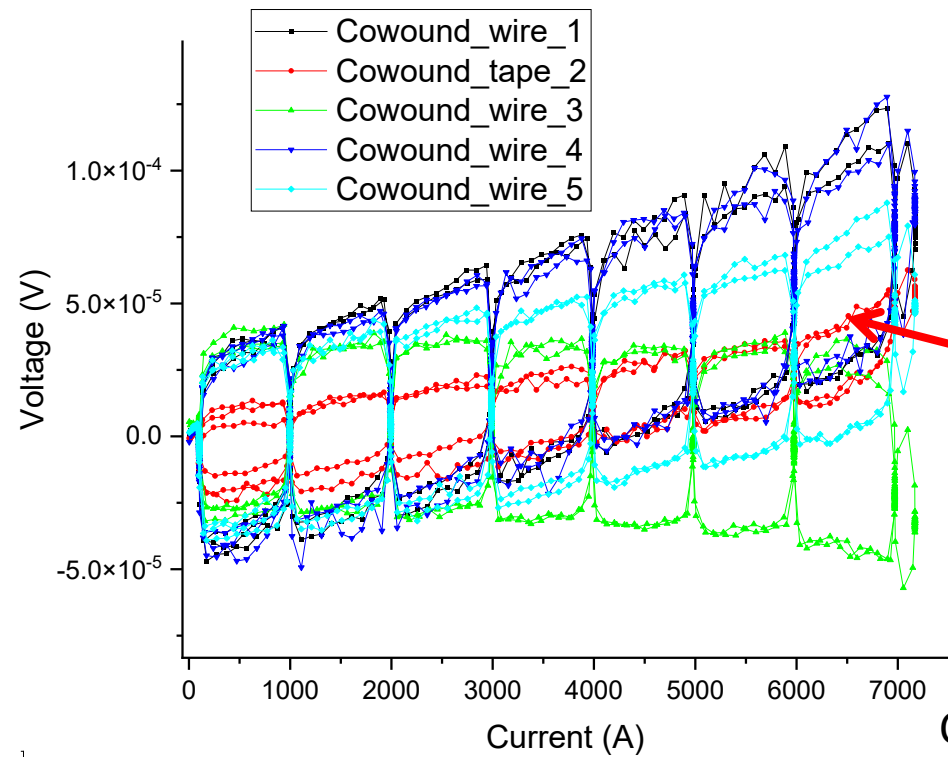


Fatigue Test	Cycles	$B_{app}$ [T]	Peak JBr stress [MPa]	Min cycle $I_{op}$ [A]	Max cycle $I_{op}$ [A]
1	69	5	79	2200	5000
2	50	10	101	2000	3200
3	127	12	107	1600	2800
4	67	12	173	3400	4600

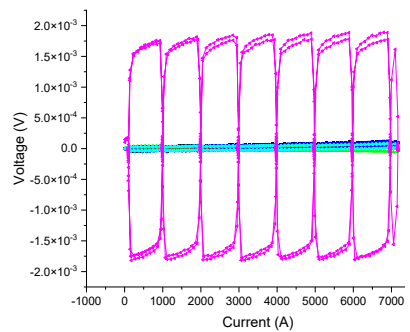
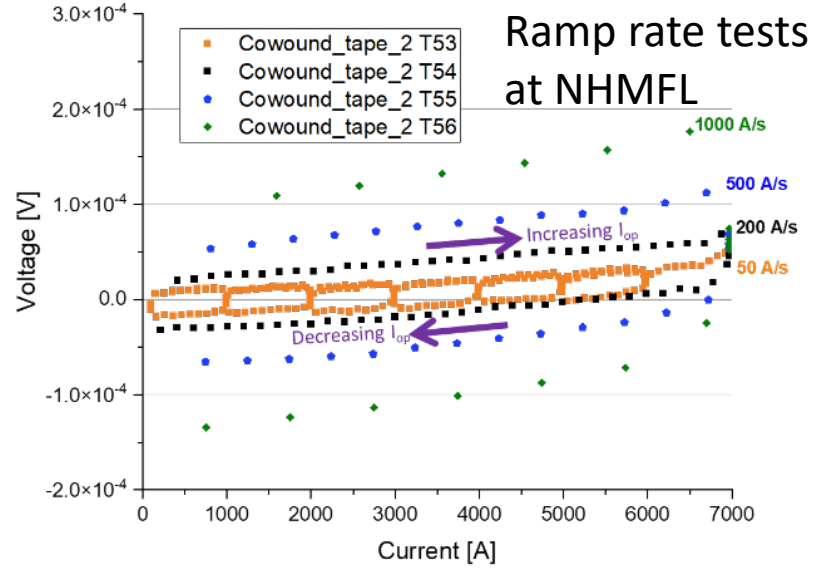




