

Recent neutron irradiation experiments on HTS coated conductors and Nb_3Sn wires

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Outline

- Neutron Irradiation
 - TRIGA reactor
 - Neutron induced damage
- HTS coated conductor for fusion magnets
 - EUROFUSION
- Nb₃Sn for accelerator magnets
 - LHC Upgrade (collaboration with CERN)
- Comparison: Coated conductors and Nb₃Sn
- Conclusions



Acknowledgments



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NEUTRON IRRADIATION AND RESULTING DEFECT STRUCTURE



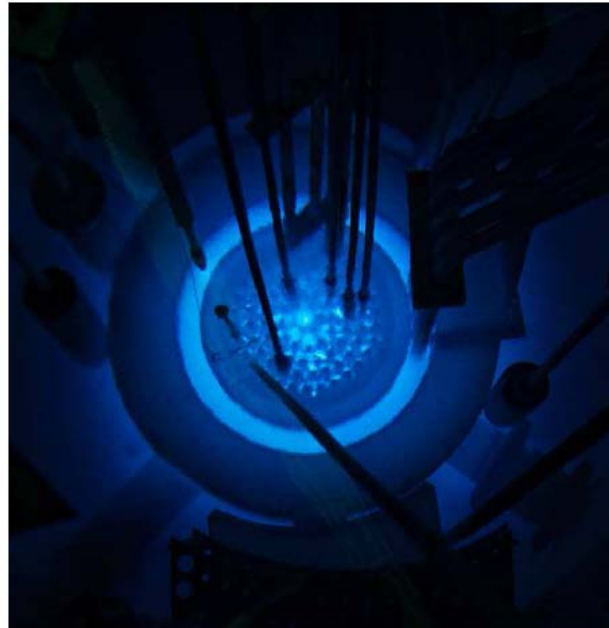
TRIGA MARK II Reactor

Neutron flux determination in 1985:

Thermal (<0.55 eV) / fast (>0.1 MeV) flux density: $6.1/7.6 \times 10^{16} \text{ m}^{-2}\text{s}^{-1}$

γ - radiation: ~ 1MGy/h

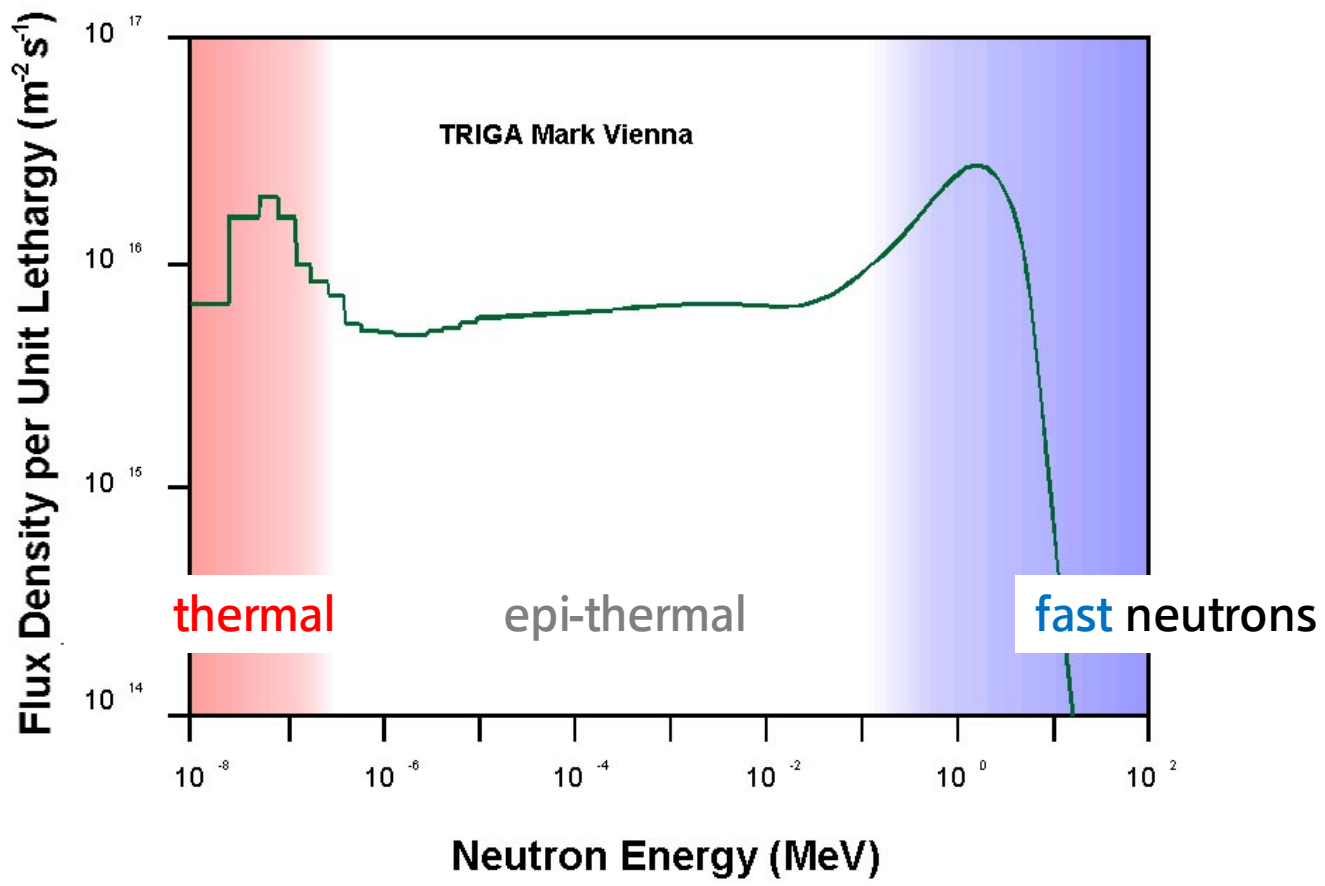
Core renewed in 2012: fast neutron flux density of $\sim 4.1 \times 10^{16} \text{ m}^{-2}\text{s}^{-1}$



Nickel monitor is used in each irradiation!



Neutron energy distribution



Neutron Irradiation: Created Defects (Cuprates)

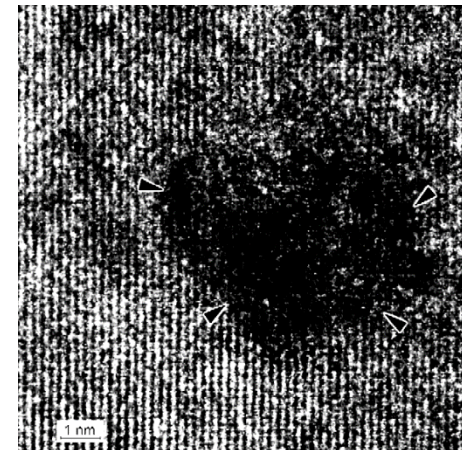
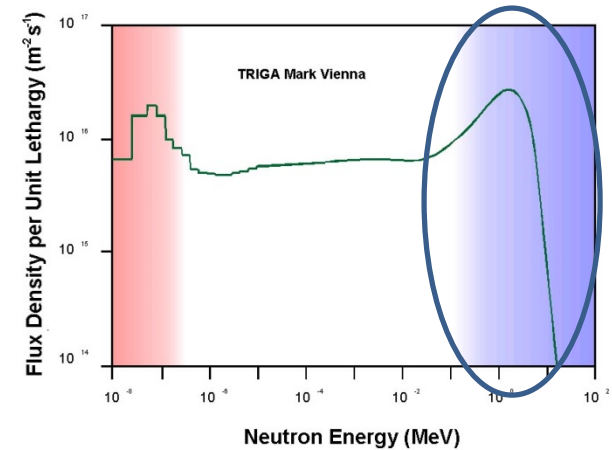
**Direct collisions
(high energy (fast) neutrons $E > 0.1$ MeV)**

Largest defects: collision cascades

$\varnothing \sim 5$ nm

Density

$5 \cdot 10^{22} \text{ m}^{-3}$ at a fluence of 10^{22} m^{-2}
($d_{av} \sim 27$ nm, $B_{\phi} \sim 3$ T)



Clusters of point defects



Defect structure YBCO: small defects

Positron annihilation lifetime spectroscopy (PALS)
Slovak University of Technology: Cu-O di-vacancies

Veterníková et al., *J. Fusion Energy* 31 (2012) 89

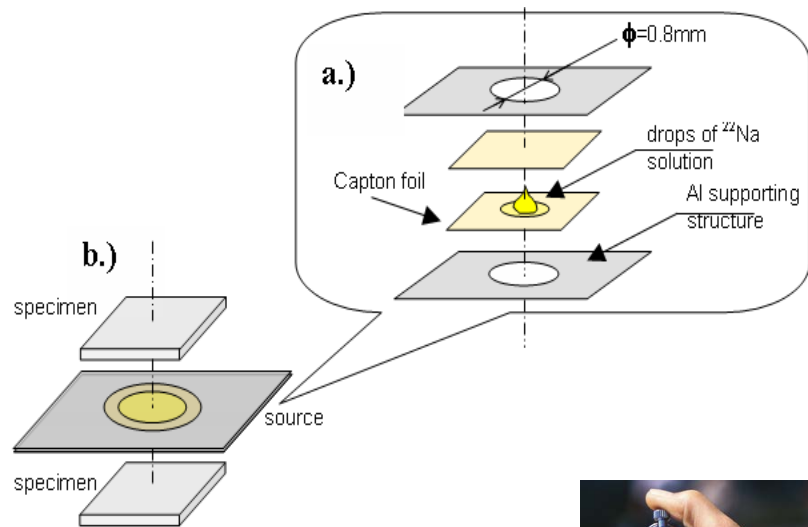
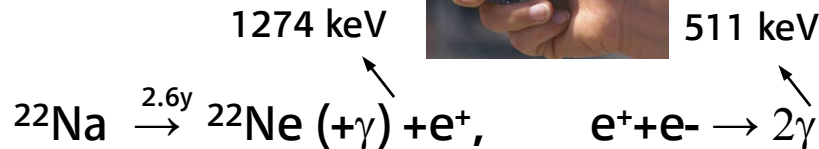


