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² Characterization of FBK SiPM sensors for the DUNE Far ³ detector 1 Photon Detection System

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ABSTRACT: The Deep Underground Neutrino Experiment (DUNE) is a long baseline neutrino 37 experiment based in the USA and composed of a Near Detector (ND) complex at FermiLab and 38 a Far Detector (FD) complex located at the SURF Underground Laboratory ~1300 km distant. 39 DUNE will study the neutrino oscillations looking for CP violation in leptonic sector starting 40 from the early 2030s. The FD modules will be composed of four Liquid Argon Time Projection 41 Chambers (LAr TPC) each one with a volume of 17kton that will exploit both charge and light 42 signals to detect neutrino interactions with Argon. The light signals produced by the scintillating 43 photons in LAr will be detected by the Photon Detection System (PDS) based on light collectors 44 coupled to Silicon Photomultipliers (SiPMs). During a test campaign, different laboratories of the 45 collaboration performed an investigation of the best SiPM candidates that fulfill the DUNE FD 46 requests. We identified two models of SiPM, produced by Hamamatsu Photonics K.K. (HPK) and 47 Fondazione Bruno Kessler (FBK), respectively. In this paper, we focus on the FBK selected model 48 showing its main features. We will describe the characterization protocol, the results at room and 49 cryogenic temperatures and the photon detection efficiency measurements. 50

51 KEYWORDS: Photon detectors for UV, visible and IR photons (solid-state), Photon detectors for

⁵² UV, visible and IR photons (solid-state) (PIN diodes, APDs, Si-PMTs, G-APDs, CCDs, EBCCDs,

53 EMCCDs, CMOS imagers, etc), Time projection Chambers, Neutrino detectors

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67 1 Introduction

DUNE (Deep Underground Neutrino Experiment) is a next-generation long baseline neutrino 68 experiment whose main goal will be a detailed study of neutrino oscillation. DUNE will consist 69 of a NEAR detector (ND) placed in proximity of the neutrino production site at Fermi National 70 Laboratory, and of a FAR detector (FD) that will be installed in the Surf Underground Laboratory 71 in South Dakota [1]. The DUNE Far Detector module one (FD1) will be a liquid argon time 72 projection chamber (LAr TPC) with an Horizontal Drift (HD) configuration and a total mass of 73 nearly 70 kt. Beyond charge signals, DUNE FD1-HD will also exploit the scintillation light of 74 argon whose peak wavelength is 127 nm [2]. Light signals will be collected in the Photon Detection 75 System (PDS) thanks to the so-called X-ARAPUCA modules. These modules allows to trap photons 76 inside a highly reflective box that contains wavelength shifting bars and visible sensitive Silicon 77 Photo-Multipliers (SiPM) sensors [3]. 78

FD1-HD will employ SiPMs produced by two different companies: Fondazione Bruno Kessler 79 (FBK) and Hamamatsu Photonics K.K (HPK) [4]. Both models are designed for the use at cryogenic 80 temperatures and have an effective area of around 36 mm², while they have different characteris-81 tics in terms of the cell pitch, the breakdown voltage and the quenching resistor. These models 82 have been selected after an R&D phase, carried out by the PDS Consortium, in collaboration with 83 the manufacturers, looking for the prototypes that addressed the technical requirements for the 84 FD1-HD. The tests concerning FBK CRYO-NUV-HD-3T sensors, that will be presented in this 85 paper, have been performed in seven different test sites of the PDS Consortium: Bologna (Istituto 86

87 Nazionale di Fisica Nucleare and Università di Bologna), DeKalb (Northern Illinois University,

88 Department of Physics), Ferrara (Istituto Nazionale di Fisica Nucleare and Università di Ferrara),

89 Madrid (CIEMAT, Centro de Investigaciones Energéticas, Medioambientales y Tecnológicas), Mi-

⁹⁰ lano (Istituto Nazionale di Fisica Nucleare and Università di Milano-Bicocca), Prague (Institute of

Physics, Czech Academy of Sciences), and Valencia (Instituto de Física Corpuscular).

The paper is organized as follows: in the first section 2.3 a detailed description of the main features of the FBK sensors customized for DUNE compared to the other FBK models. In the second section 3 there is a description of the measurements performed by the PDS consortium members to characterize the SiPMs at cryogenic temperatures with a adescription of the setup and procedure used. Then, a dedicated section 4 describes the Photo Detection Efficiency (PDE) measurements. Eventually, there will be the discussions of the results and the conclusions.