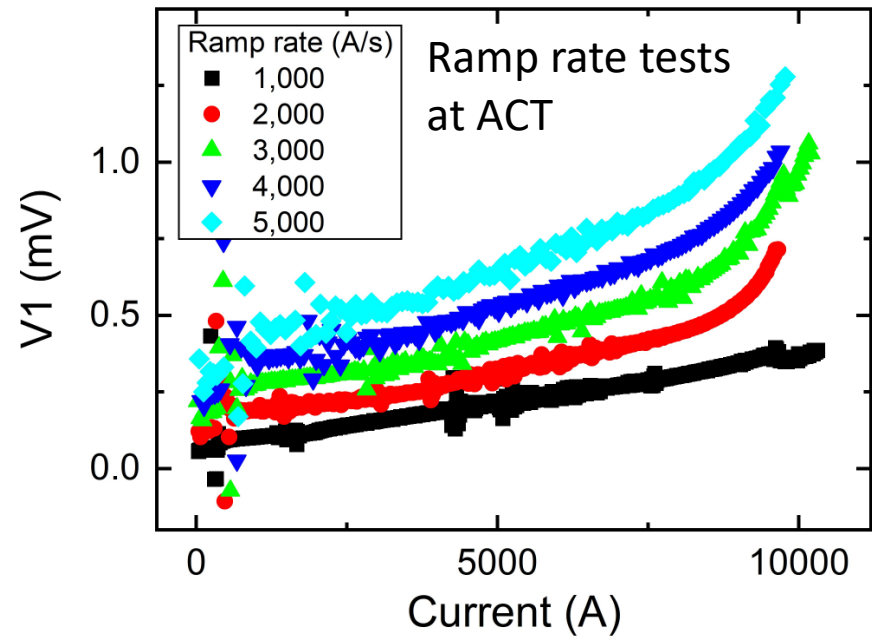
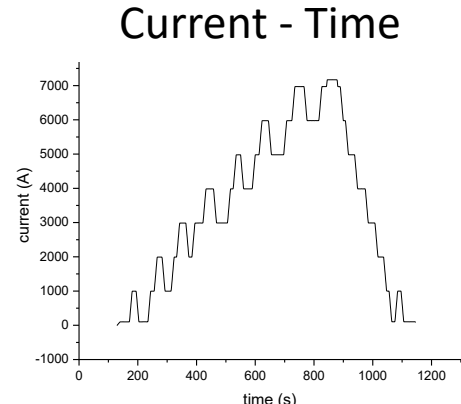
# 4 K self-field testing demonstrated fast ramp rates with stable operation despite effects of magnetization and motion on voltages