Table 1 Typical lifetime for bulk and defects [22–24]

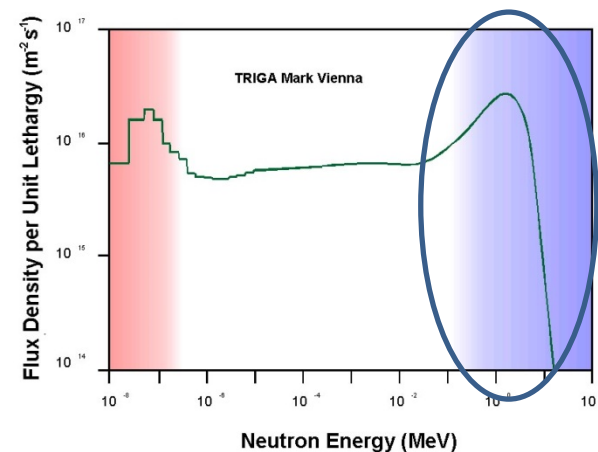
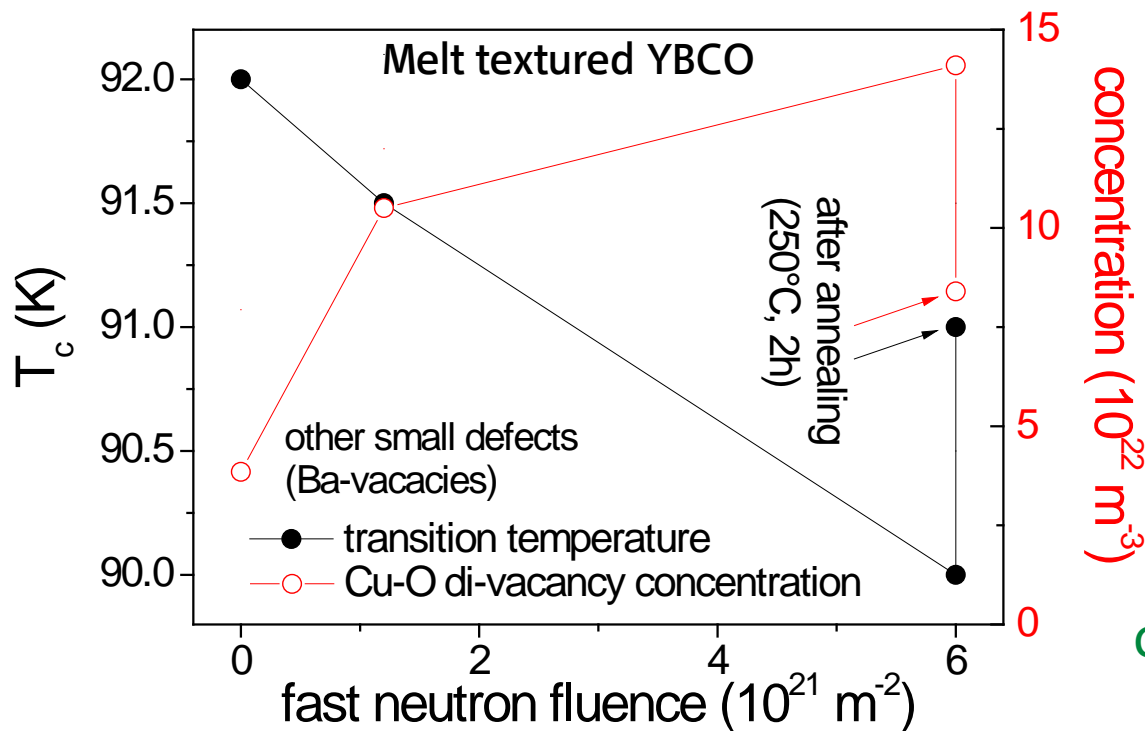
	Lifetime (ps)	Binding energy (eV)
YBa ₂ Cu ₃ O ₇ [22]	159	–
YBa ₂ Cu ₃ O ₇ [23]	190	
O vacancy	~170	~0.2
O vacancy cluster (2–4 vacancies)	181–190	0.1–0.2
Cu (1) vacancy	207	1.1
Cu (2) vacancy	182	0.7
Y vacancy	206	2.7
Ba vacancy	263	3.5
Cu (1)–O (1) di-vacancy	236	1.5



Defect structure YBCO: small defects

Positron annihilation lifetime spectroscopy (PALS): Cu-O di-vacancies

Veterníková et al., J. Fusion Energy 31 (2012) 89



Chudý et al.,
SUST 25 (2012) 075017

Cu-O di-vacancy concentration: highly non-linear with fluence!

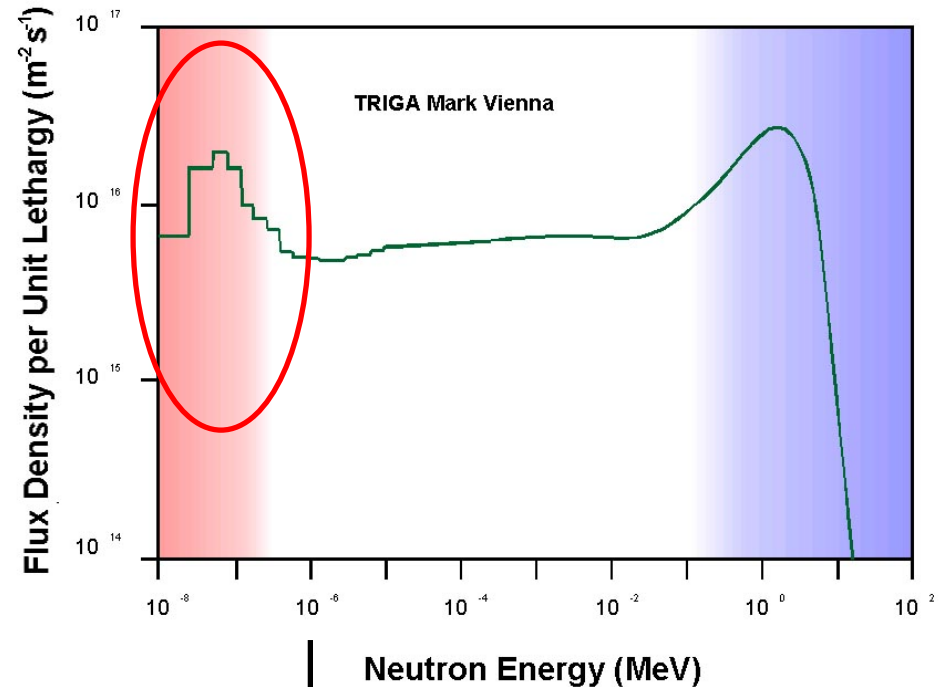
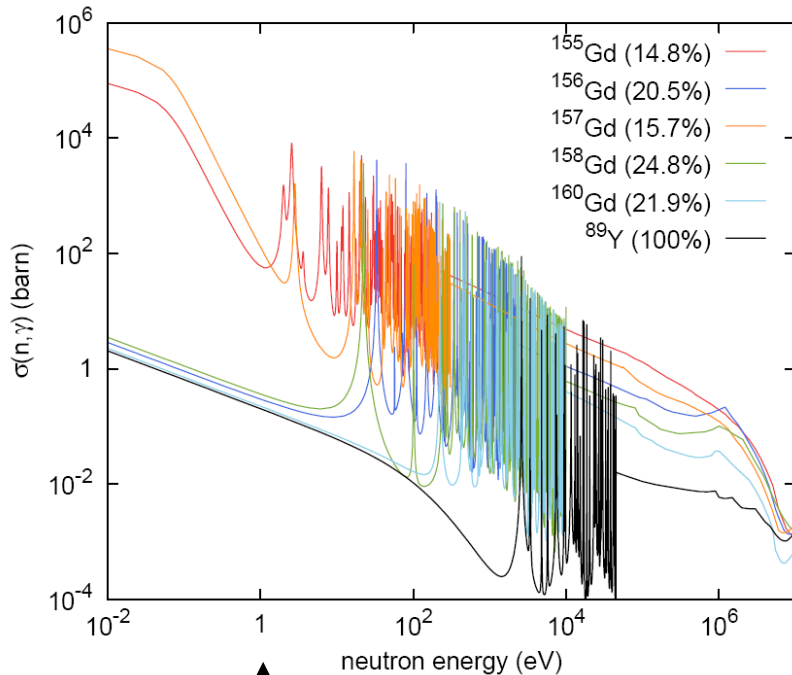


Neutron Irradiation: Created Defects

Neutron capture reactions (low energy neutrons)



