

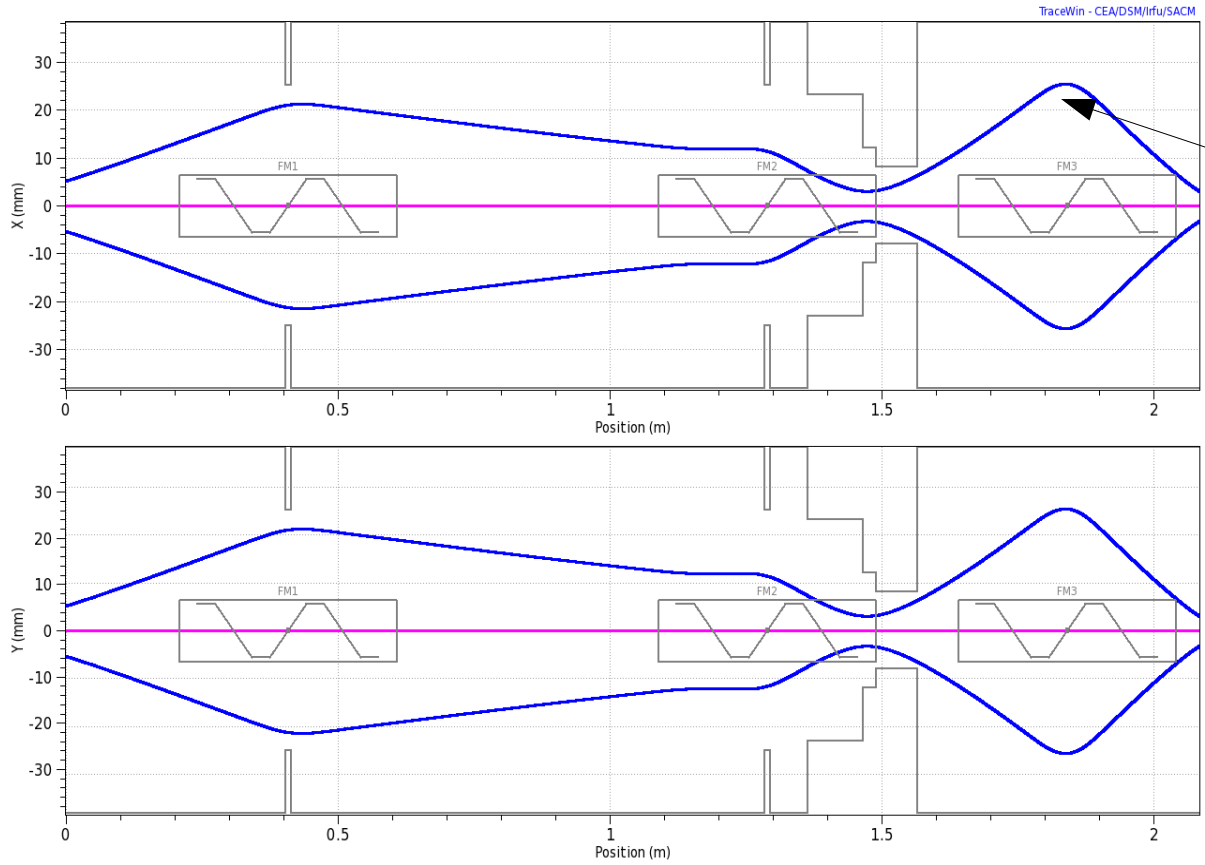


LEBT Simulations Recent Work

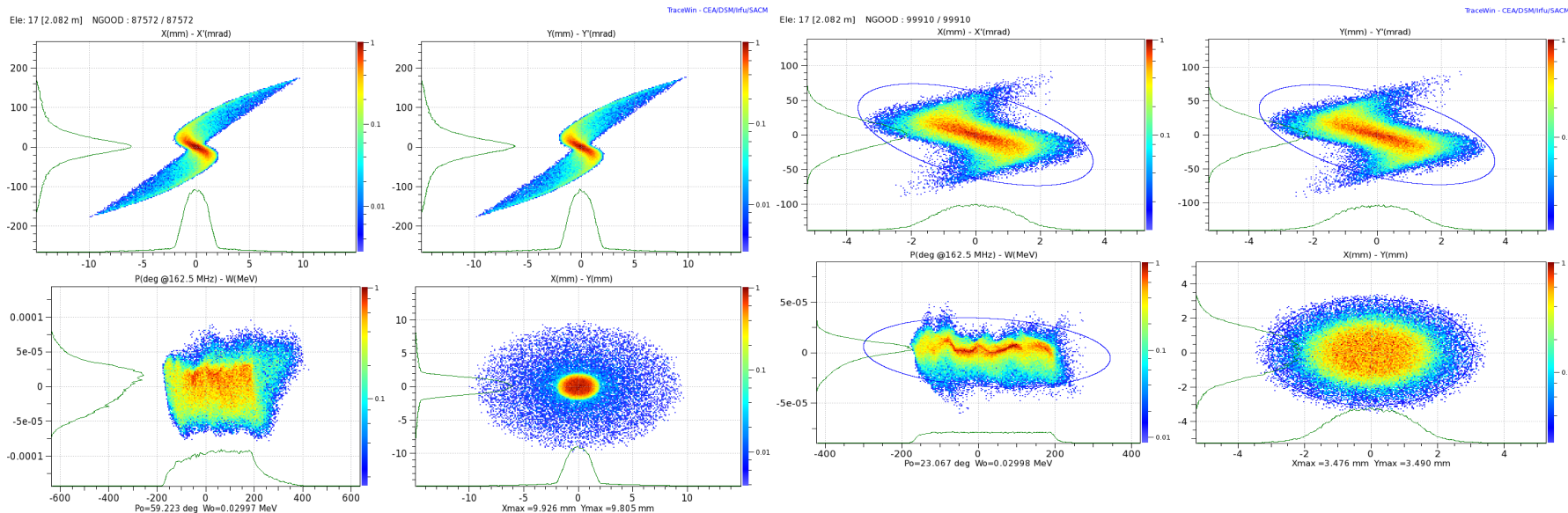
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