Thermal and Structural Analysis of Targets and Windows Materials, Irradiation Data and Fracture Toughness R. Gates, D. Wootan, B. Schmitt, J. Deibler

Pacific Northwest NATIONAL LABORATORY

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Approach

Integrated Design Analysis and Simulation, Thermal, Mechanical, and Irradiation Effects: PNNL has extensive capabilities with proven performance of target designs in challenging complex nuclear/thermal environments. Core design expertise includes molecular dynamics, and kinetic Monte Carlo modeling. Radiation transport and heating is typically accomplished with MCNPX. The primary thermo mechanical modeling tools include ANSYS and MathCad. Three dimensional component modeling is completed using SolidWorks 3D modeling capabilities interfaced with ANSYS facilitating rapid parametric modeling. Advanced numerical methods to address nonlinear dynamics is completed using LSDYNA if required. Multi-physics modeling capabilities address complex conditions including irradiation energy deposition, heat conduction, convection, radiation, thermal gradients, dynamic transient analysis, linear and nonlinear stress analysis, modal analysis, and irradiated material property changes over the lifetime of the component. PNNL applies an integrated analytical modeling approach compliant with intent of ASME Codes, meeting QA requirements, and correlated with experimental data to confirm the integrity and safety of complex in-reactor and accelerator driven components.



Pulsed Be Beam Window Results - Peak Transient Δ Temp. 320 K Below Creep Range , Plastic Strains at Center ~5.9%, 2mm and 4mm < 1%. Irradiated Be Elongation is 1-3%, Unirradiated YS at 320 C is ~200 Mpa (29 ksi). Irradiated YS and UTS are Higher than Unirradiated

Additive Manufacturing - Benefits				
Esprication of Extremely Complex Near Net	E Modulus Applied Thermal Thermal Shock of Elasticity UTS Tensile Delta T (K) = Stress Pa Bts=UTS/(CTE*E Parameter	1 ANSYS 14.0 JAN 4 2013 09:18:34 FLOT NO. 1 NODAL SOLUTION 1 MNSYS 800 09:50:51 09:50:51 800 PLOT NO. 1 1	Energy	120 GeV
Shape Components – Geometric Lattice Structures,	Material Pa Strength Pa EDD/Cp CTE*E*DeltaT *DeltaT) (UTS*K)/(E*CTE)	SIEF=1 SUB =100 TIME=.100E-04 TEMP (AVG) RSYS=0 640 640 640	sigma radius	1.5 mm
Cooling Channels that Conform, Design for Function	Beryllium 3.03E+11 4.48E+08 308 1.07E+09 0.418 27771	EFACT=1 AVRES=Mat DMX =. 165E-04 SMN =20 SMX =1075_81	period	1.3300 sec
Innovative Integrated Window and Target Designs with	Carbon Reinforced Carbon 8.00E+10 2.00E+08 449 2.87E+07 6.967 125000 Graphite 8.00E+09 1.40E+07 951 1.14E+07 1.227 192500	M 480 20 137.312 254.624 371.936 480 0 137.312 254.624 400 0 137.312 137.312 137.312 137.312 137.312 137.312 137.312 137.312 137.312 137.312 137.312 137.312 137.324 137.344 137	pulse	1.60E+14 protons
Thermally and Structurally Optimized Components.	Silicon Carbide	606.56 723.872 841.184 958.496 1075.81	power	2.3 MW
High Strength and Stillness with Low Density	Graphite Composite 1.40E+11 1.40E+08 740 3.11E+08 0.450 41667 Benullium Connor 1.15E+11 1.21E+09 1267 2.62E+09 0.450 90070		current	0.0193 mA
Methods – Laser Deposition, E-Beam Deposition, Shaped Metal Deposition	Invar - Fe Ni 1.48E+11 7.17E+08 1150 7.11E+08 1.008 12169 CVD Diamond 1.05E+12 1.50E+09 1305 1.37E+09 1.095 2857143 Titanium Ti-6Al-4V 1.12E+11 1.14E+09 1147 1.16E+09 0.984 7445	Beam Window, Ti Mod 1, 12/28/12 .1 .2 .4 .6 .8 1	pulse length	10 micro-sec
Concerns – Fatigue Life May be Lower than Wrought Components. Limited Alloys Ti, Al, SS but growing	Candidate Materials - Young's Modulus, UTS, Delta T, Thermal Stress, Resistance and Shock Parameters	Ti-6Al-4V Beam Window Results – Peak Δ Temp.1075 C and Stress 600 Mpa, (87 ksi) at Center, Requires Cooling, Exceeds YS, UTS at Temp	2.3 MW Beam Parameters used for Window Designs	