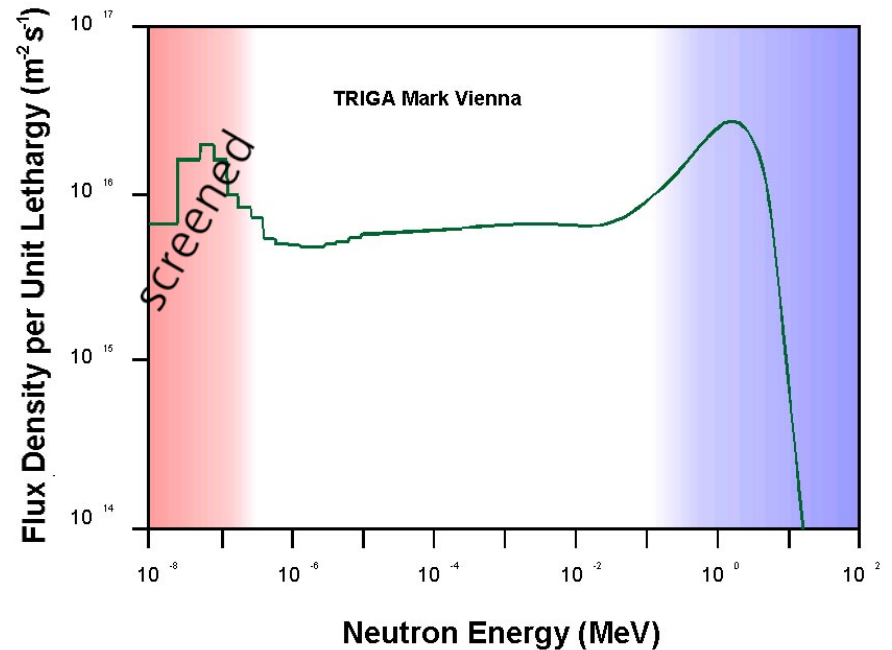
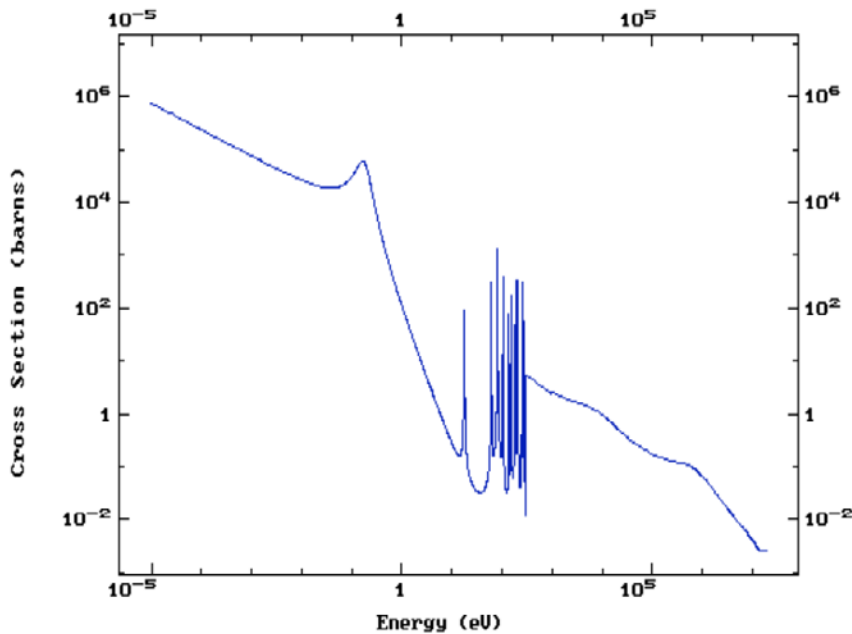
Recoil energy: $\sim 30 \text{ eV} \rightarrow$ single displaced atom



Shielding of thermal neutrons

Irradiation inside Cd-foil: Removes the low energy neutrons ($E < 0.55$ eV)
 Better simulation of a fusion spectrum

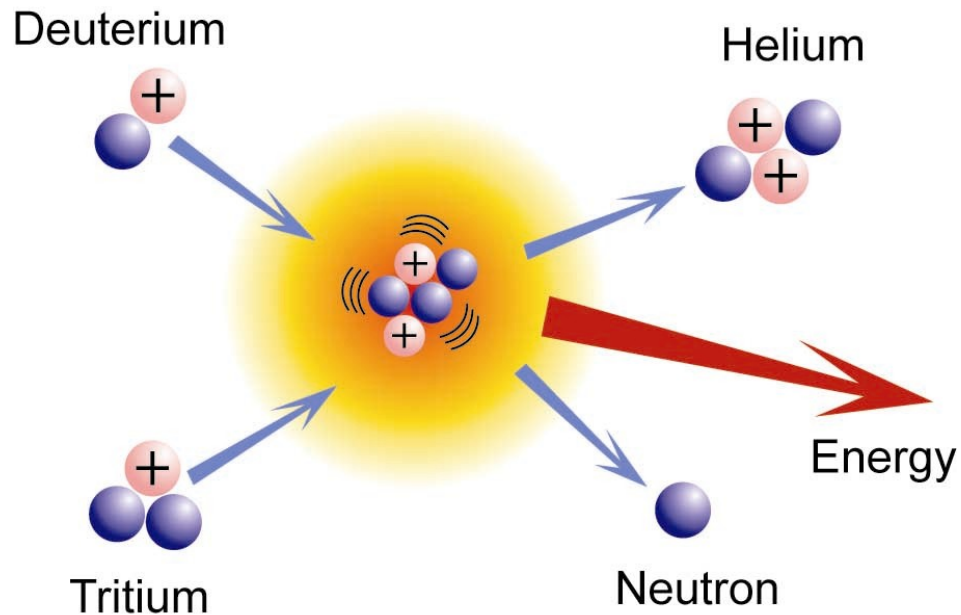
Cadmium



HTS COATED CONDUCTORS FOR FUSION MAGNETS



Nuclear Fusion

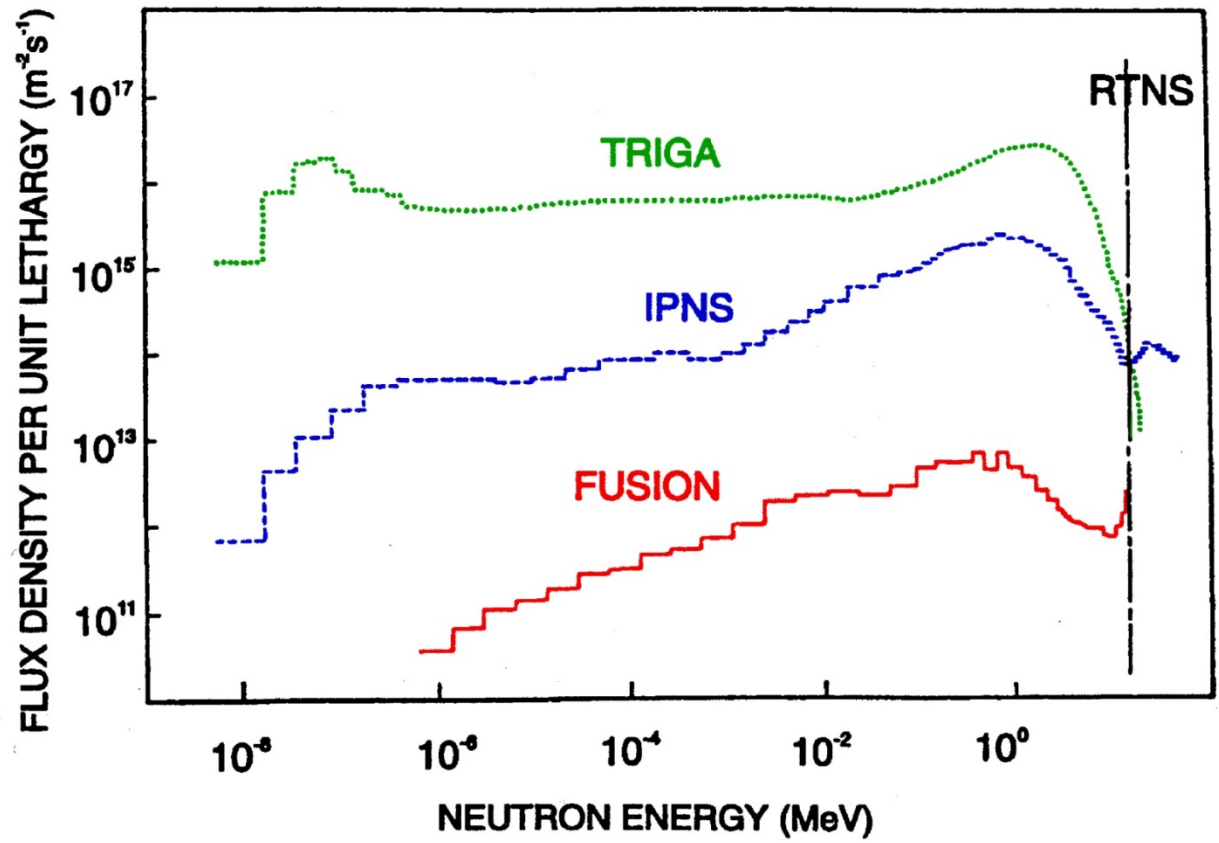


Production of 14 MeV neutrons – deposition of energy in the “first wall” → substantial material problems ($\sim 1 \text{ MW/m}^2$)!

At the magnet location: Attenuation by a factor of $\sim 10^6$. Scattering processes lead to a “thermalization” of the neutrons!



