

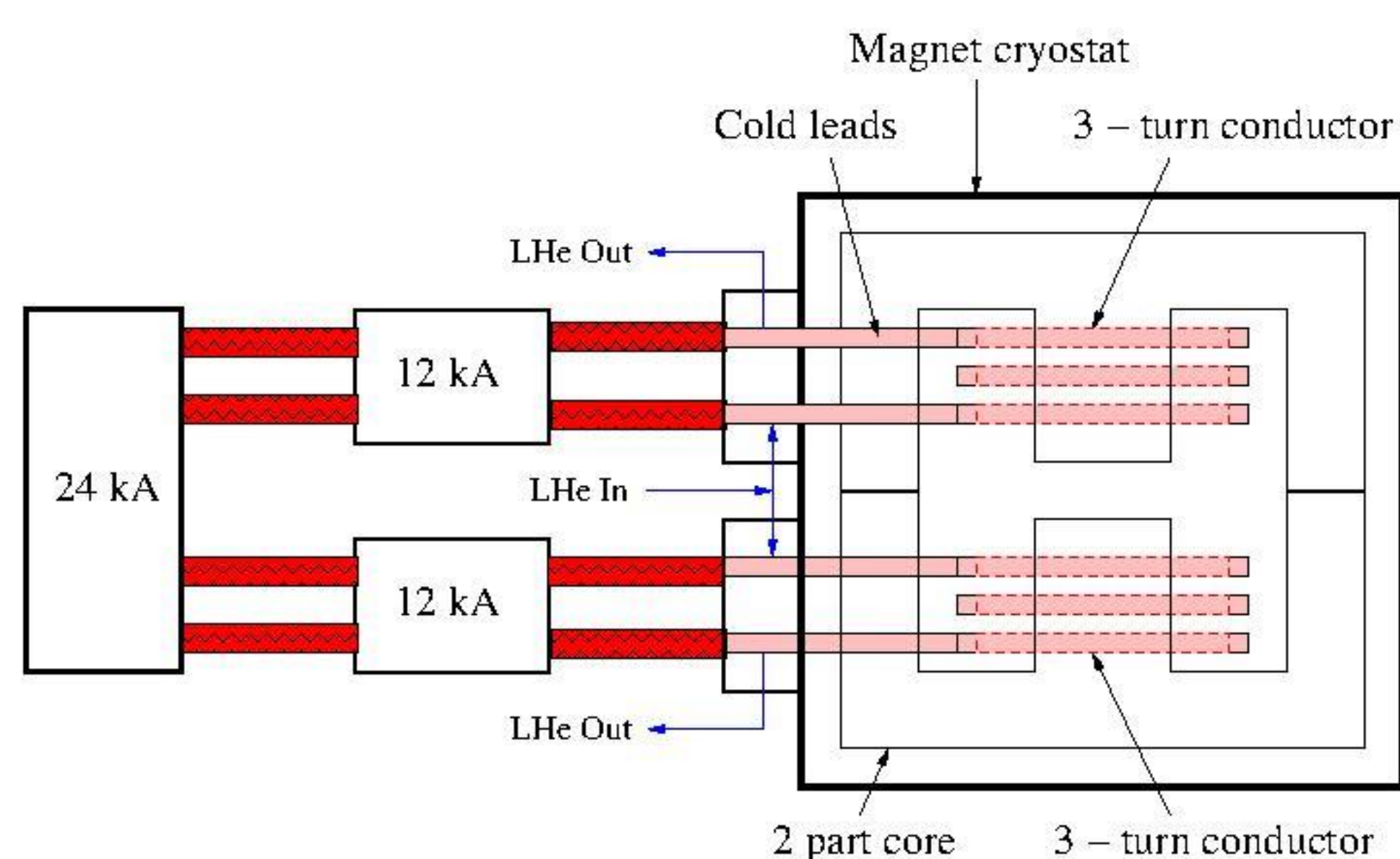
# RAPID-CYCLING HTS MAGNET FOR MUON ACCELERATION