98 2 SiPM features

99 2.1 NUV-HD-Cryo Technology

Over the years, FBK has developed various technologies of SiPMs to obtain optimal performances 100 to meet the requirements of different experiments and applications. Silicon Photomultipliers are 101 matrices of Single-photon avalanche diodes (SPADs) each one with an integrated quenching resistor 102 and connected together in parallel forming a single sensor. Depending on the type of epitaxial 103 layer used for the fabrication, we can distinguish two families of technologies: p-on-n junction 104 with an n-type epitaxial layer labeled as FBK NUV-HD technologies characterized by a peak 105 detection efficiency in the near-UV[5], and n-on-p junction with a p-type epitaxial layer named 106 FBK RGB/NIR-HD, featuring a peak detection efficiency at longer wavelengths[6][7]. Starting 107 from the standard NUV-HD technology, a customization of the electric field was implemented to 108 develop the NUV-HD-Cryo SiPM technology for cryogenic applications such as in the DarkSide 109 experiment. Strengths of this technology are a very low dark count rate in the order of few mHz/mm² 110 at cryogenic temperature and a lower afterpulsing probability, as a result of a low peak value of the 111 electric field compared to the standard FBK technology[8]. 112

113 2.2 DUNE Customization

In the framework of the DUNE experiment, a dedicated customization of the NUV-HD-Crvo SiPM 114 technology was carried out to improve the performance of the detectors to better comply with the 115 experiment requirements. The gain of a SiPM microcell, defined as the number of carriers generated 116 during an avalanche process, is a key factor to improve the signal to noise ratio enhancing the output 117 signal. During the avalanche build-up the number of generated carriers is proportional to the active 118 area of the microcell, thus increasing the cell size the gain increases. However, this gain increment 119 comes with a drawback of a higher correlated noise (optical crosstalk), because the generation of 120 secondary photons is proportional to the amount of carrier flowing during the avalanche. The aim 121 of the DUNE customization was to modify the standard SiPM structure to obtain a device that 122 combines a high gain and a limited crosstalk. This has been done by increasing the number of 123 Deep Trench Isolation (DTI) between neighboring cells. Two different layout splits were produced 124 and tested to evaluate the best option for the DUNE experiment, a $30\mu m$ cell pitch device with a 125 standard single DTI to be used as a reference, and a $54\mu m$ cell pitch device with three DTIs. 126



Figure 1. a) Cross-section of the $30\mu m$ cell pitch device with a standard single DTI $(1T - 30\mu m)$, b) Cross-section of the $54\mu m$ cell pitch device with three DTIs $(3T - 54\mu m)$.

In figure1 the cross-sections of the two different layout splits with all the basic features of the 127 cell structure are depicted. The high-field region (pink structures in the figure) where the avalanche 128 takes place is implemented by a high energy ion implantation. The quenching resistors, which 129 are needed to quench and subsequently recharge the microcells, are represented in red, while the 130 metal contacts are shown in black. On the top part of the cell, a passivation layer is represented in 131 light blue. Each cell of the SiPM is separated by deep trenches (gray structures) filled with silicon 132 dioxide that are effective to electrically isolate the cells and also partially optically isolate nearby 133 cells from the crosstalk photons. 134

135 2.3 Features at room temperature

In this section the results of a functional characterization of the two layout splits are reported providing a comparison in terms of gain, crosstalk and PDE. The measurements were acquired placing the devices in a climatic chamber at 20 degrees Celsius following a procedure described in a dedicated paper[9]. The PDE was measured at room temperature by using a pulsed mode technique with a setup featuring an integration sphere and LEDs of different wavelength, for further details refers to [10].

In figure 2 the gain as a function of the overvoltage is shown. The gain of the triple trench is approximately 2.6 times the gain of the single trench split.

In figure 3 the direct crosstalk probability as a function of the overvoltage is reported. The single trench layout exhibits a slightly higher value with respect to the triple trench. Measurements were performed on test structures of $1 \times 1 \text{ mm}^2$ active area without any protection resin on top of the devices.