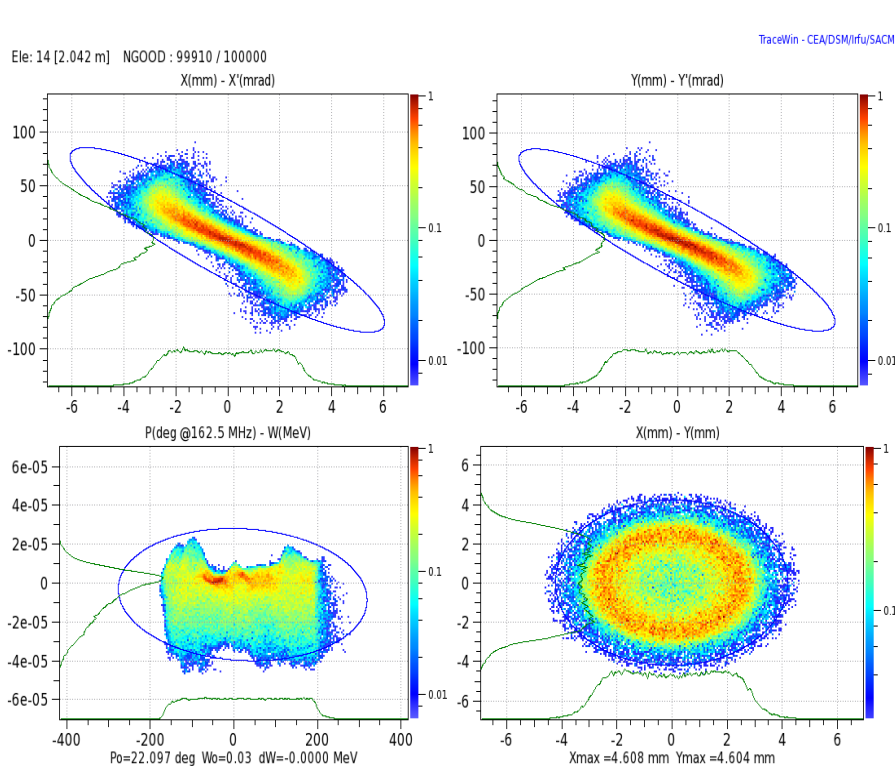
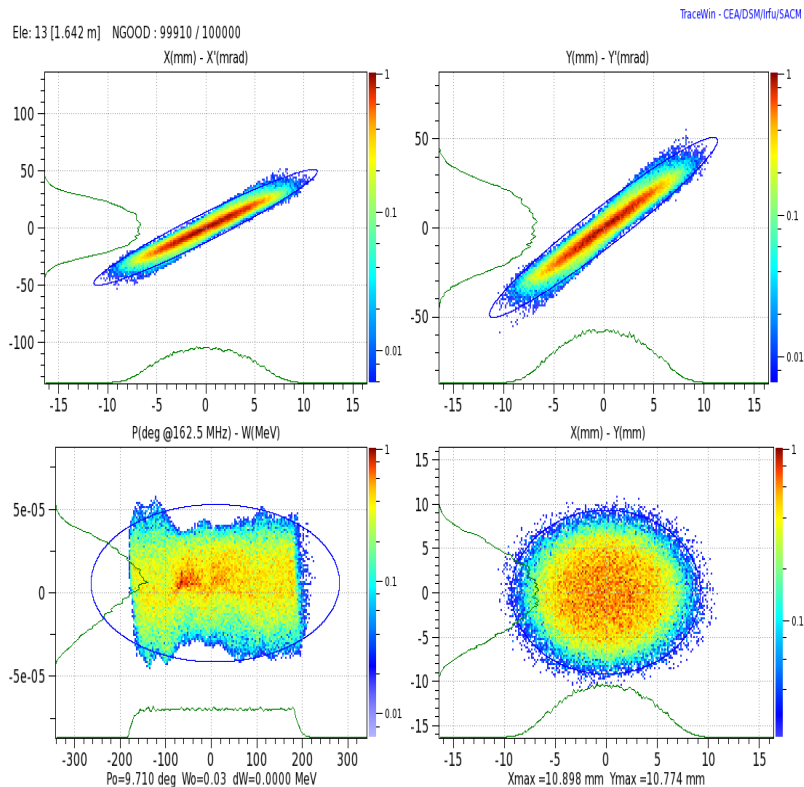
**Full beam size
> 1/2 solenoid
aperture in
solenoid 3**