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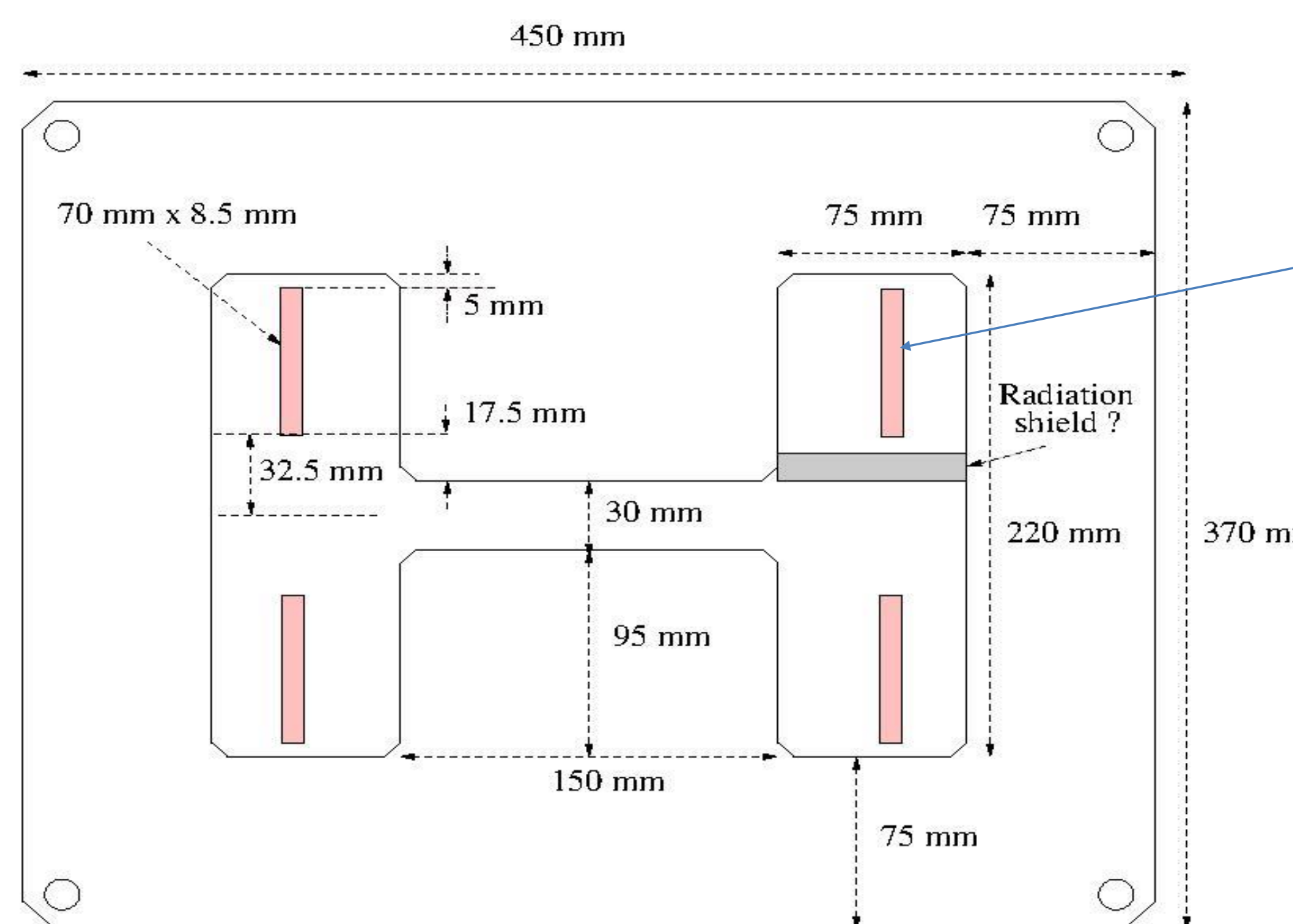
A very wide range of operational temperatures of the HTS (YBCO) superconductor makes it suitable for the construction of rapid-cycling magnets required for the muon acceleration. The measured [3] very low power loss of the 0.4 T magnet operating at 300 T/s suggested a realistic possibility of the HTS-based accelerator magnet with much higher magnetic field and ramp rate. The magnet core and the HTS cable designs for the 2 T field in the 30 mm beam gap are presented. The simulation of the HTS cable hysteresis power loss for the 1000 T/s ramp rate is discussed in terms of the operational temperatures and required cryogenic power.

## RAPID-CYCLING HTS MAGNET CONCEPT



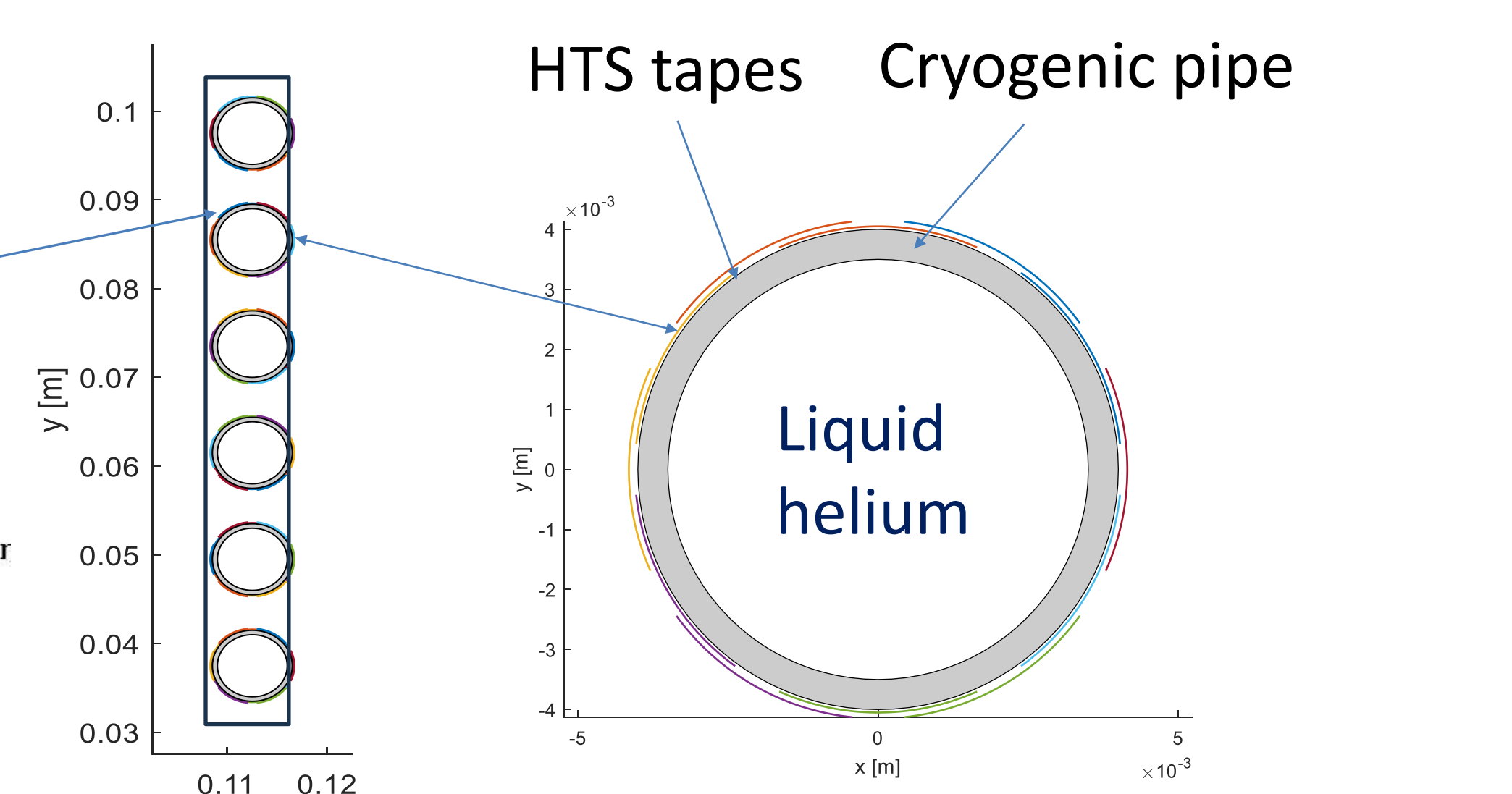
- Magnet core placed inside the cryostat
- No vacuum beam pipe
- Two 3-turn coils, each powered by 12 kA supply
- HTS conductor cooled with supercritical helium
- Current leads cold ends with spliced HTS tapes cooled through heat conduction from the conductor coil
- Magnet core LCW cooling provided to interior of cryostat