The PDE at 435 nm as a function of the overvoltage is shown in figure 4. Measurements were performed on a test structure of $1x1mm^2$ active area with an epoxy resin layer of approximately 500 μm on top of the devices to to smooth the oscillations in the PDE spectrum created by the constructive and destructive interferences caused by the top ARC on SiPM area. PDE increases with increasing overvoltage thanks to the increased triggering probability, reaching a saturation level at higher overvoltage. The two different splits exhibit similar values as expected from the similar geometrical fill factor between the two layouts (75% and 77%).

As reported in this section, the two different layout splits exhibit similar Optical Crosstalk and PDE while the gain of the triple trench is 2.6 times the gain of the single trench split. The $54\mu m$ cell



Figure 2. Comparison of the Gain as a function of the overvoltage between the two different splits $(1T - 30\mu m; 3T - 54\mu m)$.



Figure 3. Comparison of the direct crosstalk probability as a function of the overvoltage between the two different splits $(1T - 30\mu m; 3T - 54\mu m)$.

¹⁵⁷ pitch device with three DTIs was selected for the DUNE experiment for its higher gain.

158 **3** Cryogenic characterization

159 3.1 Experimental apparatus and procedure

Different institutions belonging to the PDS consortium of the DUNE collaboration were involved in the characterization of the sensors. These are: INFN and University of Bologna, INFN and University of Ferrara, CIEMAT Madrid, INFN and University of Milano Bicocca, INFN and University of Napoli, FZU Prague and IFIC Valencia. In addition, researchers from INFN and University of Napoli performed a dedicated measurement of the SiPM Photodetection Efficiency at liquid argon temperature, through a specific setup which will be described in section 4.



Figure 4. Comparison of the Photon Detection Efficiency (PDE) at 435nm as a function of the overvoltage between the two different splits $(1T - 30\mu m; 3T - 54\mu m)$.



Figure 5. Setup used for the characterization of the sensors. a) Sketch of the apparatus used for IV measurements. b) Sketch of the apparatus used for DCR study, c) Temperature of the sensor during the diving in LN2 phase.

In order to guarantee compatible results in all the laboratories, each apparatus used for the tests complies with common specifications decided by the photon detection system consortium of DUNE. A detailed description of the prototype of the setup and the protocol followed during the measurements are provided in this section. Each laboratory have chosen similar solutions with same or best specifications.

The core of the setup consists of a liquid nitrogen dewar where the sensors are placed in order to perform tests at cryogenic temperatures. Depending on the type of measurements to perform, different commercial instruments, with different features, have been used. A picture that shows a sketch of the apparatus is shown in figure 5. The apparatus is also instrumented with a mechanical linear stage that allows to dive the sensors in liquid nitrogen following a controlled thermal profile. This can be done thanks to a temperature sensor placed in the proximity of the SiPM. An example of a typical thermal profile during the diving phase is shown in figure 5-c.

The SiPMs IV measurements have been performed by a commercial source meter unit (SMU) directly connected to the SiPM through triaxial cables while the Dark count rate (DCR) characterization required a more complex apparatus that exploit the SMU to bias the SiPM with a stabilized voltage, a cryogenic amplification stage and an oscilloscope to acquire the signals. For the IV measurements, the minimum requirements for the SMU are (0-60) V voltage range, 10 pA precision, 6 digit resolution used with cables whose loss is less than 10 pA.

For the dark noise and gain measurements, the amplification stage is common for all the labs and is described in a dedicated paper [11]. The output of the amplifier is connected to the input of a digital oscilloscope, whose minimum requirements, established by the PDS consortium, are 1 GHz bandwidth, 5 Gs/s and 8 bit resolution. The DCR measurement is performed in a completely dark environment at three different values of over voltage V_{OV} , acquiring the waveforms with a trigger threshold of 0.5 photoelectron. We perform a dedicated analysis based on single signals observing their temporal and amplitude distributions.

The measurements sequence has also been defined to be common to all the labs involved in the test characterization. It has been organized as follows:

- IV curve at room temperature;
- 1^{st} diving phase;
- IV curve at LN2 during the first thermal cycle;
- 18 thermal cycles;
- IV curve at LN2 at the 19^{th} thermal cycle;
- DCR at three different values of V_{OV} during the 20th thermal cycle.

All the results are then compared and organized together to obtain common results that will be presented in this paper in section 3.2.

