



**U.S. MAGNET  
DEVELOPMENT  
PROGRAM**



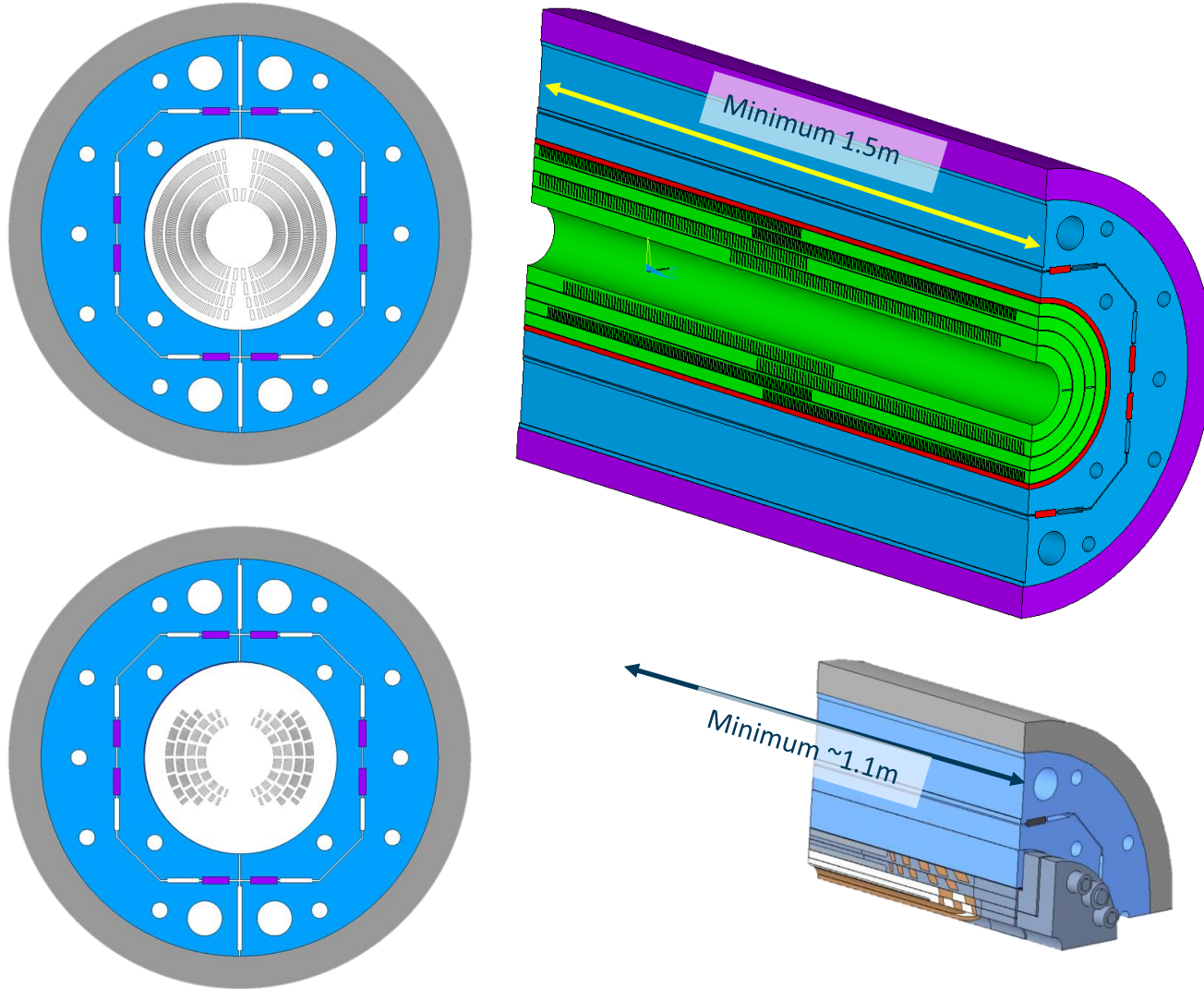
# Utility Structure Design, update on:

- CCT6 with de-bonded 1<sup>st</sup> layer
- SMCT analysis plan

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Alexander Zlobin, Igor Novitski (SMCT team)

**8th annual collaboration meeting of the US Magnet Development Program**  
(MDP CM-2024)  
2024-04-30

# Compatibility with magnets and test facilities



## Magnets

- CCT6
  - 2 layers with a spacer
  - 4 Layers with protective a (split) cylinder
- SMCT
  - 2 or 4 layers with a spacer
  - Axial preload?
- Hybrid configurations

## Facilities

- LBNL at 4.2K
  - 860 mm OD compatible with the current cryostat
- FERMILAB at 1.9K
  - 860 mm OD compatible with HFVMTF (additional magnetic shielding will be required)
  - Coldmass OD would be limited to ~750 mm by the current test facility

# CCT6

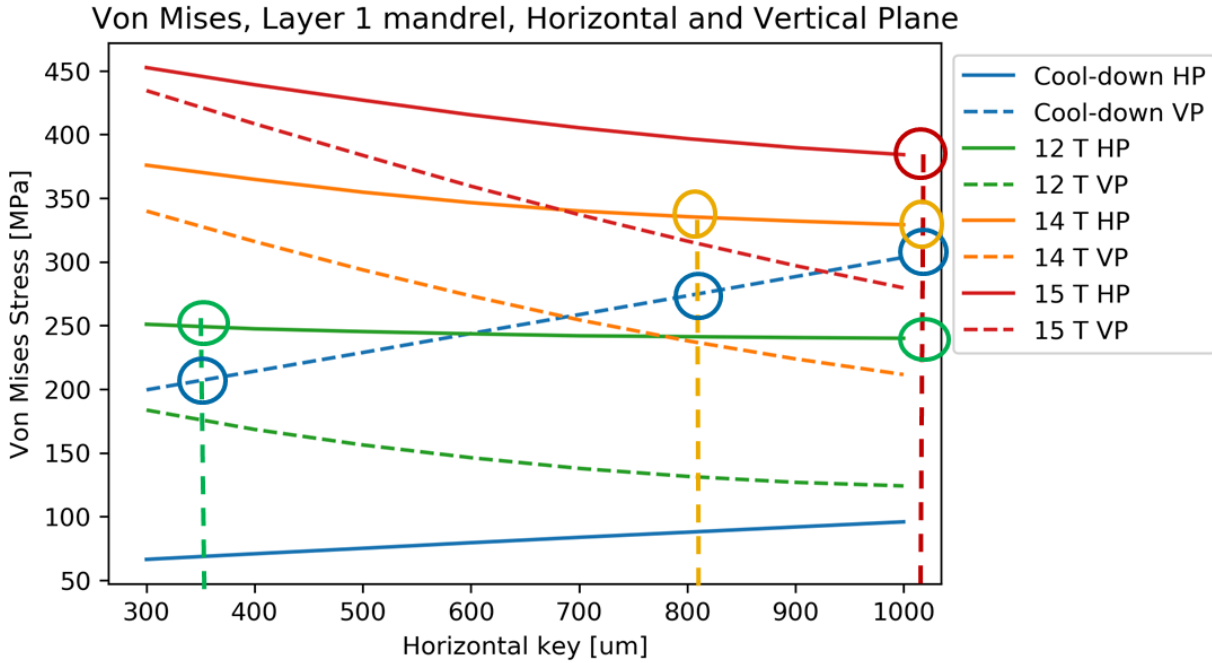
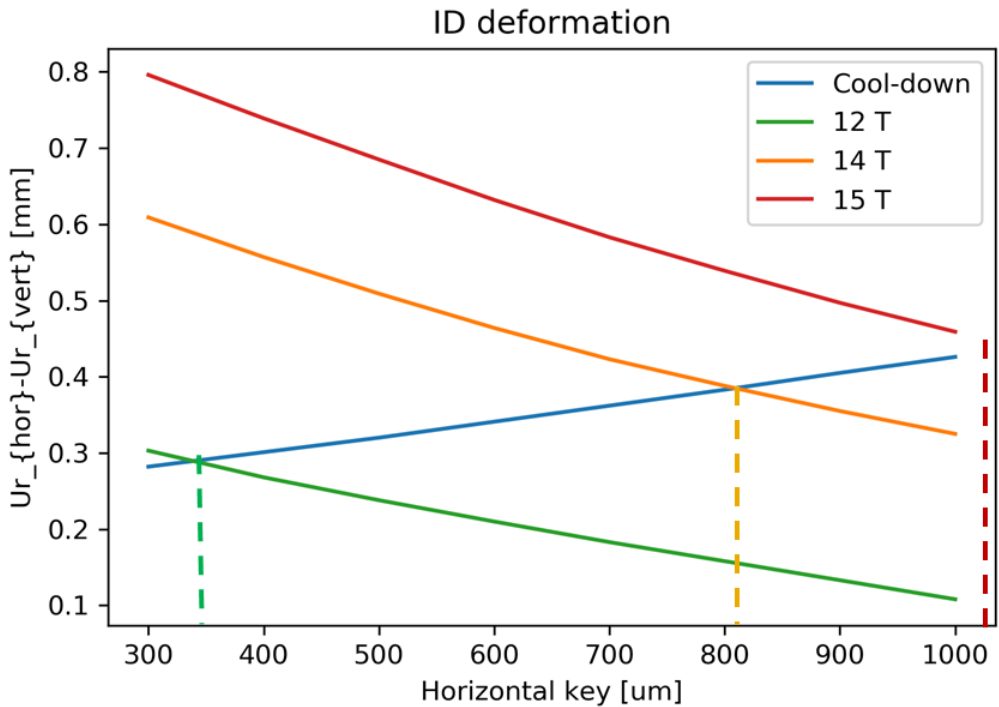
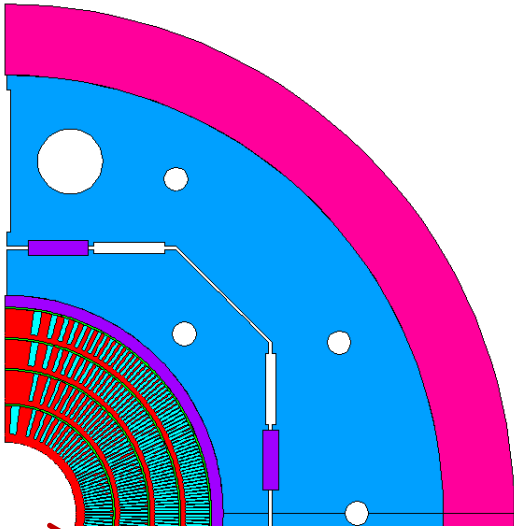
Conductor and mandrel stress  
in case of 1<sup>st</sup> layer conductor  
interface debonding