Co-wound Tape-2 provided the best indicator of cable transition



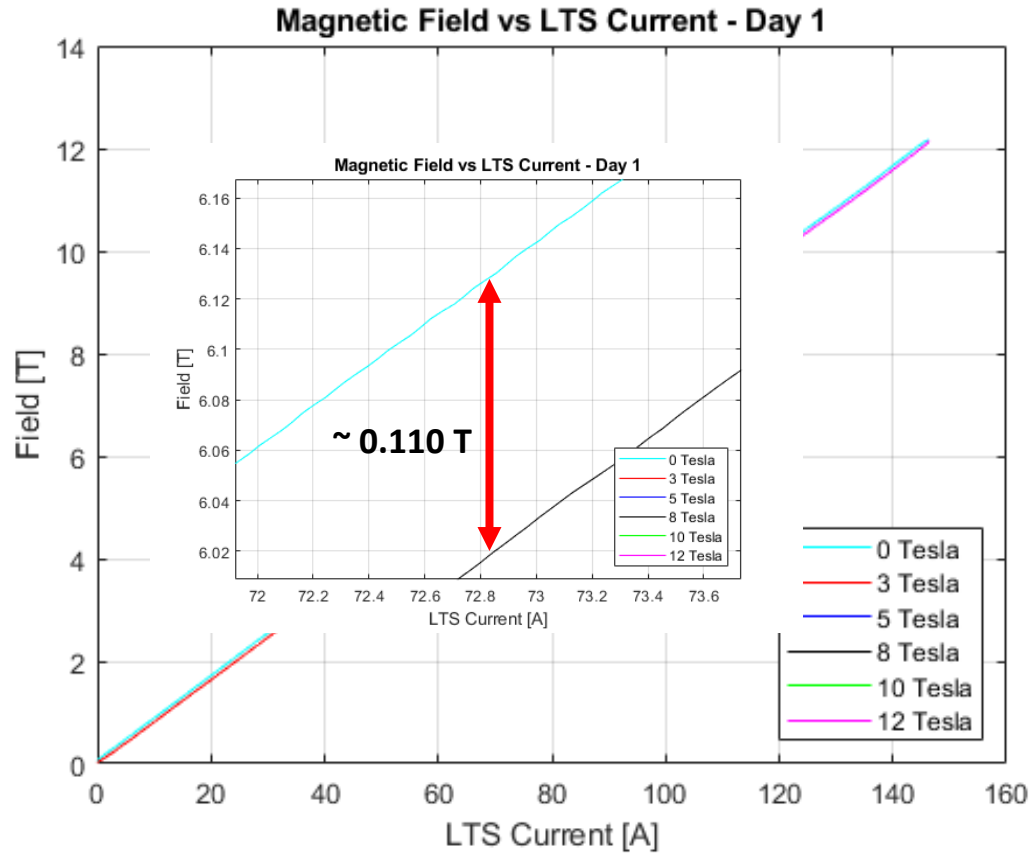
Not co-wound  
Wire-7: Inductance dominates response



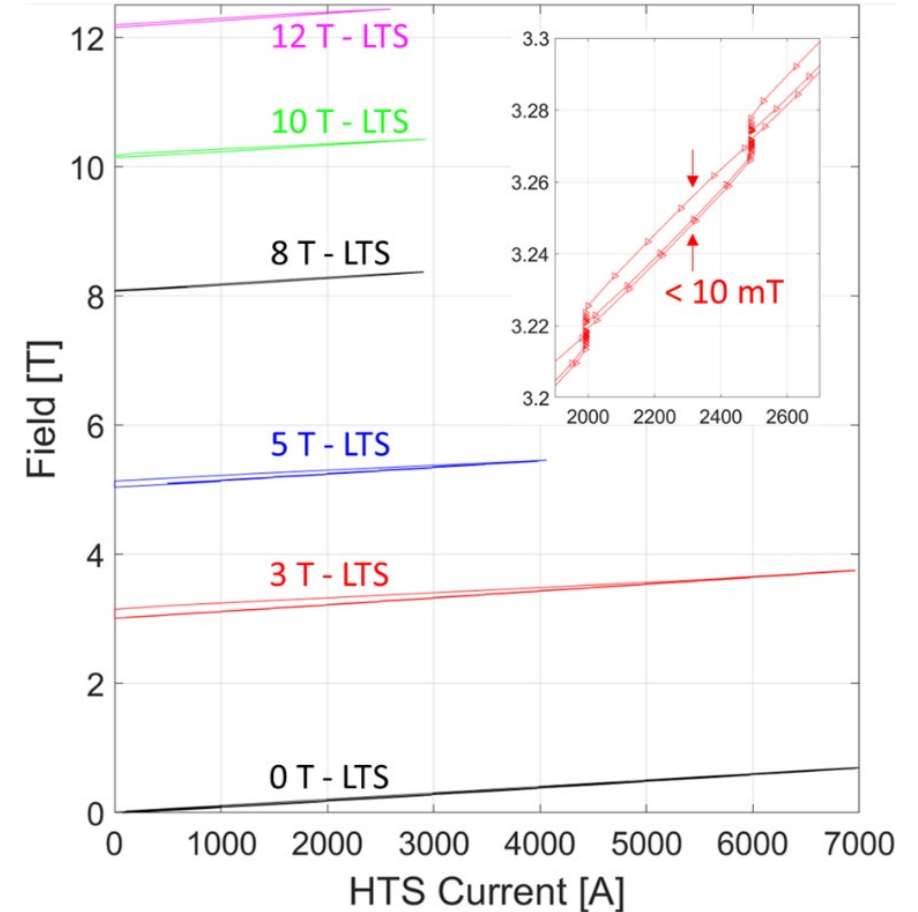
Voltages nominally at the same location behave differently depending on how inductance and motion are compensated.