201 **3.2** Cryogenic characterization results

With the setup described in section 3.1, the different laboratories performed an investigation of 202 the main features of the FBK-TT SiPMs. We initially measured the current-voltage (IV) curve at 203 room temperature and at LN2 both at the first immersion and after 19 thermal cycles. The IV curve 204 allowed us to obtain the breakdown voltage (V_{BD}) and the quenching resistor (R_q) . The breakdown 205 voltage V_{BD} has been estimated looking at the peak of the normalized derivative of the IV curve in 206 the reverse region, as decided within the PDS consortium. The maximum of the curve $I^{-1}dI/dV$ 207 has been fitted with a polynomial function of 2^{nd} degree in order to estimate the best value of V_{BD} . 208 In the forward region of the IV curve, a linear fit in the range [1.2-1.5] V allowed us to assign the 209 value of the global quenching resistor of the sensor as the reciprocal of the angular coefficient. The 210 value of the quenching resistor of each cell (R_q) can be then easily derived assuming equal resistors 211 for each cell. In figure 6 are shown two examples of the measured IV and the fits in the forward and 212 reverse regions while SiPM is kept at room temperature. 213



Figure 6. Left side: IV curve in reverse mode (REV). The normalized derivative and the parabolic fit are also shown in the plot. Right side: IV curve in the forward (FW) region.



Figure 7. On the left part: histogram of the differences in the breakdown voltage values measured before and after the thermal cycles with a Gaussian distribution superimposed. On the right figure: histogram of the differences in the quenching resistor values measured before and after the thermal cycles with a Gaussian distribution superimposed.

In the table1 are summarized the main parameters obtained during IV measurements at room temperature and at LN2 after the 19^{th} thermal cycle.

Temperature	V_{bd} (V)	$R_q(k\Omega)$
300 K	33.0±0.1	560 ±10
77 K	27.08±0.03	2640±70

Table 1. Mean values for breakdown voltage and quenching resistor obtained from the various laboratories both at room temperature and at liquid nitrogen temperature.

In order to check the resilience of the sensors to the thermal stresses, we decided to check sensor by sensor the variation of both breakdown voltage and quenching resistor before and after



Figure 8. On the left part an example of a scatter plot of amplitude VS time delay between consecutive events (top) and the corresponding x-axis projection histogram (bottom). In the right part of the figure the amplitude histogram of single signals in logaritmic-scale is shown, it corresponds to the y-axis projection of the figure on the left. Yellow curves superimposed to the distribution represent the Gaussian fits of the 1p.e., 2p.e. and 3p.e. peaks.

the thermal cycle. Figure 7 shows on the left the histogram for the breakdown voltage difference 218 where V_{BD}^{pre} and V_{BD}^{post} represent respectively the value at the 1st and at the 19th thermal cycle. The 219 distribution is centered at 0 V as expected if no damages occur, and has a width calculated as the 220 standard deviation of the Gaussian distribution of (31 ± 2) mV. On the right part instead is shown the 221 histogram of the resistors difference of the entire SiPMs (as calculated from the direct IV curve) 222 measured after the thermal stresses $(R_{\text{SiPM}}^{\text{post}})$ and the one measured before $(R_{\text{SiPM}}^{\text{pre}})$. Also this last 223 distribution is centered at 0Ω and it has a standard deviation of $(2.5 \pm 0.1)\Omega$ which is negligible, 224 considering that the systematic uncertainty in the measurements of the resistor due to the electrical 225 contacts at room and LN2 temperature can be estimated as few Ohms. 226

No values distant more than 70 mV and 10Ω in the absolute value of the breakdown and quenching resistor respectively, have been found, indicating a good reproducibility of the measurements and no substantial variations in the SiPM main characteristics after thermal stresses.

After IV characterization each test site studied the behaviour of the SiPM in a completely dark 230 environment at liquid nitrogen temperature. Thanks to the apparatus described in section 3.1, the 231 acquired waveforms have been used to determine the temporal happening of single events and their 232 amplitude. A typical example of 2-dim plot amplitute VS time delay, with all the components of 233 the correlated noise, is shown in figure 8 on the left side. As clearly visible from the temporal 234 distribution of the events, these SiPMs are affected by the so called burst effect, for which trains 235 of consecutive pulses at kHz-rate happened. This phenomenon is better described in a dedicated 236 paper [12] and is even present in the HPK lot of DUNE SiPMs [4]. On the right part of the figure 237 the amplitude distribution of the events is shown. 238

