

OPTICAL STOCHASTIC COOLING IN IOTA

Gene Kafka (IIT/ FNAL), Valeri Lebedev (FNAL)

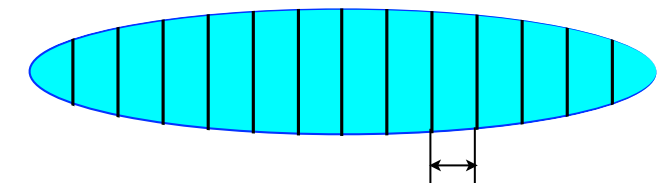
OSC PRINCIPLES

- ▶ Microwave stochastic cooling suggested by Van der Meer (1969)
- ▶ OSC was suggested by Zolotarev, Zholents and Mikhailichenko (1994)

$$\lambda f_0 \approx \frac{W}{N} \Leftrightarrow \lambda \approx \frac{1}{N_{\text{sample}}}$$

- ▶ OSC works like MICROWAVE STOCHASTIC COOLING, but
 - exploits the superior bandwidth of optical amplifiers $\sim 10^{14}$ Hz.
 - can deliver damping rates 4 orders of magnitude larger
- ▶ UNDULATORS suggested to be used for both the PICKUP and KICKER in order to support the same optical range as the amplifier

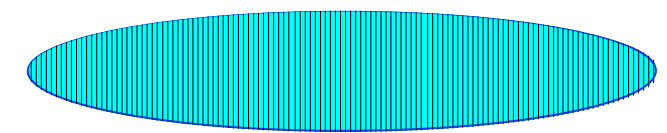
MICROWAVE SLICING



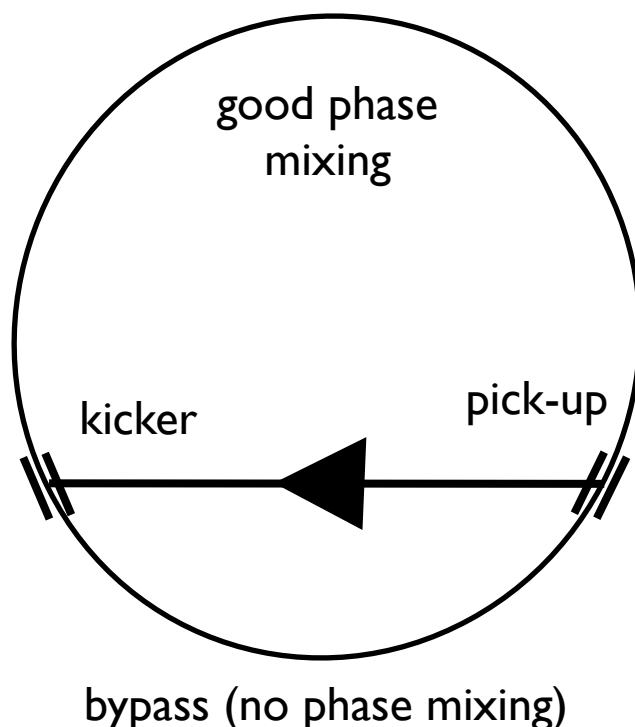
sample length: ~ 10 cm

$$N_{\text{sample}} = N \frac{\Delta \ell}{\ell_b}$$