# Key values to minimize the deformation

## Von Mises stress in the mandrel in 1<sup>st</sup> layer



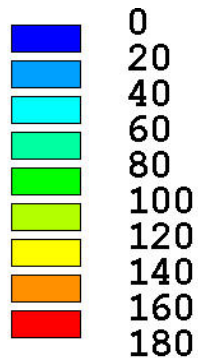
# Stress in the coil (von Mises)

COOL-DOWN

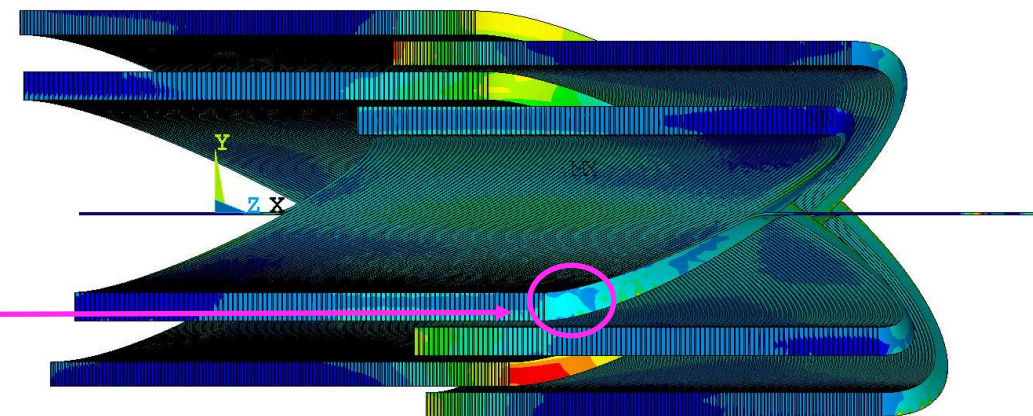
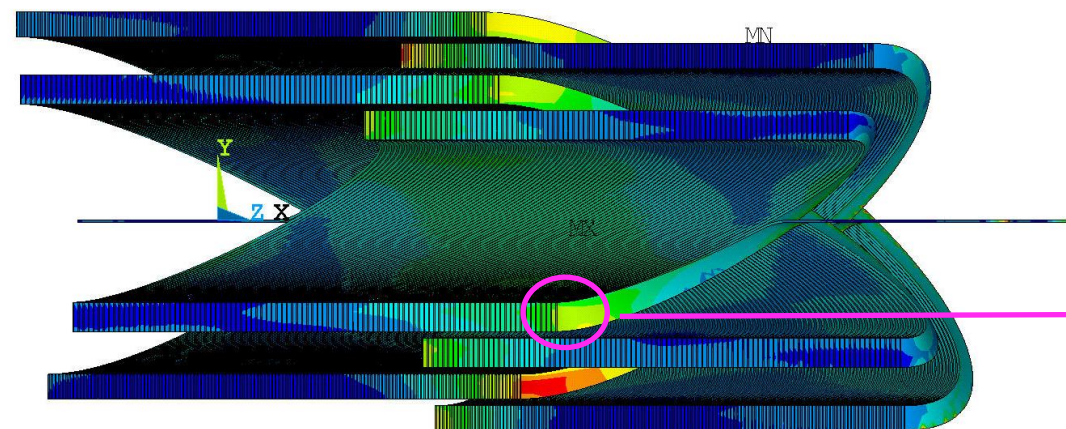
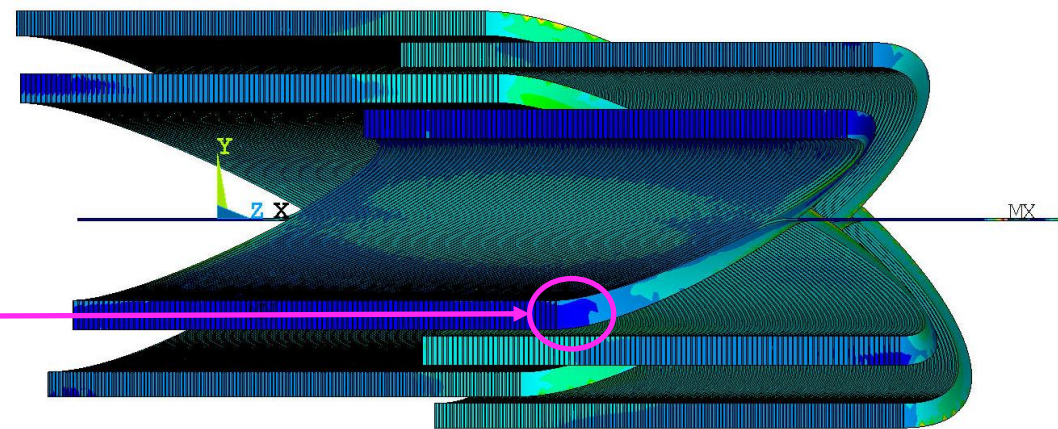
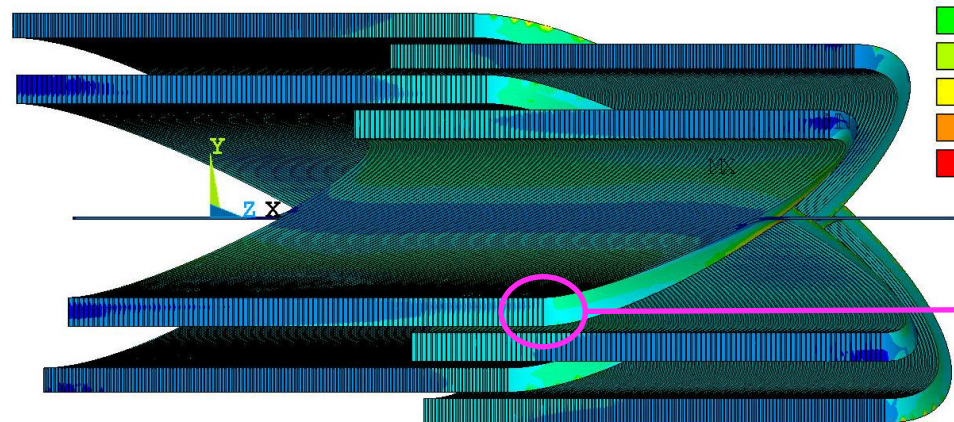
15T

L1 BONDED

L1 DE-BONDED



MPa



Overall reduction of stress in the de-bonded layer (~40MPa)



