



Development of Indian High Intensity Proton Accelerator (In Collaboration with Fermilab Project-X)

Shekhar Mishra

Project-X, Fermilab

International Collaboration Coordinator

Talk Given at BARC/DAE March 22nd, 2011





- Ph.D., Experimental Nuclear Physics, University of South Carolina and Los Alamos National Laboratory (LANL) (1987)
- Research Associate, LANL, 87-89
 - Principle Investigator of 3 experiments at LANL
- Research Associate, Fermilab, 89-91
 - Lead Author and only RA on experimental proposal E789
- Staff Scientist Fermilab, 91-Present (Scientist-II)
 - Physicist in Charge, Fermilab Experiment E789, 1992-93
 - Main Injector Department
 - Main Injector and Recycler Accelerator Physics Team 1991-2003
 - Member of the Fermilab Run Coordinator team, 1994-95
 - Head of the Main Injector Commissioning, Fermilab, 1998-99
 - Head, Main Injector Department, Fermilab, 1999- 2003
 - Head of the Recycler Ring Commissioning, 2001-03
 - Program Leader, ILC R&D at Fermilab, 2003-2005.
 - Deputy ILC/SRF Program Director, Fermilab, 2005-2010
 - Project-X, International Collaboration Coordinator, 2010-Present
- Adjunct Professor, University of Delhi
 - Supervise Ph.D. student, Chair Ph.D. Thesis committee



TO SOUGAR

My Laboratory: Fermilab



The Fermilab Tevatron has now passed on the energy frontier to LHC, following 25 years as the highest energy particle collider in the world.

Fermilab operates the highest power long baseline neutrino beam in the world. But will face stiff competition from J-PARC

India Collaboration Development



- In 2002, International Linear Collider
 - Discussed collaboration with Prof. V. S. Ramamurthy
 - Nov. 2003 Indian and US Institutions Interaction meeting
 - 19 US Scientists and mangers came to this meeting and site visit
 - 2004 DAE and DST formed a working group to develop collaboration, all DAE lab directors were member
 - 2004, SRF was chosen as the technology for ILC
 - 2006 Umbrella MOU signed
 - 2007 an Addendum to collaborate on SRF was signed
 - Pitamber Singh and Jishnu Dewedi visited Fermilab
- In 2008, Fermilab and US attention shifted from ILC to High Intensity Proton Accelerator
 - Dr. Pier Oddone, Director, Fermilab, wrote a letter to Dr. Anil Kakodkar, Secretary, DAE inviting India to collaborate on High Intensity Proton Accelerator
 - Dr. Kakodkar sent a very positive response
 - Jan 2009, During the signing of the Addendum MOU III at Indore, Dr. Kakodkar and Dr. Oddone met privately
 - Concept of "Total Project Collaboration" emerged
 - Fermilab changed the HIPA design from Pulsed to CW
 - Supplement I to Addendum MOU III was developed
 - Oct 2009, Dr. Banerjee, Dr. Bhandari and Dr. Sahni, visited Fermilab
 - Jan 2010, Dr. Dennis Kovar, Assistant Secretary, US-DOE-HEP visited DAE
 - Idea of three Phase Collaboration Developed
 - Brinkman, Director, US-DOE-OS met with Dr. Banerjee and Dr. Grover several time



Status: MOU and Agreement



- In Feb 2010, Shekhar Mishra made first US government presentation on behalf of DOE at DAE-OYC
 - US-India Civil Nuclear Working Group
- May 2010, Dr. Banerjee requested US-DOE for a Road Map for this collaboration
 - Mr. Dennial Poneman Deputy Secretary, Dr. Brinkman, Dr. Miller, Dr. Banerjee and Ms. Meera Shankar, Indian Ambassador met in Washington to discuss this Road Map
 - Supplement I to Addendum MOU III and additional MOUs were discussed
 - Dr. Poneman and Dr. Banerjee agreed to develop DOE-DAE agreement
- Oct 2010 IIFC meeting to discuss these documents in detail
 - Dr. Banerjee gave IIFC action items for Indian XII Plan.
- US-DOE and Indian-DAE are working on the text of an agreement for the Phase III of this collaboration.
 - US-DOE has obtained Circular-175 for this collaboration
 - The Circular 175 procedure seeks to confirm that the making of treaties and other international agreements by the United States is carried out within constitutional and other legal limitations, with due consideration of the agreement's foreign policy implications, and with appropriate involvement by the State Department.
 - Fermilab, US-DOE, US-SD,... has gone over this collaboration with India
 - A high level agreement document is with DAE at present
 - As soon as that is signed, we will develop addendums to this agreement for Phase-III
 - Dr. Kakodkar and Dr. Banerjee has already discussed the high level contents with Dr. Oddone, Dr. Kovar and Dr. Brinkman





- In Summer 2010, Dr. Srikumar Banerjee, Secretary, Department of Atomic Energy, India, has formed two Indian committee for the Indian side of IIFC management.
 - DAE-ACFAP (Apex Committee to Formulate Action Plan)
 - Dr S. Banerjee- Chairman
 - Dr. S. Kailas, Convener
 - IC-IIFC (Internal Committee for Indian Institutions & Fermilab Collaboration (IC-IIFC) with participating institutions
 - Bhabha Atomic Research Centre
 - Raja Ramanna Centre for Advanced Technology
 - Variable Energy Cyclotron Centre
 - Inter-University Accelerator Centre
 - Indira Gandhi Centre for Atomic Research
 - Dr. R. K. Bhandari, Chairman
 - Dr. V. C. Sahni, Convener
 - Dr. P. Singh, Member-Secretary
- IC-IIFC to develop the technical part of this collaboration
 - Working with IC-IIFC we have developed several documents, 3 additional Addendum MOUs and Project Documents



IIFC Joint Management









- A multi-institutional collaboration has been established to execute the Project X RD&D Program.
 - Being organized as a "national project with international participation".
 - Fermilab as lead laboratory with ultimate responsibility
 - International participation via "in-kind" contributions, established through bi-lateral MOUs.
 - Collaborators assume responsibility for components and sub-system design, development, and construction.
 - National Collaboration
 - **MOU signatories:**

ANL	ORNL/SNS
BNL	MSU
Cornell	TJNAF
Fermilab	SLAC
LBNL	ILC/ART

International Collaboration MOU				
	Indian Institutions:			
	BARC/Mumbai			
	IUAC/Delhi			
	RRCAT/Indore			
	VECC/Kolkata			



Indian Nuclear Program



- Indian 3rd Stage program focuses on utilization of thorium.
- Paths of converting Thorium into fissile material:
 - Fast Breeder Reactor
 - AHWR
 - Accelerator Driven System
- ADS is the only system that could remove the Indian dependence on foreign Uranium.
- In ADS high-energy proton beam generates neutrons directly through spallation reaction.
 - Efficient Accelerator
 - Accelerator → Spallation Target
 - Reactor









Beam Energy and Power





Beam power needed to drive a 0.8 GW ADS sub-critical core as a function of k_{src} , the effective neutron multiplication factor.

Beam Power → 1-2 MW

Neutron yield as a function of proton energy for one set of target and moderator condition

Beam Energy 1-2 GeV









Beam Parameter	Parameter value or range for the Nuclear Energy Demonstration Experiment
Beam Power	1-2 MW
Beam Energy	1-2 GeV
Beam Time Structure	Continuous Wave
Beam trips (1 <t<10 sec)<="" td=""><td>< 5000 per year</td></t<10>	< 5000 per year
Beam trips (10 sec < t < 5 mins)	< 2500 per year
Beam trips ($t > 5$ mins)	< 50 per year
Availability	≻ 50%



Key Technology Issues





Technology Demonstration Facility



Technology Demonstration



		Transmutation	Industrial-Scale	Power
		Demonstration	Transmutation	Generation
Front-End System	Performance			
	Reliability			
Accelerating	RF Structure Development			
System	and Performance			
	Linac Cost Optimization			
	Reliability			
RF Plant	Performance			
	Cost Optimization			
	Reliability			
Beam Delivery	Performance			
Target Systems	Performance			
	Reliability			
Instrumentation and Control	Performance			
Beam Dynamics	Emittance/halo growth/beamloss			
	Lattice design			
Reliability	Rapid SCL Fault Recovery			
	System Reliability			
	Engineering Analysis			

Green: Ready, Yellow: May be ready, Red: More R&D

Px: Reference Design Configuration





- 3-GeV, 1-mA, CW linac, 325 and 650 MHz, provides beam for rare processes, nuclear and energy programs
 - ~3 MW; flexible provision for beam requirements supporting multiple users
 - < 5% of beam is sent to the Main Injector</p>
- Reference Design for 3-8 GeV acceleration: pulsed linac
 - Linac would be 1300 MHz with <5% duty cycle</p>





 A multi-MW Proton Source with 1-2 GeV, ~2MW, CW proton beam could be the accelerator, spallation target, and accelerator, target and reactor interface, technology demonstration project corresponding to 10s of MW electrical power production.





SRF Accelerator Design





- Ion source
- Radio Frequency Quadrupole
- Medium Energy Beam Transport (MEBT), including the bunching cavities
- Three accelerating sections based on <u>325 MHz Single-Spoke Resonators (SSR)</u>
- Two accelerating sections of <u>650 MHz elliptical cavities</u>.

Fermilab

Radio Frequency Quadrupole



- The Radio Frequency Quadrupole is placed after the ion source for simultaneous
 - focusing, bunching and accelerating the low energy ion beams with high transmission and good beam quality (low emittance).
- The Beam dynamics of 2.5 RFQ accelerator for HIPA has been studied for operating frequencies of 325 and 162.5 MHz using the codes PARMTEQM/TOUTATIS. (Rao, BARC)
 - The simulations have been done using two different techniques: LANL technique and Non-adiabatique technique.



Parameters	Values	Units
Ions	H-	
Frequency	162.5	MHz
Vane voltage	108	kV
Peak Field	21.5	MV/m
R0	0.72	cm
Transmission (p)	98.9	%
Length	4.01	cm

Table 3: Parameters of 162.5 MHz RFQ

Figure 4: Evolution of emittances along RFQ.



RFQ at Fermilab



- Fermilab is developing a High Intensity Front End Test Facility for HIPA.
 - Indian colleagues (BARC) are participating in this activity.



- BARC could propose to fabricate two CW-RFQ of the design that is being developed in collaboration with Fermilab.
 - Send one to Fermilab and test it with beam



- Extensive design of the SRF accelerator layout and beam optics has been carried using five families of cavities
 - Increase the acceleration efficiency
 - Minimize the cost
 - Reduce the beam loss
 - Operation at higher intensity





- Accelerator design and its interplay with engineering:
 - The SC linac lattice is independent of beam current, wave numbers (phase advance per unit period length) of transverse and longitudinal oscillations should be smooth through the SC linac and should change only gradually in order to avoid possible mismatch.
 - Longitudinal phase advance (under zero beam condition) is smooth without discontinuities throughout the SC linac to avoid halo excitation.
 - Length of the focusing period is kept short, especially in the low energy section where space charge dominates.
 - Matching between each cryomodule is smooth to avoid halo generation and emittance growth.
 - Beam matching is achieved by adjusting the gradients and phases of the outermost elements of each side of the transition.