Neutron Energy Distribution

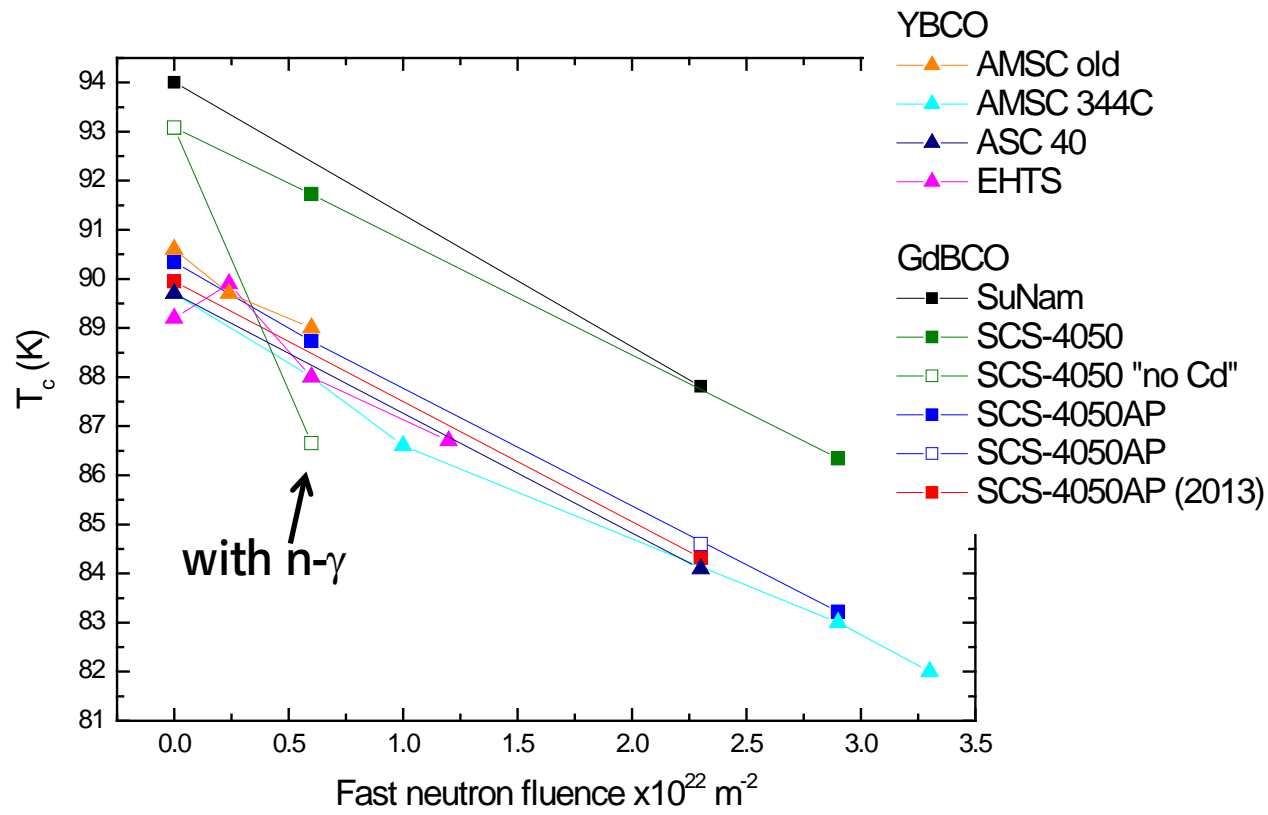


Samples

- **AMSC 344C Amperium (ASC-40)**
 - RABiTS template
 - REBCO by MOD Y:Dy:Ba:Cu=1:0.5:2:3 (1.2 μm)
 - Brass laminated
- SuperPower SCS4050/SCS4050-AP
 - Hastelloy MgO-IBAD Template
 - GdBCO by MOD (1 μm)
 - BZO nano-particles (SCS4050-AP)
- SuNam
 - SS MgO-IBAD Template
 - GdBCO by RCE-DR (1.35 μm)



Decrease in Transition Temperature

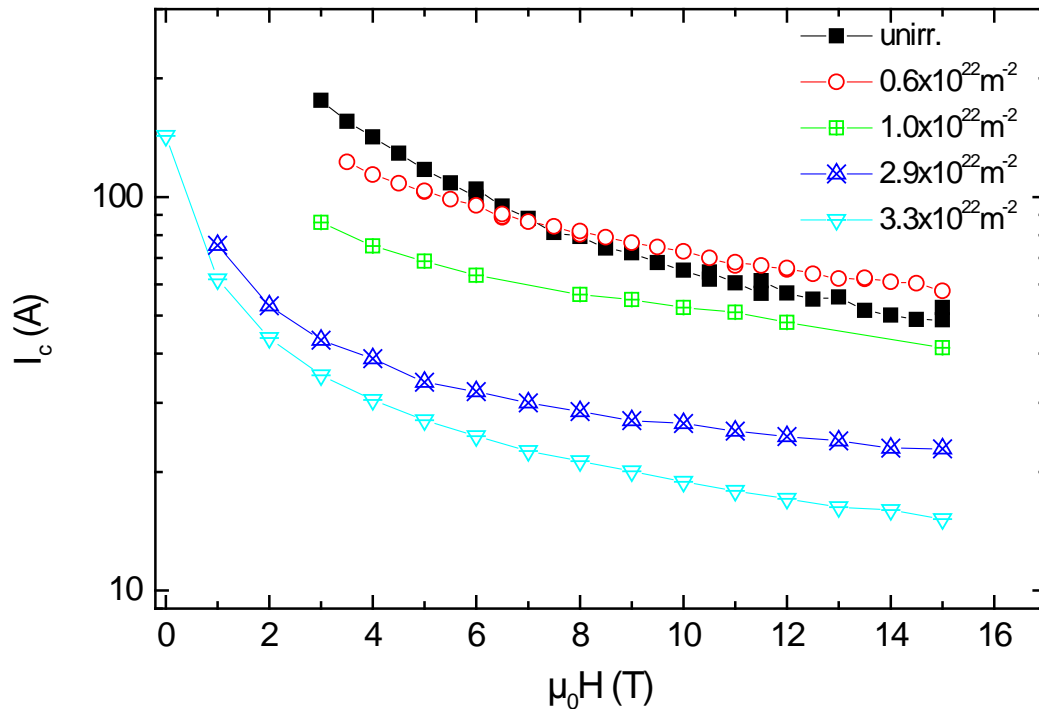


Decrease in T_c : ~ 2.5 K at a fluence of 10^{22} m^{-2} (2.7%)



Critical currents of 344C (AMSC old)

H||ab @ 50 K

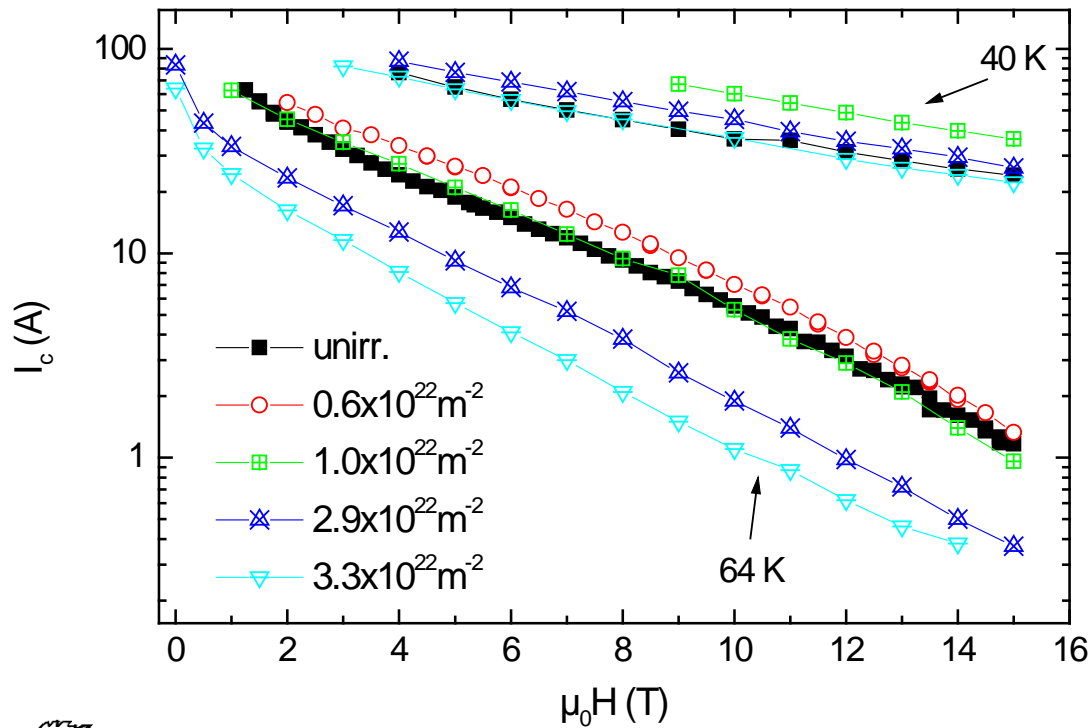


- Small I_c enhancement at high fields after irradiation to $0.6 \cdot 10^{22} \text{ m}^{-2}$
- Strong I_c reduction at higher fluences



Critical currents of 344C

H||c @ 64 K and 40 K

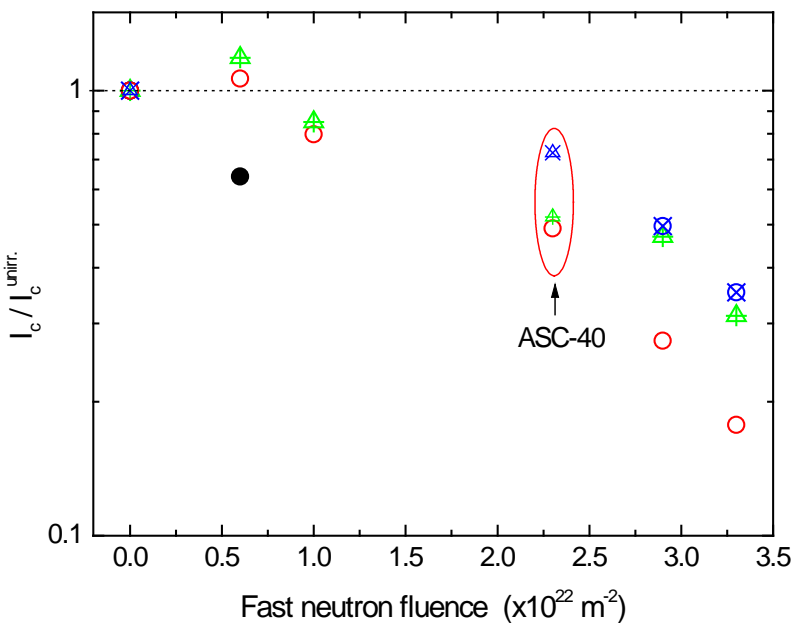


- Temperature dependent I_c enhancement
- Degradation starts after irradiation to $1.0 \cdot 10^{22} \text{ m}^{-2}$ at 64 K and after $2.9 \cdot 10^{22} \text{ m}^{-2}$ at 40 K.