Figure 9 summarizes the main results we obtained for the gain and the correlated noise characterization. The results are in accordance with the values provided by the vendor. The gain spans from ~ $4.5 \cdot 10^6$ to ~ $9 \cdot 10^6$ in the range [3.5-7] V of overvoltage which is within DUNE



Figure 9. Results of the carachterization of the SiPMs. a) Gain as a function of the overvoltage. b) Dark count rate as a function of the overvoltage. c) Afterpulse and d) Direct plus delayed crosstalk percentage as a function of the overvoltage.

requirements. For the DCR, which is a key parameter in the choice of the photodetectors for the 242 DUNE FD, we can see that the values are included in the rage [50-80] mHz/mm² for the tested 243 overvoltages. It is worth noting that these values include the burst effect that increase the overall 244 dark counts and is correlated to to ionizing radiation that crosses the sensor [12]. Since DUNE FD 245 will be underground and will exploit purified materials, we thus expect a reduction of the burst effect 246 with respect to that measured in surface laboratories during the characterization, and consequently a 247 decrease in the global DCR when the SiPMs will be operated in the FD. However, even with bursts, 248 the measured values for the DCR are within DUNE requirements. The trend of the correlated noise 249 is shown in figure 9c and 9d for afterpulse and crosstalk effects respectively. Also all these values 250 are compliant with DUNE specifications. 251

252 4 PDE at cryogenic temperatures

The absolute PDE is a key performance parameter of SiPMs. PDE is commonly defined as the product of three factors: the SiPM's fill factor, the probability of avalanche triggering, and the silicon's quantum efficiency (QE). QE measures the likelihood of incident photons generating an electron-hole pair within the sensor's sensitive volume and depends on photon wavelength. At
low temperatures the wider energy band gap reduces the quantum efficiency. Furthemore, at
approximatively 80-90K, carrier freeze-out effects may lead to a decrease in PDE [13]. In [14],
a a slight decrease in PDE with decreasing temperature was observed for the CRYO-NUV-HD
technology. Therefore, it is essential to directly measure the PDE at the temperature of operation
(87K in case of liquid argon) for the DUNE customized FBK NUV-HD-cryo 3T production.
The measurement of the PDE involves characterizing the SiPM response under a calibrated light
source. In addition, when determining the PDE, is crucial to account for the intrinsic SiPMs

source. In addition, when determining the PDE, is crucial to account for the intrinsic SiPMs secondary counts arising from delayed correlated noise (after-pulses and delayed optical crosstalk).

266 4.1 Experimental Setup

The measurement detailed in this paper were conducted by using the setup called Vacuum Emission Reflectivity Absorbance (VERA) built at TRIUMF in Vancouver to characterize the response of SiPMs at cryogenic temperatures [15].

In this setup, the SiPM sample under test was mounted on a cold finger cooled by liquid nitrogen 270 and regulated by a control system to maintain the temperature with an accuracy better than 1 K. The 271 setup is consisting of a vacuum chamber coupled with a light source from a Resonance Lyman-Alpha 272 DC Lamp and a VM200 Resonance monochromator. In order to measure the absolute incident 273 light flux into the SiPM the light was directed toward a Photo-Diode (AXUV 100G). The AXUV 274 100G Photo-Diode was previously calibrated, at LAr temperature, against a NIST calibrated Photo-275 Diode (XUV-100C). The SiPM and the AXUV 100G photodiode are both placed on a movable 276 arm which allows for remote x-y positioning. The incident light selected by monochromator is 277 directed alternatively toward the SiPM under test and the Photo-Diode. In order to avoid geometric 278 factors the light spot (1.2mm diameter) in contained within the area of both sensors. Throughout 279 the measurement, light stability was monitored by an Hamamatsu PMT (R8486) after reflection by 280 a gold coated mirror. The VERA system has already been used to measure the PDE at cryogenic 281 operating temperature in the context of the nEXO ([16],[17]) and DarkSide experiments. A layout 282 of the hardware setup is shown in figure 10. 283