CW Linac (RMS) Beam Envelopes



TraceWin - CEA/DSM/Irfu/SACM

Lattice V 3.8.4 (650 MHz to 3 GeV)



TOP: Transverse horizontal and vertical envelopes **BOTTOM:** Longitudinal envelope



Beam Dynamics









- Matching between each cryomodule is smooth to avoid halo generation and emittance growth.
 - Beam matching is achieved by adjusting the gradients and phases of the outermost elements of each side of the transition.
- Lattice design is robust to allow for spread in designed parameters
 - Spread in cavity gradient, operation of linac with failed beam line elements, misalignments etc.





Steering Error Correction





Beam Centroid Position

<u>RED</u>: steering correction <u>**OFF**</u>



Transverse Emittance

BLUE: steering correction **ON**

- Misalignments ±1 mm for all elements (specification ±0.5 mm)
- RF jitter of 0.5 ° x 0.5 % in the front-end & 1 ° x 1% RF jitter in the highenergy part was implemented.
- 100 seeds and 1 million macro-particles per seed.
- 1 corrector,+ 1 BPM per solenoid/doublet/quad; BPM resolution = 30 μm
- Beam centroid is corrected to ± 1mm; Emittance increase < 20%.
- The uncorrected seeds predict losses above 100 W/m; corrected no losses





- Working gradient of the cavities are limited by the peak surface magnetic field & cryogenic losses.
 - Maximum surface field which is chosen to protect the RF cavity from quenching.
 - 60 mT for all the 325 MHz cavities
 - 70 mT for all the 650 MHz cavities.
 - Cryogenic losses per cavity should be less than 25 W.







Ion source, RFQ						
	SSR0 S	SR1 SS	R2 <mark>β=0</mark>	.6 <mark>β=0.</mark> 9	9	
			->		-	
MEBT	325 MHz, 2	2.5-160 Me	e <u>V</u> 650	MHz, 0.16	5-3 GeV	<u>Arun</u>
	SSR0	SSR1	SSR2	LE	HE	HE (2-3Gev)
# Cavities	18	20	40	36	96	56
# Solenoids	18	20	20	0	0	0
# Quadrupoles	0	0	0	24	24	14
# Cryomodules	1	2	4	6	12	7
Length (m)	11.38	16.8	34.86	61.93	184.8	107.8
Position (m)	0	11.38	28.18	63.04	124.97	309.77
Period Length (m)	0.61	0.8	1.6	5	15.4	15.4
# periods	18	20	20	12	12	7
Transition Ene (MeV)	10.18	42.57	160.53	515.38	2056	3028
Transition β	0.146	0.291	0.52	0.763	0.95	0.97

325 MHz spoke cavities family





SSR0 - design SSR1 – prototyping, testing SSR2 - design

Parameters of the Single-Spoke Resonator cavities

cavity type	β _G	Freq MHz	Beam pipe ø, mm	V _{a, max} MeV	E _{max} MV/m	B _{max} mT	R/Q, Ω	G, Ω	*Q _{0,2K} ×10 ⁹	P _{max,2K} W
SSR0	β=0.114	325	30	0.6	32	39	108	50	6.5	0.5
SSR1	β=0.215	325	30	1.47	28	43	242	84	11.0	0.8
SSR2	β=0.42	325	40	3.34	32	60	292	109	13.0	2.9



325 MHz Cavity Result





Eacc > 15 MV/m for Q > 1e10 HIPA Design needs < 10 MV/m



650 MHz Cavity Design Parameters







650 MHz: β=0.61

650 MHz: β=0.9



β	0.61	0.9
R/Q, Ohm	378	638
G-factor, Ohm	191	255
Max. gain per cavity, MeV (on crest)	11.3	19.9
Gradient, MeV/m	16.1	19.2
Max. Surface electric field, MV/m	36.4	37.3
E _{pk} /E _{acc}	2.26	2
Max surf magnetic field, mT	68	72
B _{pk} /E _{acc}	4.21	3.75

Cavity Accelerating Gradient









- Cavity Design and Fabrication:
 - Niobium purchased from Industry
 - Nb QA/QC at Laboratory
 - Cavity Fabricated by lab/Industry
 - Cavity QA/QC at Laboratory
- Cavity Process and low power test at Laboratory
 - Bulk processing at lab/industry
 - Fine processing, assembly
 - Vertical Test Stand at laboratory
- Dressed Cavity (He vessel, Tuner, Coupler) at Lab
 - Start at lab but work to transfer this technology to industry
- High Power Test of Dressed Cavity at Lab
 - Horizontal Test Stand
- Cavity String and Cryomodule Fabrication at Laboratory
- Cryomodule Testing at Full Power at lab
 - Cryomodule Test Stand

Cavity & Cryomodule Fabrication









- Under the Addendum MOU III and its Supplement I, Indian Institute and Fermilab Collaboration are jointly developing the design and fabrication of Cavity in India.
 - SSR1 Cavity is under fabrication at IUAC
 - Fermilab transferred all the drawings and tooling information to IUAC.
 - IUAC with a local industry has developed all the infrastructure for this cavity fabrication
 - First two prototype fabrication is progress. These two will be processed and tested at Fermilab.
 - Future processing and testing in India.
 - These will be also dressed (VECC) and 325 MHz power coupler attached in India (BARC).
 - Elliptical Cavities are under fabrication at RRCAT and VECC
 - RRCAT engineering have made many visits to Fermilab and US industries for the development of the cavity fabrication infrastructure in India.
 - Development of cavity fabrication technology using 1.3 GHz cavity
 - Excellent prototype results.



Fabrication of SSR1



SSR1 cavities are under fabrication at IUAC



Major components of SSR1 – β = 0.22, f = 325 MHz





Figure 6: Electron beam welding setups showing, (a) above – outer shell, (b) below – spoke halves.





- RRCAT in collaboration with IUAC is developing elliptical 1.3 GHz cavities
 - Indian engineers were trained at Fermilab and US industry
- Three 1-cell 1.3 GHz (β=1) cavities have been built by RRCAT, in collaboration with IUAC
 - Two 1-cells were inspected, processed and tested at Fermilab
 - TE1CAT001: Quench at 19 MV/m, Q0 at max gradient > 1.5 E+10
 - TE1CAT002: Quench at 21 MV/m, Q0 at max gradient > 1.0 E+10
 - TE1CAT002 : 2nd test after CBP Quench at 23 MV/m, Q0 > 1.5 E+10
 - A third has recently been built using improved weld parameters and handling, based on feedback received, and will be processed and tested at Fermilab
- A fourth 1.3 GHz 1-cell and one 1.3 GHz 5-cell Cavity with straight end tubes to be built later this year; to be processed and tested at FNAL



1300 MHz Cavity: Forming and Machining



RRCAT: Developed forming tooling & process for 1.3 GHz SCRF cavity.



Forming



Inspection



Machining



Formed Niobium Half cell

120 T - HYDRAULIC PRESS




Equator Welding





Setting inside IUAC EBW Chamber



Frequency measurement



Mechanical inspection

This work was carried out by RRCAT in collaboration with Fermilab and IUAC.

Significant input was provided by DESY and US Company AES



IIFC Collaborative work





Figure 8: Quality factor Q_0 as a function of accelerating gradient at 2 K, on the second 1.3 GHz single cell cavity.



TE1CAT003 with RRCAT-IUAC &

FNAL team members





- Preliminary 1-cell design for both betas was presented at LINAC10 (MOP099 by S. Barbanotti et al.)
- 5-cell β=0.9 cavity design nearly final



- Cavity fabrication
 - Ordered six prototype β =0.9 1-cells from industry (AES), first two expected July 2011
 - Will order 2 prototype β =0.9 5-cells soon
- Cavity infrastructure development for process and test in progress



650 MHz IIFC Progress



 650 MHz β=0.9 1-cell and 5-cell cavities to be built, based on experienced gained from 1.3 GHz work at RRCAT and IUAC.



Die- Punch Set at RRCAT



Die-Punch Set mounted on Press at RRCAT



Aluminum blank, 3mm thickness



Beginning of forming trials with aluminum





- Simulations of 650 MHz β =0.61 5-cell cavity at VECC
 - Design comparison using FNAL design input: 2D-SLANS [FNAL], 3D-HFSS [VECC], 3D-CST [VECC], 2D-SUPERFISH [VECC]
 - Some modifications to FNAL design also simulated in 3D-HFSS
 - Fruitful interactions of VECC staff with Fermilab and JLab RF designers have occurred



CST MWS simulation for elliptical SCRF cavity at VECC



End Group Development (RRCAT)





Development of prototype in Low RRR Nb completed at Workshop, RRCAT.





Baroscopic examination

High RRR end group Machining in progress

Concept

Machine out entire end group from a single billet of Nb. Billet is cheaper.
 Material from bore used for making HOM coupler and Form teil.

Advantages

- **1.**Easy manufacturing, Less Fabrication time.
- 2. Just 6 EB weld Joints instead of 13.
- 3. Pre Weld Etching reduced.
- 4. No pull out operations.
- 5. Machining operations. Better control on tolerances.
- 6. Rejections go down. Error in later welding stages causes complete rejection of job.
- 7. LOWER COST: \$16500 per end group \$27000. (Machining costs in India)

Spoke Resonator Cryomodule







Prototype SSR cryomodule









Initiated 650 MHz Cryomodule (CW type)

650 MHz cryomodule team

- Design Effort is spearheaded by Tom Peterson (Sub Proj.Manager FNAL)
- Prashant Khare, (with 4 engineers from RRCAT) is leading Indian effort.
 (Acts as point of contact for Indian Institutions)
- Yuriy Orlov (Fermilab point of contact)

Design status

- Completed Cross Cultural study of designs prevalent at other accelerator laboratories (Jointly by RRCAT and Fermilab)
- Finalized the Overall mechanical and thermal design. A closed-ended cryomodule similar to TESLA-Type selected as an initial baseline.
 Despite Choosing the Tesla Type as a baseline
 - Designs differ due to various kinds of requirements as this will be a CW cryomodule
 - Generally means adapting but not copying design concepts for Project X
- Completed the design of Vacuum vessel, Thermal Shields and concurrent prototyping of cavity support system is in progress.
- Value engineering of entire cryomodule forms a significant part of the effort.



The Approach





AT RRCAT

<u>Unique Features:-</u> As compared to conventional Tesla type Cryomodule.

650 MHz Cryomodule has a heat load of 25 W/cavity as it operates in CW mode. Earlier it was 0.9 W/cavity.

The size of the cavity is almost two times i.e. 400mm dia.