## HTS MAGNET DESIGN



- Core: 0.45 m (H) x 0.370 m (V)
- Beam gap: 150 mm (H) x 30 mm (V)
- Core laminations: Fe3%Si (0.1 mm)
- 2 T field generated by 2 x 36 kA current
- Core saturation: 2 T, B-field linear: +/- 1.7 T
- Ramp rate: 1000 T/s
- Repetition rate: 5 Hz

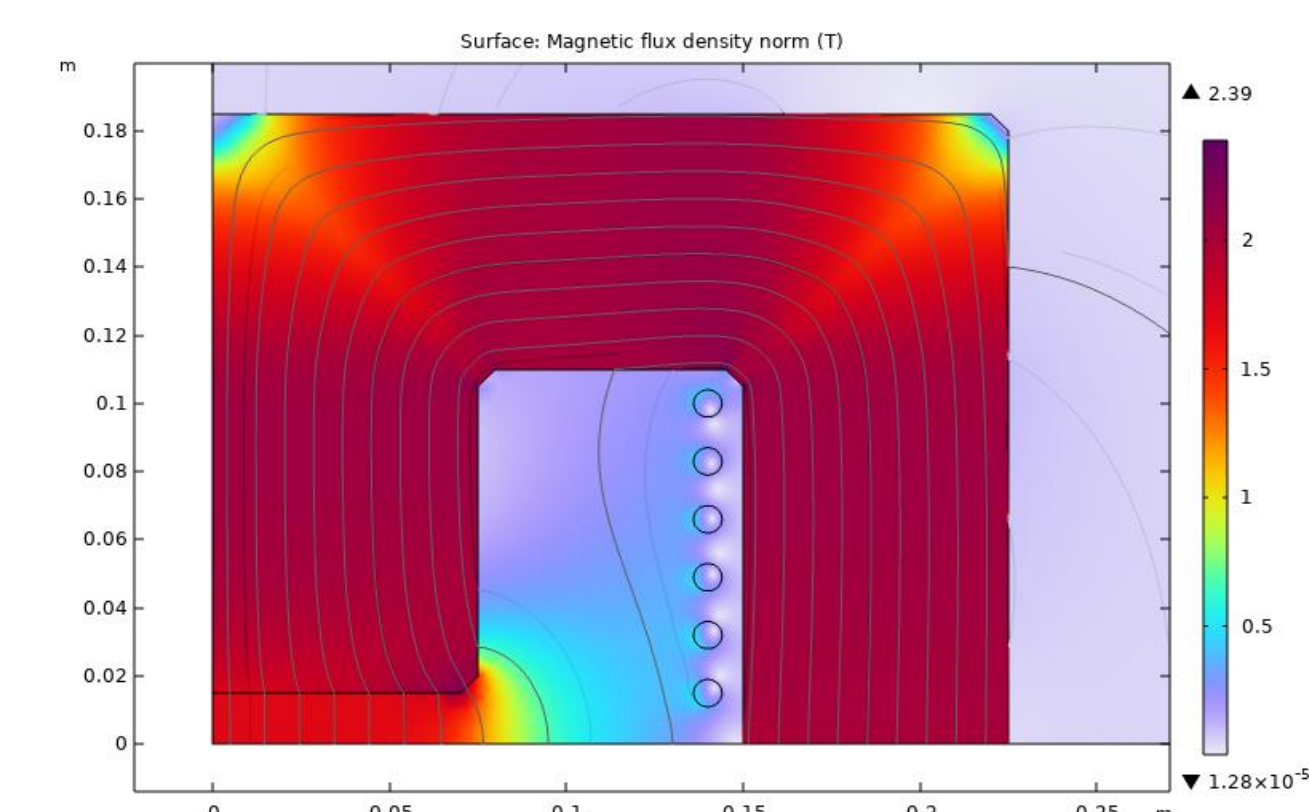
## HTS CABLE DESIGN



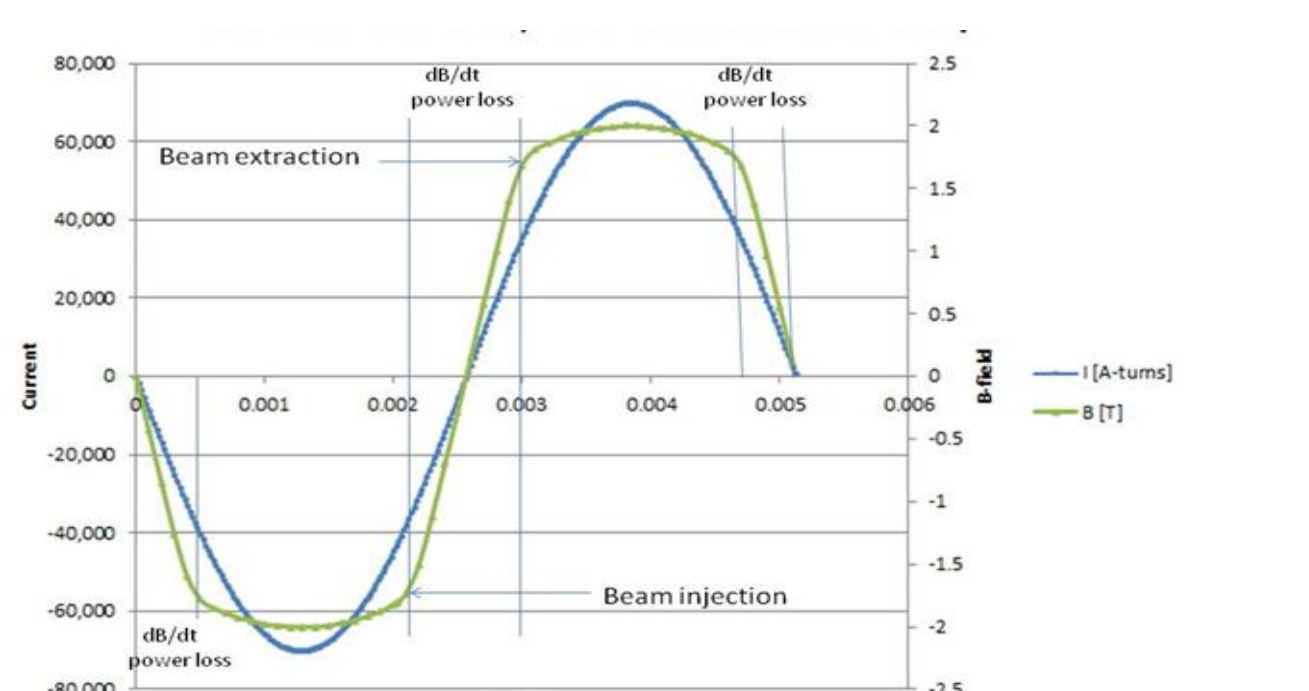
- Six sub-cables form magnet cable.
- Sub-cable consists of 12 2-mm REBCO tapes wrapped at 10 cm pitch over SS cryogenic pipe (8 mm x 0.5 mm).
- Current per sub-cable 6 kA.
- Cable current 36 kA.
- Magnet energizing current 72 kA.
- Liquid helium: 5.5 K @ 0.28 MPa, volume 2 L / m

## SIMULATION OF HTS CABLE HYSTERESIS LOSS AT 2T\_1000 T/S\_15 K

### B-field simulation of magnet core



Magnet core simulation in COMSOL. HTS sub-cables position optimized for minimum perpendicular B-field.



### Hysteresis loss of twisted HTS tapes in B<sub>PERP</sub>

$$Q_{\text{hyst}} = B_{\text{max}} \times N \times I_c \times \frac{w}{\pi \cos(\alpha)} \quad [1]$$