# Reasonable Screening Current Induced Field

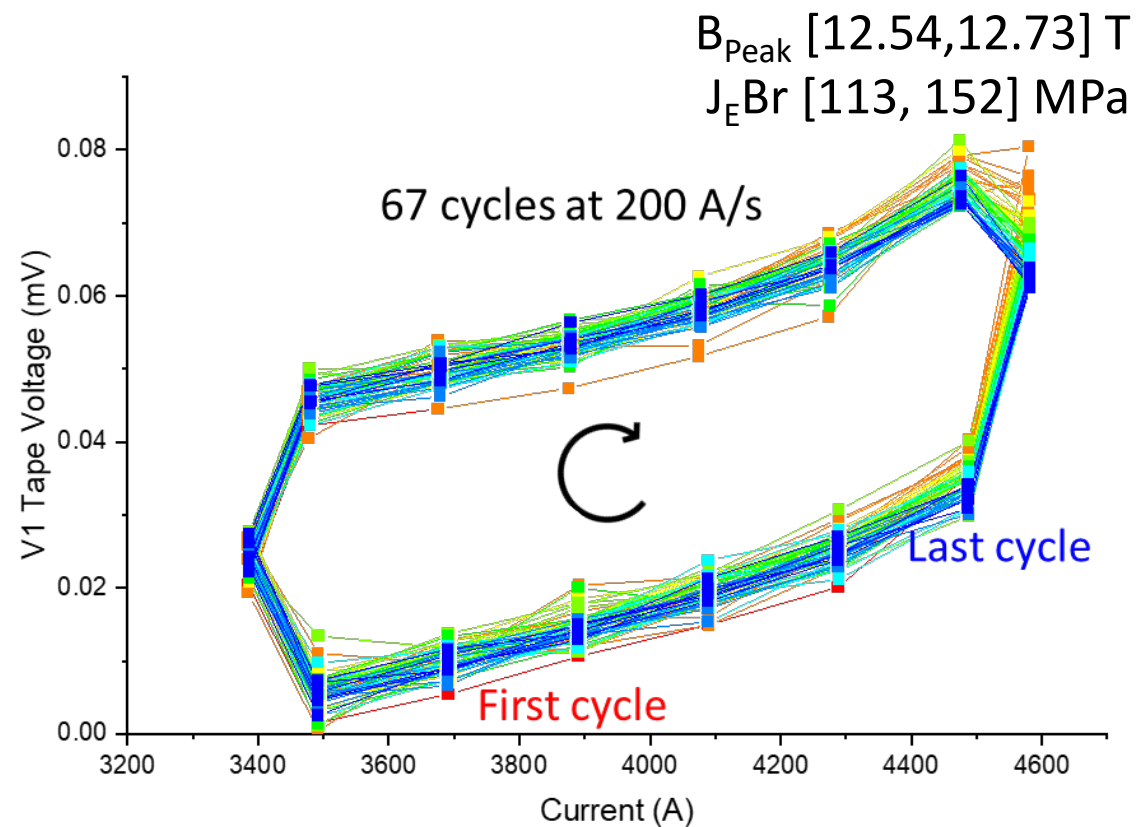
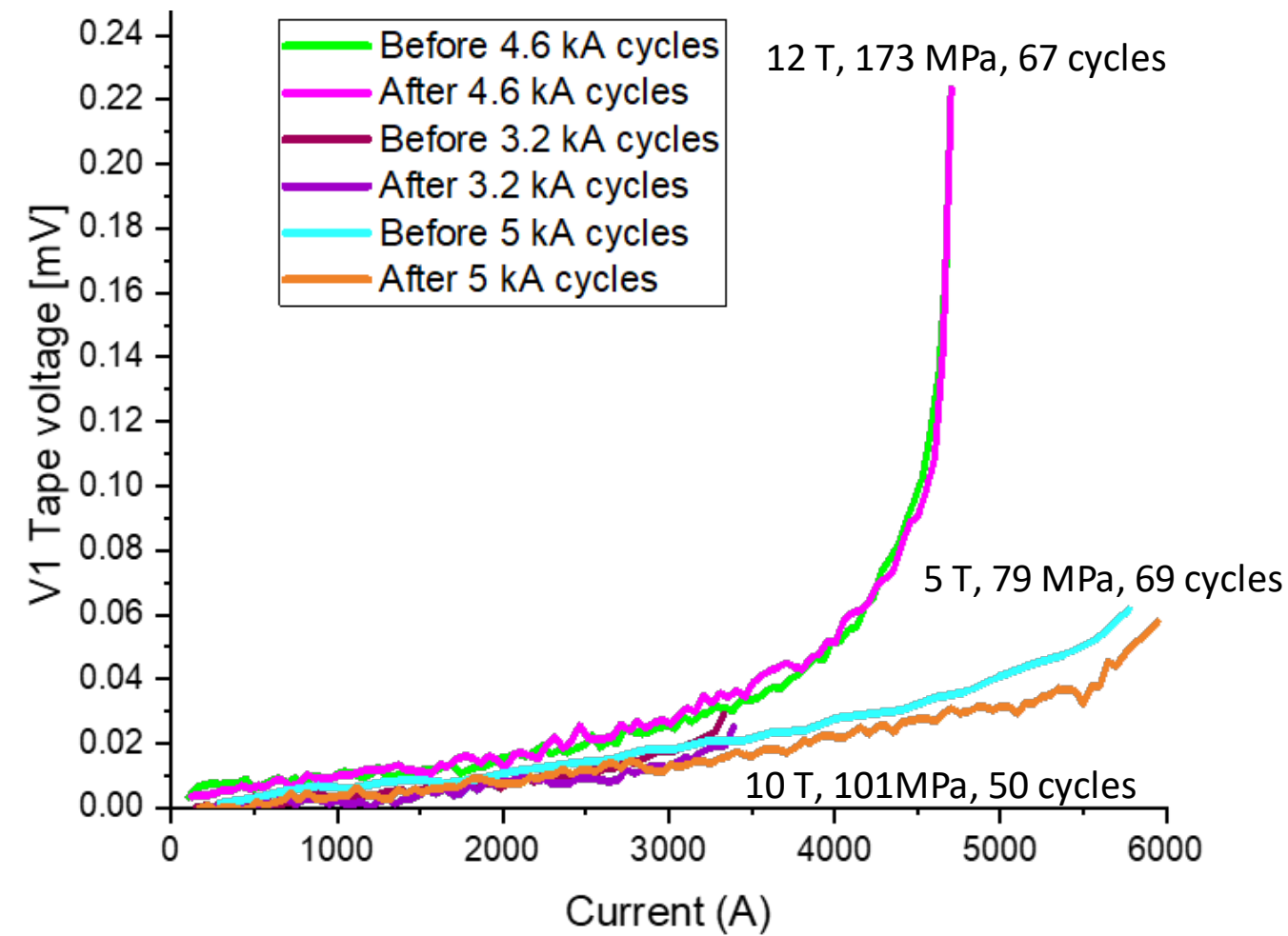


Excess field max is 163 mT  
 And decays over time of measurements at high field



Expected 0.102 mT/A  
 Measured range 0.082 to 0.112 mT/A  
 Median: 0.102 Average: 0.102