- Various cryomodule designs from laboratories around the world have been reviewed by Fermilab and RRCAT to understand "the state of the art" and to supplement our design concepts
 - Designs differ due to various kinds of requirements
 - Generally means adapting but not copying design concepts for Project X
- Overall mechanical and thermal design based on a closed-ended TESLA-style cryomodule has been selected as an initial baseline
 - Design incorporates unique features for high dynamic heat loads at 2 K (~25 W/cavity)
 - CW operation and RF power tightly constrain cavity tune and microphonics





(Tesla Style-Stand Alone Concept Fermilab)









650 MHz CRYOMODULE & ITS SUBSYSTEMS





650 MHz SCRF CAVITY-UNDER FABRICATION AT RRCAT



He VESSEL to be fabricated



CAVITY SUPORT SYSTEMUNDER PROTOTYPING AT RRCAT



50



THERMAL SHIELD UNDER DESIGNING AT RRCAT



CRYOGENIC SUPPORT POST UNDER PROTOTYPING AT RRCAT



SCRF Cavity supported on HGR pipe



- The model incorporates a modified Cavity support system.
- 2K helium supply line includes a bellow in vertical configuration



Steady State & Transient Thermal Analysis







- 1. Mass flow rate- 24 gm/sec
- 2. Convection heat transfer coefficient-200 W/m2K
- 3. Heat load:
 - Through support post: 10 watt per support post
 Through coupler input: 2 watt per coupler input
- A. Cool down reached in 10.7 Hour
- **B.** Max temperature gradient is found to be less than 40 K at finger weld region
- C. Fig. shows the temperature plot of 70 K thermal shield after 10.7 hours

Snippets of Prototyping & Testing





Cryogenic Support Post



Load Testing of Cryogenic Support Post prototype at RRCAT





Laser welding of Cavity Support system at RRCAT



System

Change)