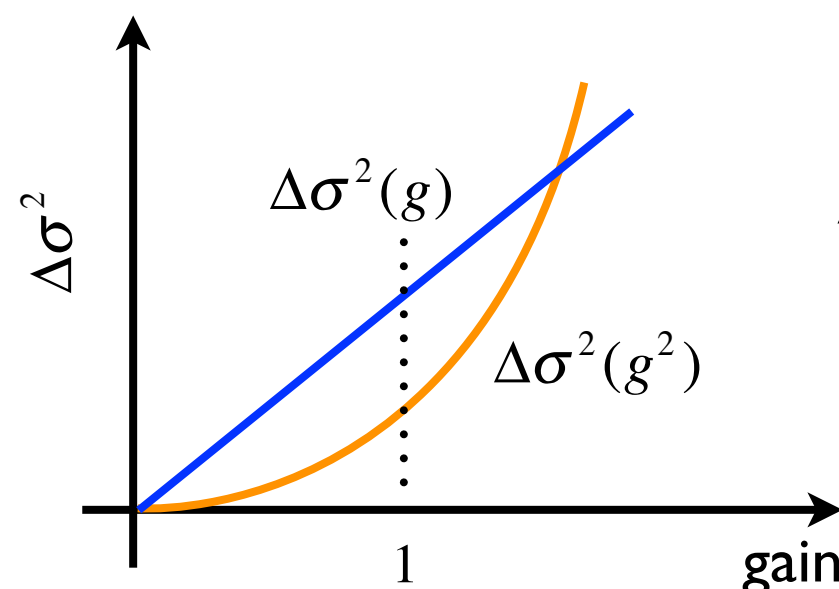
OPTICAL SLICING



sample length: ~ 1 μm



Stochastic Cooling Basics



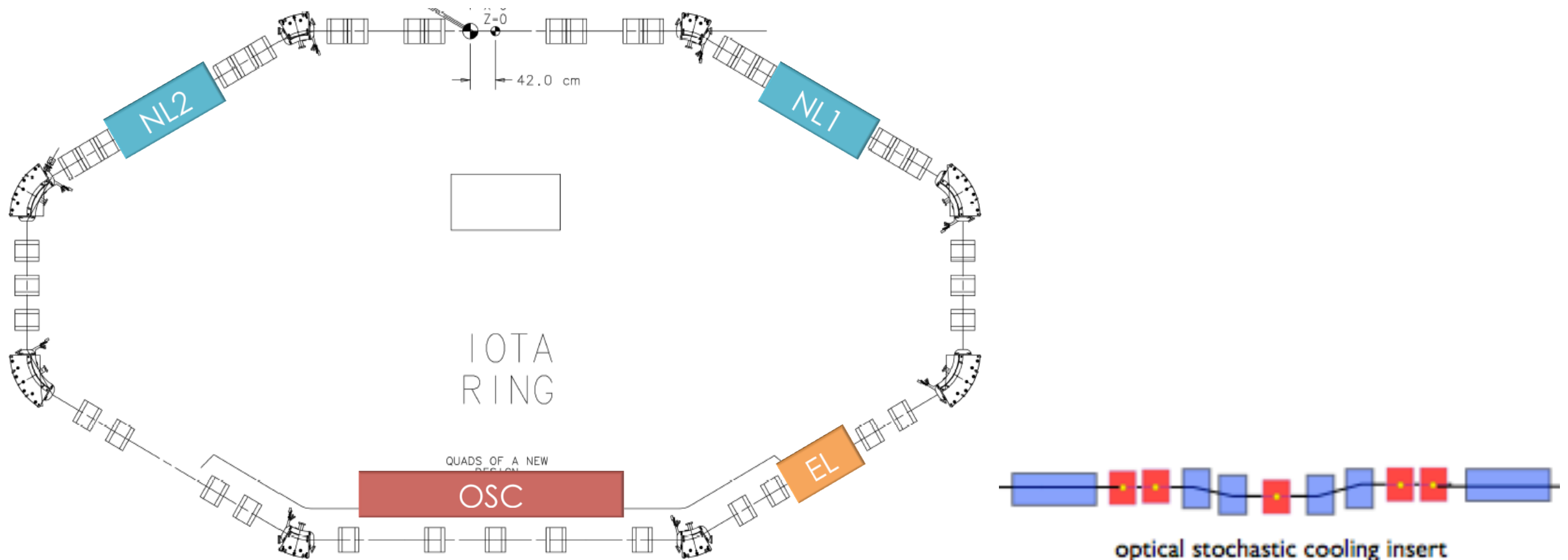
$$\Delta x(t) = \underbrace{-\frac{g}{N} x_i(t)}_{\text{cooling}} + \underbrace{\frac{g}{N} \sum_{k \neq i}^N x_k(t)}_{\text{heating}}$$

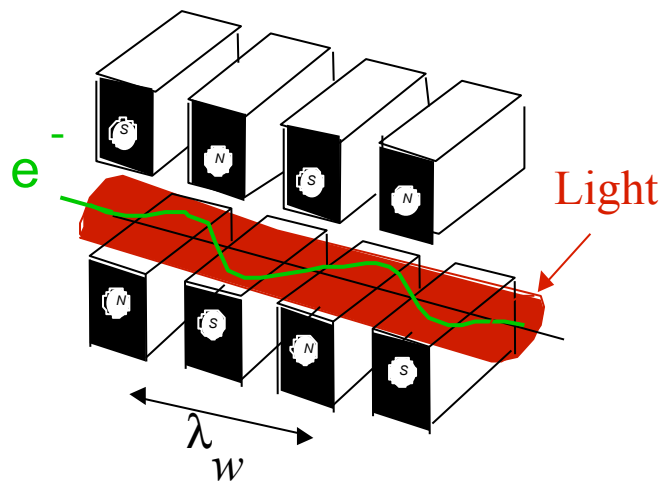
$$-\frac{\Delta(x^2)}{x_{rms}^2} = \frac{\boxed{2g} - \boxed{g^2}}{N_s}$$

TEST OF OSC IN IOTA

- ▶ OSC was first attempted in BATES in 2007
 - ▶ existing electron synchrotron
 - ▶ did not receive enough support
- ▶ Will be one of several tests in IOTA
 - ▶ test in small electron ring is cost effective

IOTA Parameters in OSC mode	Value
Circumference	40 m
Nominal Beam energy	100 MeV
Bending field	4.8 kG
Transverse RMS emittances, $\epsilon_x = \epsilon_y$	11.5 nm
RMS momentum spread	1.23×10^{-4}
SR damping times (ampl.), $\tau_s / (\tau_x)$	1.4 / 0.67 s