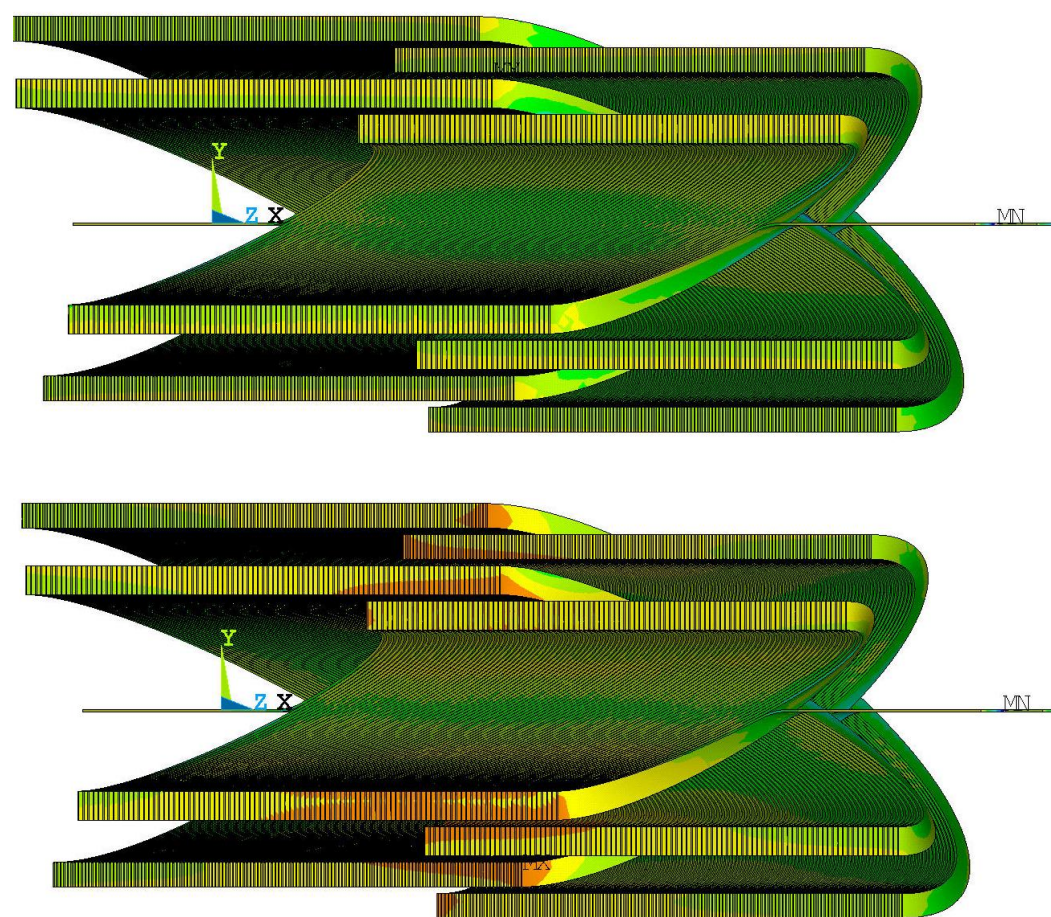
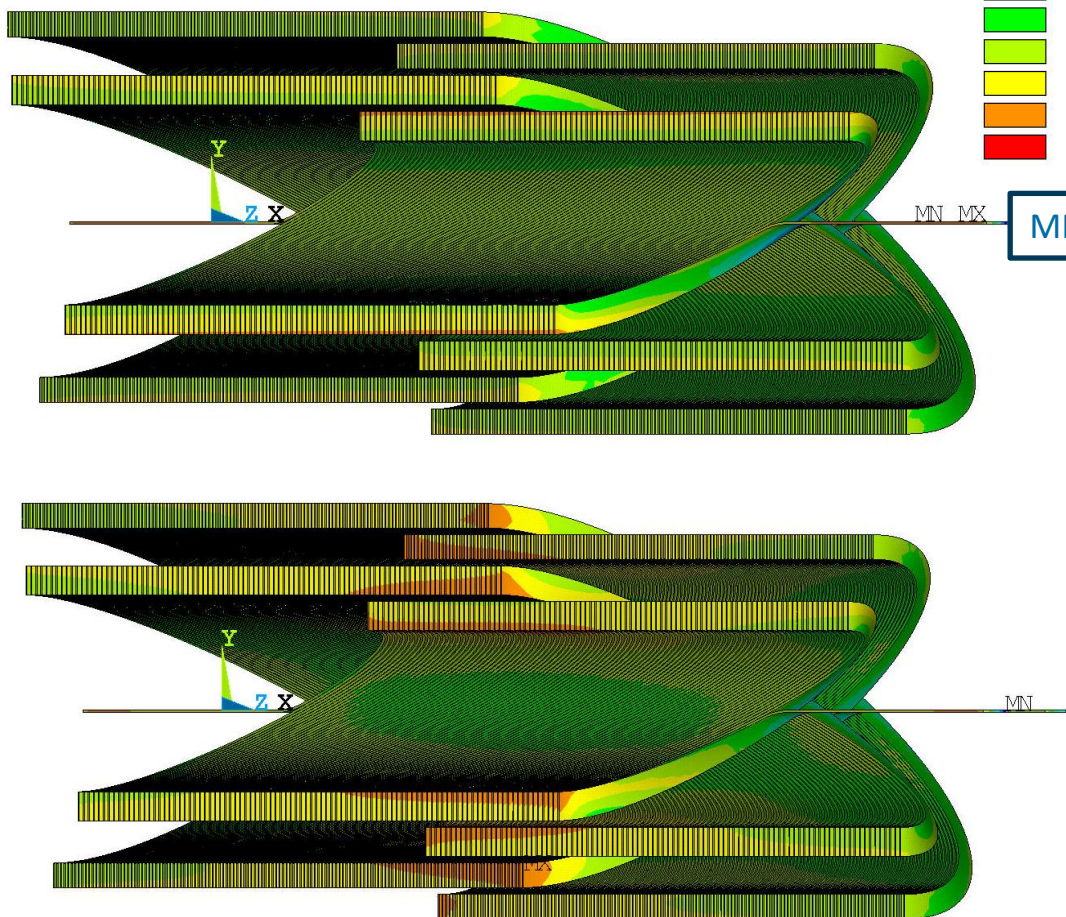
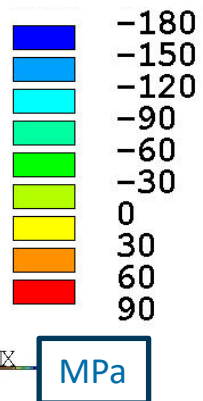
# Stress in the coil (Azimuthal)