								-									1	1					
Calculat	e Thickn	iess requ	ired fo	r G11 tu	be								Fg+($\otimes -$	-	_							
	Dimens	ion in re	d can l	e chang	ged for va	riation o	of inputs							Ŷ	1		At the ba	ase of tube	·				ald W
00 - (61	Tuba							Load per	Support po	ost, w	100	Kg		• •	_ +		I ensile s	stress due t	o bending	and direct	compress	$on \rho = -$	21 A
oboran	Tube	60		_		_		Lateral L	Jau, Fy		50	κġ	L				o:	· · -	1 [4FgL	w]			
E		100100		F	- 0	E100		Height of	cavity load	i Centre, L	630	mm					Simplifyi	ng c —	$\sigma \ \pi d^2$	πd.		An onn.	s are in si
Factor A	45.1	103180	14	Facto	и D =	5133.	56	-						11-			Next to	check fr	or elactiv	instaßi	2	Et	
Factor A =	πd^2	Facto	$rB = \frac{r}{\pi q}$	1				Poisson	's Ratio G1	uо	0.2						ineacted	CHECKI		, materia	1.5√3	$1 - \mu^2 d$	
				-									T P 4	1		-				1	- 12 II		1 147-
	Thickn	ess Req	1.5	mm	Consid	ering Ben	ding and											Simplifyin	ng	$t^2 = -$	54541	μ 41	<u></u>
					Direct	Compress	sion						d	1							2 E	Lπe	ί π.
																		Ref: SS	C Magne	t Cryos	at Suspe	nsion S	ystem Desi
			0550					Young's	Modulus G	11, Eo	28	Gpa			_			Advand	ces in Cr	gogenic	Engineer	ing ¥ol 3	33. p227
Factor C:	4.5E-11	I Factor L	6550.	sz Facto	or E= 311.94			roungs	Modulus G	11, EO	2.8E+10	Pa			*	-							
	$1.5\sqrt{3}/1$	- 112 -		F.L	1			o ultimat	e G11		276	Moa	Cross sect	tion area o	of G11 tub	e A - rrdt							
Factor C =	2 E	Fac	tor $D = -$	πd F	actor $E = \frac{1}{\pi}$			σ ultimat	• G11		2.8E+08	Pa	Momentic	of Inertia I	- TTI ³ t -	(m/8)d ^a t							
								Eactorio	f Safetu		4		Where OF	D of tube	d = 2r	(1110)4 (
	Thickn	ness req	0.53	mm	Consid	ering Elas	tic	σ allowat	ole G11		6.9E+07	Pa											
					Instabil	ity							F, is lateral	compone	ent of ship	ping, han	dling and s	eismio loa	d				
						-							"W" is load i	Der SUDDO	ortpost		1						
													4L? is the dis	stance of	C.G. of c	old mass	from base	of support	post				
Calculate	e Contac	ct Pressu	re of th	e Joint a	and Maxiı	num Axi	al Load L	imit															
																			From 2	93K to 10	(Source:	cryogenics	s.nist.gov)
ID of SS E	Disc, d1	1 38.1	1 mm	Poiss	on's Ratio	68304 Dis	c μ1=	0.3		Young's N	Aodulus S	S304 Disc	. E1=	200	Gpa=	200000) N/mm2		AL/L AL6	061T6		3.7	mm/m
ID of G11T	ube, d2 =	86.1	1 mm	Poiss	on's Ratio	G11 Tube	μ2=	0.2		Young's P	Aodulus G	11 Tube,	E2 =	28	Gipa =	28000	N/mm2		AL/L G10	Tube(Warp	9	2	mmim
OD of G11	Tube, d3 =	= 88.9	mm	Poiss	on's Ratio	5S304 Rin	g µ3⊧	0.3		Young's P	/lodulus S	S304 Ring	. E3=	200	Gpa=	200000) N/mm2		AL/LAIS	S304		2.6	mm/m
OD of SS	Disc, d4	4 114.3	mm			_	_	_										· •					
Dismetral	Interferen	nce betwee	n Digo a	nd Tube	51 0.41	7 00	_	_									3	_		(Tu)	ba(2)		
Diametral	Clearance	e between	Disc an	i Tube δι	0 0.3	3 mm			P	$(K_{1} + K_{2})$	+ 8.		8.K. +	$\delta_{-}(K_{*} + 1)$	K-)		6			< 10	00(2)		
		1							$P_i = \frac{1}{2}$	Ke		$P_{\phi} =$	$(K_{\pm} + K_{\pm})(I$	$K_1 + K_2$	- K_K3		2	Dis	c(1) 🖡				
Thickness	s of SS304	4 Disc/Rin	ig, h		19 mm												8	0.0	2-1				
									P ₁ is inner	contact p	essure be	tween dise	and tube		h X	$\sim \sim$	1///			77<	King(3)		
									P _o is outer	contact p	ressure be	tweentuk	e and ring					1 1	1	_			
FrictionC	oeff SS30)4 Disc and	d G11 Tub	e, f1	0	.3																	
	oeff SS30	14 Pipe and	4 G11 Tuk																				
FrictionC		24 Filling and	a can r a	ie, f2	0	.3		-	d_2 [d_2	+ d ₁ ²		$d_2 \left[d_3^2 + c \right]$		<u>da</u>	_2 d <u>š</u>			31					
FrictionC	0.00051	, ing an	K2 -	e, F2		.3	0.000	K	$_1 = \frac{d_0}{E_1} \left[\frac{d_0}{d_0} \right]$	$\frac{+d_1^2}{-d_1^2} - \mu_1$	$K_2 =$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$	$\frac{i_2^2}{i_2^2} + \mu_2 \bigg] = K$	$C_3 = \frac{d_2}{E_2} \bigg[\frac{1}{d} \bigg]$	$\frac{2 d_3^2}{d_3^2 - d_2^2}$		<i>—</i>	31	\rightarrow				
FrictionC k1=	0.00051	1	К2 =	e, F2 0.096	673	.3 K3 =	0.0991	19	$1 = \frac{d_2}{E_1} \left[\frac{d_2}{d_2^2} \right]$	$\frac{+d_1^2}{-d_1^2} - \mu$	$K_2 =$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$	$\frac{d\hat{z}}{d\hat{z}} + \mu_2 \bigg] K$	$C_3 = \frac{d_2}{E_2} \left[\frac{1}{d} \right]$	$\frac{2d_3}{d_3^2 - d_2^2}$		<u> </u>	d1 d2	_>				
FrictionC k1 =	0.00051	1 1	K2 =	0.096	573 194	.3 K3 =	0.0991	19	$\frac{d_2}{E_1} = \frac{d_2}{E_1} \begin{bmatrix} \frac{d_2}{d_2} \\ \frac{d_3}{d_2} \end{bmatrix}$	$\frac{+d_1^2}{-d_1^2} - \mu_1$ + d_2^2	K ₂ =	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$ $\frac{d_3}{d_4^2 + c}$	$\frac{ds}{dz} + \mu_2 = K$	$C_3 = \frac{d_2}{E_2} \bigg[\frac{1}{d_3} \bigg]$	$\frac{2 d_3}{d_3^2 - d_2^2}$		~	d1 d2 d3	\rightarrow				
FrictionC k1= K4 =	0.00051	l I	K2 = K5 =	0.096 0.000	673 194	.3 K3 = K6 =	0.0991	19 17 A	$I_1 = \frac{d_2}{E_1} \left[\frac{d_3}{d_2} \right]$ $I_4 = \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$	$\frac{+d_1^2}{-d_1^2} - \mu_1$ $\frac{+d_2^2}{-d_2^2} - \mu_1$	$K_2 = K_5 = K_5 =$	$\frac{d_{3}}{E_{2}} \left[\frac{d_{3}^{2} + a}{d_{3}^{2} - a} \right]$ $\frac{d_{3}}{E_{3}} \left[\frac{d_{4}^{2} + a}{d_{4}^{2} - a} \right]$	$\frac{d\hat{s}}{d\hat{z}} + \mu_2 \left[K \\ \frac{d\hat{s}}{d\hat{s}} + \mu_3 \right] K$	$C_3 = \frac{d_2}{E_2} \left[\frac{1}{d} \right]$ $C_6 = \frac{d_3}{E_2} \left[\frac{1}{d} \right]$	$\frac{2 d_3}{d_3^2 - d_2^2}$ $\frac{2 d_2^2}{d_3^2 - d_2^2}$	<	<	d1 d2 d3 d4	\rightarrow	>			
FrictionC k1= K4=	0.00051	1 1	K2 = K5 =	0.096 0.00	573 194	.3 K3 = K6 =	0.0991	19 17 A	$f_1 = \frac{d_2}{E_1} \left[\frac{d_2}{d_2} \right]$ $f_4 = \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$	$\frac{+d_1^2}{-d_1^2} - \mu_1$ $\frac{+d_2^2}{-d_2^2} - \mu_1$	$K_2 = K_5 = K_5 =$	$\frac{d_{3}}{E_{2}} \left[\frac{d_{3}^{2} + a}{d_{3}^{2} - a} \right]$ $\frac{d_{3}}{E_{3}} \left[\frac{d_{4}^{2} + a}{d_{4}^{2} - a} \right]$	$\frac{d\hat{g}}{d\hat{g}} + \mu_2 \bigg] K$ $\frac{d\hat{g}}{d\hat{g}} + \mu_3 \bigg] K$	$X_3 = \frac{d_2}{E_2} \left[\frac{1}{d} \right]$ $X_6 = \frac{d_3}{E_2} \left[\frac{1}{d} \right]$	$\frac{2 d_{3}}{d_{3}^{2} - d_{2}^{2}}$ $\frac{-2 d_{2}^{2}}{d_{3}^{2} - d_{2}^{2}}$	<	~	d1 d2 d3 d4	\rightarrow	>			
FrictionC k1 = K4 = Po =	0.00051	I I I N/mm2	K2 = K5 =	0.096 0.00	573 194	.3 K3 = K6 =	0.0991	19 17 A	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_2} \right]$ $a = \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$	$\frac{+d_1^2}{-d_1^2} - \mu_1$ $\frac{+d_2^2}{-d_2^2} - \mu_1$	$K_2 =$ $K_5 =$	$\frac{d_{2}}{E_{2}} \left[\frac{d_{3}^{2} + c}{d_{3}^{2} - c} \right]$ $\frac{d_{3}}{E_{3}} \left[\frac{d_{4}^{2} + c}{d_{4}^{2} - c} \right]$	$\frac{d\hat{g}}{d\hat{g}} + \mu_2 \left[K \\ \frac{d\hat{g}}{d\hat{g}} + \mu_3 \right] K$	$K_3 = \frac{d_2}{E_2} \left[\frac{1}{a} \right]$ $K_6 = \frac{d_3}{E_2} \left[\frac{1}{a} \right]$	$\frac{2 d_{3}}{d_{3}^{2} - d_{2}^{2}}$ $\frac{-2 d_{2}^{2}}{d_{3}^{2} - d_{2}^{2}}$	<	<	d1 d2 d3 d4	\rightarrow	>			
FrictionC k1 = K4 = Po =	0.00051 0.09861 50.31	1 1 1 N/mm2	K2 = K5 =	0.096	573 194	.3 КЗ = К6 =	0.0991	19 17 A	$F_{a} = \frac{d_{2}}{E_{1}} \left[\frac{d_{2}}{d_{2}} \right]$ $F_{a} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{3}} \right]$ $F_{a} = f_{2}\pi d$	$\frac{+ d_1^2}{- d_2^2} - \mu$ $\frac{+ d_2^2}{- d_2^2} - \mu$ $_{3hP_0}$	$K_2 = K_5 = F_t = f_1 \pi a$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + c}{d_4^2 - c} \right]$ d_2hP_i	$\frac{d\hat{s}}{d\hat{s}} + \mu_2 = K$ $\frac{d\hat{s}}{d\hat{s}} + \mu_3 = K$	$K_3 = \frac{d_2}{E_2} \left[\frac{1}{a} K_6 = \frac{d_3}{E_2} \right]$	$\frac{2 d_{3}}{d_{3}^{2} - d_{2}^{2}}$ $-\frac{2 d_{2}^{2}}{d_{3}^{2} - d_{2}^{2}}$	<	<	d1 d2 d3 d4	\rightarrow	>			
FrictionC k1= K4 = Po =	0.00051 0.09861 50.31	I N/mm2	K2 = K5 =	e, F2 0.096 0.00	573 194	.3 K3 = K6 =	0.0991	19 17 A	$F_{4} = \frac{d_{2}}{E_{1}} \left[\frac{d_{2}}{d_{2}} \right]$ $F_{4} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{3}} \right]$ $F_{a} = f_{2}\pi d$	$\frac{+d_1^2}{-d_1^2} - \mu$ $\frac{+d_2^2}{-d_2^2} - \mu$ $_{3}hP_0$	$K_2 = K_5 = F_t = f_1 \pi c$	$\frac{d_{2}}{E_{2}} \left[\frac{d_{3}^{2} + c}{d_{3}^{2} - c} \right]$ $\frac{d_{3}}{E_{3}} \left[\frac{d_{4}^{2} + c}{d_{4}^{2} - c} \right]$ $d_{2}hP_{1}$	$\frac{d\hat{s}}{d\hat{s}} + \mu_2 = K$ $\frac{d\hat{s}}{d\hat{s}} + \mu_3 = K$	$K_3 = \frac{d_2}{E_2} \bigg[\frac{1}{a} \bigg]$ $K_6 = \frac{d_3}{E_2} \bigg[\frac{1}{a} \bigg]$	$\frac{2 d_5}{d_5^2 - d_2^2}$ $\frac{2 d_5^2}{d_5^2 - d_2^2}$	<		d1 d2 d3 d4		>			