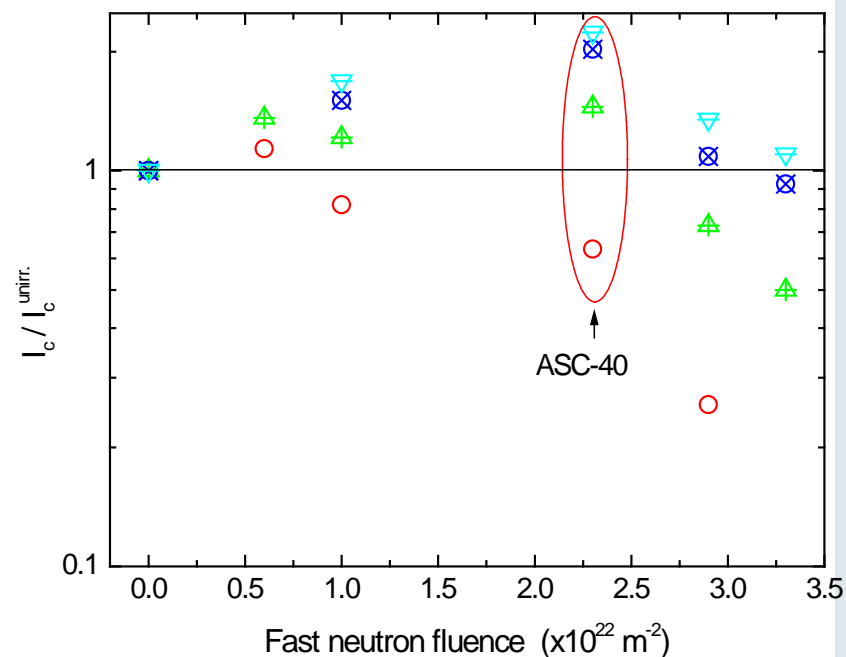


Normalized Critical Currents

H||ab 15 T



H||c 15 T



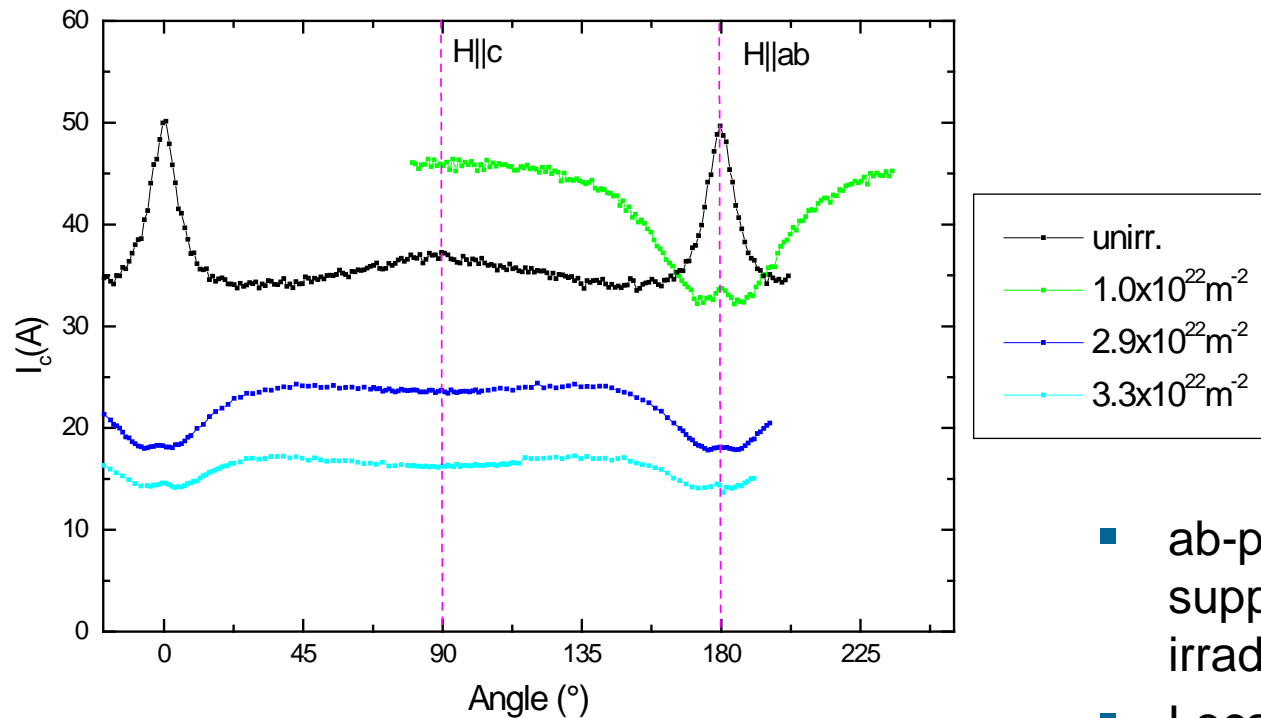
Maximum at low fluence.

Maximum at around $2.3 \cdot 10^{22} \text{ m}^{-2}$.
Lower temperatures: Slower degradation.



I_c -Anisotropy

344C @ 64 K / 2 T

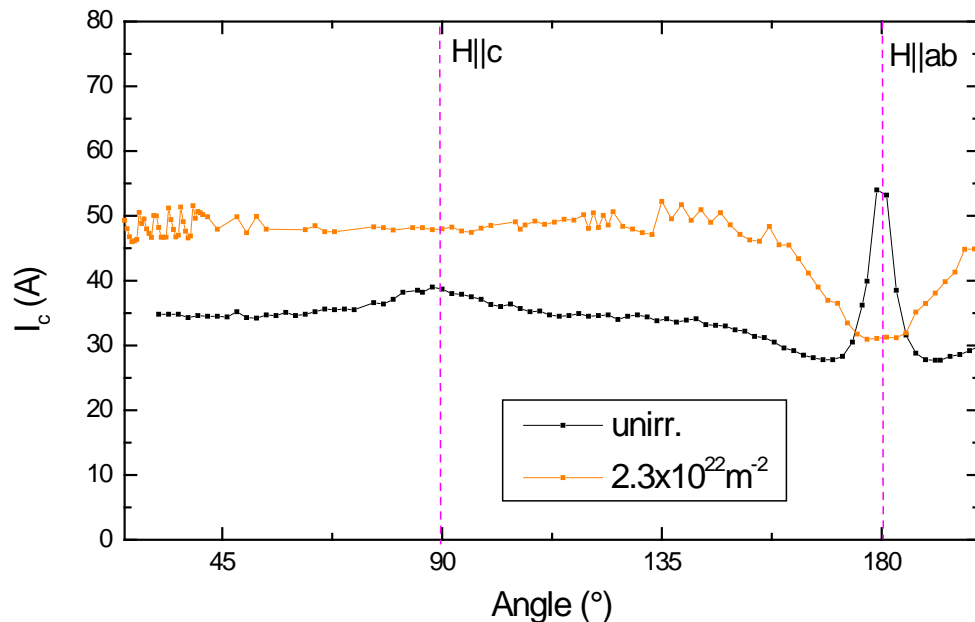


- ab-peak heavily suppressed after first irradiation step
- Local minimums are found close to main field orientations



I_c -Anisotropy

ASC-40 @ 60 K / 5 T

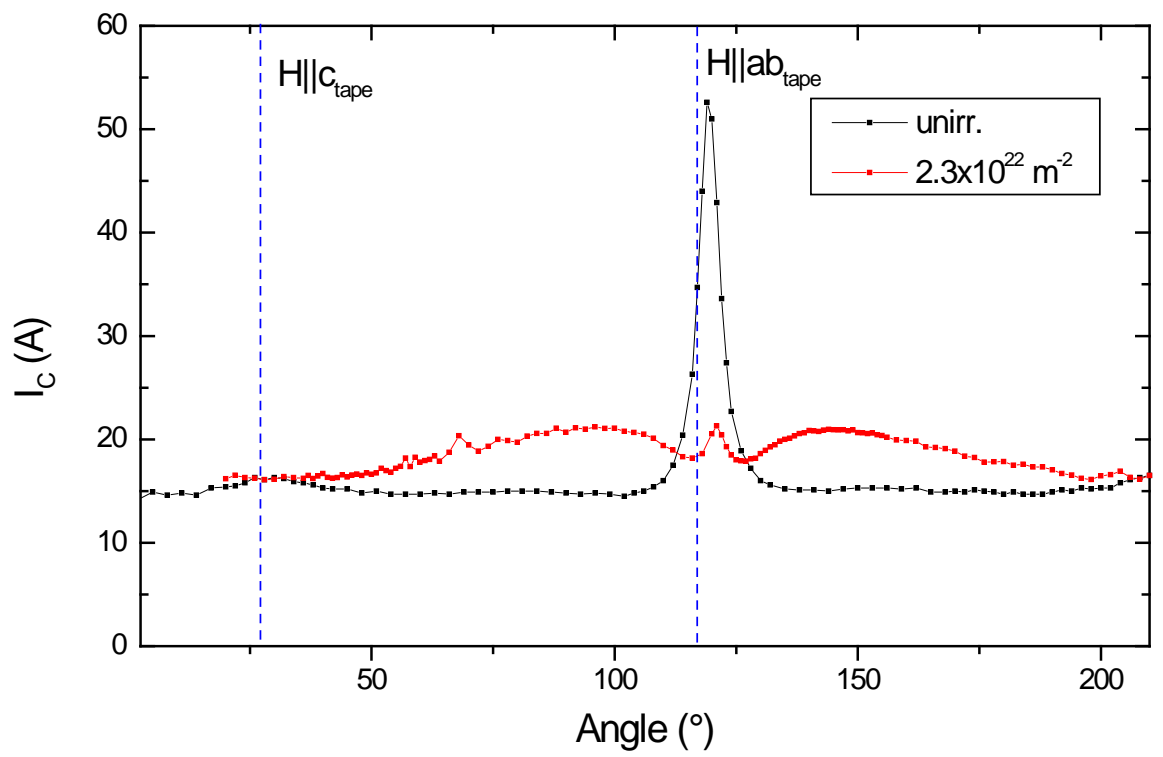


- ab-peak heavily suppressed after irradiation
- Peaks in pristine tape turns into minimums after irradiation