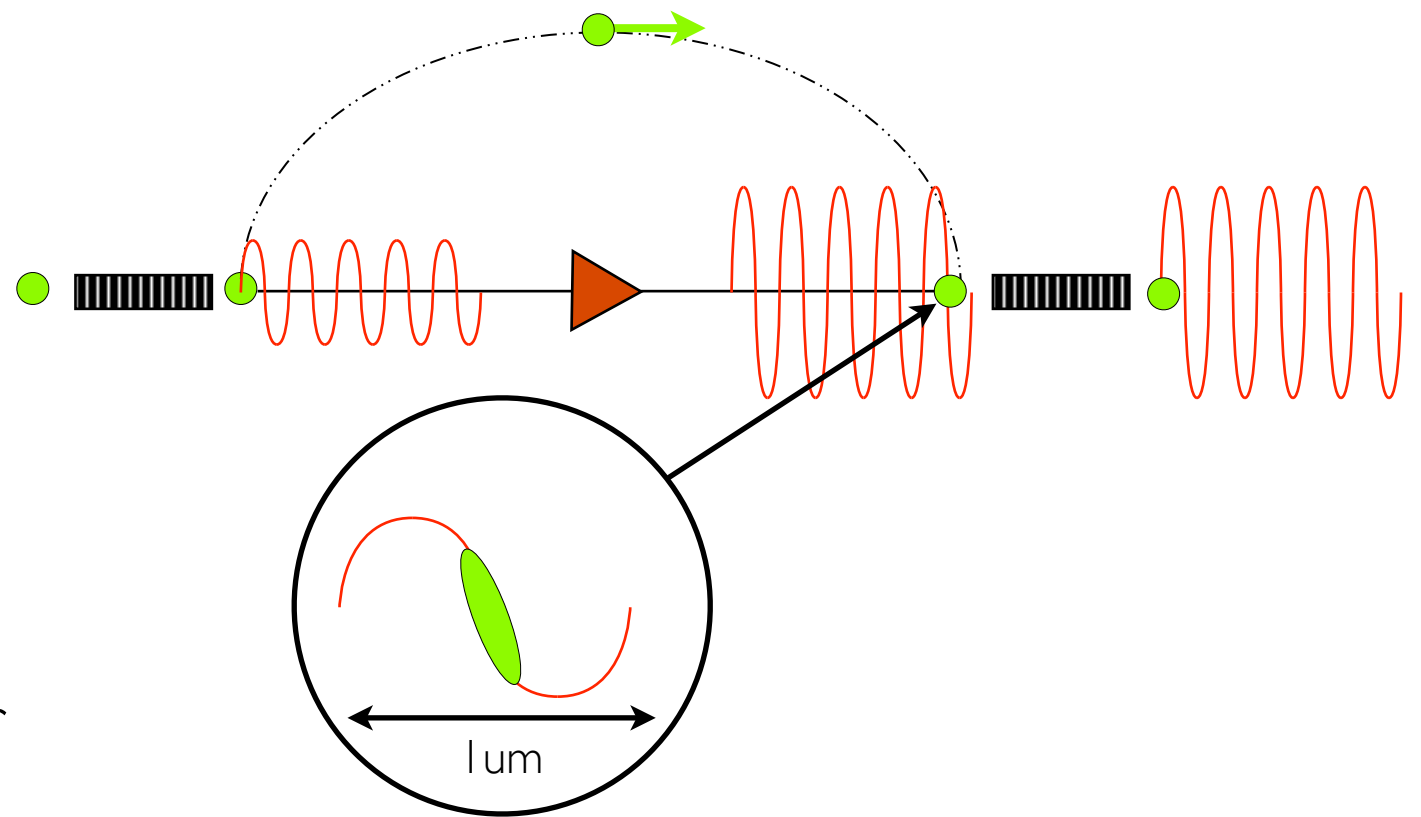


undulator period

laser wavelength

undulator parameter

$$\lambda_w = \frac{2\gamma^2 \lambda_L}{\left(1 + \frac{K^2}{2}\right)}$$



Only longitudinal kicks are effective for cooling:

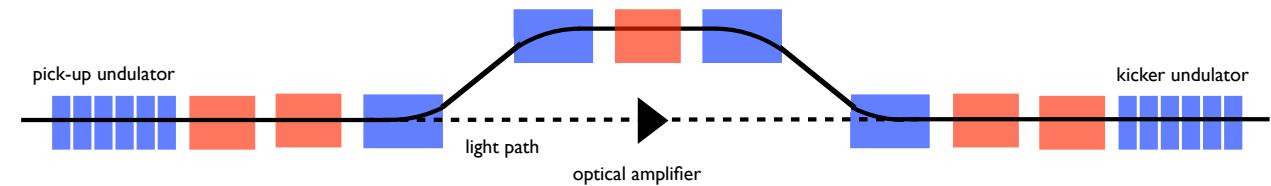
$$\Delta\delta_i = \underbrace{\kappa \sin(k\Delta s_i)}_{\text{cooling}} - \underbrace{\kappa \sum_{k \neq i}^N \sin(k\Delta s_i + \psi_{ik})}_{\text{heating}}$$

particle delay

- ▶ At optimum cooling rate is:
 - $\sim (\text{bandwidth}) / (\text{number of slices in the sample})$
- ▶ Correction signal is proportional to longitudinal position change
- ▶ Only longitudinal kicks are effective
 - longitudinal cooling requires s-x coupling
 - transverse cooling requires x-y coupling

- Pickup-to-kicker Transfer Matrix (vertical plane is uncoupled and omitted)

$$\begin{bmatrix} x \\ \theta_x \\ s \\ \Delta p / p \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} & 0 & M_{16} \\ M_{21} & M_{22} & 0 & M_{26} \\ M_{51} & M_{52} & 1 & M_{56} \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x \\ \theta_x \\ s \\ \Delta p / p \end{bmatrix}$$



- Partial slip factor (pickup-to-kicker) describes a particle's longitudinal displacement

$$\tilde{M}_{56} = C\eta_{pk} = M_{51}D_p + M_{52}D'_p + M_{56}$$

- First order approximation of the longitudinal kick in the pickup:

$$\Delta\delta = \kappa\Delta s = \kappa \left(M_{51}x + M_{52}\theta_x + M_{56} \frac{\Delta p}{p} \right)$$