FrictionC k1 = K4 = Po = Pi - Fo =	0.00051 0.09861 50.31 56.02 8009	1 1 1 N/mm2 31.3 N	K2 = K5 =	0.096 0.00	573 194 Kg	.3 K3 = K6 =	0.0991	19 17 A	$F_{a} = \frac{d_{a}}{E_{1}} \left[\frac{d_{a}}{d_{2}} \right]$ $F_{a} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{3}} \right]$ $F_{a} = f_{2}\pi d$	$\frac{+d_1^2}{-d_1^2} - \mu$ $\frac{+d_2^2}{-d_2^2} - \mu$ $_{3hP_0}$	$K_2 = K_5 = F_t = f_1 \pi t$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + c}{d_4^2 - c} \right]$ d_2hP_1	$\frac{d_{1}^{2}}{d_{2}^{2}} + \mu_{2} \end{bmatrix} K$ $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3} \end{bmatrix} K$	$\zeta_3 = \frac{d_2}{E_2} \left[\frac{1}{a} \zeta_3 + \frac{d_3}{E_2} \right]$	$\frac{2 d_{5}}{d_{5}^{2} - d_{2}^{2}}$ $\frac{2 d_{5}^{2}}{d_{5}^{2} - d_{2}^{2}}$	<	<	d1 d2 d3 d4		>			
FrictionC k1 = K4 = Po = Pi - Fo =	0.00051 0.09861 50.31 56.02 8009	1 1 1 N/mm2 91.3 N	K2 = K5 =	0.096 0.00	573 194 Kg	.3 K3= K6=	0.0991	19 17 A	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_2} \right]$ $F_4 = \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$ $F_6 = f_2 \pi d_3$	$\frac{+d_1^2}{-d_1^2} - \mu_1$ $\frac{+d_2^2}{-d_2^2} - \mu_2$ shPo	$\begin{bmatrix} K_2 \\ K_5 \end{bmatrix} = K_5 = F_t = f_1 \pi t$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + c}{d_4^2 - c} \right]$ d_2hP_1	$\frac{d\hat{s}}{d\hat{z}} + \mu_2 = K$ $\frac{d\hat{s}}{d\hat{z}} + \mu_3 = K$	$\zeta_3 = \frac{d_2}{E_2} \left[\frac{1}{a} \right]$ $\zeta_6 = \frac{d_3}{E_2} \left[\frac{1}{a} \right]$	$\frac{2 d_{\tilde{S}}}{d_{\tilde{S}}^2 - d_{\tilde{Z}}^2}$ $\frac{2 d_{\tilde{S}}^2}{d_{\tilde{S}}^2 - d_{\tilde{Z}}^2}$	<	<	d1 d2 d3 d4	\rightarrow	>			
FrictionC k1= K4= Po= Pi- Fo= Fi=	0.00051 0.09861 50.31 56.02 8009 8636	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	K2 = K5 =	e, F2 0.096 0.00 1172.58 H 8813.17 H	194 Kg	.3 K3= K6=	0.0991	7	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_2} \right]$ $a = \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$ $F_0 = f_2 \pi d_3$	$\frac{+d_1^2}{-d_1^2} - \mu_1$ $\frac{+d_2^2}{-d_2^2} - \mu_2$ $_{3hP_0}$	$\begin{bmatrix} K_2 \\ K_5 \end{bmatrix} = K_5 = F_t = f_1 \pi v$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + c}{d_4^2 - c} \right]$ $\frac{d_3}{d_4^2 - c}$ $\frac{d_3}{d_4^2 - c}$	$\left[\frac{d\hat{z}}{d\hat{z}} + \mu_2\right] = K$ $\left[\frac{d\hat{z}}{d\hat{z}} + \mu_3\right] = K$	$\zeta_3 = \frac{d_2}{E_2} \left[\frac{1}{a} \zeta_6 + \frac{d_3}{E_2} \right] $	$\frac{2 d_{\tilde{S}}}{d_{\tilde{S}}^2 - d_{\tilde{Z}}^2}$ $\frac{2 d_{\tilde{S}}^2}{d_{\tilde{S}}^2 - d_{\tilde{Z}}^2}$	<	<	d1 d2 d3 d4		>			
FrictionC k1= K4 = Po = Fo = Fi =	0.00051 0.09861 50.31 56.02 8009 8636	1 N/mm2 1 N/mm2 11.3 N	K2 = K5 =	0.036 0.00 172.58 H 8813.17 H	573 194 Kg	.3 K3 = K6 =	0.0991	7	$f_{4} = \frac{d_{2}}{E_{1}} \left[\frac{d_{2}}{d_{1}} \right]$ $f_{4} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{3}} \right]$ $F_{o} = f_{2} \pi d$	$\frac{+d_{2}^{2}}{-d_{1}^{2}} - \mu_{1}^{2}$ $\frac{+d_{2}^{2}}{-d_{2}^{2}} - \mu_{2}^{2}$ $_{3}hP_{3}$	$\begin{bmatrix} K_2 \\ K_3 \end{bmatrix} = K_5 = F_i = f_1 \pi i$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + c}{d_3^2 - c} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + c}{d_4^2 - c} \right]$ d_2hP_1	$\left[\frac{d\hat{z}}{d\hat{z}} + \mu_z\right] K$ $\left[\frac{d\hat{z}}{d\hat{z}} + \mu_3\right] K$	$\zeta_3 = \frac{d_2}{E_2} \left[\frac{1}{c} \right]$ $\zeta_6 = \frac{d_3}{E_2} \left[\frac{1}{c} \right]$	$\frac{2 d_{3}}{d_{3}^{2} - d_{2}^{2}}$ $\frac{2 d_{3}^{2}}{d_{3}^{2} - d_{2}^{2}}$ $\frac{2 d_{3}^{2}}{d_{3}^{2} - d_{2}^{2}}$	<	<	d1 d2 d3 d4		>			
FrictionC k1= K4 = Po = Pi- Fo = Fi =	0.00051 0.09861 50.31 56.02 8009 8636	1 N/mm2 11 N/mm2 31.3 N	K2 = K5 = = {	e, F2 0.036 0.00 172.58 H 8813.17 H	573 194 Kg	.3 K3 = K6 =	0.0991	7	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_2} \right]$ $F_4 = \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$ $F_6 = f_2 \pi d$	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu_{z}$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu_{z}$ $_{3}hP_{3}$	$K_2 = K_5 = K_5 = F_t = f_1 \pi t$	$\frac{d_2}{E_2} \left[\frac{d_3^2 + a}{d_3^2 - a} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + a}{d_4^2 - a} \right]$ $I_2 h P_1$	$\frac{d\hat{s}}{d\hat{z}} + \mu_2 \bigg] K$ $\frac{d\hat{s}}{d\hat{s}} + \mu_3 \bigg] K$	$c_3 = \frac{d_2}{E_2} \left[\frac{1}{c} c_3 + \frac{d_3}{E_2} \right] $ $c_6 = \frac{d_3}{E_2} \left[\frac{1}{c} c_3 + \frac{d_3}{E_2} \right] $	$\frac{2 d_{\tilde{S}}}{d_{\tilde{S}}^2 - d_{\tilde{S}}^2}$ $\frac{2 d_{\tilde{S}}^2}{d_{\tilde{S}}^2 - d_{\tilde{S}}^2}$	<		d1 d2 d3 d4		>			
FrictionC k1 = K4 = Po = Pi - Fo = Fi = Now C	0.00051 0.09861 50.31 56.02 8009 8636 heck wi	1 N/mm2 31.3 N 39.1 N hether F	K2 = K5 = Recom	0.096 0.00 0.00 0.00 0.00 0.00 0.00 0.00	573 194 Kg d Interfe	.3 K6 =	0.0991	3 7 511 tube	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_1} \right]$ $F_4 = \frac{d_3}{E_2} \left[\frac{d_3}{d_2} \right]$ $F_6 = f_2 \pi d$ and SS3	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu_{z}$	$K_2 = K_5 = F_i = f_1 \pi i$ is Feas	$\frac{d_2}{E_2} \left[\frac{d_3^2 + a}{d_3^2 - a} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + a}{d_4^2 - a} \right]$ $\frac{d_3}{d_4^2 - a} \left[\frac{d_4^2 + a}{d_4^2 - a} \right]$ ible for	$\frac{d\hat{s}}{d\hat{s}} + \mu_2 = K$ $\frac{d\hat{s}}{d\hat{s}} + \mu_3 = K$ Assembly	$c_3 = \frac{d_2}{E_2} \left[\frac{1}{a} \right]$ $c_6 = \frac{d_3}{E_2} \left[\frac{1}{a} \right]$ $y \text{ During}$	$\frac{2 d_{\tilde{S}}}{d_{\tilde{S}}^2 - d_{\tilde{Z}}^2}$ $\frac{2 d_{\tilde{S}}^2}{d_{\tilde{S}}^2 - d_{\tilde{Z}}^2}$ g Shrin	k Fittin		d1 d2 d3 d4		>			
FrictionC k1= K4 = Po = Pi - Fo = Fi = Now C	0.00051 0.09861 50.31 56.02 8009 8636 heck wi	1 N/mm2 91.3 N 39.1 N hether F	K2 = K5 = = {	0.096 0.096 0.00 0.00 0.00 0.00 0.00 0.0	kg d Interfe	.3 K3 = K6 =	0.0991	9 7 A 611 tube	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_1} \right]$ $f_4 = \frac{d_2}{E_2} \left[\frac{d_3}{d_2} \right]$ $F_6 = f_2 \pi d_3$ and SS3	$\frac{+d_1^2}{-d_2^2} - \mu$ $\frac{+d_2^2}{-d_2^2} - \mu$ $\frac{+d_2^2}{-d_2^2} - \mu$ $\frac{hP_0}{2}$ 04 Disc	$K_2 = K_3 = K_5 = F_1 = f_1 \pi \sigma$ is Feas	$\frac{d_2}{E_2} \left[\frac{d_2^2 + a}{d_2^2 - a} \right]$ $\frac{d_3}{E_3} \left[\frac{d_2^2 + a}{d_4^2 - a} \right]$ $\frac{d_3}{d_4^2 - a}$ ible for	$\frac{d\hat{s}}{d\hat{s}} + \mu_2 = K$ $\frac{d\hat{s}}{d\hat{s}} + \mu_3 = K$ Assembly	$c_3 = \frac{d_2}{E_2} \left[\frac{1}{d} \right]$ $c_6 = \frac{d_3}{E_2} \left[\frac{1}{d} \right]$ $y During$	$\frac{2}{d_{2}^{2}} - d_{2}^{2}$ $\frac{2}{d_{2}^{2}} - d_{2}^{2}$ $\frac{2}{d_{2}^{2}} - d_{2}^{2}$ $\frac{2}{d_{2}^{2}} - d_{2}^{2}$	k Fittin		d1 d2 d3 d4		>			
FrictionC k1 = k4 = Po = Pi - Fo = Fi = Now C	0.00051 0.09861 50.31 56.02 8009 8636 heck wi	1 N/mm2 31.3 N 39.1 N hether F	K2 = K5 = = Recom	172.58 H 8813.17 H mende	Kg d Interfe	.3 K3 = K6 = rence b	0.0991 0.0960 etween (SS shrink	3 7 611 tube age	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_1} \right]$ $a = \frac{d_2}{E_2} \left[\frac{d_2}{d_1} \right]$ $F_0 = f_2 \pi d_1$ and SS3 OD SS30	$\frac{+dz}{-dz} - \mu$ $\frac{+dz}{-dz} - \mu$ $\frac{+dz}{-dz} - \mu$ shPs 04 Disc	$K_2 = K_5 = F_i = f_2 \pi a$ is Feas Effecti	$\frac{d_2}{E_2} \left[\frac{d_2^2}{d_2^2} + \frac{d_2}{d_2} \right]$ $\frac{d_3}{d_2} \left[\frac{d_4^2}{d_4^2} + \frac{d_4^2}{d_4^2} + \frac{d_2hP_1}{d_4^2} \right]$ ible for	$\frac{1}{a_{2}^{2}} + \mu_{2} = K$ $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3} = K$ Assembly trai	$c_3 = \frac{d_2}{E_2} \left[\frac{d_3}{E_2} \right]$ $c_6 = \frac{d_3}{E_2} \left[\frac{d_3}{E_2} \right]$ $y During$	$\frac{2}{4\frac{5}{2}} = \frac{4}{2\frac{5}{2}}$ $\frac{2}{4\frac{5}{2}} = \frac{4}{2\frac{5}{2}}$ $\frac{2}{4\frac{5}{2}} = \frac{4}{2\frac{5}{2}}$ g Shrin	k Fittin		d1 d2 d3 d4		>			Image: Second
FrietionC k1 = K4 = Po = Fo = Fi = Now C Min ID 0	0.00051 0.09861 50.31 56.02 8009 8636 heck wl	N/mm2 N/mm2 91.3 N 39.1 N hether F	K2 = K5 = = Recom	172.58 H mende al [Kg d Interfe Max OD SS	.3 K3 = K6 = rence b 3304 nk	0.0991 0.0960 etween (SS shrink upto 80K	5 7 5 11 tube age	$= \frac{d_2}{E_1} \left[\frac{d_3}{d_1} \right]$ $= \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$ $F_3 = f_2 \pi d$ and SS3 OD SS30 after Shri	$\frac{+d_z^2}{-d_z^2} - \mu$ $\frac{+d_z^2}{-d_z^2} - \mu$ ghP_g 04 Disc 4 nk	$K_2 = K_5 = F_1 = f_2 \pi a$ is Feas Effecti Cleara	$\frac{d_2}{B_2} \left[\frac{d_2^2 + a}{d_3^2 - a} \right]$ $\frac{d_3}{d_3^2} \left[\frac{d_1^2 + a}{d_4^2 - a} \right]$ $\frac{d_3}{d_4^2 - a}$ $\frac{d_3}{d_4^2 - a}$ $\frac{d_4}{d_4^2 -$	$\frac{d\hat{s}}{d\hat{s}} + \mu_2 = K$ $\frac{d\hat{s}}{d\hat{s}} + \mu_3 = K$ Assembly tral ssembly	$c_{s} = \frac{d_{2}}{E_{2}} \left[\frac{1}{e} \right]$ $c_{s} = \frac{d_{3}}{E_{2}} \left[\frac{1}{e} \right]$ $y During$	2 45 45 - 42 2 45 15 - 42 15 - 42	k Fittin		d1 d2 d3 d4		>			