L1 BONDED

L1 DE-BONDED

COOL-DOWN

15T



Azimuthal stress remain nearly the same



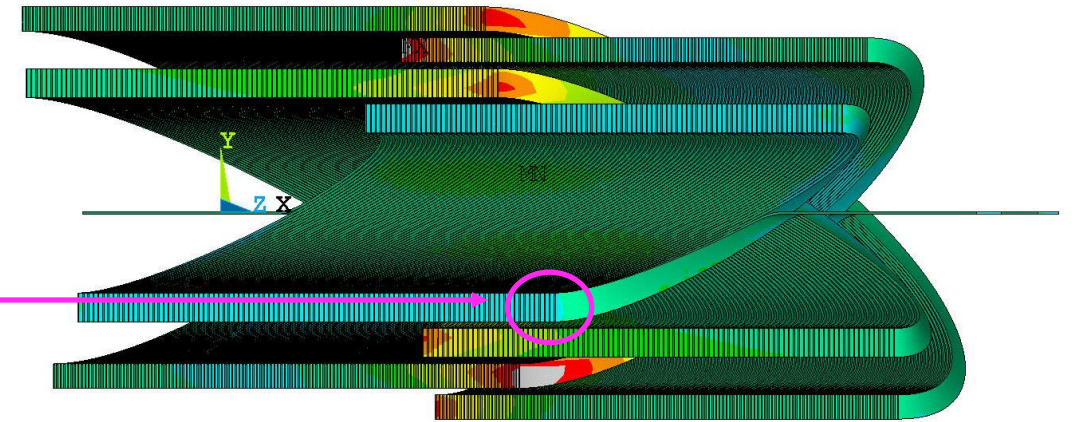
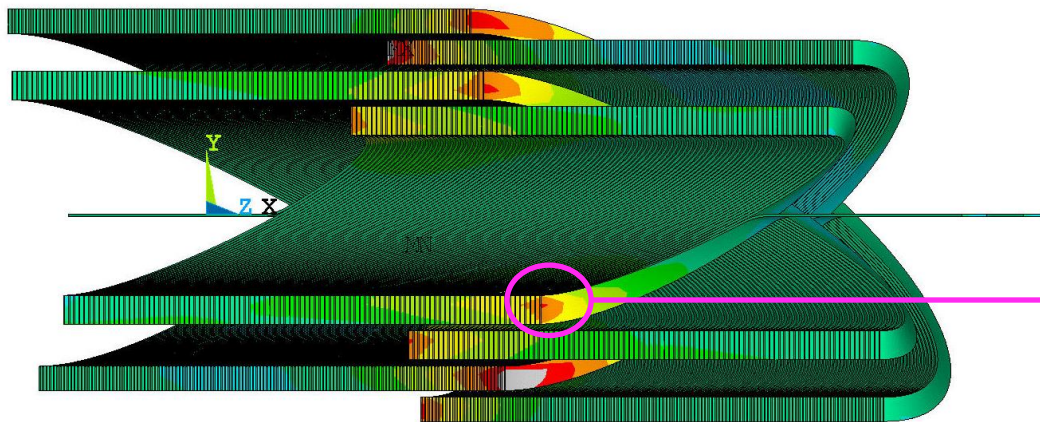
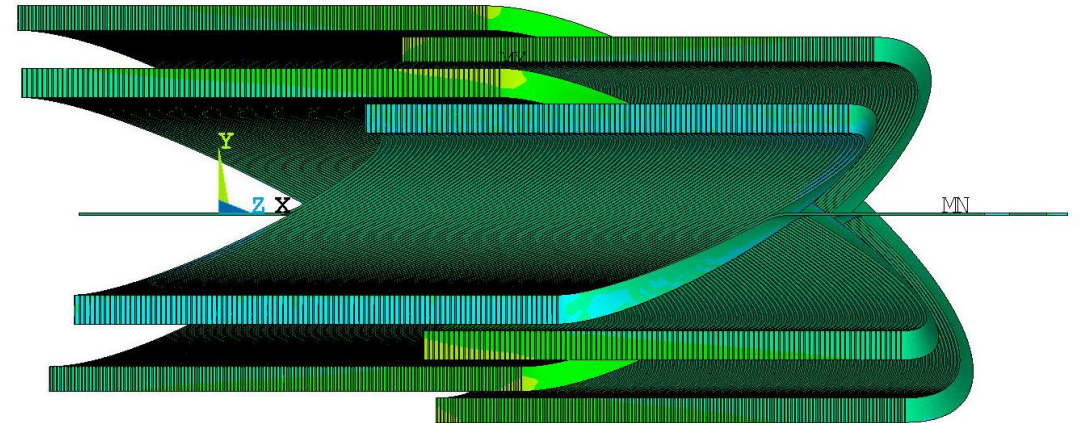
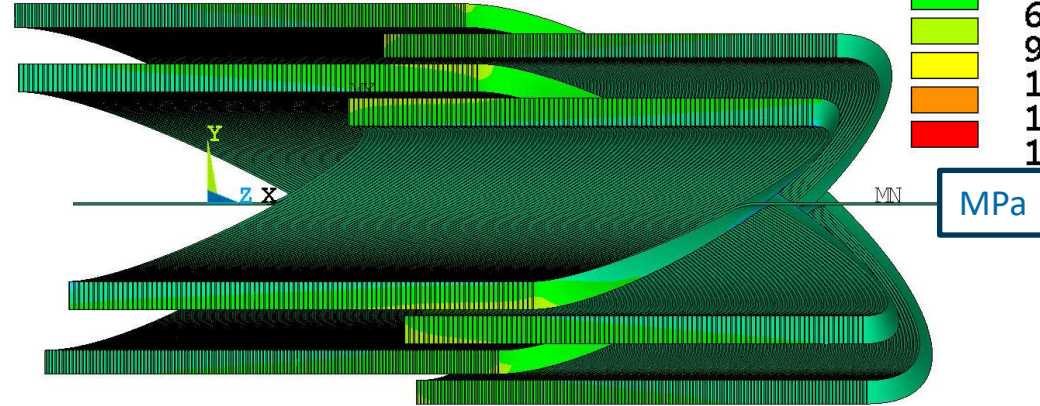
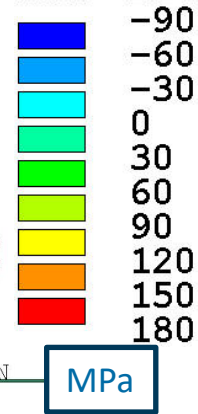
# Stress in the coil (Axial)

L1 BONDED

L1 DE-BONDED

COOL-DOWN

15T



Significant reduction of the axial stress after debonding

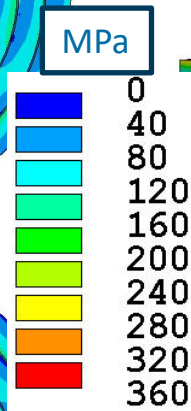
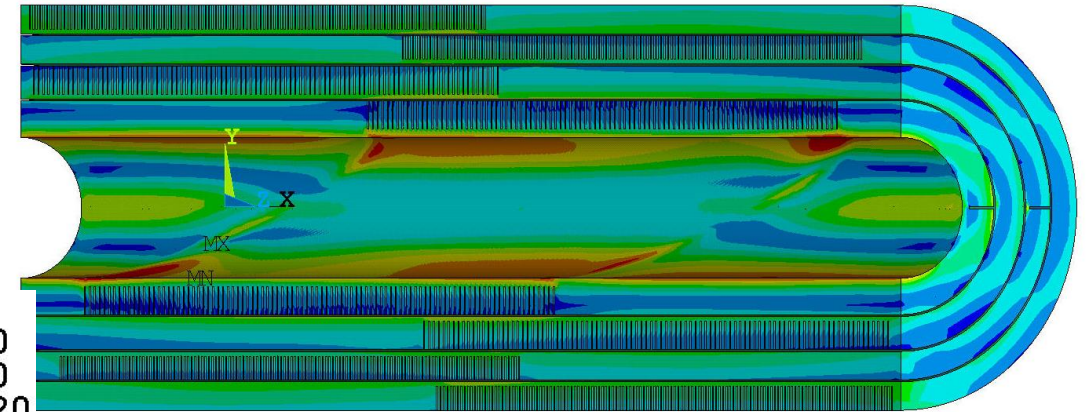
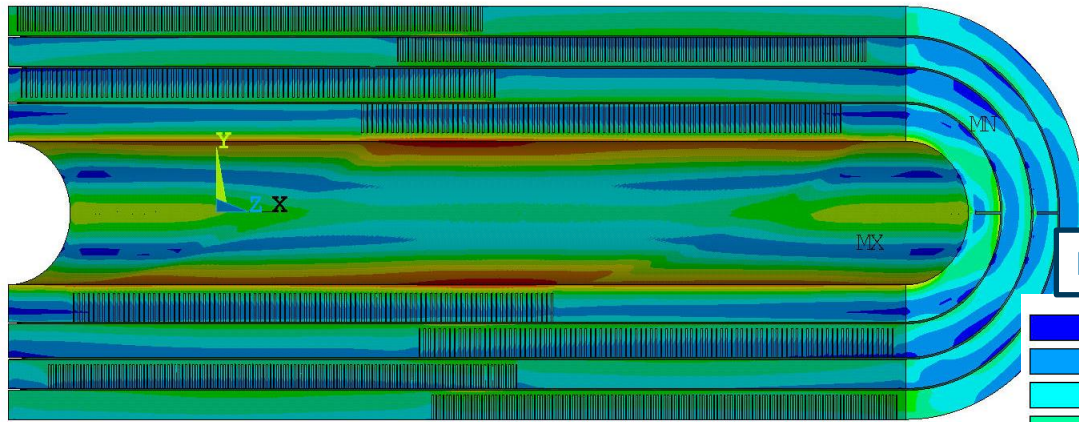


# Stress in the mandrel (von Mises)

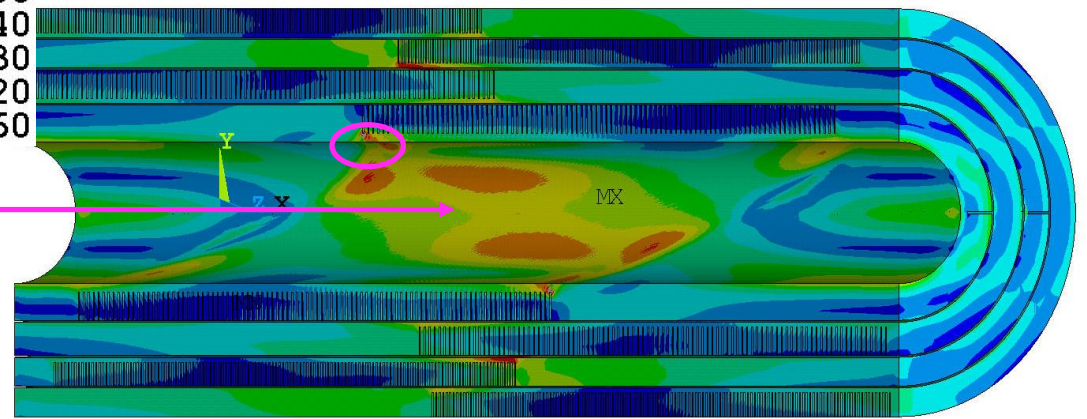
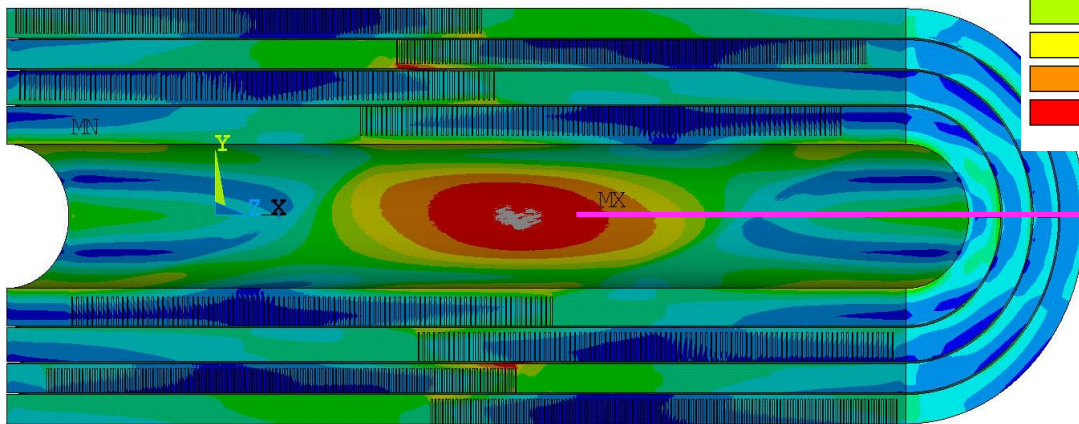
L1 BONDED