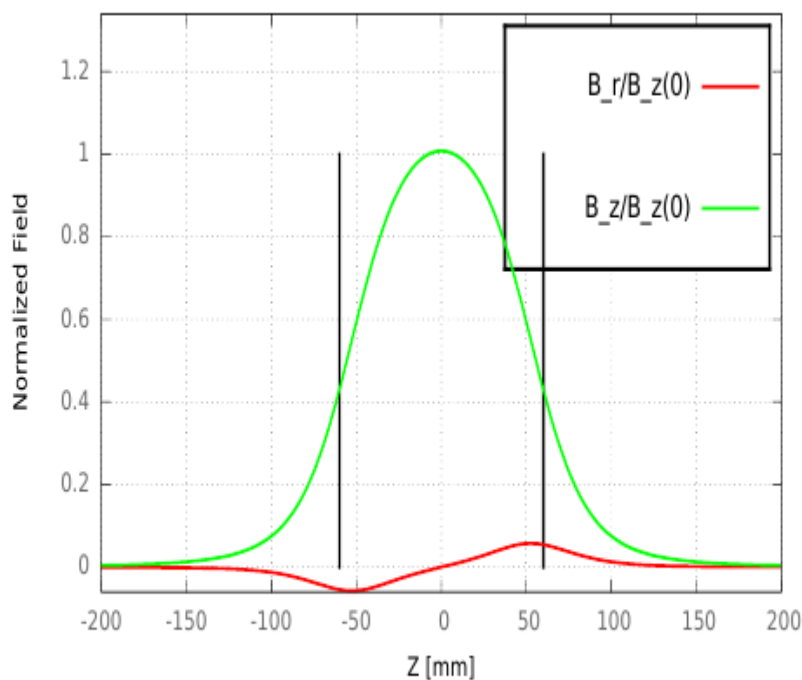


“matched” to RFQ (core parameters)

Beta = beta RFQ
alpha = 1/2 alpha RFQ

Upstream and Downstream of Sol 3





(a) PXIE solenoid field B_z and B_r at an offset $r = 10$ mm. The vertical lines indicate the physical boundaries of the solenoid.

(b) LEBT Solenoid Parameters

| Parameter | Value | Units |
|----------------------------|---------|------------------|
| Min inner diameter | 80 | mm |
| Max physical length | 140 | mm |
| Strength $\int B_z^2 dz$ | 0.03 | T-m ² |
| Peak Current | 300 | A |
| Power dissipation | 0.8-1.0 | keV-ns |
| Dipole corrector coils | 4 | |
| Peak Dipole Coil Current | 10 | A |
| Dipole coil field integral | 0.5 | T-m |



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- PX DocDB Document 1015-v2 estimates the impact of the spherical aberration in the PXIE Solenoid in a manner similar to what is outlined here.