I_c -Anisotropy

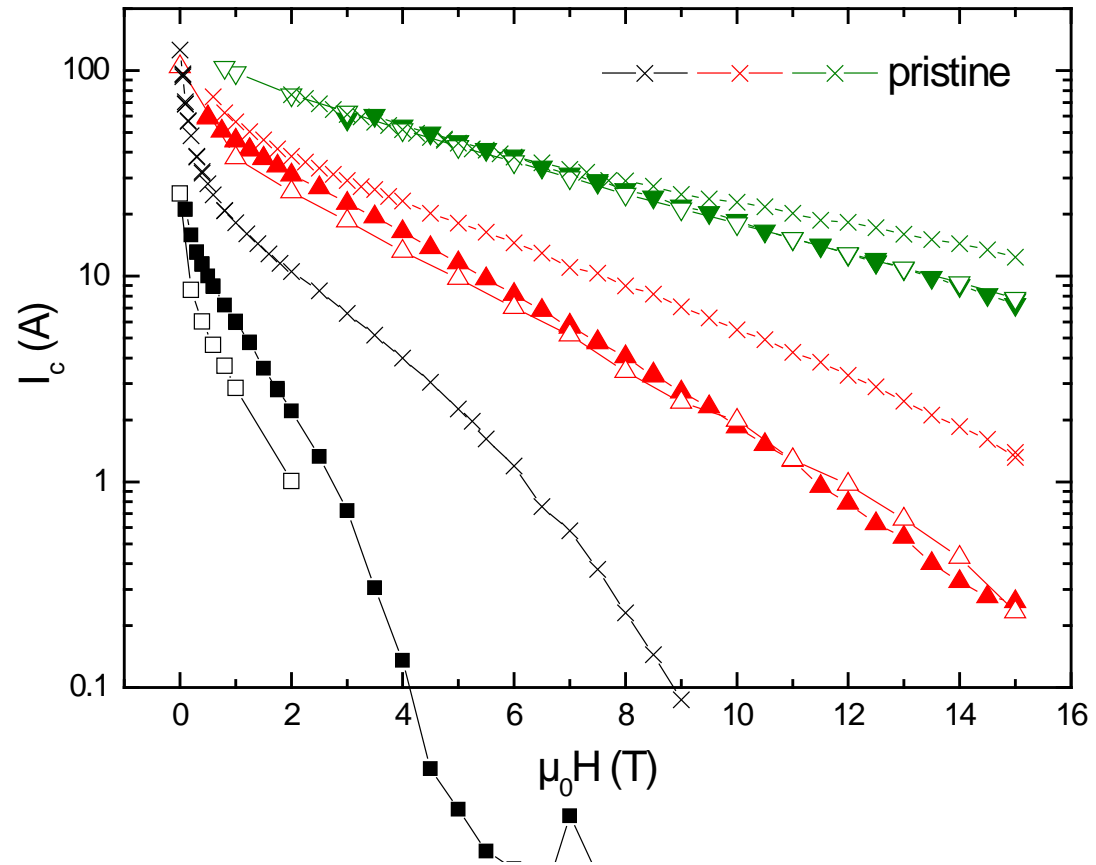
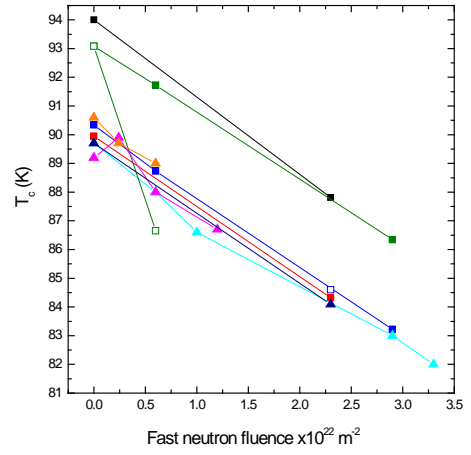
SuNam @ 5 T / 64 K



**WHICH DEFECTS ARE RESPONSIBLE
FOR FLUX PINNING/DEGRADATION?**



Large vs. small defects



SCS4050
 $0.6 \times 10^{22} \text{ m}^{-2}$
 (unshielded)
 $T_c = 86.65 \text{ K}$
 —■— 77 K
 —▲— 64 K
 —▼— 50 K

$2.9 \times 10^{22} \text{ m}^{-2}$
 (shielded)
 $T_c = 86.35 \text{ K}$
 —□— 77 K
 —△— 64 K
 —▽— 50 K

Density of collision cascades differ by a factor of about 5!



Displaced atoms

1) Without Cd-screen (fast/thermal neutron fluence: $6/5 \cdot 10^{21} \text{ m}^{-2}$)

$$n\text{-}\gamma: 5 \cdot 10^{21} \text{ m}^{-2} \cdot 61 \text{ kbarn} \cdot 0.145 \text{ (Gd-155)} \cdot 1/13 = 3 \cdot 10^{-4} \text{ dpa}$$

$$n\text{-}\gamma: 5 \cdot 10^{21} \text{ m}^{-2} \cdot 254 \text{ kbarn} \cdot 0.157 \text{ (Gd-157)} \cdot 1/13 = 1.5 \cdot 10^{-3} \text{ dpa}$$

$$\text{Cascades: } 3 \cdot 10^{22} \text{ m}^{-3} \cdot 500 / 2.7 \cdot 10^{28} \text{ m}^{-3} = 5.5 \cdot 10^{-4} \text{ dpa}$$

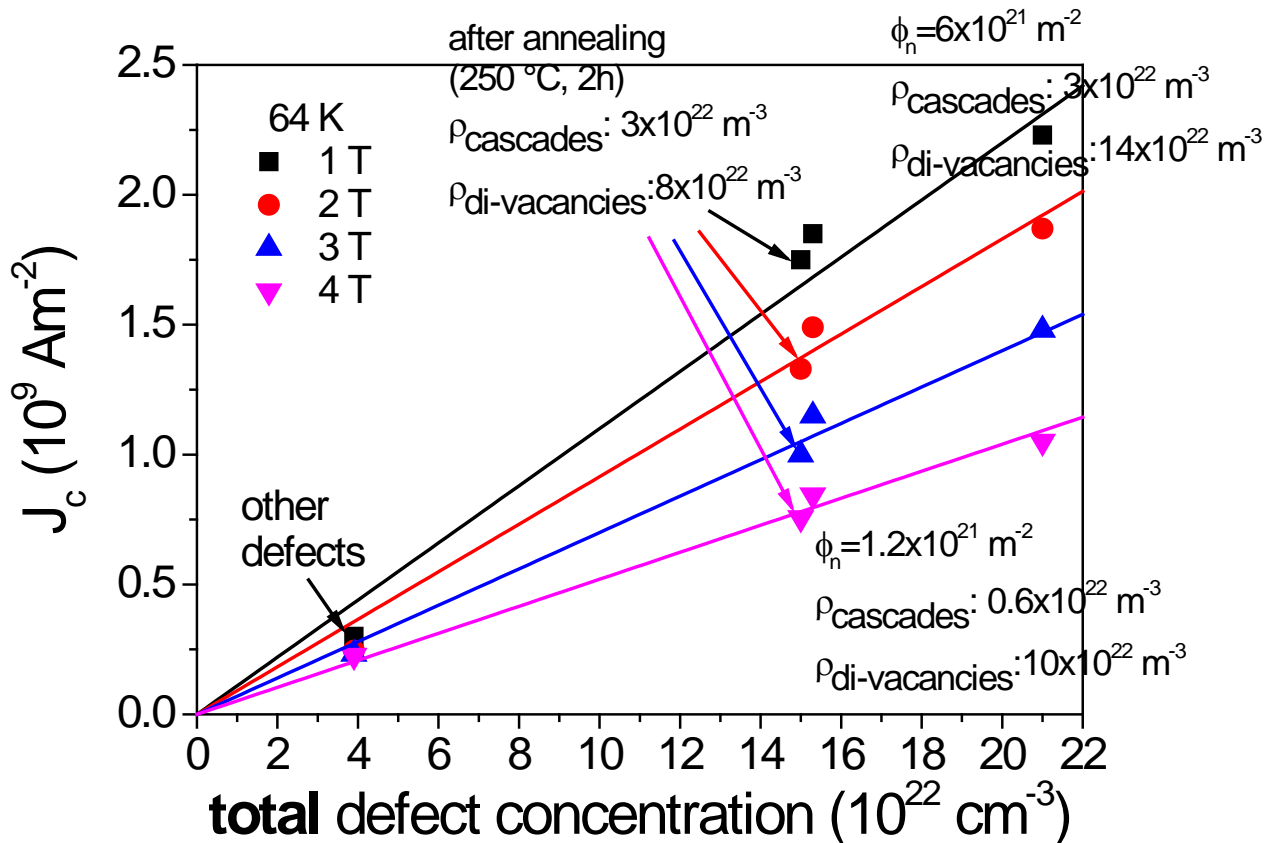
Total: $2.3 \cdot 10^{-3} \text{ dpa}$

2) With Cd-screen (fast neutron fluence: $2.9 \cdot 10^{22} \text{ m}^{-2}$)

$$\text{Cascades: } 1.45 \cdot 10^{23} \text{ m}^{-3} \cdot 500 / 2.7 \cdot 10^{28} \text{ m}^{-3} = \mathbf{2.6 \cdot 10^{-3} \text{ dpa}}$$



Large vs. small defects (melt textured YBCO)



Linear scaling with total (cascades+di-vacancies+original) defect density!
 Different "stable dpa" similar J_c .