FrietionC k1= K4= Po= Pi- Fo= Fi= Now C Min ID C	0.00051 0.09861 50.31 56.02 8009 8636 heck wl	1 N/mm2 1 N/mm2 11.3 N 33.1 N hether I Max	K2 = K5 = = Recom	172.58 H 8813.17 H mender al f	Kg d Interfe Max OD St before Shri	.3 K3 = K6 = rence bo	0.0991 0.0960 etween (SS shrink upto 80K	9 7 A	$\frac{d_2}{d_1} = \frac{d_2}{d_1} \begin{bmatrix} \frac{d_2}{d_2} \\ \frac{d_3}{d_2} \end{bmatrix}$ $F_a = f_2 \pi d$ and SS3 OD SS30 after Shri mm	$\frac{+d_z^2}{-d_z^2} - \mu$ $\frac{+d_z^2}{-d_z^2} - \mu$ shPs 04 Disc 4 nk.	K ₂ = K ₅ = Λ ₂ πι is Feas Effecti Cleara mm	$\frac{d_2}{E_2} \left[\frac{d_2^2 + a}{d_3^2 - a} \right]$ $\frac{d_3}{E_3} \left[\frac{d_4^2 + a}{d_4^2 - a} \right]$ $\frac{d_3}{d_4^2 - a}$ $\frac{d_4}{d_4^2 - a$	$\frac{12}{d_2^2} + \mu_2 = K$ $\frac{d_3^2}{d_3^2} + \mu_3 = K$ Assembly trai ssembly	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{2}} + \frac{d_{3}}{E_{2}} \right] \left[\frac{d_{3}}{d_{2}} +$	2 45 3 - 42 2 45 2 45 45 - 42 9 9 9 9 9 9 9 9 9 9 9 9 9	k Fittin		d1 d2 d3 d4		>			
FrietionC k1= K4 = Po = Po = Fo = Fi = Now C Min ID C mm	0.00051 0.09861 50.31 56.02 8009 8636 heck wl	1 N/mm2 2 N/mm2 31.3 N 33.1 N hether F Max Interf	K2 = K5 = Recom Diametri erence m 457	172.58 H mende	Kg d Interfe Max OD SS before Shri mm 86 557		0.0991 0.0960 SS shrink upto 80K mm	9 7 A	$\frac{d_2}{z_1} \begin{bmatrix} \frac{d_2}{d_2} \\ \frac{d_3}{d_2} \end{bmatrix}$ $\frac{d_3}{z_2} \begin{bmatrix} \frac{d_3}{d_3} \\ \frac{d_3}{d_3} \end{bmatrix}$ $\frac{d_3}{z_2} = f_2 \pi d$ and SS3 OD SS30 after Shri mm as 332	$\frac{+\frac{d_z^2}{-d_z^2} - \mu}{\frac{+\frac{d_z^2}{-d_z^2} - \mu}{-\frac{d_z^2}{-d_z^2} - \mu}}$ 04 Disc 4 nk	$K_{2} = K_{5} = f_{1}\pi a$ $is Feas$ Effecti Cleara mm	$\frac{d_2}{E_2} \left[\frac{d_2^2 + a}{d_3^2 - a} \right]$ $\frac{d_3}{E_2} \left[\frac{d_1^2 + a}{d_2^2 - a} \right]$ $\frac{d_3}{d_2} \left[\frac{d_1^2 + a}{d_2^2 - a} \right]$ $\frac{d_2 h P_1}{h}$ $\frac{h P_1}{h}$ $\frac{h P_1}{h}$ $\frac{h P_2}{h}$ $\frac{h P_1}{h}$ $\frac{h P_2}{h}$ $\frac{h P_1}{h}$ $\frac{h P_2}{h}$ $h $	$\frac{i\frac{\pi}{2}}{d2} + \mu_2$ K $\frac{d\hat{s}}{d2} + \mu_3$ K Assembly tral ssembly	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{E_{2}} \right]$ $c_{8} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{E_{2}} \right]$ $y During$	2 45 13 - 42 2 42 13 - 42 14 - 42 15 - 42	k Fittin		d1 d2 d3 d4		>			
FrietionC k1= K4 = Po = Po = Po = Fo = Fi = Now C Min ID C mm 86	0.00051 0.09861 50.31 56.02 8009 8636 heck wi	N/mm2 N/mm2	K2 = K5 = = Recom Diametr erence m .457	172.58 H 8813.17 H mende	Kg d Interfe Max OD St before Shri mm 86.557	3 K3 = K6 = rence bo	0.0991 0.0960 SS shrink upto 80K mm 0.225	9 7 A G11 tube	$t = \frac{d_2}{E_1} \left[\frac{d_2}{d_2} \right]$ $t = \frac{d_3}{E_2} \left[\frac{d_3}{d_3} \right]$ $F_a = f_2 \pi d$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_z^2}{-d_z^2} - \mu$ $\frac{+d_z^2}{-d_z^2} - \mu$ $_{3}nP_3$ 04 Disc 4 nk	$K_2 = K_5 $	$\frac{d_2}{B_2} \left[\frac{d_2^2 + a}{d_3^2 - a} \right]$ $\frac{d_3}{B_2} \left[\frac{d_2^2 + a}{d_4^2 - a} \right]$ $\frac{d_3}{B_2} \left[\frac{d_3}{B_2} \right$	$\frac{d\hat{z}}{d\hat{z}} + \mu_z$ K $\frac{d\hat{z}}{d\hat{z}} + \mu_3$ K Assembly tral	$c_3 = \frac{d_2}{E_2} \left[\frac{d_3}{E_2} \right]$ $c_4 = \frac{d_3}{E_2} \left[\frac{d_3}{E_2} \right]$	2 45 13 - 42 14 - 42 1	k Fittin		d1 d2 d3 d4		>			
FrietionC k1= K4 = Po = Pi - Fo = Fi = Now C Min ID C mm 86	0.00051 0.09981 50.31 56.02 8009 8636 heck wi	N/mm2 N/mm2 31.3 N 33.1 N hether f Max Interf 0	K2 = K5 = Biametr erence m .457	172.58 H 8813.17 H mende	Kg d Interfe Max OD St before Shri mm 86.557	3 K3 = K6 = S304 nk	0.0991 0.0960 2tween (SS shrink upto 80K mm 0.225	is K	$a = \frac{d_2}{E_2} \left[\frac{d_2}{d_2} \right]$ $a = \frac{d_2}{E_2} \left[\frac{d_2}{d_2} \right]$ $F_0 = f_2 \pi d$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_z^2}{-d_z^2} - \mu$ $\frac{+d_z^2}{-d_z^2} - \mu$ shPs 04 Disc 4	$K_{2} = K_{3} = K_{4} = K_{5} = K_{5$	$\frac{d_2}{d_3} \left[\frac{d_2^2}{d_3^2} + \frac{d_3}{d_3^2} + \frac{d_3^2}{d_3^2} + \frac{d_3^2}{d_4^2} + \frac{d_4^2}{d_4^2} + \frac{d_4^2}{d_4^2}$	$\frac{d_2^2}{d_3^2} + \mu_3$ K Assembly tral	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{E_{2}} \right]$ $c_{8} = \frac{d_{3}}{E_{2}} \left[\frac{1}{E_{2}} \right]$ $y During$	2 d 5 13 - d 2 2 d 5 13 - d 2 13	k Fittin	2 <i>P</i> ₁ <i>d</i> ² ₂	d1 d2 d3 d4		>			
FrietionC K1 = K4 = Po = Fo = Fi = Now C Min ID C mm 86 Calcula	0.00051 0.09561 50.31 55.02 8009 8636 heck wi 311	N/mm2 N/mm2 91.3 N 39.1 N hether I Interf mi 0 ssses in	K2 = K5 = E Recom Diamete erence m 457	172.58 H 8813.17 H mende al f t	Kg d Interfe Max OD St before Shri mm 86.557 of Disc, T	3 K3 = K6 = rence bo	0.0991 0.0960 etween (SS shrink upto 80K mm 0.225	is 7 A G11 tube	$f_{\pm} = \frac{d_{\pm}}{B_{\pm}} \left[\frac{d_{\pm}}{d_{\pm}} \right]$ $f_{\pm} = \frac{d_{\pm}}{B_{\pm}} \left[\frac{d_{\pm}}{d_{\pm}} \right]$ $F_{a} = f_{\pm}\pi d$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ shPs 04 Disc 4 nk	$K_2 = K_5 = K_5 = f_2 \pi a$ is Feas Effecti Cleara mm -0.2	$\frac{d_2}{d_3} \left[\frac{d_2^2}{d_3^2} + \frac{d_2}{d_3^2} \right]$ $\frac{d_2}{d_3^2} \left[\frac{d_2^2}{d_4^2} + \frac{d_2^2}{d_4^2} + \frac{d_2^2}{d_4^2} \right]$ ible for ic Diametric for A 32	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{3}$ K $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3}$ K Assembly tral ssembly $\sigma_{rd_{1}D(cc)}$	$c_3 = \frac{d_2}{E_2} \left[\frac{1}{d_2} \right]$ $c_4 = \frac{d_3}{E_2} \left[\frac{1}{d_2} \right]$ $y \text{ During}$ $= 0$	² d ₂ d ₁ ² - d ₂ ² d ₁ ² - d ₂ ² d ₂ ⁴ - d ₂ ² g Shrin	k Fittin	$\frac{2P_i d_2^2}{d_z^2 - d_z^2}$	d1 d2 d3 d4		>			
FrietionC k1 = k4 = Po = Po = Fi = Now C Min ID C mm 86 Calcula	0.00051 0.09861 50.31 56.02 8009 8636 heck with a11	N/mm2 N/mm2 31.3 N 39.1 N hether F Max Interf mi 0	K2 = K5 = E Recom Diametu erence m .457	1172.58 H mende	×g d Interfe Max OD St before Shri mm 86.557	3 K3 = K6 = 3304 nk	0.0991 0.0960 SS shrink upto 80K mm 0.225	is 7 A 311 tube	$\frac{d_2}{d_1} = \frac{d_2}{d_1} \begin{bmatrix} \frac{d_2}{d_2} \\ \frac{d_1}{d_2} \end{bmatrix}$ $\frac{d_2}{d_2} = \frac{d_2}{d_2} \begin{bmatrix} \frac{d_1}{d_2} \\ \frac{d_2}{d_1} \end{bmatrix}$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_z^2}{-d_z^2} - \mu$ $\frac{+d_z^2}{-d_z^2} - \mu$ shPs 04 Disc 4	K ₂ = k ₅ = k ₆ = f ₁ π is Feas Effecti Cleara mm -0.2	$\frac{d_2}{d_3} \left[\frac{d_2^2}{d_3^2} + \frac{c}{d_3^2} - \frac{c}{d_3^2} \right]$ $\frac{d_3}{d_3} \left[\frac{d_2^2}{d_4^2} + \frac{c}{d_4^2} - \frac{c}{d_4^2} + \frac{c}{d_4^2} - \frac{c}{d_4^2} \right]$ ible for ve Diamenoe for A 32	$\frac{d}{d} = \frac{d}{d} + \mu_3$ K Assembly tral ssembly	$c_3 = \frac{d_2}{E_2} \left[\frac{1}{d_2} \right]$ $c_4 = \frac{d_3}{E_2} \left[\frac{1}{d_2} \right]$ $y \text{ During}$ $= 0$	$\sigma_{ed_1}^{2 d_2}$	k Fittin	$\frac{2P_1d_2^2}{d_2^2 - d_1^2}$	d1 d2 d3 d4		>			
FrietionC k1 = K4 = Po = Fo = Fo = Fi = Now C Min ID C mm 86 Calcula	0.00051 0.09861 50.31 56.02 8009 8636 heck with att 1 1	N/mm2 N/mm2 81.3 N 39.1 N hether F Max Interf mi 0 csses in 1	K2 = K5 = = Recom Diameto erence m .457	e, f2 0.096 0.00 1172.58 8813.17 mende al [t	Kg d Interfe Max OD St before Shri mm 86.557	3 K3 = K6 = rence bo 3304 nk	0.0991 0.0960 Etween (SS shrink upto 80K mm 0.225	3 7 7 611 tube	and SS3 $and SS3$ $CD SS30$ $after Shrimmer 86.332$	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{h}{2}hP_{z}$ 04 Disc	$K_2 = K_3 = K_4$ $K_5 = K_5$ $K_6 = K_5$ is Feas Effecti Cleara mm -0.2	$\frac{d_2}{d_3} \left[\frac{d_2}{d_3} + \frac{1}{2} + \frac{1}{2} \right]$ $\frac{d_2}{d_3} \left[\frac{d_2}{d_4} + \frac{1}{2} + \frac{1}{2} \right]$ $\frac{d_2}{d_4} \left[\frac{d_2}{d_4} + \frac{1}{2} + \frac{1}{2} + \frac{1}{2} \right]$ $\frac{d_2}{d_4} \left[\frac{d_2}{d_4} + \frac{1}{2} + \frac{1}{2} + \frac{1}{2} \right]$ $\frac{d_2}{d_4} \left[\frac{d_2}{d_4} + \frac{1}{2} + \frac{1}{2} + \frac{1}{2} \right]$ $\frac{d_2}{d_4} \left[\frac{d_2}{d_4} + \frac{1}{2} + \frac{1}{2} + \frac{1}{2} + \frac{1}{2} \right]$ $\frac{d_2}{d_4} \left[\frac{d_2}{d_4} + \frac{1}{2} + 1$	$\frac{dz}{dz} + \mu_3$ K $\frac{dz}{dz} + \mu_3$ K Assembly tral ssembly $\sigma_{r,d_1,D(uc)}$	$c_3 = \frac{d_2}{E_2} \left[\frac{d_3}{E_1} \right]$ $c_4 = \frac{d_3}{E_2} \left[\frac{d_3}{E_2} \right]$ $y \text{ During}$ $= 0$ $= -P_4$	σ_{cd_1}	k Fittin	$\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$	d1 d2 d3 d4		>			