Solenoid Field Expansion



The field of an axi-symmetric solenoid can be expanded based on based on the on-axis form of $B_z(z)$

$$B_z(r, z) = B(z) - \frac{r^2}{2} B''(z) + \frac{r^4}{64} \frac{d^4 B(z)}{dz^4} - \dots$$

$$B_r(r, z) = -\frac{r}{2} B'(z) + \frac{r^3}{16} \frac{d^3 B(z)}{dz^3} - \dots$$



By integrating the equations of motion in cylindrical coordinates, one can show that in the short solenoid approximation (r is constant through the solenoid, the the radial kick experienced by a particle is

$$\Delta r' = -\frac{r}{f_0} [1 + C_1 r^2 + C_2 r^4]$$

C_1 and C_2 are known as the spherical aberration coefficients. These coefficients are determined by the field shape, and here the latter depends only on the on-axis shape of B_z .

$$\frac{1}{f_0} = \left(\frac{q}{2\beta_z \gamma c} \right)^2 \int_{-\infty}^{\infty} B^2(z) dz$$



$$C_1 = \frac{1}{2} \frac{\int [B'(z)]^2 dz}{\int B^2(z) dz},$$

$$C_2 = \frac{5}{64} \frac{\int [B''(z)]^2 dz}{\int B^2(z) dz}$$

Emittance Growth due to Spherical Aberrations



$$\Delta\epsilon_{x,y} = \frac{R^4}{2\sqrt{6}f_0} \sqrt{\frac{C_1^2}{12} + \frac{C_1C_2}{5}R^2 + \frac{C_2^2}{8}R^4}$$

This expression is obtained by computing the emittance increase of a spatially uniform beam of radius R with zero emittance ($r'=0$) receiving a radially dependent kick from the lens.

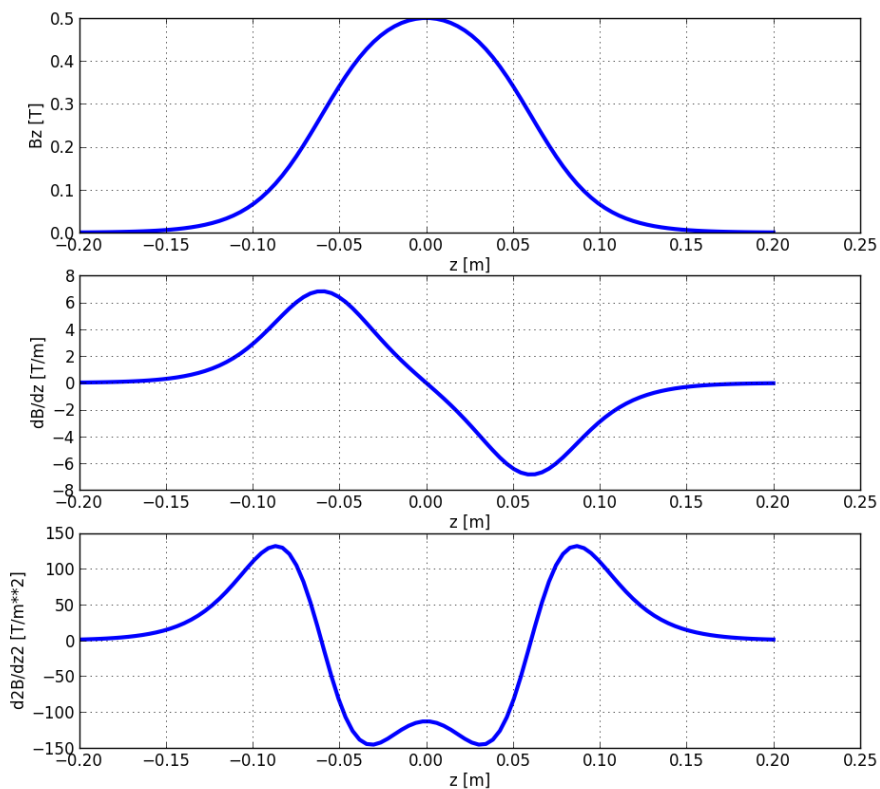


For numerical estimates, a number of sufficiently differentiable analytic forms for B(z) can be used. A popular one is

$$B(z) = \frac{B_0}{2 \tanh(L/2R)} \left[\tanh \frac{z + L/2}{R} - \tanh \frac{z - L/2}{R} \right]$$