- Cooling rates per turn:

$$\begin{bmatrix} \lambda_x \\ \lambda_s \end{bmatrix} = \frac{\kappa}{2} \begin{bmatrix} M_{56} - \tilde{M}_{56} \\ C\eta_{pk} \end{bmatrix}$$

- x-y coupling outside the bypass allows for redistribution of horizontal damping rate into both transverse planes

Cooling Range

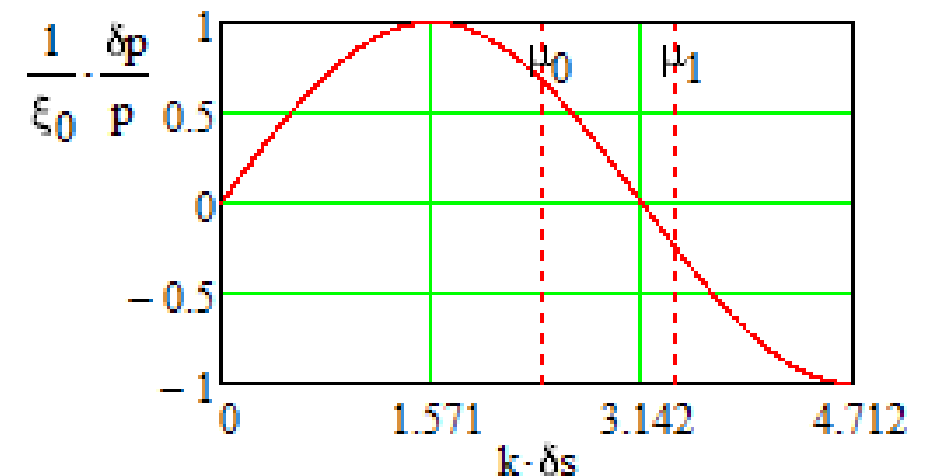
- ▶ Cooling force depends on Δs nonlinearly:

$$\Delta\delta = \kappa \sin(k\Delta s)$$

- ▶ where $k\Delta s = a_x \sin(\psi_x) + a_p \sin(\psi_p)$

- ▶ a_x and a_p are the amplitudes of longitudinal displacements in cooling chicane due to transverse and longitudinal motions (betatron and synchrotron radiation) in units of laser space

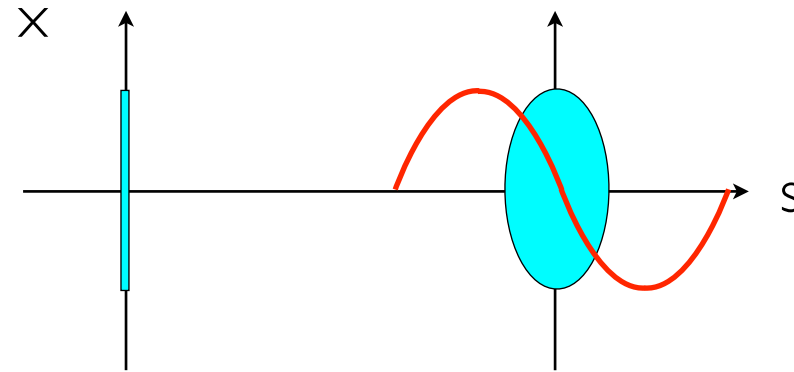
- ▶ Damping requires both lengthening amplitudes (a_x and a_p) to be smaller than $\mu_0 = 2.405 \rightarrow$ this determines the cooling area boundary



Optical Amplifier

- ▶ Ti: Sapphire Optical Amplifier (2mm thick)
 - ▶ wide bandwidth
 - ▶ can deliver significant amplification with only ~ 1 mm delay
 - ▶ Allows operation in CW regime

- ▶ A zero length sample will lengthen on its way from the pickup to the kicker



- ▶ Both $\Delta p/p$ and ε contribute to the sample lengthening $\sigma_{\Delta s}^2 = \sigma_{\Delta s \varepsilon}^2 + \sigma_{\Delta s p}^2$