$I_c$  = critical current per tape

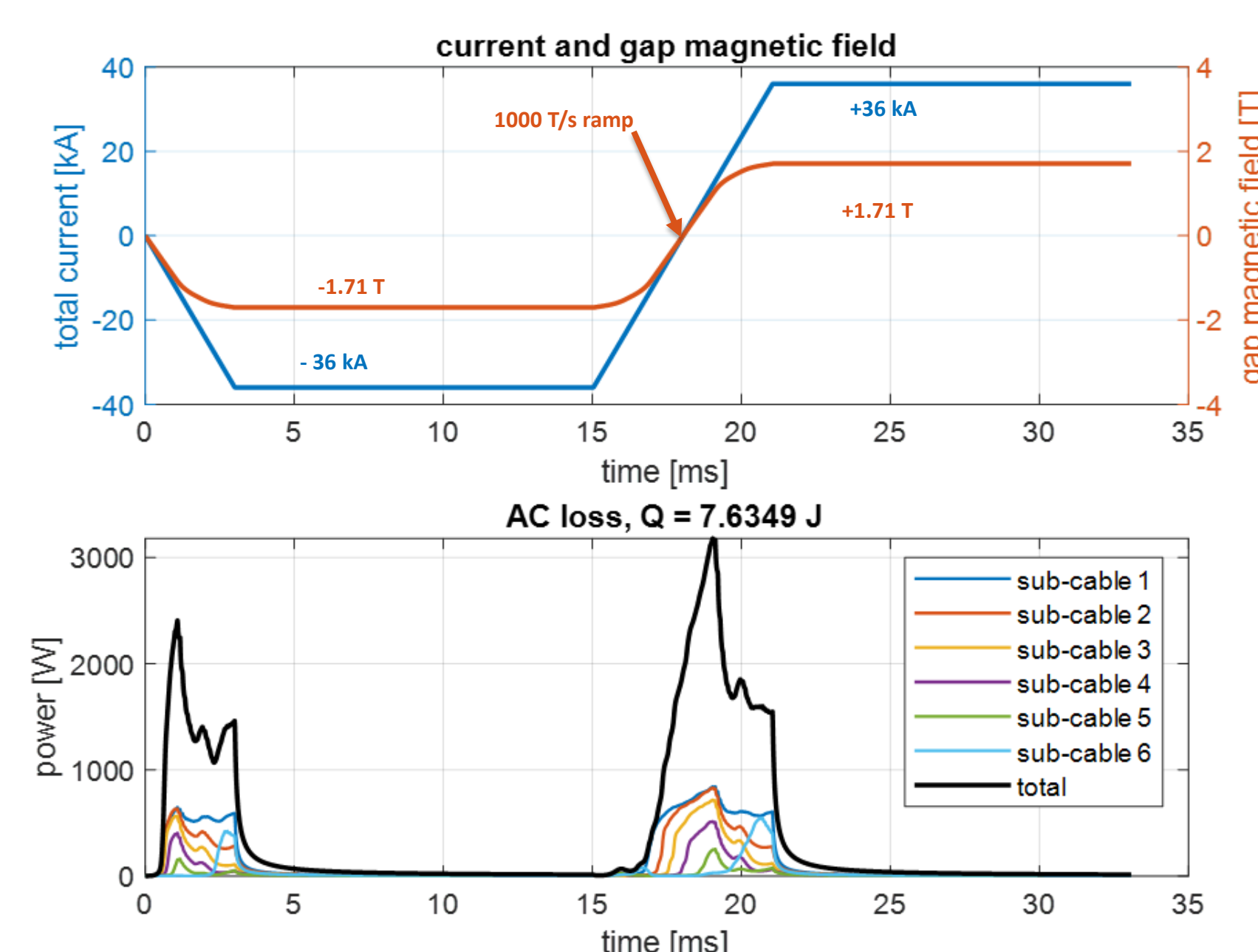
$N \times I_c$  = critical current per sub-cable

$\alpha$  = tape lay angle ( $0^\circ$  = straight tape)

$\frac{w}{\pi \cos(\alpha)}$  = effective tape width & length

Operational current  $I_o = 0.5 I_c$

Operational temperature  $T_o = 15 K$



## PROJECTION OF HTS CABLE HYSTERESIS LOSS AT 5.5 K

### Scaling hysteresis loss from 15 K to 5.5 K

• Effect of He specific heat