FrietionC k1 = k4 = Po = Po = Po = Fi = Now C Min ID C mm 86 Calcula	0.00051 0.03561 50.31 8009 8636 heck wl 311	N/mm2 N/mm2 31.3 N 39.1 N hether f Max Interf 0 0 sses in 304	K2 = K5 = Recom Diametri erence m .457	172.58 H mende al f terial c	×g d Interfe Max OD SS before Shri mm 86.557	3 K3 = K6 = S304 nk	0.0991 0.0960 etween (SS shrink upto 805 mm 0.225 1 Ring	3 7 8 311 tube	$\frac{d_2}{d_1} = \frac{d_2}{d_2} \left[\frac{d_2}{d_2} \right]$ $\frac{d_3}{d_2} = \frac{d_4}{d_2} \left[\frac{d_4}{d_3} \right]$ and SS3 oD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $s^{3}AP_{S}$ O4 Disc 4 nk	$K_2 = K_3 = K_5 $	$\frac{d_2}{E_2} \left[\frac{d_2}{d_1} + c \\ \frac{d_2}{d_2} + c \\ \frac{d_3}{d_4} + c \\ \frac{d_4}{E_3} \left[\frac{d_4}{d_4} + c \\ \frac{d_4}{d_4} + c $	$\frac{d_{12}^{22}}{d_{13}^{2} + \mu_{2}} = K$ $\frac{d_{12}^{22} + \mu_{3}}{d_{13}^{2} + \mu_{3}} = K$ Assembly $tral ssembly \sigma_{r, d_{1}, Ducc} \sigma_{r, d_{2}, Ducc}$	$c_3 = \frac{d_2}{E_2} \left[\frac{d_3}{d_2} \right]$ $c_6 = \frac{d_3}{E_2} \left[\frac{d_3}{d_2} \right]$ $y \text{ During}$ $= 0$ $= -P_6$	$\frac{2 \ d_{\Sigma}}{g \ d_{\Sigma}} = \frac{2 \ d_{\Sigma}}{d_{\Sigma}}$ $\frac{2 \ d_{\Sigma}}{d_{\Sigma}} = -d_{\Sigma}^{2}$ $g \ Shrin$ $\sigma_{c \ d_{\Sigma} l}$	k Fittin	$\frac{2P_{i}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}-d_{1}^{2})}{d_{2}^{2}-d_{1}^{2}}$	d1 d2 d3 d4		>			
FrietionC k1= K4= Po= Fo= Fi= Now C Min ID C mm 86 Calcula Inner E	0.00051 0.09861 50.31 50.31 50.31 8009 8636 heck with attraction of the second	1 N/mm2 N/mm2 31.3 N hether I Max Max 0 ssess in 304 =	K2 = K5 = Recom Diametri erence m .457 the Ma	172.58 H 8813.17 H mende al f tterial c	Kg d Interfe Max OD St before Shri mm 86.557 of Disc, T	3 K3 = K6 = rence bo 3304 nk ube and	0.0991 0.0960 2000 2000 2000 2000 2000 2000 2000	is N/mm2	$I = \frac{d_2}{E_1} \left[\frac{d_2}{d_2} \right]$ $I = \frac{d_2}{E_2} \left[\frac{d_2}{d_$	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ ghP_{3} 04 Disc 4 nk	$K_2 = K_3 = K_5 = A\pi a$ is Feas Effecti Cleara mm -0.2	$\frac{d_2}{d_2} \left[\frac{d_2}{d_1} + \alpha \right]$ $\frac{d_2}{d_2} \left[\frac{d_2}{d_1} + \alpha \right]$ $\frac{d_2}{d_2} \left[\frac{d_2}{d_2} +$	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{2} \end{bmatrix} K$ $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3} \end{bmatrix} K$ Assembly tral ssembly $\sigma_{r,d_{1},Disc}$ $\sigma_{r,d_{2},Disc}$	$c_3 = \frac{d_2}{E_2} \left[\frac{d_3}{E_1} \right]$ $c_4 = \frac{d_3}{E_2} \left[\frac{d_3}{E_2} \right]$ $y \text{ During}$ $= 0$ $= -P_i$	$\frac{2 \ d_{z}}{d_{z}} - d_{z}$ $\frac{2 \ d_{z}}{d_{z}} - d_{z}$ $g \ Shrin $ $\sigma_{c \ d_{2} A}$	k Fitting plac = - plac = -	$\frac{2P_1d_2^2}{d_2^2 - d_1^2}$ $\frac{P_1(d_2^2 + c}{d_2^2 - d}$	d1 d2 d3 d4		>			
FrietionC k1= k4 = Po = Po = Fi = Now C Min ID C mm 86 Calcula	0.00051 0.09561 50.31 50.32 8009 8636 heck wl 311 1 1 1 1 1 1 1 1 1 1 1 1	N/mm2 N/mm2 31.3 N 39.1 N hether f Max Interf 0 0 sses in 1 304	K2 = K5 = Recom Diametr erence m. 457 the Ma	e, 12 0.096 0.00 1172.58 H 8813.17 H mende sal f t t t t t t t t t t t t t t t t t t t	×g d Interfe Max OD S3 before Shri mm 86.557 of Disc, T	3 K3 = K6 = 3304 nk rRd2 =	0.0991 0.0960 etween (SS shrink upto 80K mm 0.225 1 Ring -56.02	is N/mm2	$a = \frac{d_{E_1}}{E_2} \begin{bmatrix} d_{E_1} \\ d_{E_2} \end{bmatrix}$ $a = \frac{d_{E_1}}{E_2} \begin{bmatrix} d_{E_2} \\ d_{E_2} \end{bmatrix}$ $a = f_{E_1} \pi d$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $s_{AP_{B}}$ 04 Disc 4 nk	$K_2 = K_5 $	$\frac{d_2}{d_3} = \frac{d_3}{d_4} + \frac{d_1}{d_4} + $	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{3}$ K $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3}$ K Assembly tral ssembly $\sigma_{r,d_{1},Disc}$ $\sigma_{r,d_{2},Disc}$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{2}} \right]$ $c_{5} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{2}} \right]$ $y During$ $= 0$ $= -P_{i}$	$\frac{2 \cdot d_{z}}{q_{z}^{2} - d_{z}^{2}}$ $\frac{2 \cdot d_{z}^{2}}{q_{z}^{2} - d_{z}^{2}}$ $g \text{ Shrin}$ $\sigma_{c \cdot d_{2} L}$ $\sigma_{c \cdot d_{2} L}$	k Fittin	$\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}+d_{1}^{2})}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}+d_{1}^{2})}{d_{2}^{2}-d_{1}^{2}}$	d1 d2 d3 d4 d4 d4 d4					
FrietionC K1 = K4 = Po = Fo = Fi = Now C Min ID C mm 86 Calcula Inner E	0.00051 0.09861 50.31 56.02 8003 8636 heck with attraction of the strength of the stren	1 N/mm2 31.3 N 33.1 N hether f Max Interf mi 0 3304 = = -13	K2 = K5 = Diametu erence m. .457 the Ma 0 N/ 9.32 N/	e, 12 0.096 0.00 172.58 8813.17 mende al [terial (mm2 mm2	Kg d Interfe Max OD St before Shri mm 88.557 of Disc, T	3 K3 = K6 = rence b 3304 nk ube and rRd2 = rC,d2 =	0.0991 0.0960 2tween (SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30	s A	$a = \frac{d_2}{E_2} \left[\frac{d_2}{d_2} \right]$ $a = \frac{d_2}{E_2} \left[\frac{d_2}{d_2} \right]$ $F_0 = f_2 \pi d$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{3hP_{S}}{04 \text{ Disc}}$ 64 Disc 4 nk	$K_2 = K_5 = K_5 = K_5$ $K_5 = f_0 \pi a$ is Feas Effecti Cleara mm -0.2	$\frac{d_2}{B_2} \left[\frac{d_2}{d_1} + c \\ B_2 \left[\frac{d_2}{d_2} + c \\ B_3 \left[\frac{d_2}{d_2} + c \\ A_2 + B_3 \right] \right]$	$\frac{d_{2}^{2}}{\sigma_{r}} + \mu_{2} = K$ Assembly trai ssembly $\sigma_{r} d_{1} Disc$ $\sigma_{r} d_{2} Disc^{1}$	$c_3 = \frac{d_2}{E_2} \left[\frac{d_3}{E_2} \right]$ $c_4 = \frac{d_3}{E_2} \left[\frac{d_3}{E_2} \right]$ $y \text{ During}$ $= 0$ $= -P_4$	$\frac{2 \ d_{z}}{ z_{z}^{2} - d_{z}^{2} }$ $\frac{2 \ d_{z}^{2}}{ z_{z}^{2} - d_{z}^{2} }$ $g \ Shrin$ $\sigma_{c \ d_{2}l}$ $\sigma_{c \ d_{2}l}$	k Fittin Disc = - Disc = - Disc = -	$\frac{2P_{i}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}+d_{2}^{2})}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}+d_{2}^{2})}{d_{2}^{2}-d_{1}^{2}}$	d1 d2 d3 d4 d4 d4 d4 d4 d4		>			
FrietionC K1 = K4 = Po = Po = Fi = Now C Min ID C mm 86 Calcula Inner E	0.00051 0.09961 50.31 50.31 8009 8636 heck wi 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 N/mm2 31.3 N 39.1 N hether F Max Interf min 0 ssess in 1 304 = = -13	K2 = K5 = Diametri erence m. 457 the Ma 9.32 N/	e, f2 0.096 0.00 1172.58 H 8813.17 H 8813.17 H al f t t t t t t t t t t t t t t t t t t t	×g d Interfe Max OD SS before Shri mm 86.557 of Disc, T	<pre>3 K3 = K6 = K6 = S304 nk vRd2 = vC,d2 =</pre>	0.0991 0.0960 2tween (SS shrink upto 80k mm 0.225 1 Ring -56.02 -83.30	s N/mm2	$a = \frac{d_2}{E_1} \left[\frac{d_2}{d_1} \right]$ $a = \frac{d_3}{E_2} \left[\frac{d_3}{d_2} \right]$ $a = f_2 \pi a$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ synPg 04 Disc 4 nk	K2 = K5 =	$\frac{d_2}{d_2} = \frac{d_2}{d_3} + \frac{d_1}{d_4} + $	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{3} = K$ $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3} = K$ Assembly $\sigma_{rd_{2},011}$ $\sigma_{rd_{2},011}$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{6} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $y \text{ During}$ $= 0$ $= -P_{4}$ $= -P_{4}$	$\frac{2}{3} = -d\frac{2}{3}$ $\frac{2}{3} = -d\frac{2}{3}$ $\frac{2}{3} = -d\frac{2}{3}$ $g \text{ Shrin}$ $\sigma_{c,d_{2},4}$ $\sigma_{c,d_{2},4}$	k Fitting $p_{isc} = -$ $p_{isc} = -$ $p_{isc} = -$	$\frac{2P_1d_2^2}{d_2^2 - d_1^2}$ $\frac{1}{d_2^2 - d_1^2}$ $\frac{P_1(d_2^2 + d_2^2)}{d_2^2 - d_2^2}$ $\frac{P_2(d_2^2 + d_2^2)}{d_2^2 - d_2^2}$	$\frac{d1}{d2} \\ \frac{d2}{d3} \\ \frac{d4}{d4} \\ \frac{d1}{2} \\ \frac{d1}{2} \\ \frac{d2}{2} \\ \frac{d2}{d4} \\ \frac{d2}{d$					