L1 DE-BONDED

COOL-DOWN



15T



Bending (and stress) in the center of the mandrel is reduced

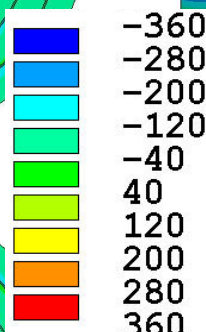
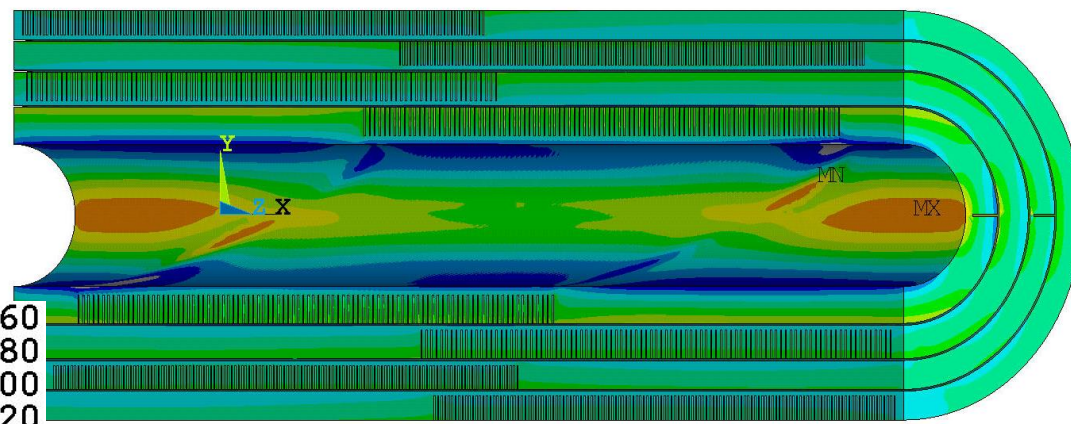
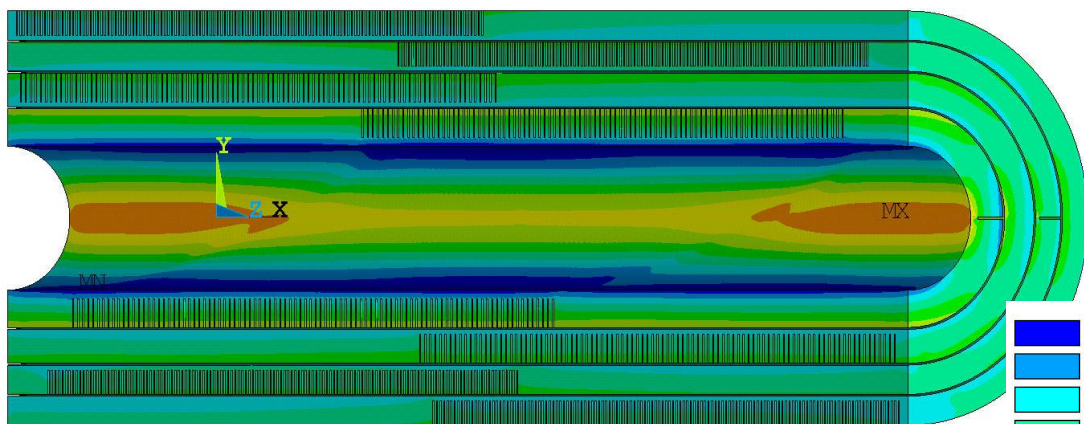


# Stress in the mandrel (Azimuthal)

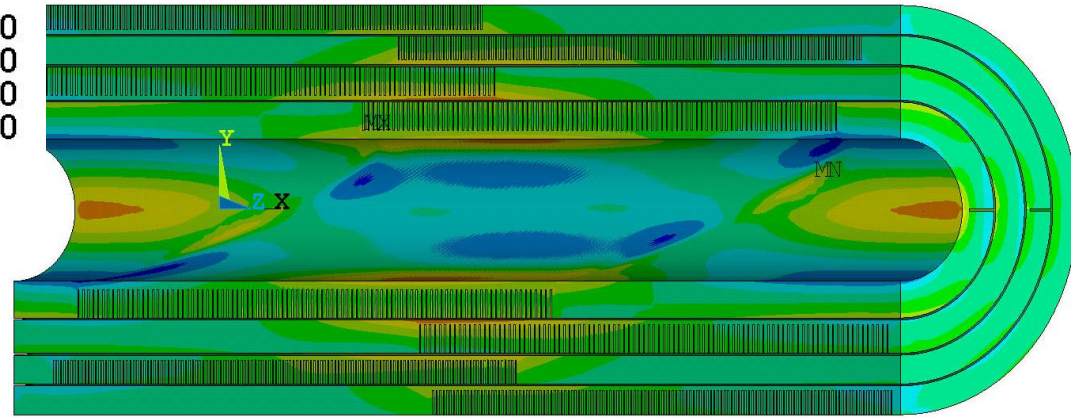
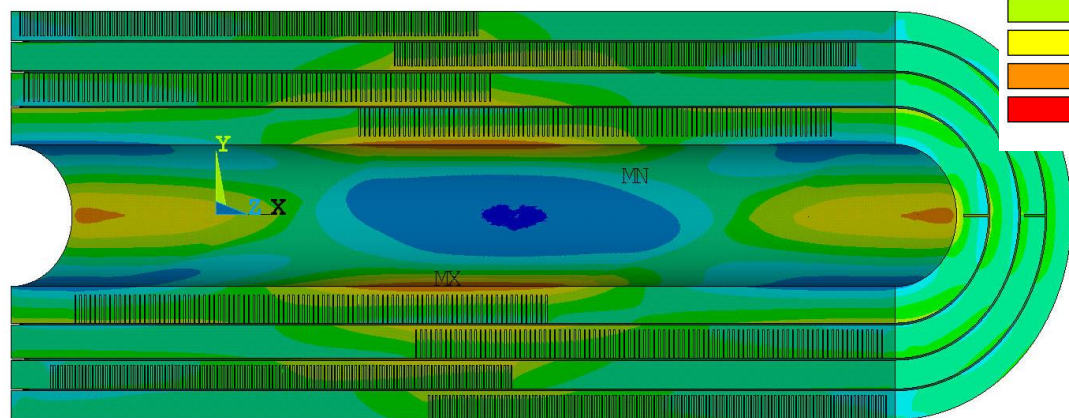
L1 BONDED