$C_p$  (5.5 K)  $\sim 6 \times C_p$  (15 K)

$Q_{\text{hyst}}$  (5.5 K)  $\sim 0.17 Q_{\text{hyst}}$  (15 K)

• Effect of operational temperature [2]

Operational  $T_{\text{max}} = T_o + 5 K$

$N_{\text{HTS}}$  (10 K)  $\sim 0.67 N_{\text{HTS}}$  (20 K)

[2] C. Senatore et al., <https://arxiv.org/1512.01930>

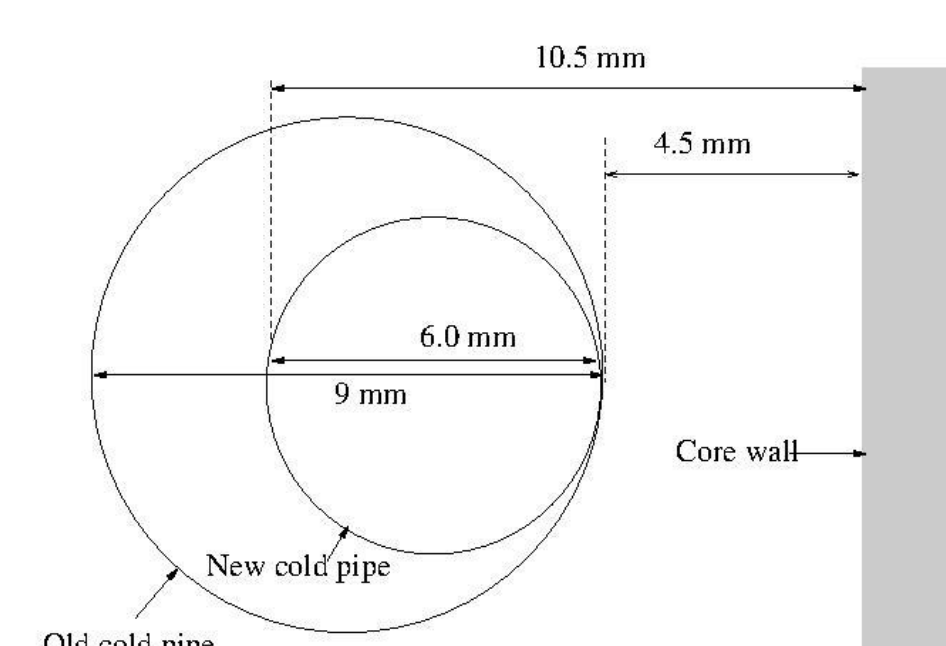
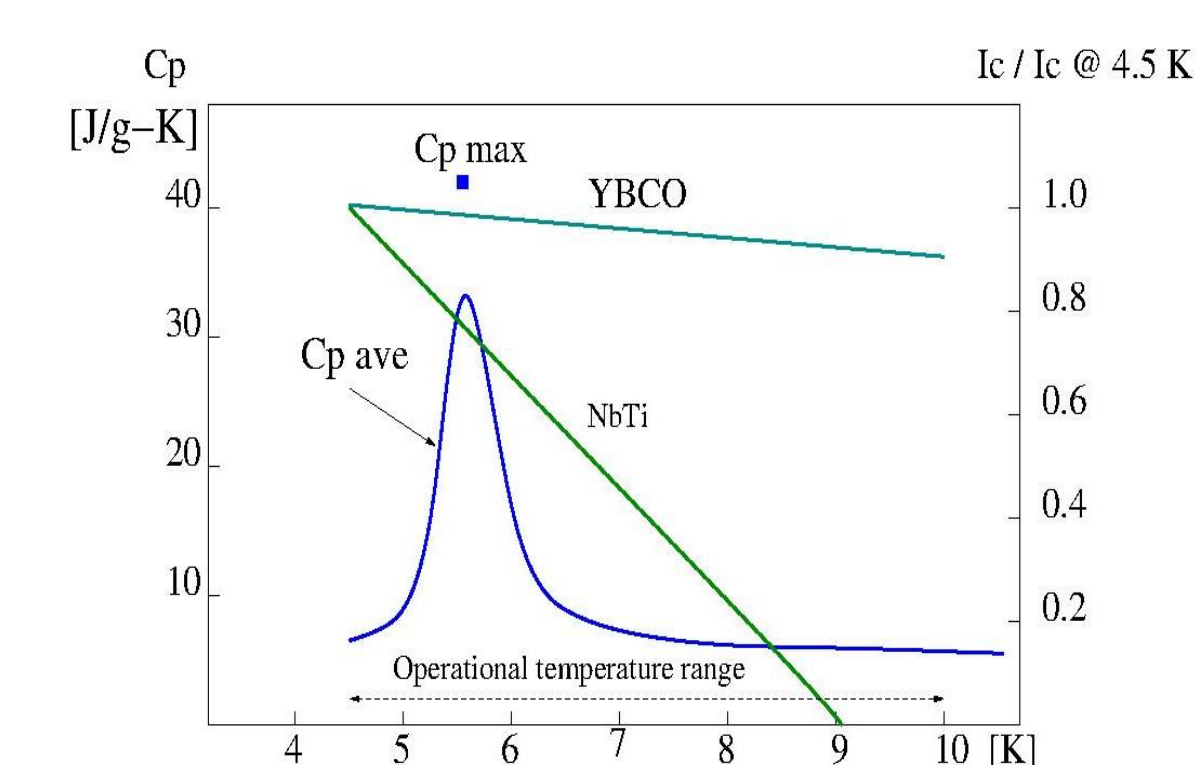
• Effect of B-field exposure