Another one, well-suited to short solenoids is the so-called Glaser model

$$B(z) = \frac{B_0}{1 + (z/(L/2))^2}$$

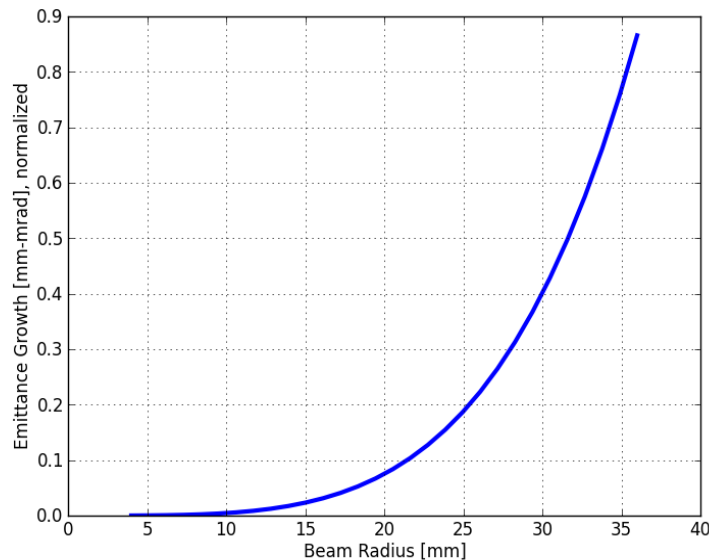


atanh analytic form

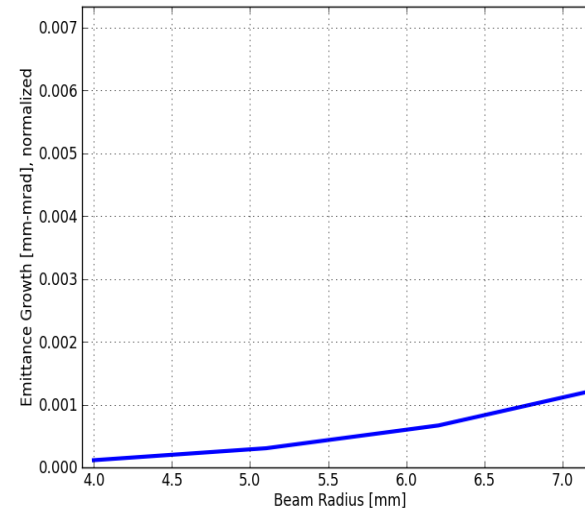
Numerically computed
first and second derivatives