The SiPM PDE was measured both in photon-counting mode and current mode. In the first 284 case, the SiPM signal was amplified by a dedicated two-stage amplifier and then acquired by a 285 CAEN DT5730B Digitizer Module. The SiPM pulses in this case are individually reconstructed 286 and counted in order to estimate the SiPM rate which will be compared with absolute photon 287 flux measured by Photo-Diode. When measured in current mode, a Keysight B2985 low noise 288 picoammeter¹ were used for both the SiPM and the Photo-Diode. To minimize the noise induced 289 on the Photo-Diode by other sources, a shielded low noise triax cable (Keithley 7078-TRX-1) were 290 used. A MIDAS-Labview based control system [18] served as system interface and provided slow 291 control of the entire hardware system. 292

¹RMS noise with open input of ~140 aA



Figure 10. Hardware setup used for PDE measurement of FBK NUV-HD-cryo 3T sample at 87 K

293 4.2 PDE measurement procedure

The first step is to quantify the delayed correlated noise contribution of the SiPM under test as 294 a function of the applied overvoltage. To achieve this, the light wavelength was set to 420 nm 295 and light level was adjusted on a proper level to allow at same time for the pulse-counting of the 296 individual waveforms and the S/N of the photodiode high enough to measure the light from DC 297 lamp. Tipically, Photo-Diode currents of the order of ~ 50 fA, were measured in these conditions. 298 Since photons inducing avalanches and dark noise are uncorrelated events, they can be distinguished 299 from correlated delayed avalanches by analyzing the time distribution of all pulse events relative to 300 the primary pulse, as demonstrated in Ref. [19]. The total pulse rate, computed as function of the 301 time difference, t, from the primary pulse (t = 0) is given by: 302

$$R(t) = R_{DC}(t) + R_{CDA}(t) + R_0(t)$$
(4.1)

where $R_{DC}(t)$ is the dark count rate, $R_{CDA}(t)$ is the rate of correlated delayed avalanches per pulse, and $R_0(t)$ is the rate of the photon induced avalanche detected by the SiPMs due to light source. In figure 11 the pulse rate R(t) measured at 87 K under 420 nm illumination, is shown as function of the time difference with respect to the primary pulse. As shown in [19] the rate of correlated delayed pulses is expected to vanish at sufficiently larger time. The primary pulse rate



Figure 11. Observed pulse rate R(t) measured at 87K and 420 nm as a function of time differences with respect to the primary pulse for FBK NUV-HD-cryo 3T sample. The distribution is shown when SiPM is biased at 3, 5, 7 V overvoltages.

³⁰⁸ $R(t) = R_{DC}(t) + R_0(t)$, due to dark count and light source, can then be estimated from the figure ³⁰⁹ 11, performing a weighted mean of the asymptotic rate at long times (t > 1 × 10³ ns). ³¹⁰ Since R_{DC} is independently measured in the absence of light (with the Iris closed), by using the

Since R_{DC} is independently measured in the absence of light (with the Iris closed), by using the same method of the rate plot, the true photon-induced rate $R_0(t)$ can be measured. The SiPM PDE at 420 *nm* can be obtained dividing the measured SiPM primary count rate by the the photon flux Φ_0 measured by moving the calibrated photodiode under the light beam and defined as

$$\Phi_0 = \frac{(I - I_{DCR})\lambda}{R(\lambda)hc}$$
(4.2)

where *I* and I_{DCR} are the photodiode currents with and without illumination, respectively, R is the photodiode responsivity at the wavelength λ , *h* is Planck's constant and *c* is the speed of light. The PDE at 420 *nm* then is given by

$$PDE_{420} = \frac{R_0(t)}{\Phi_0} \tag{4.3}$$

³¹⁷ By following this procedure, the quantity PDE_{420} has been measured as a function of the ³¹⁸ applied overvoltage from 3 V up to 8 V (Fig. 12).

Measuring the PDE in counting mode is too time-consuming to be performed at every wavelength. The PDE as function of wavelength values can be determined by measuring the currents of the photodiode and the SiPM for wavelengths scanned by monochromator. Specifically, the SiPM current at a given wavelength λ and applied overvoltage V is connected to the PDE through the following formula

$$I_{SIPM}(V,\lambda) - I_{SIPM}^{DCR}(V) = \Phi_0(\lambda) \times PDE(V,\lambda) \times f(V)$$
(4.4)



Figure 12. Photon Detection Efficiency measured at 420 nm and 87K as a function of the applied overvoltage for the FBK NUV-HD-cryo 3T sample.