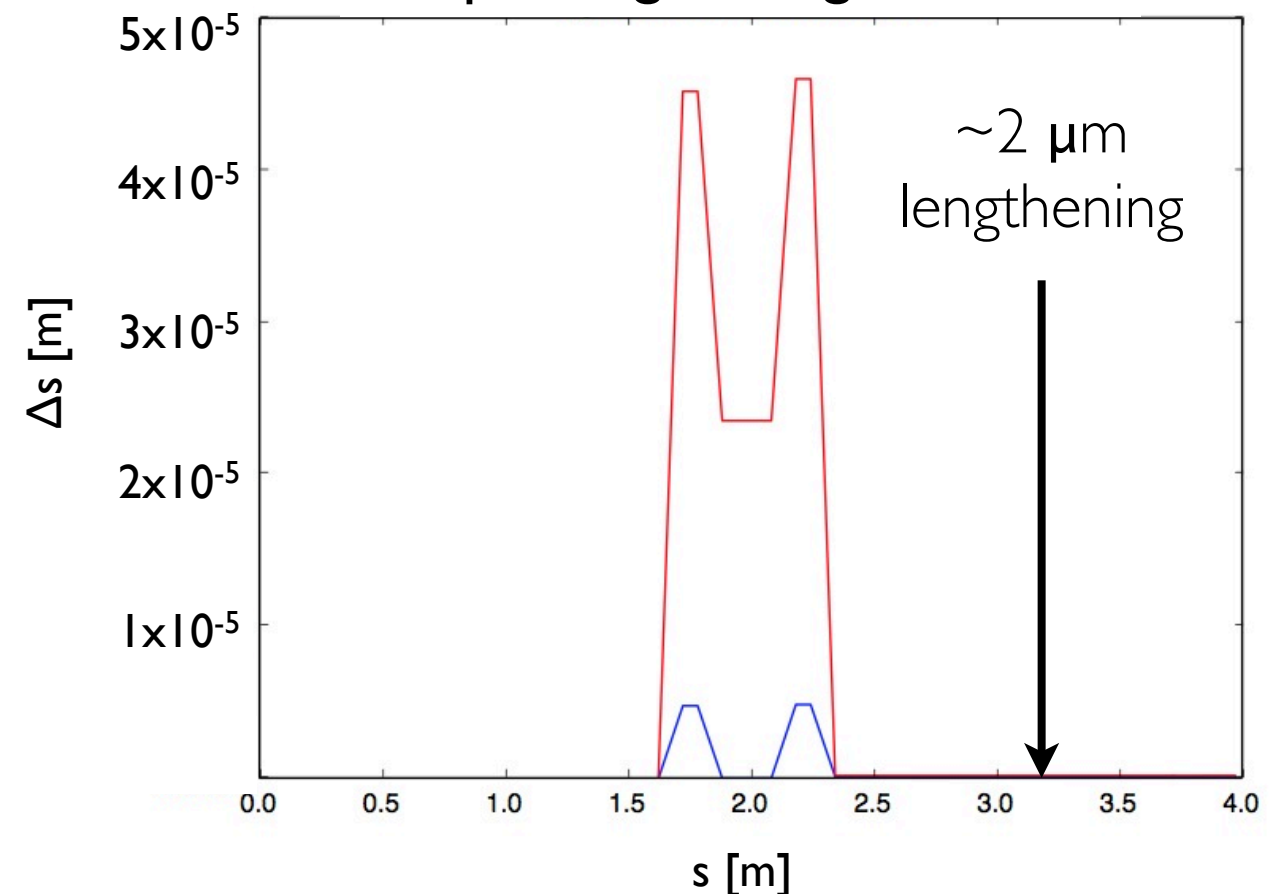
- ▶ For a Gaussian distribution:

$$\sigma_{\Delta s \varepsilon}^2 = \varepsilon \left(\beta_p M_{51}^2 - 2\alpha_p M_{51} M_{52} + \gamma_p M_{52}^2 \right)$$

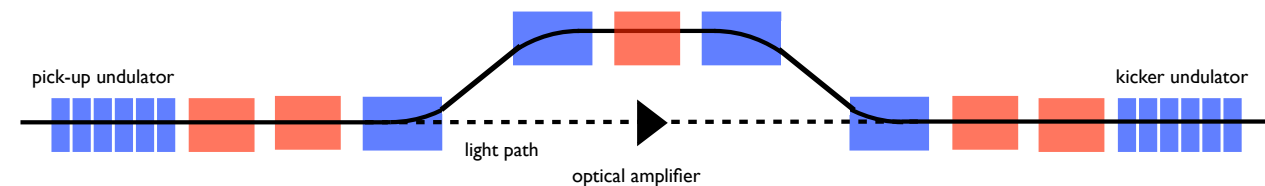
$$\sigma_{\Delta s p}^2 = \sigma_p^2 \left(M_{51} D_p - M_{52} D'_p + M_{56} \right)^2$$

- ▶ In the linear approximation, β_p and α_p do not affect damping rates, but affect sample lengthening and consequently the cooling range

Sample lengthening in chicane



- ▶ The first approximation of cooling dynamics are determined by the:
 - orbit offset, h
 - path lengthening, δs
 - defocusing strength of the chicane quad, Φ
 - D^* and β^* in the center of the chicane
- ▶ δs is set by the delay in the amplifier
- ▶ $\Phi D^* h$ is set by the ratio of decrements
- ▶ The dispersion invariant, A , in the dipoles determines the equilibrium emittance.