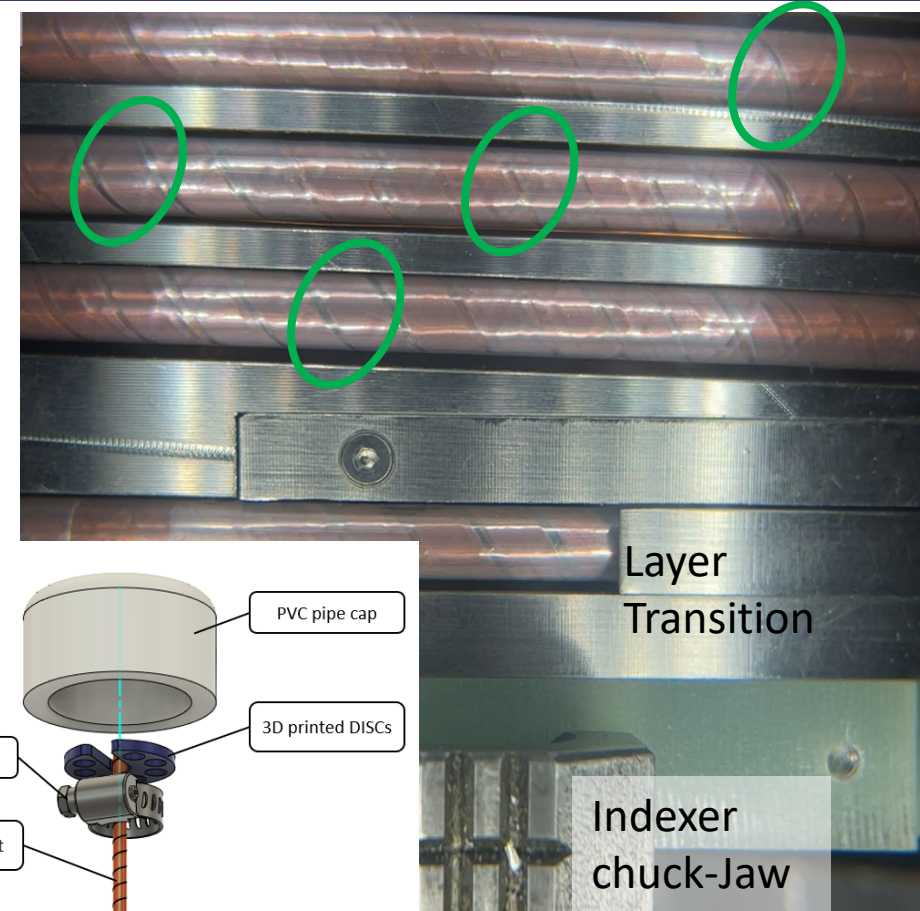
# No performance change after fatigue cycles