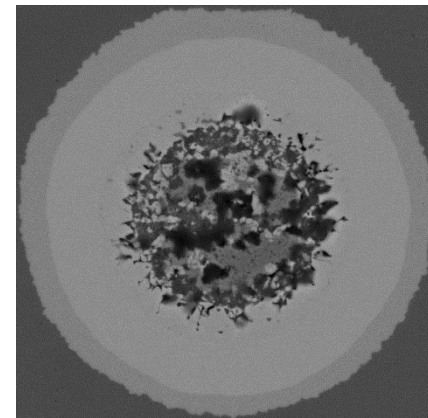
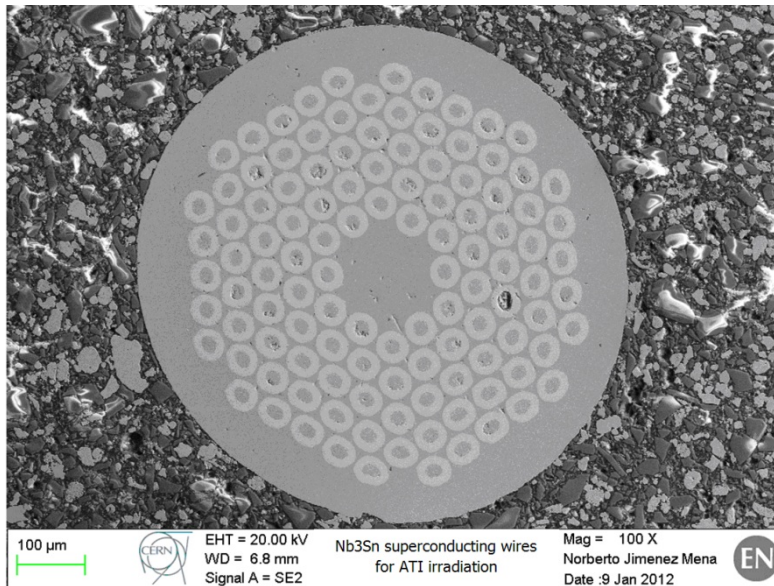


Nb_3Sn FOR ACCELERATOR MAGNETS

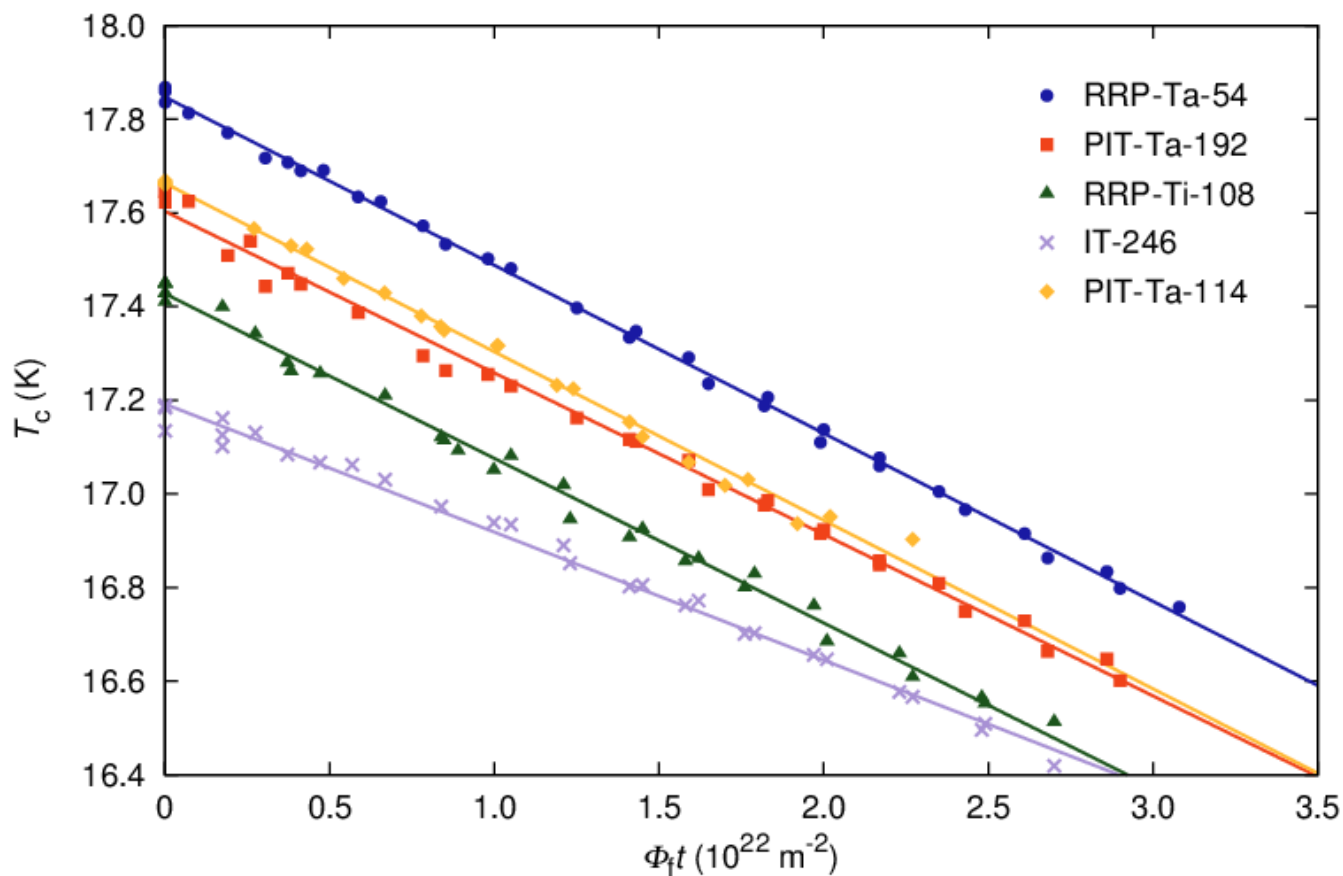


5 types of state-of-the-art Nb₃Sn wires

- Ta-alloyed RRP (restack-rod process), 54 sub-elements
- Ti-alloyed RRP, 108 sub-elements
- Binary IT (internal tin), 246 sub-elements
- Ta-alloyed PIT (powder-in-tube), 192 sub-elements
- Ta-alloyed PIT, 114 sub-elements



Decrease in Transition Temperature: Nb₃Sn

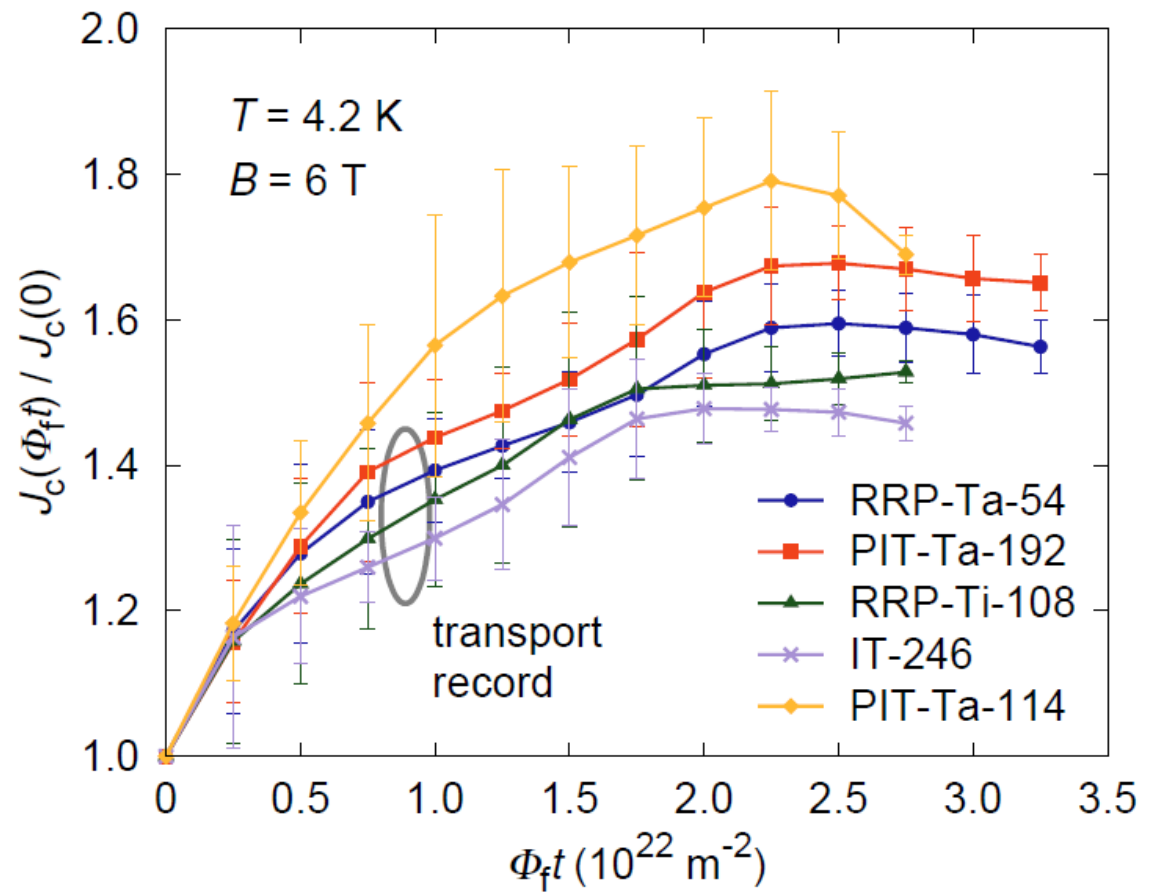
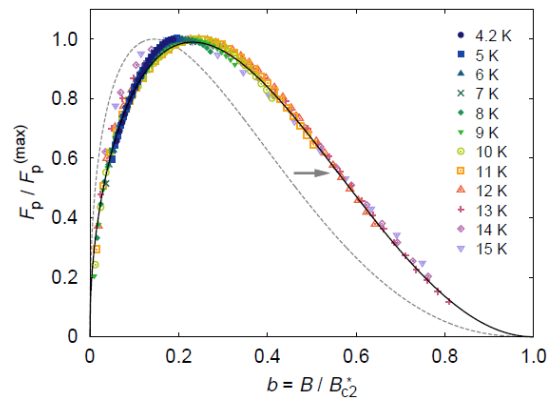


Decrease in T_c : ~ 0.35 K at a fluence of 10^{22} m^{-2} (2%)