$D_{\text{cryo-pipe}}$  (5.5 K) = 0.67  $D_{\text{cryo-pipe}}$  (15 K)

$\langle B \rangle$  @  $D = 6 \text{ mm}$   $\Rightarrow \sim \frac{1}{2} \langle B \rangle$  @  $D = 9 \text{ mm}$

$Q_{\text{hyst}}$  (0.5 B)  $\sim 0.5 Q_{\text{hyst}}$  (B)

•  $Q_{\text{hyst}}$  (5.5 K) = 0.056  $Q_{\text{hyst}}$  (15 K)



### Projected hysteresis loss at 5.5 K for full magnet:

$$Q_{\text{hyst}} (5.5 K) = 4 \times 7.8 \text{ J/m} \times 0.056 = 1.75 \text{ J/m}$$

## PROJECTED CRYOGENIC POWER @ 2T\_1 KT/S\_5 Hz\_5.5 K

COP (300 K  $\rightarrow$  5.5 K): 1.9 %, Cryo-plant efficiency: 20 %

$$P_{\text{CRYO}} = 1.75 \text{ J/m} \times 0.019^{-1} \times 0.20^{-1} \times 5 \text{ s}^{-1} = 2.3 \text{ kW/m}$$

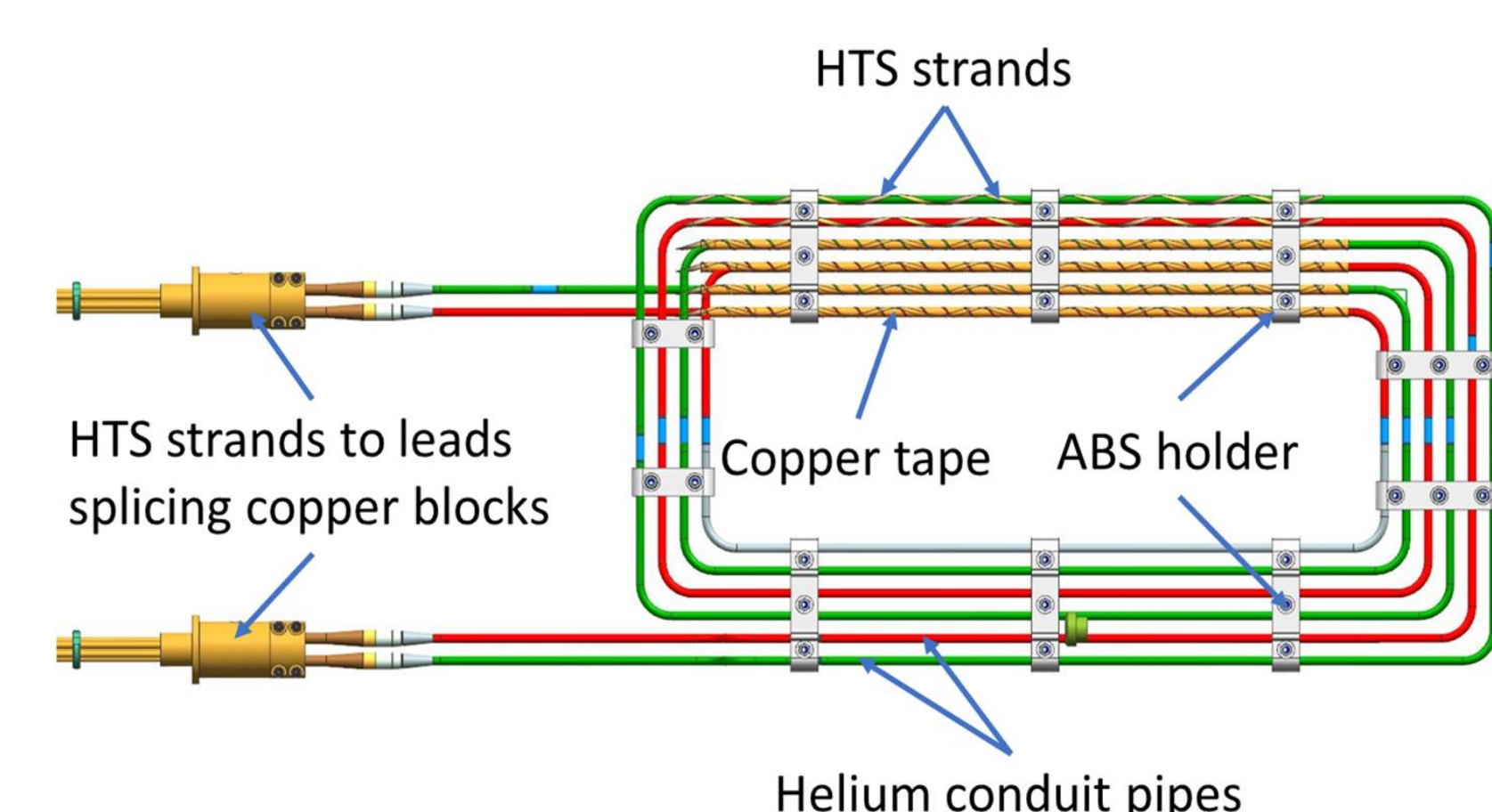
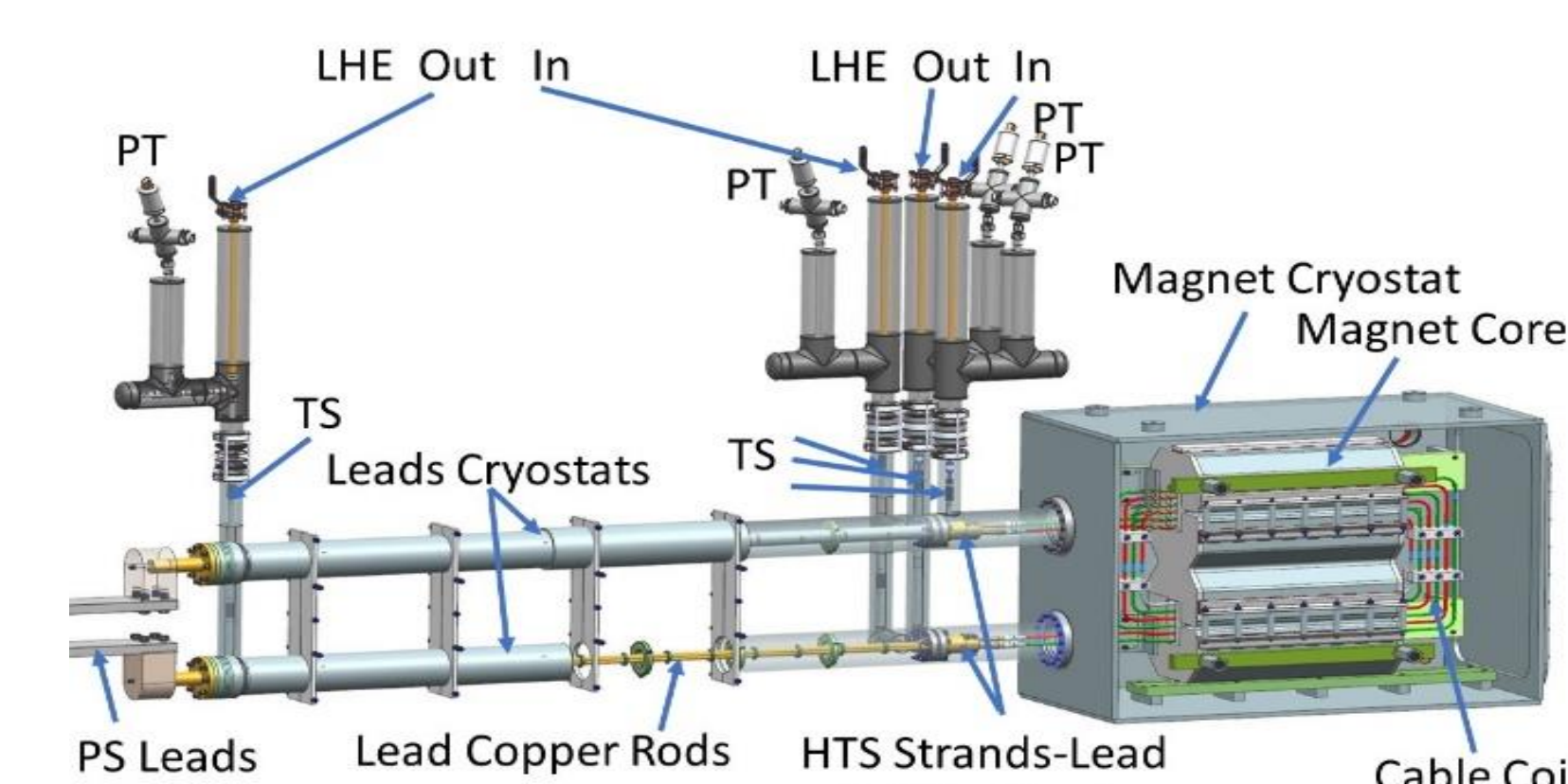
FNAL Booster:  $P_{\text{LCW}}$  (Cu, 0.7 T, 30 T/s, 15 s<sup>-1</sup>) = 8.6 kW/m

Sine-wave current wave-form & B-field response. Core saturates at about 2 T. Current to B-field linear in +/- 1.7 T.