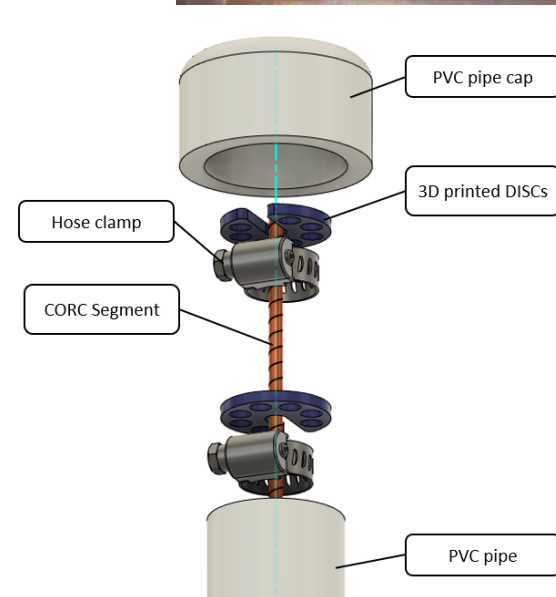
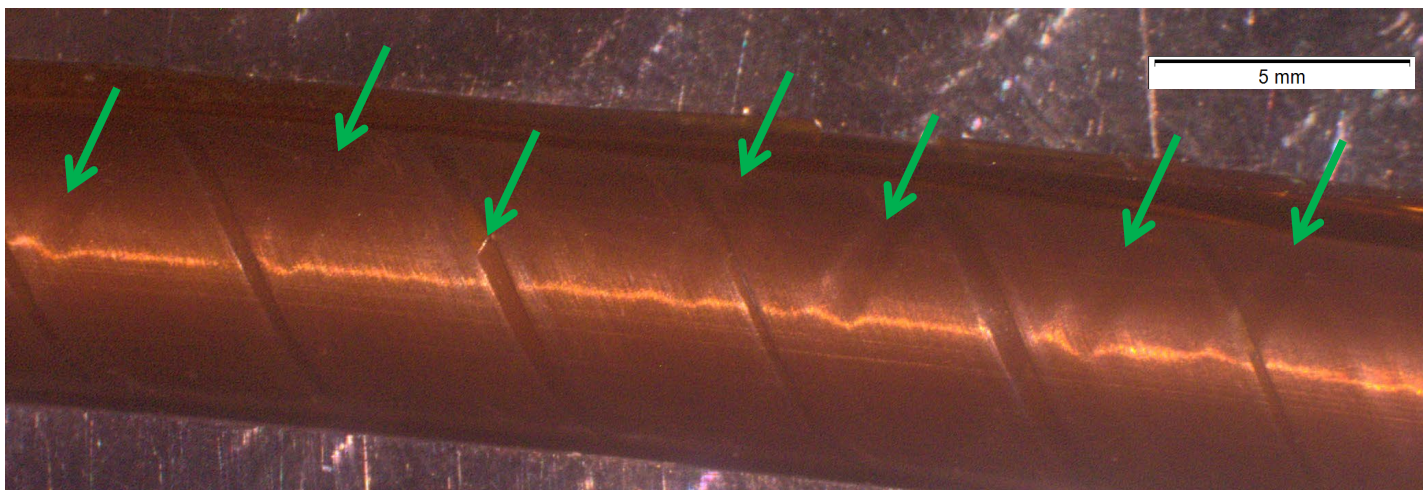
Fatigue Test	Cycles	$B_{app}$ [T]	Peak JBr stress [MPa]	Min cycle $I_{op}$ [A]	Max cycle $I_{op}$ [A]
1	69	5	79	2200	5000
2	50	10	101	2000	3200
3	127	12	107	1600	2800
4	67	12	173	3400	4600

# Prototype OH CORC Solenoid Postmortem: So-far So-good

- No visible degradation, pinch points or significant conductor deformation
- Evidence of Lorentz forces by next layer impressions in the copper.
- Conductor removed from each layer without unbending
- Developing postmortem techniques for the next coils with higher stresses:
  - Control coil for comparison
  - Cross section images: secure, diamond wire saw, VPI, polish, tape centroid analysis, tape gap analysis