L1 DE-BONDED

COOL-DOWN



15T



Azimuthal stress in the center is reduced

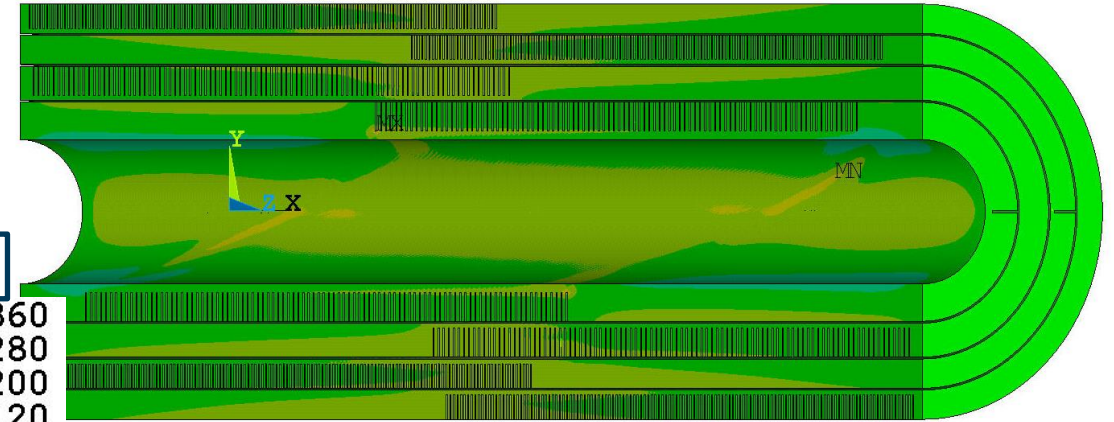
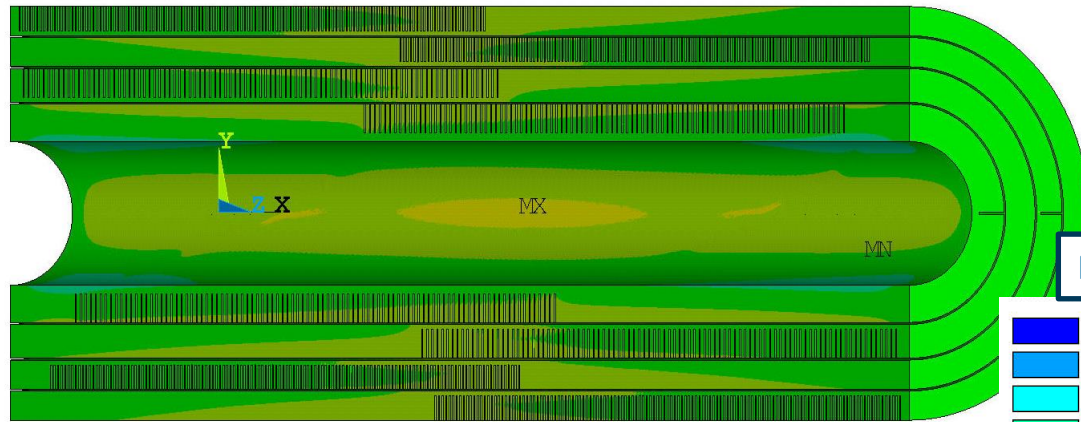


# Stress in the mandrel (Axial)

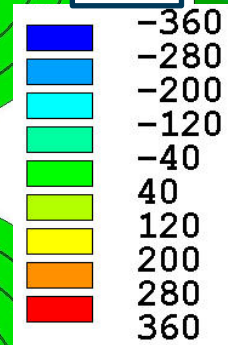
L1 BONDED

L1 DE-BONDED

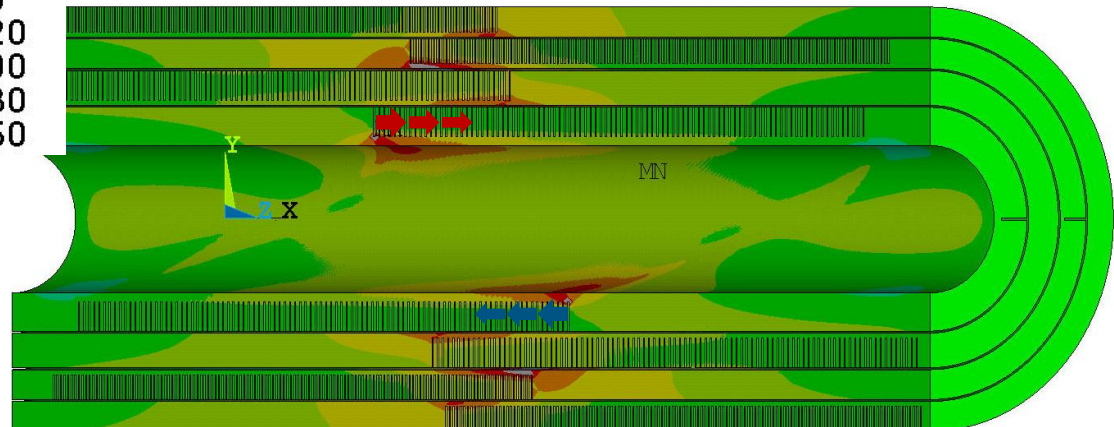
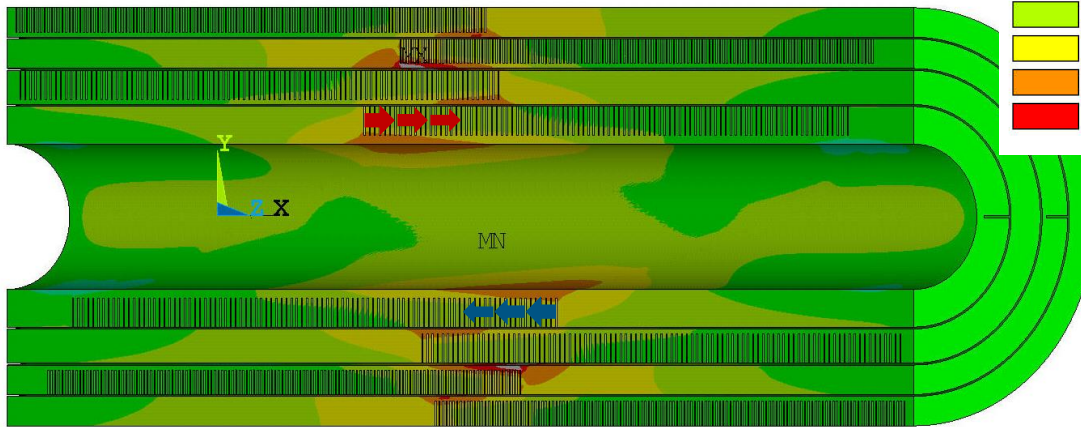
COOL-DOWN



MPa



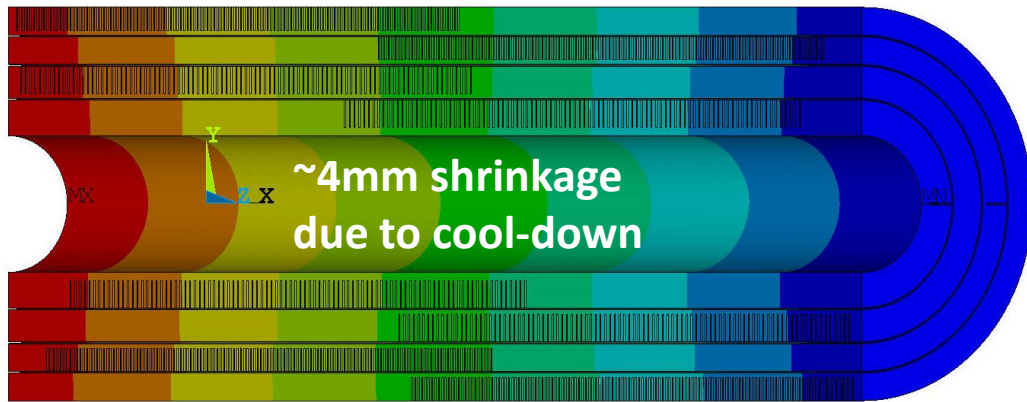
15T



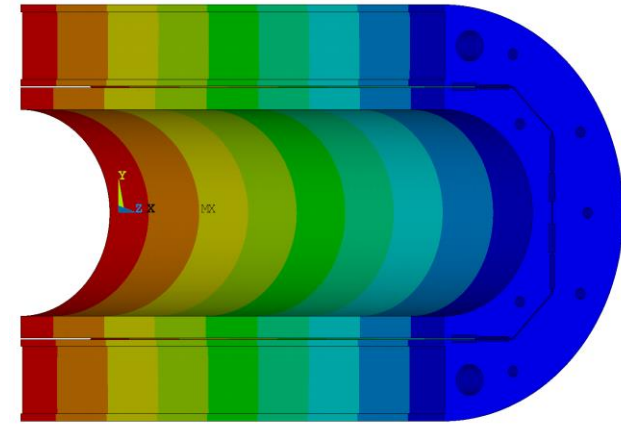
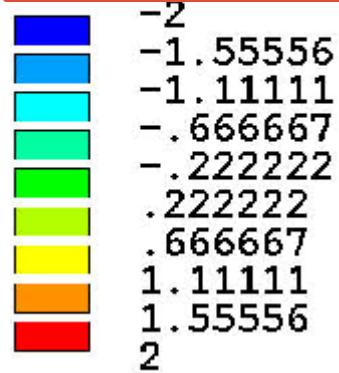
Local increase of the axial tension in the mandrel