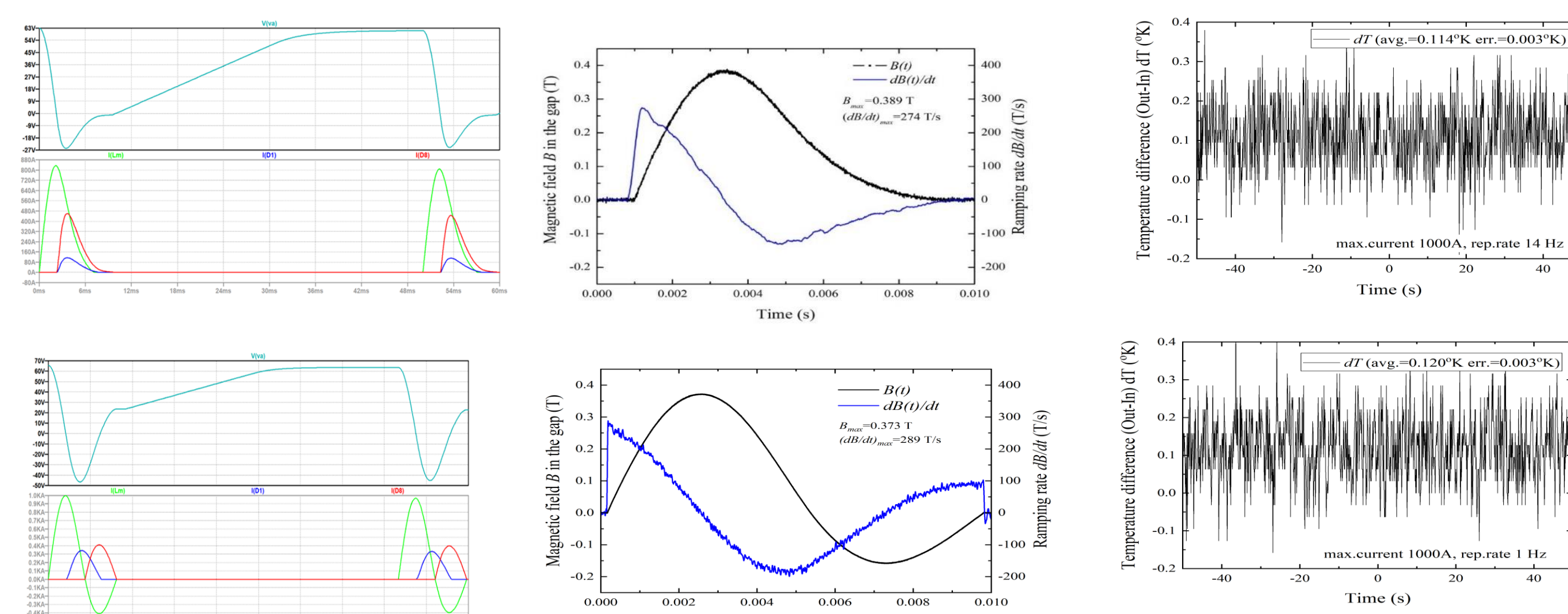
Hysteresis loss (¼ magnet) @ 2 T\_1 kT/s\_15 K = 7.8 J/m. Sine-wave current represented by step function. Colors show hysteresis loss of individual sub-cables.

[1] Numerical calculation, see also Solovyov et al., <https://doi.org/10.1088/1361-6668/ach08e>

## RAPID-CYCLING HTS MAGNET POWER TEST AT 0.4 T\_300 T/S\_10 Hz\_5.5 K [3]



- ❑ Cable split to 2 parallel sub-cables, each 0.5 kA.
- ❑ Two sub-cables (1 kA) make 3 turns.
- ❑ YBCO tapes (2.5 mm x 0.1 mm) wrapped at 10 cm pitch over helium conduit pipe.
- ❑ Cu tape wrapped over YBCO tapes @ 5 cm pitch.
- ❑ ABS holders/spacers hold cable structure and secure position within magnet core cable space.
- ❑ MLI (40 layers) wrapped over cable assembly.
- ❑ LHe: 5.5 K, 0.28 MPa, 2.5 g/s.



Unipolar & bipolar energizing current & magnetic field generated by discharge capacitor bank: 960  $\mu\text{F}$  @ 80 V.

[3] Henryk Piekarz, Brad Claypool, Steve Hays, Matt Kufer, Vladimir Shiltsev, «Record High Ramping Rates in HTS Based Supercond. Accelerator Magnet», MT 27, IEEE Transation on Applied Superconductivity, 32 (2022) 6, 4100404

HTS cable temp. rise @ 300 T/s. Top @ 1Hz, Bottom @ 10 Hz.  $\Delta T$  (10 Hz – 1 Hz) < +/- 0.003 K.  $Q_{\text{cable}} < 0.06 \text{ W/m}$



1 – Magnet, 2- Current leads, 3- Power supply, 4 – Control electronics, 5- Liquid Helium lines