$$M_{56} \approx 2\Delta s,$$

$$\tilde{M}_{56} \approx 2\Delta s - \Phi D^* h,$$

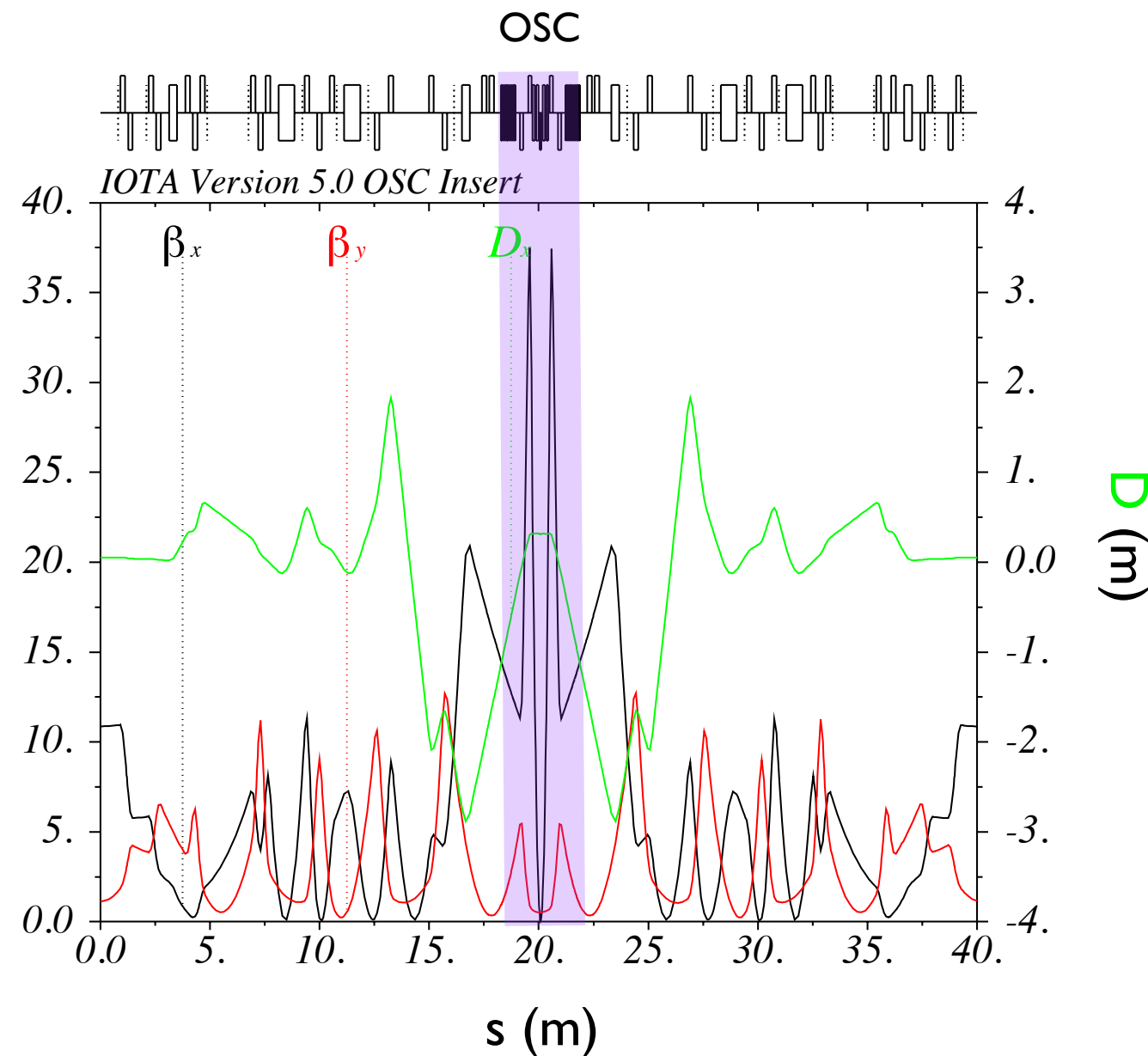
$$\lambda_x / \lambda_s \approx \Phi D^* h / (2\Delta s - \Phi D^* h),$$

$$n_{\sigma x} \approx \frac{\mu_0}{k\sigma_p} (2\Delta s - \Phi D^* h),$$

$$n_{\sigma x} \approx \frac{\mu_0}{2kh\Phi\sqrt{\epsilon\beta^*}},$$

$$\Phi D^* h \approx \frac{\mu_0}{2kn_{\sigma x}} \sqrt{\frac{A^*}{\epsilon}}$$

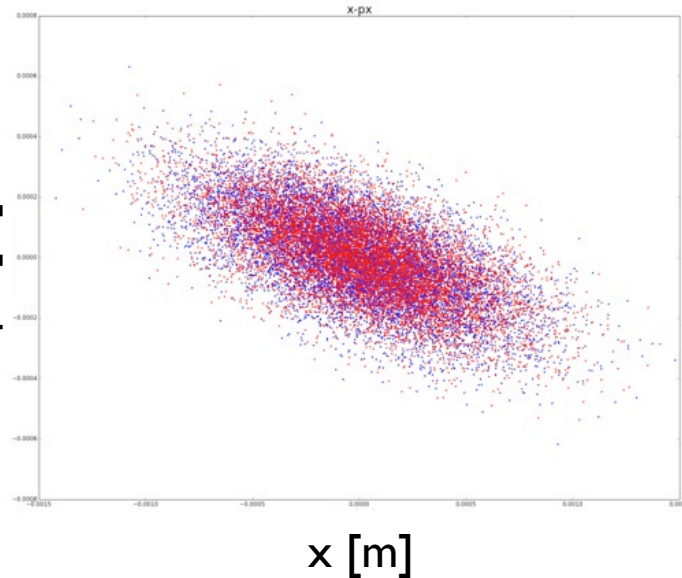
Cooling Chicane Parameters	Value
Delay in the chicane, Δs	2 mm
Horizontal beam offset, h	2.01 cm
M_{56}	4.8 kG
D^*/β^*	30 cm / 0.8 cm
Cooling rates ratio, $\lambda_x = \lambda_y / \lambda_s$	1.18
Cooling ranges (before OSC)	2.1 / 3.2
Dipole: magnetic field * length	4.22 kG * 10 cm
Strength of central quad, GdL	1.58 kG