Thermal Heat Transfer Modeling – ANSYS transient heat transfer modeling used to calculate thermal profiles accounting for material properties, proton beam energy deposition, beam pulse rates, conduction, convection, radiation and gap conductance. Cooling methods are dependent on specific configurations and include, air, helium, pressurized helium,

Energy Deposition, implantation depth and irradiation damage (dpa) – calculated using internationally recognized standard methods using SRIM (formerly TRIM), see D.Wootan. Provides a common basis of comparison for

helium-neon gas mixtures, liquid metals, water and steam.



Target for Reactor Neutrino Anomaly - Thermal Model of 30 MeV Proton Tungsten Target 1745 K (2681 F) ; High Pressure He Cooling , Yttrium Hydride Moderation and U-235 Fission Foils, Dispersion Alloy W-4Re-0.26HfC High Temp Strength, Re Improves Low Temp Ductility (DBTT), 1ppm O2 in He Limits W Oxidation. Stress Rupture Limit at 1745 K and 4000 psi is ~100 hrs. for pure W, ~10,000 psi for Alloy

Irradiation Damage C/C - Trends in Isotropic Graphite and Carbon Reinforced Carbon with Pseudoplatic Fracture Behavior, Resistance to Thermal Shock and Good Creep resistance.

Irradiation Induced Creep in Be – Temperature, Stress and Irradiation Effects on Creep Rate,

data from different irradiation sources. Provides a method of comparing and correlating neutron fluence data parameters from data sources such as the Advanced Test Reactor (ATR) to charged particle, proton beam, parameters.



Design Stress Limitations for Tungsten Alloys

YS of pure W at 500 C ~ 500 Mpa (75 Ksi) at 1773 K the Alloy UTS is ~ 413 Mpa (60 Ksi), The Design Creep Stress Limit is ~20 Mpa (3 Ksi)

S. Sharafat et al, UCLA

Fracture Strength of Interpenetrating Phase **Composites** – Each phase interconnected e.g. C/Al or Al2O3/Al composites Porous preform (15-25%) infiltrated with light metals at high temps and pressures. Improves properties over monolithic Material Properties:

Low CTE, Higher Thermal Conductivity, Increase in Young's Modulus, Higher Flexure Strengths ~X2, Higher Fracture Toughness than Ceramic Pre-Form,

- Elastic Modulus (E) Increases with Increasing dpa
- Coefficient of Thermal Expansion (CTE) Decreases with Increasing dpa
- Thermal Conductivity Decreases with Increasing dpa
- Changes Occur at Relatively Low 1 dpa
- Ref. J.A. Vreeling et.al., "Graphite Irradiation Testing for HTR Technology..." 2008, and M.Roedig et.al., Post Irradiation Testing of Samples from PARIDE 3 and 4..."2004, Journal of Nuclear Materials







Impact of Thermal Cycling.

T. Etter et al. Materials Science and Engineering

Conclusions:

before thermal cycling

after thermal cycling

- High Temperature Properties and Irradiation induced Property Changes, Deformations, Swelling, Creep, Embrittlement Often Dominate Material Selection and Design Process.
- Extending Component Lifetimes Requires Carefully Integrated Solutions for Materials and Design Configurations (beam parameters, cooling, hot gaps, expansion relief, etc.).
- New Additive Manufacturing Techniques Offer Potential Benefits. Design for Function.
- Irradiated Property Testing / Performance is Key

Contact: Robert Gates, 1-509-372-4090, ro.gates@pnnl.gov