# Mandrel vs yoke axial displacement (bonded case)

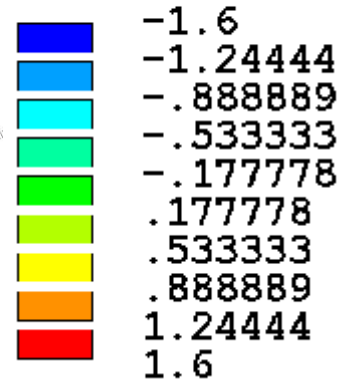
COOL-DOWN



DMX =2.0692  
 SMN =-1.99206  
 SMX =1.99138



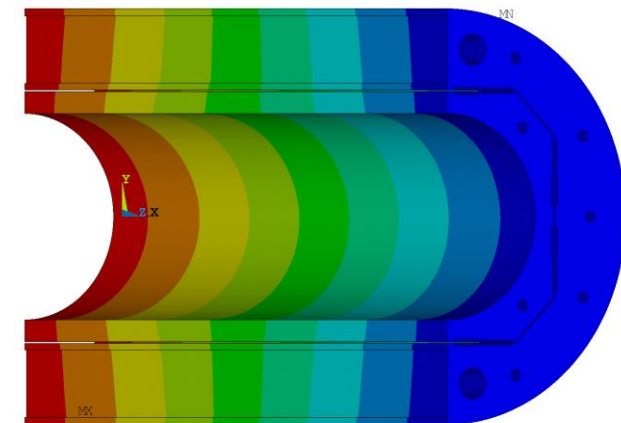
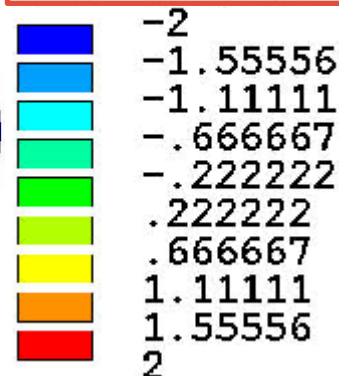
DMX =1.86449  
 SMN =-1.57696  
 SMX =1.57739



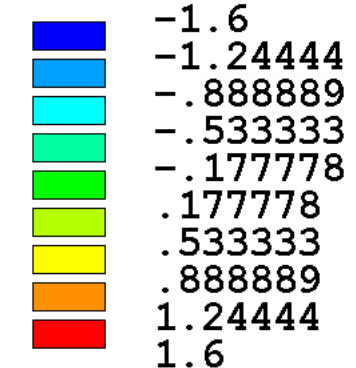
15T



DMX =1.99712  
 SMN =-1.89893  
 SMX =1.89908



DMX =1.80669  
 SMN =-1.53519  
 SMX =1.53543



Highest axial forces are localized near the center of the magnet.  
 External axial system ineffective to provide compression.

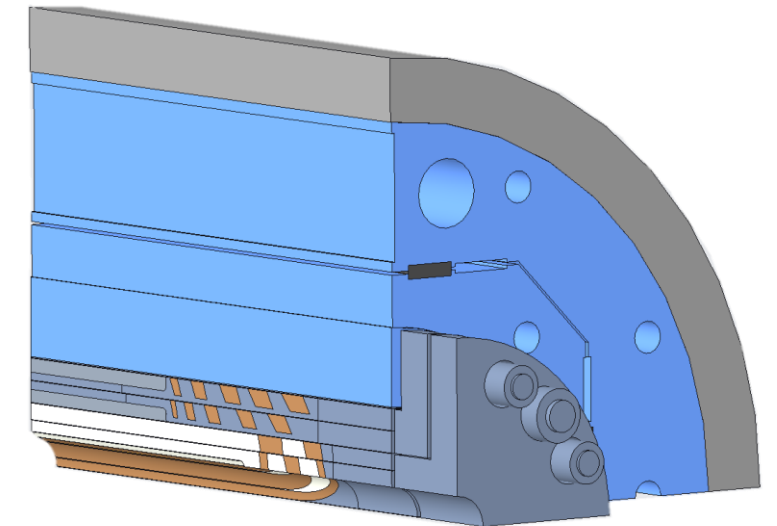
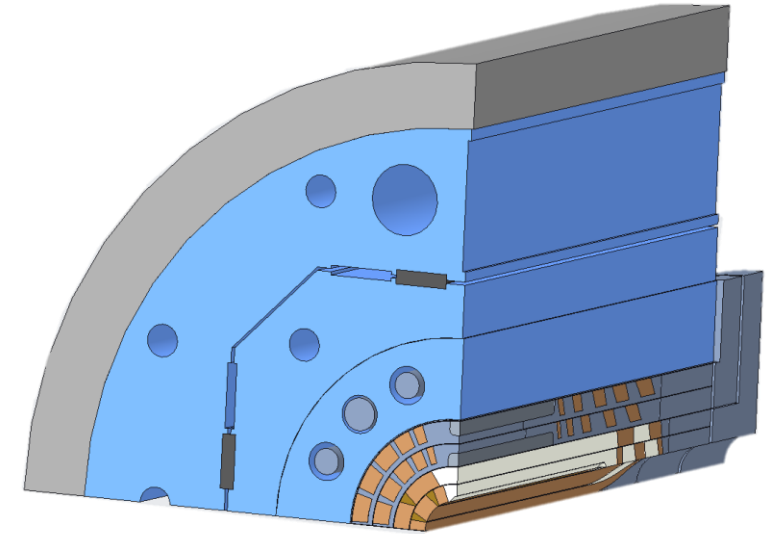


# SMCT

First steps towards  
mechanical analysis with  
the Utility Structure

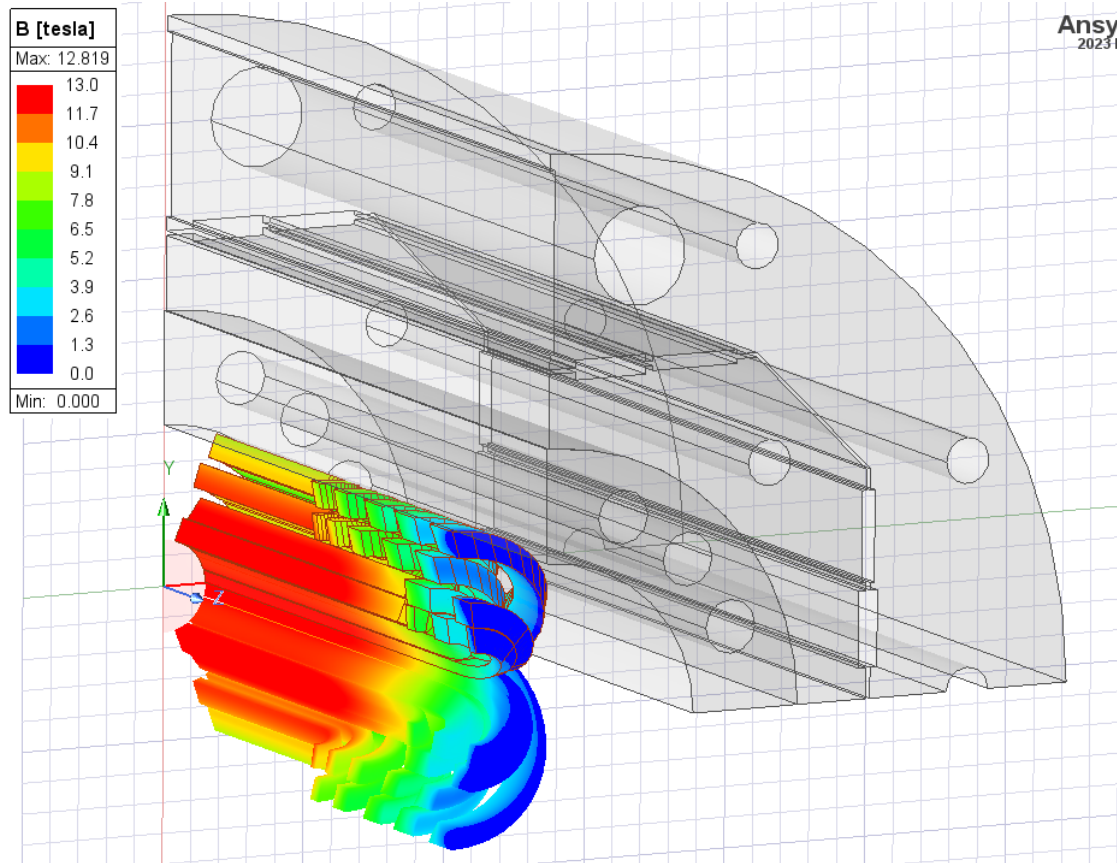
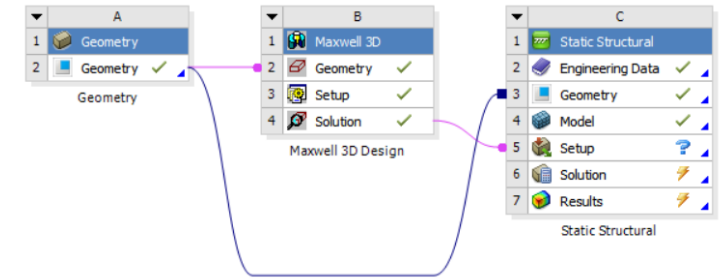
# Setting up mechanical analysis of the SMCT in Utility Structure