where $I_{SIPM}(V, \lambda)$ and $I_{SIPM}^{DCR}(V)$ are the SiPM current with and without illumination at the wavelength λ , $\Phi_0(\lambda)$ is the photon flux rate measured with photodiode for light illumination at wavelength λ , and f(V) is a correction factor that accounts for the SiPM gain and for the correlated avalanche noise, which artifically increase the total SiPM output current. It can be written as

$$f(V) \sim q_e \times (1 + ECF) \times G \tag{4.5}$$

where *ECF* is the extra charge factor and *G* is the SiPM gain. It is possible to consider f(V) as a function of the applied bias voltage and to be wavelength-independent because it depends only on the intrinsic characteristics of the SiPM.

In this work f(V) is estimated at 87K by illuminating SiPMs with continous light source at 420 nm as follows:

$$f(V) = \frac{I_{SIPM}(V, 420) - I_{SIPM}^{DCR}(V)}{\Phi_0(420) \times PDE(V, 420)}$$
(4.6)

where we take advantage of the fact that the quantity PDE(V, 420) was previously measured in counting mode.

Once we extracted the wavelength independent factor f(V) for each bias voltage it is possible to measure the PDE for a different wavelength as follows:

$$PDE(V,\lambda) = \frac{I_{SIPM}(V,\lambda) - I_{SIPM}^{DCR}(V)}{\Phi_0(\lambda) \times f(V)}$$
(4.7)

where $\Phi_0(\lambda)$ is defined in eq.4.2, $I_{SIPM}(V, \lambda)$ and $I_{SIPM}^{DCR}(V)$ are the SiPM current with and without the λ illumination. Figure 13 shows the PDE as a function of illumination wavelength, ranging



Figure 13. Photon Detection Efficiency measured at 87K as a function of the wavelength in the range 350-600 nm and of the applied overvoltages 3, 5 and 7 V for the FBK NUV-HD-cryo 3T sample.

from 350 nm to 600 nm in 10 nm increments, and SIPM overvoltage, varying for 3, 5 and 7 V. The error bars on each point includes statistical and systematic uncertainties.

The PDE measurement have been performed at 87 K temperature. The obtained results are in excellent agreement with the measurements performed at 90 K, as reported in [14]. We also report in figure 14 a comparison of the PDE measured at FBK Institute for the same device at room temperature (300 K) at wavelenght of 420 nm.

345 **5** Conclusions

In this paper we described the characteristics and the measurements performed to the NUV-HD-cryo 347 3T SiPM from FBK in order to validate this sensor for the DUNE PDS. FBK sucesfully developed 348 this sensor for DUNE with proprietary technologies aiming a high gain while keeping low the 349 cross-talk probability. FBK together with the DUNE PDS consortium performed the validation 350 tests of these sensors whose results are shown in this publication.

The FBK NUV-HD-cryo 3T sensor, together with HPK S13360-9935 were selected for the DUNE FD1-HD PDS. Comparing the FBK and the HPK sensors, both provide similar characteristics in terms of gain and correlated noise but the sensor from FBK requires a larger over-voltage for a similar PDE, nevertheless, as the breakdown voltage is lower than for the HPK sensors, the operation voltage (for the same PDE) is lower that the required by the HPK sensors.

³⁵⁶ During the DCR measurements, the appearance of pulse trains (bursts), as also happens with ³⁵⁷ the HPK sensors, increases the DCR value expected at cryogenic temperatures but still meets the



Figure 14. Photon Detection Efficiency measured at FBK for 420 nm and 300 K as a function of the overvoltage (blue dots) and the one measured at TRIUMF for 420 nm and 87 K (red dots) for the FBK NUV-HD-cryo 3T sample. The dashed area represents the region of systematic error in the measurement at 87 K.

DUNE requirements. Those requirements are not very strict because DCR will be dominated by the 358 radiogenic background (39Ar) and achieving the lowest possible DCR is not a critical requirement. 359 Still, a complete understanding of the origin of the DCR burst and the optimal layout of the array 360 field may require further investigation, mainly for experiments with tighter radiogenic constraints. 361 We also presented a method and the results of the sensor PDE measurement in the wavelengths 362 range from 350 nm to 600 nm at liquid argon temperature of 87K in order to validate its performance 363 for the DUNE experiment. Within the measurement errors, no reduction with respect to room 364 temperature PDE have been observed. 365

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