- Energy reduced from 150 MeV to reduce ϵ , σ_p and undulator period and length
- Operating at the coupling resonance $Q_x/Q_y = 6.36/2.36$ reduces horizontal emittance and introduces vertical damping
- Small β^* is required to minimize sample lengthening due to betatron motion

OSC SECOND ORDER OPTICS

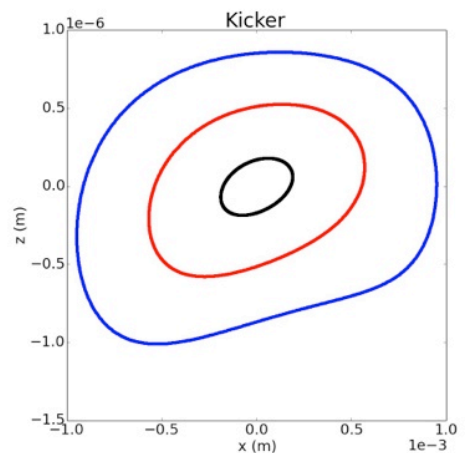
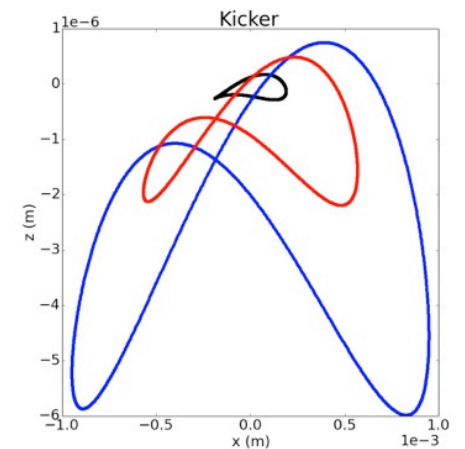
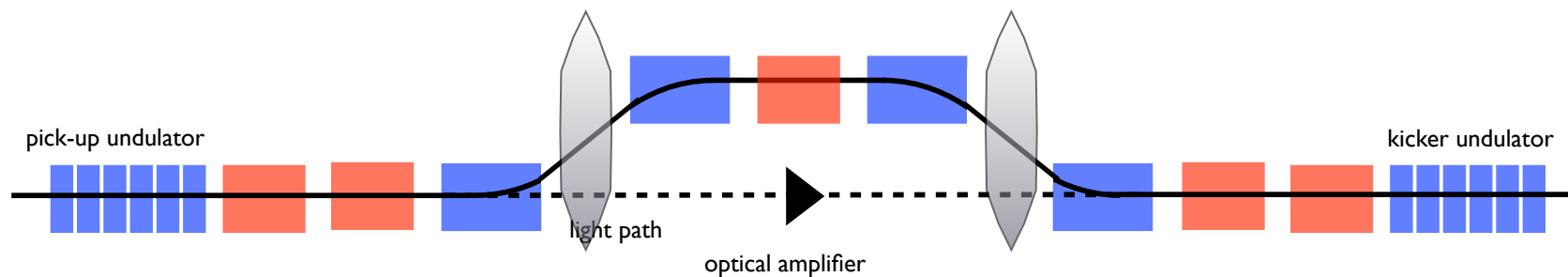
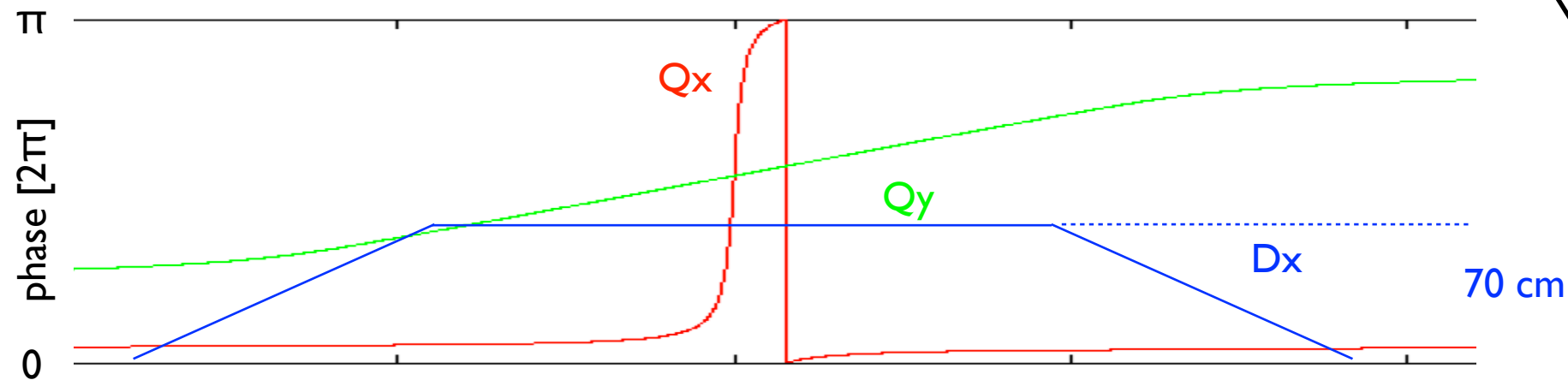
Using a realistic IOTA beam to develop second order optics



$$\Sigma_{beam} = V_{[6 \times 6]} \epsilon_{[6 \times 6]} V_{[6 \times 6]}^T =$$