Inside terminal riser support



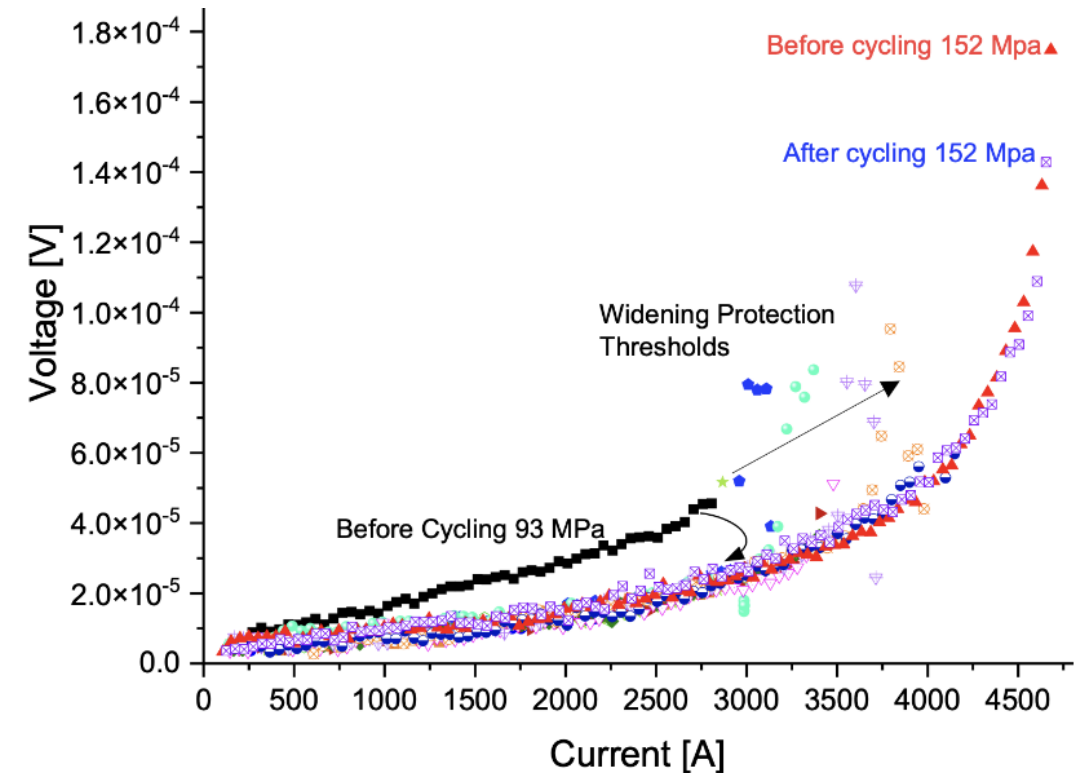
**Epoxy VPI fixture** for cross sections from bent coil turns (G. Murphy)

# Multiple Key Results From Each High Field Coil Test



- **No signs of degradation from low-cycle fatigue**
  - Higher quench currents and apparent  $I_C$  after cycling ( $>50$  cycles,  $> 170$  MPa)
- **High ramp rates are manageable**
- **Complex mix of phenomena in voltages**
  - Further analysis needed to identify contributions: cable motion, strand motion, screening currents, contact resistance, current sharing, strand degradation, co-wound voltage-tap wire motion
  - Quench detection challenges (false positives, transient voltage spikes, change in current sharing dissipation, or local quenches)
    - Must be conservative on quench detection
  - We could benefit from alternative diagnostics to deconvolute behaviors
  - **Matched inductance voltage taps significantly improve quench monitoring**
  - **The cable appears very stable, despite the dynamic behavior of the coil**
- **Screening currents are manageable**

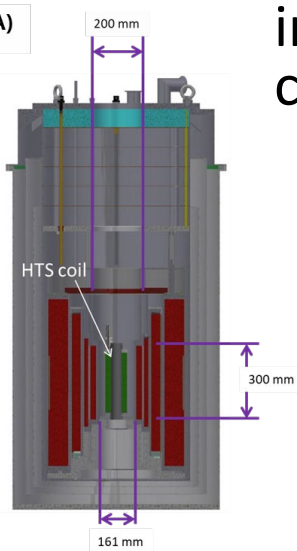
Affect initial current distributions after background field is ramped and decay as expected
- Demonstrated feasibility of dry-wound cable magnet concept
- **CORC Solenoids solenoid results confirmed by an uneventful postmortem investigation**
  - Developing a control, techniques, and experience for subsequent CORC investigations



# Solenoid Program Opportunities



- Conductor development program into tight loop magnet testing
- Ultra-High-Field tests demonstrate key capabilities and limits of conductor and cable
- Unique large-bore test bed and supporting postmortem investigation cycle demonstrates how cables and solenoids act closer to operation in affordable tests
  - Rapidly test magnet designs and isolate phenomena
  - Low-cycle fatigue test magnets in closer to final operating conditions
  - Dedicated test articles: cables, joints, diagnostics and instrumentation...
  - Validate design and modelling: mechanical reinforcement and constraints, current sharing, screening, quench, etc..
- ASC has extensive postmortem investigation capabilities
  - Material science experts and equipment, Yatestar (Reel-Reel tape evaluation), light/SEM/TEM/MO microscopy capabilities (see Bi-2212 session Postmortem investigation talk for examples)



Not a cartoon