Critical Current: Nb₃Sn

Volume pinning force

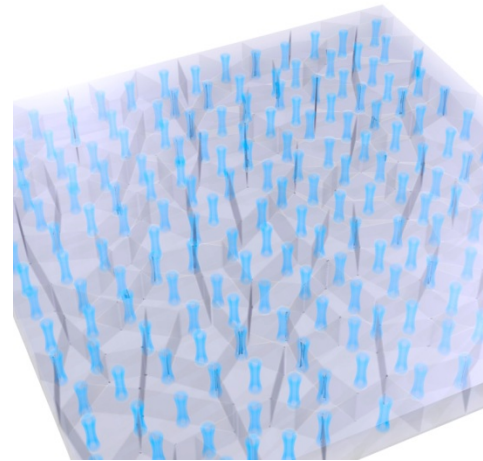
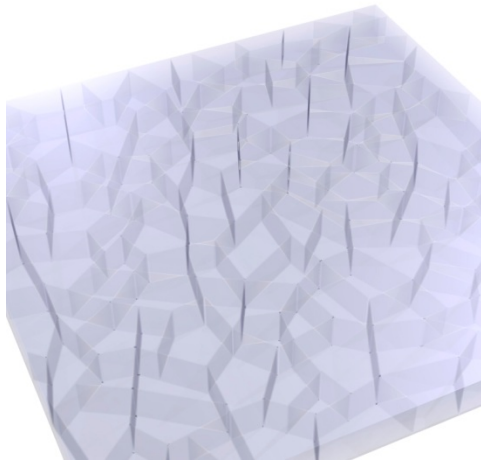


Maximum of J_c at a fluence of about $2.5 \cdot 10^{22} \text{ m}^{-2}$



Pinning Mechanism

- Possible contributions of other pinning mechanisms¹ were investigated to explain the observed shift in the pinning function
- $f(b) = \alpha b^{p_1}(1 - b)^{q_1} + \beta b^{p_2}(1 - b)^{q_2}$
- p_1 and q_1 correspond to the unirradiated state, $\alpha + \beta = 1$
- Shift can be explained with a point-pinning contribution² ($p_2 = 1, q_2 = 2$) which increases with fluence



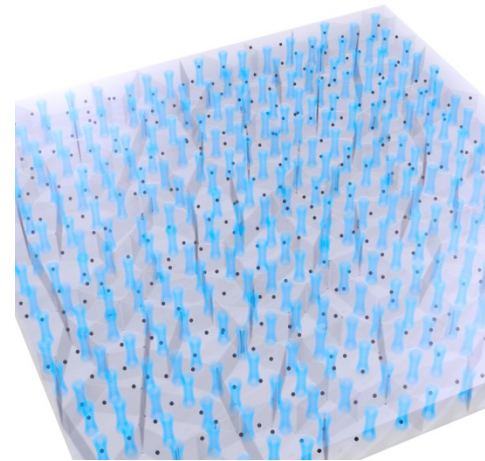
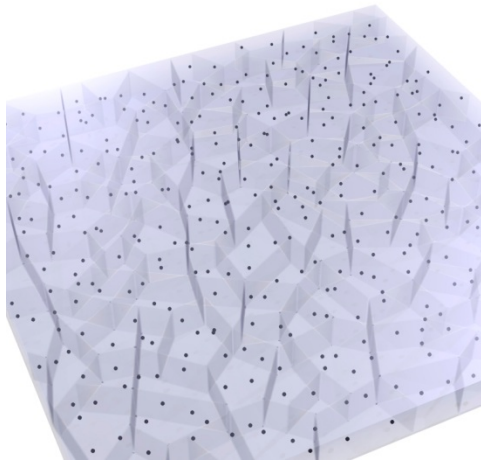
¹ D. Dew-Hughes: *Phil. Mag.* **30**, 293–305, 1974

² T. Baumgartner et al.: *Supercond. Sci. Technol.* **27**, 015005, 2014



Point Pinning

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- $f(b) = \alpha b^{p_1}(1 - b)^{q_1} + \beta b^{p_2}(1 - b)^{q_2}$
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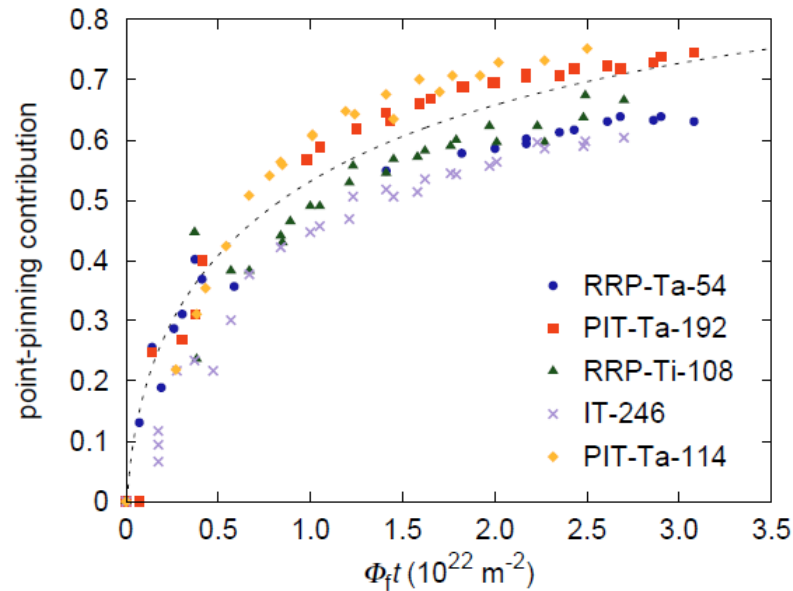


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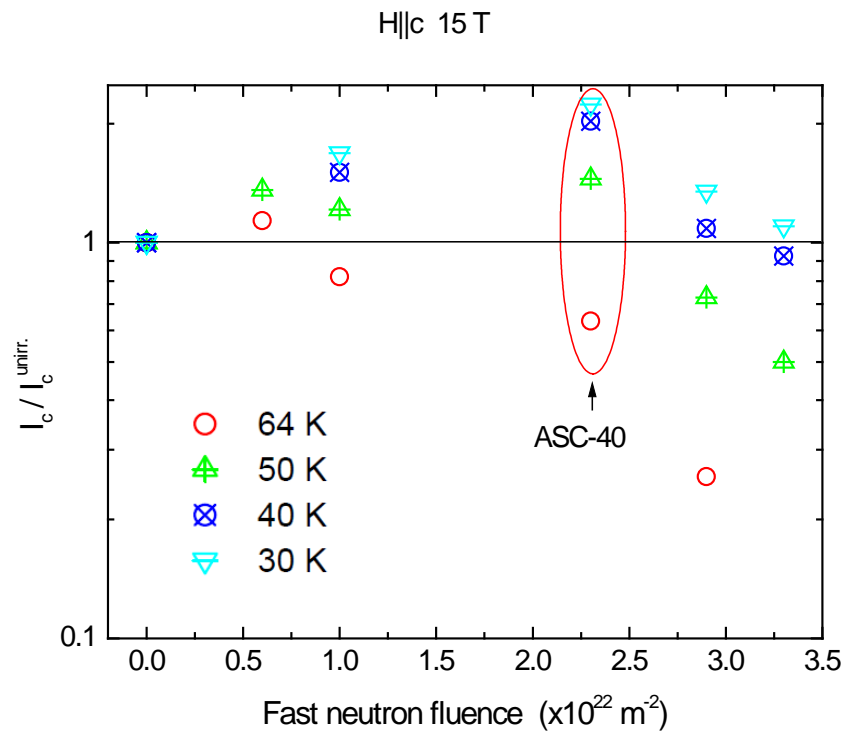
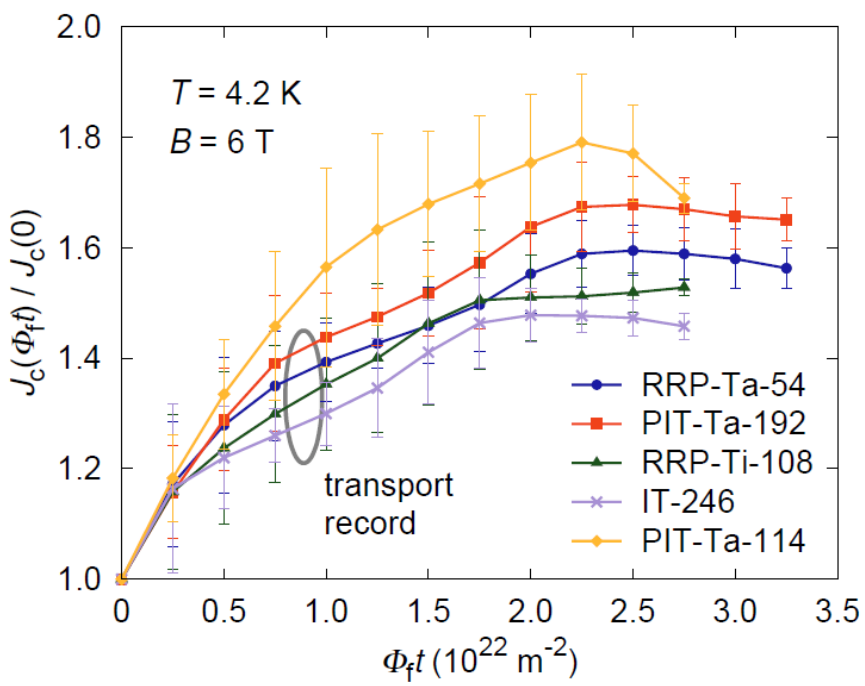
Point Pinning



- ▶ Point-pinning contribution was evaluated as a function of fast neutron fluence for all examined wires
- ▶ Same trend for all wire types
- ▶ Steep increase at low fluences, followed by saturation behavior



Critical Currents: Comparison YBCO – Nb₃Sn



Which compound is more robust against radiation?



Conclusions

- The defect structure relevant for the change of J_c following neutron irradiation has to be identified and related to the damage mechanism in order to make reliable predictions of the conductor life-time in accelerator magnets.
 - Microstructural investigations
 - Comparison of different irradiation experiments
 - Modelling of stable defects
 - Annealing?
- The radiation resistance decreases at higher temperatures. Restriction to low temperatures (LH₂?).
- Similar radiation hardness for coated conductors and Nb₃Sn at low temperatures.