For PXIE : $\epsilon_{x,y} = 0.116$ mm-mrad

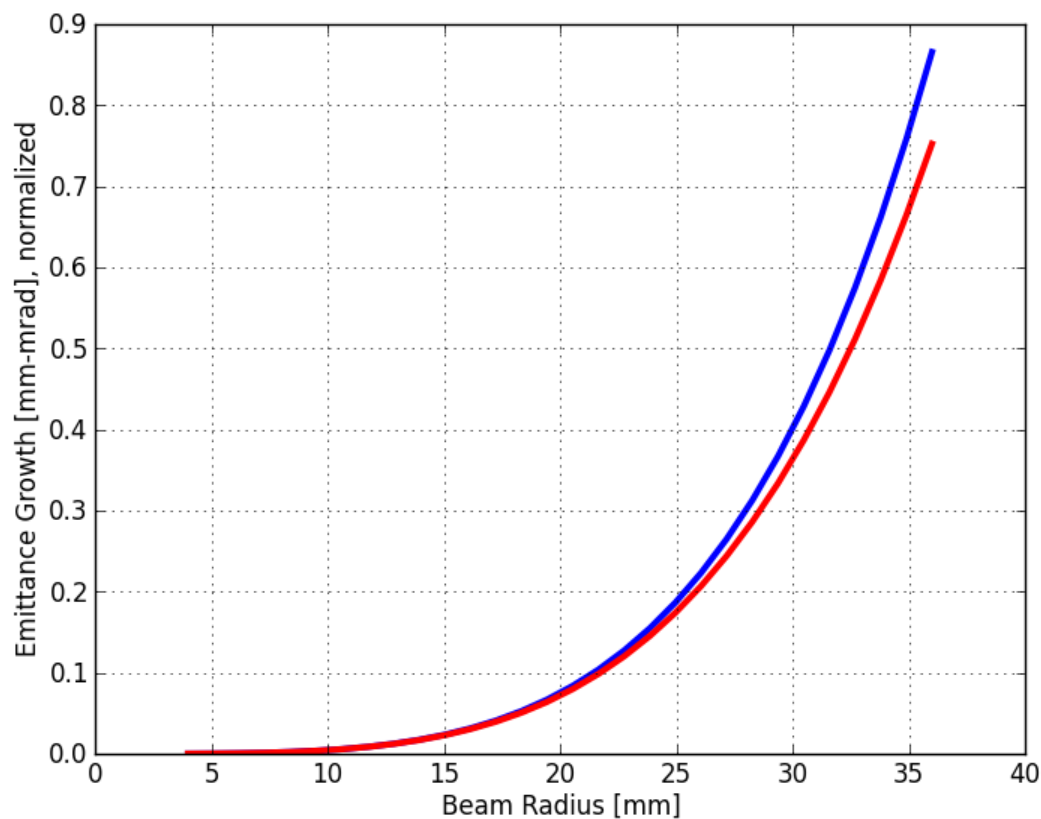


For R = 1/2 of radial aperture



$$\frac{\Delta\epsilon}{\epsilon} \simeq \frac{0.08}{0.11} = 72\%$$

Probably excessively pessimistic for a Gaussian beam.



1st order aberration
OK



Aberrations can be controlled by tailoring the solenoid excitation profile or the geometry of the external iron enclosure. Example : FETS

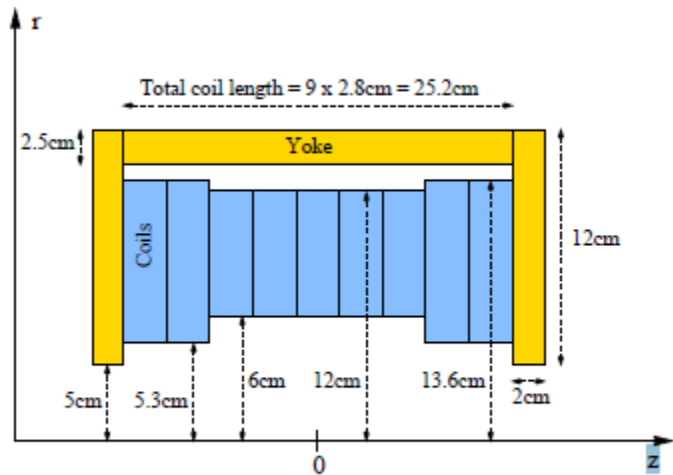


Figure 2: Schematic of the solenoid design.

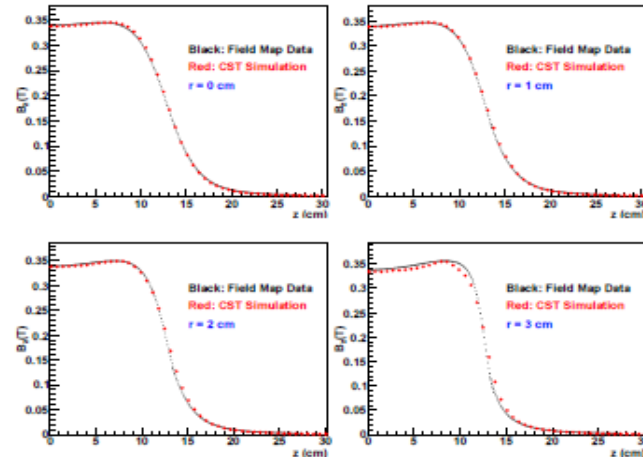


Figure 3: $B_z(z)$ measured and simulated field map distributions for one of the solenoids at different radii.



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- It appears very difficult to get a good match into the RFQ
 - The distance between Sol 3 and the RFQ entrance is critical as it determines the amplitude in Sol 3
 - **Can we improve phase space distribution and obtain a better match by tweaking Sol 3 ?**



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- confirm that emittance growth observed with TraceWin agrees with prediction for formula (this one or the one from 1015-v2)
No space charge.
 - Can we mitigate SC with sol aberrations ?
Experiment with a few solenoid axial profiles.