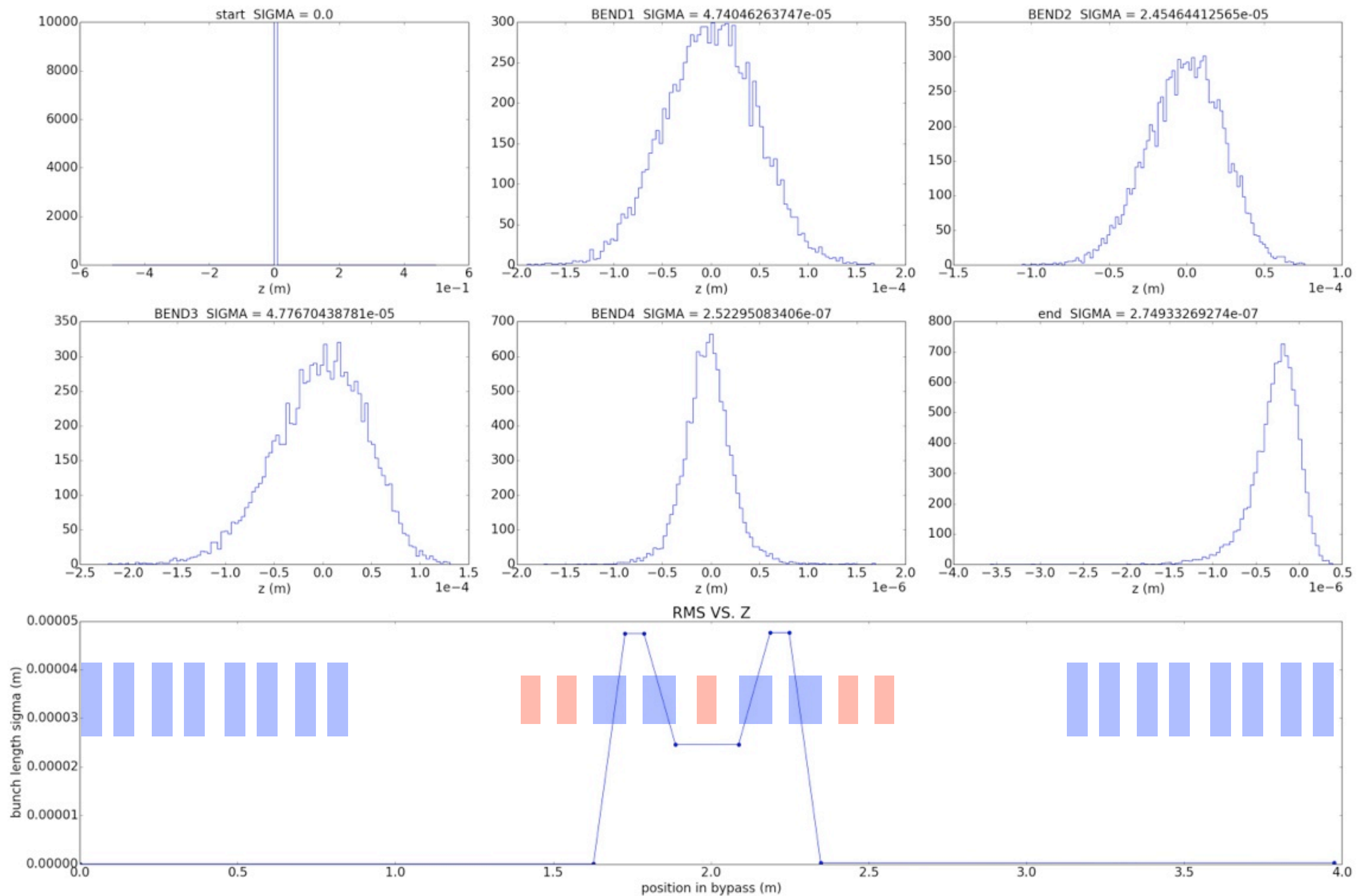
$$\begin{bmatrix} 1.417e-07 & -3.479e-08 & 0. & 0. & 1.185e-07 & -1.893e-08 \\ -3.479e-08 & 2.131e-08 & 0. & 0. & -1.169e-08 & 1.627e-08 \\ 0. & 0. & 5.509e-09 & 7.390e-09 & 0. & 0. \\ 0. & 0. & 7.390e-09 & 3.693e-08 & 0. & 0. \\ 1.185e-07 & -1.169e-08 & 0. & 0. & 1.316e-04 & 9.088e-12 \\ -1.893e-08 & 1.627e-08 & 0. & 0. & 9.088e-12 & 1.427e-08 \end{bmatrix}$$

SEXTUPOLES to correct for path lengthening due to transverse emittance



x [m]

OSC BUNCH LENGTHENING



OSC PARAMETERS

OSC Parameters	Value
Undulator parameter, K	0.6
Undulator period	4.92 cm
Radiation wavelength at zero angle	750 nm
Number of periods, m	10
Total undulator length, Lw	0.5 m
Length from OA to undulator center	1.65 m
Amplifier gain (amplitude)	10
Telescope aperture, 2a	7 mm
Damping rates ($x=y/s$)	160/140 s ⁻¹

- OSC will be tested with and without an optical amplifier

- ▶ Optics for OSC in ASTA has been developed, but the details are still being worked out; no show-stoppers have been identified.
- ▶ will aim to demonstrate cooling with and without an amplifier; the latter having a damping time that exceeds SR damping by about an order of magnitude