- Coil configuration
  - L1&2: Inner layers from 15T cos-theta coil
  - L3&4: Inner layers of SMCT
- Coil geometry not “as build” but “close enough” (some adjustments might be needed)
- Support structure – first approach
  - Support structure length reduced to 1.1 m
  - Pad inner diameter is the same as for CCT6
  - Iron filler placed between the coil and the pad
  - Axial support system resembles FNAL axial support but with full length axial rods
- Goal of the preliminary analysis – investigate SMCT preload needs without changing the established cross-section





# Ansys Maxwell and Workbench



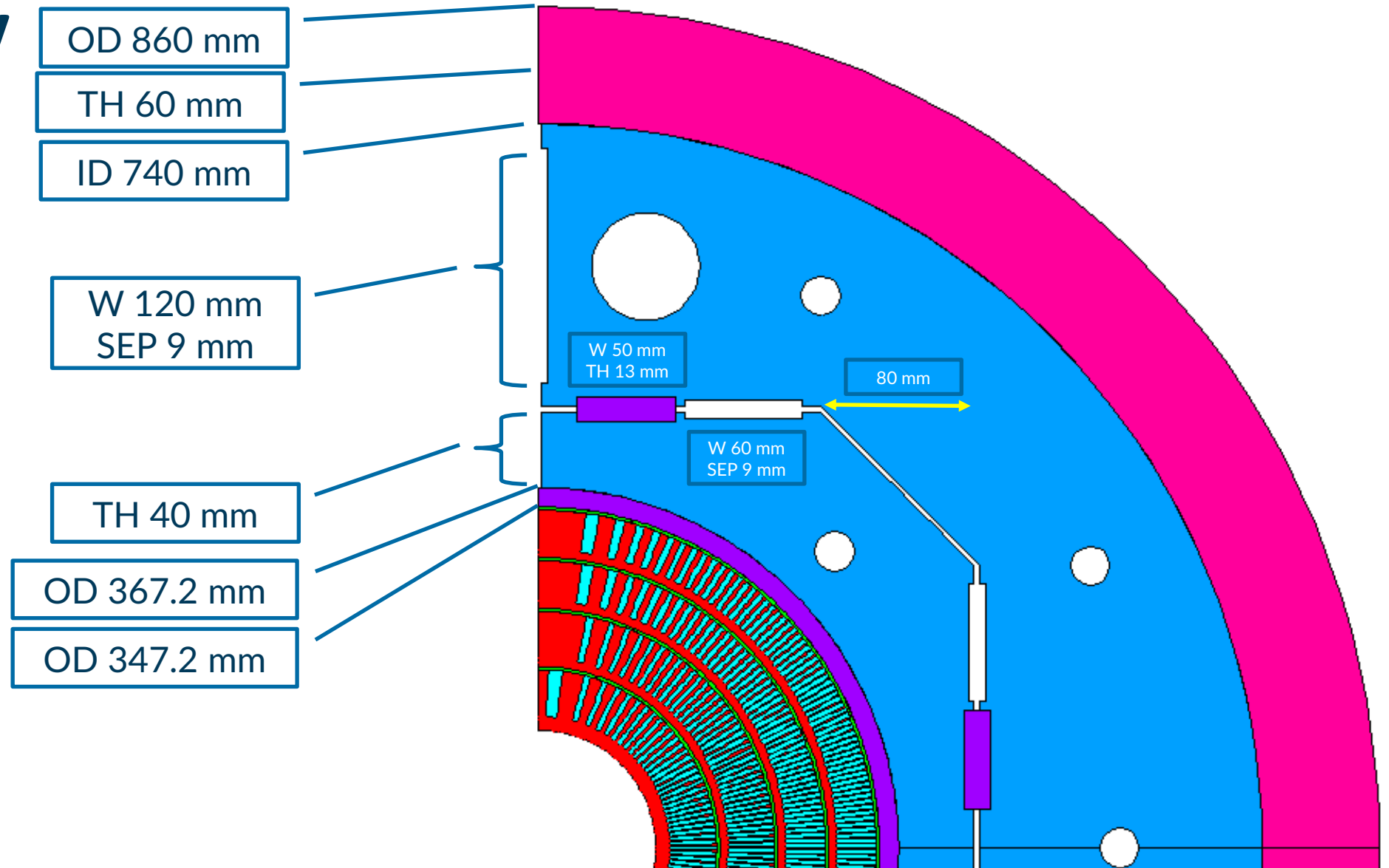
- Magnetic model in Maxwell is operational
  - First solution at 8kA and 13T has to be discussed with Sasha and Igor
- Next step is to set-up the mechanical analysis in Workbench
  - Similar setup and simulation steps as for CCT6 in ANSYS APDL
  - Magnetic forces imported from Maxwell

**Thank you!**



# Backup

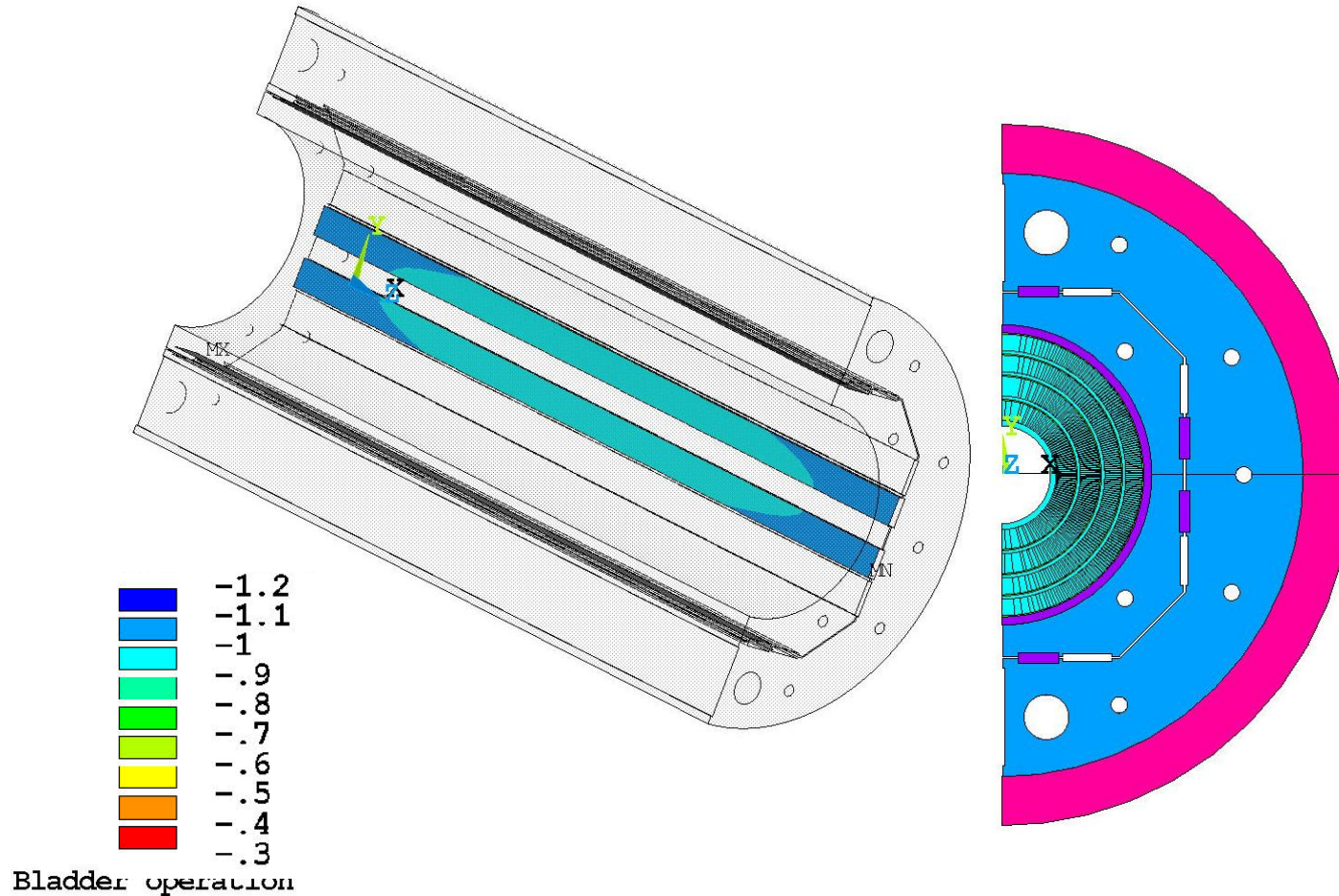
# Geometry



- Separation
  - Yoke to yoke 3 mm
  - Pad to pad 3 mm
  - Pad to yoke 3 mm



# Bladder operation at 40 MPa



- 40 MPa allows to open the key slot to about 0.9-1.1 mm
- Enough for 800 um key
- There is no space for bigger bladders
- Bladders can withstand higher pressure

# Distribution of azimuthal stress is symmetrical