FrietionC K1 = K4 = Po = Po = Fi = Now C Min ID C mm 86 Calcula Inner C	0.00051 0.03861 50.31 50.31 8009 8636 heck wl att 505c SS oF,d1 oC,d1 311	1 N/mm2 1 N/mm2 11.3 N 11.3 N 11.3 N 11.3 N 11.3 N 11.3 N 11.5	K2 = K5 = Diametu erence M57 the Ma 9.32 N/	e, 12 0.096 0.00 1172.58 8813.17 8813.17 8813.17 10 mmande	<pre>s73 s73 s73 s73 s73 s73 s73 s73 s73 s73</pre>	3 K3 = K6 = rence b 3304 nk ube and rRd2 = rC,d2 =	0.0991 0.0960 SS shrink upto 80K mm 0.225 I Ring -56.02 -83.30	s 7 A 311 tube age N/mm2 N/mm2	$\frac{d_2}{d_1} = \frac{d_2}{d_1} \begin{bmatrix} \frac{d_2}{d_2} \\ \frac{d_1}{d_2} \end{bmatrix}$ $\frac{d_2}{d_2} = \frac{d_2}{d_2} \begin{bmatrix} \frac{d_1}{d_2} \\ \frac{d_2}{d_1} \end{bmatrix}$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ s^{nPs} 04 Disc 4 nk	$K_2 = K_5 = K_5 = K_5$ $K_5 = f_0 \pi a$ is Feas Effecti Cleara mm -0.2	$\frac{d_2}{E_2} \left(\frac{d_2}{d_3} + c \\ \frac{d_3}{d_4} + c \\ \frac{d_4}{E_3} + c \\ \frac{d_4}{d_4} + \frac{d_4}{E_3} + c \\ \frac{d_4}{d_4} + c \\$	$\frac{d_{2}^{2}}{d_{3}^{2} + \mu_{2}} = K$ $\frac{d_{3}^{2}}{d_{3}^{2} + \mu_{3}} = K$ Assembly tral ssembly $\sigma_{r, d_{2}, 011}$	$c_3 = \frac{d_2}{E_2} \left[\frac{d_3}{E_2} \right]$ $c_4 = \frac{d_3}{E_2} \left[\frac{d_3}{E_2} \right]$ $y \text{ During}$ $= 0$ $= -P_i$ $= -P_i$	$\frac{2 \ d_{z}}{d_{z}} = \frac{d_{z}}{d_{z}}$ $\frac{2 \ d_{z}}{d_{z}}$ $\frac{2 \ d_{z}}{d_{z}}$ $g \ Shrin$ $\sigma_{c \ d_{2}}$ $\sigma_{c \ d_{2}}$	k Fittin $p_{isc} = -$ $p_{isc} = -$ $p_{isc} = -$	$\frac{2P_{i}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}+d_{2}^{2})}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}+d_{2}^{2})}{d_{2}^{2}-d_{1}^{2}}$			>			
FrietionC K1= K4= Po= Fo= Fo= Fo= Min ID 0 Min ID 0 Min ID 0 Min ID 0 Min ID 0 Min ID 0	0.00061 0.09661 50.31 50.31 50.32 8009 8636 heck with and 1 1 1 1 1 1 1 1 1 1 1 1 1	1 N/mm2 N/mm2 31.3 N 39.1 N hether i Max Interf 0 304 = = -13	K2 = K5 = Recom Diametri erence m .457 the Ma 9.32 N/	al r mm2 mm2	Kg d Interfe Max OD St before Shri mm 86.557 of Disc, T	-C.d2 =	0.0991 0.0960 2tween (SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30	s A A A A A A A A A A A A A A A A A A A	and SS3 $DD SS30 after Shrimmer 86.332$	$\frac{+d_s^2}{-d_s^2} - \mu$ $\frac{+d_s^2}{-d_s^2} - \mu$ $\frac{3hP_s}{04 \text{ Disc}}$ 04 Disc	K2 = K5 =	$\frac{d_2}{d_2} = \frac{d_2}{d_2} + c$ $\frac{d_3}{d_2} = c$ $\frac{d_4}{d_4} + c$ $\frac{d_3}{d_4} = \frac{d_4}{d_4} + c$ $\frac{d_4}{d_4} + c$	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{3} = K$ $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3} = K$ Assembly $Tral$ ssembly $\sigma_{rd_{2}} Dusc$ $\sigma_{rd_{2}} Dusc$ $\sigma_{rd_{2}} Dusc$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{4} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $y \text{ During}$ $= 0$ $= -P_{4}$ $= -P_{4}$ $= -P_{4}$	$\frac{2}{3} = dz$ $\frac{2}{3} = -dz$ $\frac{2}{3} = -dz$ $\frac{2}{3} = -dz$ $\sigma_{c} dz$ $\sigma_{c} dz$ $\sigma_{c} dz$	k Fittin	$\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}+a)}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}+a)}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}-a)}{d_{2}^{2}-a}$						
FrietionC k1 = K4 = Po = Po = Fi = Now C Min ID C mm 86 Calcula Inner E	0.00051 0.09561 50.31 50.31 8009 8636 heck wl att att orR,d1: orR,d1: art art art,d2	N/mm2 N/mm2 31.3 N 39.1 N hether f Max Interf 0 0 sses in 304 = = -13 = -5	K2 = K5 = E Recom Diamete erence m .457 the Ma 9.32 N/ 6.02 N/	e, f2 0.096 0.00 1172.58 8813.17 8813.17 8813.17 mende al f t t t t t t t t t t t t t t t t t t t	<pre>s73 s73 s73 s73 s74 s74 s75 s75 s75 s75 s75 s75 s75 s75 s75 s75</pre>	3 K3 = K6 = 3304 nk ube and rRd2 = rC,d2 = rRd3 =	0.0991 0.0960 2tween (SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30 -50.31	3 7 8 311 tube age N/mm2 N/mm2	$\frac{d_2}{d_1} = \frac{d_2}{d_1} \left[\frac{d_2}{d_2} \right]$ $\frac{d_2}{d_2} = \frac{d_2}{d_2} \left[\frac{d_2}{d_1} \right]$ and SS3 oD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $a_{z}^{n}AP_{s}$ O4 Disc	$K_2 = K_3 = K_4 = K_5$ $K_5 = K_5 = K_5$ $K_5 = K_5$	$\frac{d_2}{E_2} \left(\frac{d_2}{d_1} + c \\ \frac{d_2}{d_2} + c \\ \frac{d_3}{d_4} + \frac{d_4}{E_3} \right) \left(\frac{d_4}{d_4} + c \\ \frac{d_4}{d_4} + \frac{d_4}{d_4} + c \\ d$	$\frac{d_{12}^{2}}{\sigma_{12}^{2} + \mu_{2}} = K$ $\frac{d_{12}^{2} + \mu_{3}}{d_{3}^{2} + \mu_{3}} = K$ Assembly ral ssembly $\sigma_{r} d_{1} Disc$ $\sigma_{r} d_{2} Disc$ $\sigma_{r} d_{2} Cis$ $\sigma_{r} d_{3} Cis$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{5} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{2}} \right]$ $y \text{ During}$ $= 0$ $= -P_{i}$ $= -P_{i}$ $= -P_{o}$	$\frac{2 \ d_2}{q_1^2} - \frac{d_2}{q_2^2}$ $\frac{2 \ d_2}{q_2^2}$ $g \ Shrin $ $\sigma_{c \ d_2 i}$ $\sigma_{c \ d_2 i}$ $\sigma_{c \ d_2 i}$	k Fitting $p_{isc} = -$ $p_{isc} $	$\frac{2P_1d_2^2}{d_2^2 - d_1^2}$ $\frac{2P_1(d_2^2 - d_1^2)}{d_2^2 - d_1^2}$ $\frac{2P_1(d_2^2 - d_1^2)}{d_2^2 - d_1^2}$ $\frac{2P_1(d_2^2 - d_1^2)}{d_2^2 - d_1^2}$	$ \frac{d_1^2}{d_2^2} \frac{d_1^2}{d_2^2} $					
FrietionC k1= K4 = Po = Fo = Fi = Now C Min ID C mm 86 Calcula Inner E Tube C	0.00061 0.09861 50.31 50.31 8009 8636 heck with att att σR,d1 σR,d2	1 N/mm2 N/mm2 31.3 N 33.1 N hether I Max interf mi 0 3304 = = -13 = -5	K2 = K5 = Recom Diametri erence m .457 the Ma 3.32 N/ 6.02 N/	e, 12 0.096 0.00 1172.58 H 8813.17 H mende al f t terial (mm2 mm2	<pre></pre>	3 K3 = K6 = rence by 3304 nk ube and rRd2 = rRd2 = rRd3 =	0.0991 0.0960 2000 2000 2000 2000 2000 2000 2000	s 7 611 tube age N/mm2 N/mm2	and SS3 $DD SS30 after Shri mm 86.332$	$\frac{+d_s^2}{-d_s^2} - \mu$ $+d$	K ₂ = K ₅ = K ₅ = Ann is Feas Effecti Cleara mm -0.2	$\frac{d_2}{B_2} \left(\frac{d_2}{d_2} + c \right)$ $\frac{d_3}{d_4} \left(\frac{d_4}{d_4} + c \right)$ $\frac{d_4}{B_3} \left(\frac{d_4}{d_4} + c \right)$ $\frac{d_4}{B_4} \left(\frac{d_4}{d_4} +$	$\frac{dz}{dz} + \mu_2 = K$ $\frac{dz}{dz} + \mu_3 = K$ Assembly $\sigma_{r,d_2,G11} = \sigma_{r,d_2,G11} = \sigma_{r,d_$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{4} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $y \text{ During}$ $= 0$ $= -P_{4}$ $= -P_{4}$ $= -P_{6}$	$\frac{2}{3} = -dz$ $\frac{2}{3} = -dz$ $\frac{2}{3} = -dz$ $g \text{ Shrin}$ $\sigma_{cd_{2}}$ $\sigma_{cd_{2}}$ $\sigma_{cd_{2}}$	$k \text{ Fitting}$ $p_{1sc} = -$ $p_{1sc} = -$ $p_{1st} = \frac{P_1}{P_{1st}}$	$\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}+c)}{d_{2}^{2}-d}$ $\frac{(d_{3}^{2}+d_{2}^{2})}{d_{3}^{2}-d}$ $\frac{(d_{3}^{2}+d_{2}^{2})}{d_{3}^{2}-d}$						
FrietionC k1= k4 = Po = Po = Fi = Now C Min ID C Min ID C Calcula Inner E Tube C	0.00051 0.09561 50.31 50.32 8009 8636 heck will 311 1 1 1 1 1 1 1 1 1 1 1 1	N/mm2 N/mm2 31.3 N 39.1 N hether f Max Interf 0 0 sses in 1 304 = = -13 = -5 = 12	K2 = K5 = E Recom Diametri erence M 457 the Ma 9.32 N/ 6.02 N/ 28.11 N/	mm2 mm2 mm2 mm2 mm2	×g d Interfe Max OD S3 before Shri mm 86.557 Df Disc, T	3 K3 = K6 =	0.0991 0.0960 etween (SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30 -50.31 122.40	s 7 8 611 tube age N/mm2 N/mm2 N/mm2 N/mm2	$\frac{d_2}{d_1} = \frac{d_2}{d_2} \begin{bmatrix} d_2 \\ d_3 \end{bmatrix}$ $\frac{d_3}{d_1} = \frac{d_3}{d_2} \begin{bmatrix} d_3 \\ d_4 \end{bmatrix}$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $s_{z}hP_{z}$ 04 Disc 4 nk	$K_2 = K_3 = K_4 = K_5 $	$\frac{d_2}{d_2} \frac{d_2}{d_3} + c$ $\frac{d_3}{d_4} = c$ $\frac{d_4}{d_4} + \frac{d_3}{d_4} = c$ $\frac{d_4}{d_4} + \frac{d_4}{d_4} + c$ $\frac{d_2}{d_4} + c$ $\frac{d_2}$	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{3} = K$ $\frac{d_{1}^{2}}{d_{3}^{2}} + \mu_{3} = K$ Assembly $Tral ssembly \sigma_{r} d_{2} Disc \sigma_{r} d_{2} Disc \sigma_{r} d_{3} Ci1 =$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{6} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{2}} \right]$ $y \text{ During}$ $= 0$ $= -P_{i}$ $= -P_{i}$ $= -P_{o}$	$\frac{2 \ d_{2}}{g} = d_{2}$ $\frac{2 \ d_{2}}{g} = d_{2}$ $\frac{2 \ d_{2}}{g} = d_{2}$ $g \ Shrin$ $\sigma_{c \ d_{2}}$ $\sigma_{c \ d_{2}}$ $\sigma_{c \ d_{2}}$	k Fitting $p_{isc} = -$ $p_{isc} = -$ $p_{isc} = -$ $p_{isc} = -$ $p_{isc} = -$ $p_{isc} = -$ $p_{isc} = -$	$\frac{2P_{i}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{2P_{i}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}+d_{1}^{2})}{d_{2}^{2}-d}$ $\frac{d_{1}^{2}}{d_{3}^{2}-d}$ $\frac{d_{1}^{2}}{d_{3}^{2}-d}$	$\frac{d_1^2}{d_2^2}$ $\frac{d_1^2}{d_2^2}$ $\frac{d_1^2}{d_2^2}$ $\frac{d_1^2}{d_2^2}$ $\frac{d_1^2}{d_2^2}$					
FrietionC K1 = K4 = Po = Fo = Fi = Now C Min ID C mm 86 Calcula Inner E Tube 6	0.00061 0.09861 50.31 50.31 50.31 8636 heck wl all 1 1 1 1 1 1 σR,d1 σR,d1 σR,d2 σC,d2	1 N/mm2 1 N/mm2 13.3 N hether I Max Max 1 N/mm2 13.3 N hether I 1 N/mm2 13.3 N hether I 1 N/mm2 13.5 N 14.5 N 15.5 N 1	K2 = K5 = Becom Comment erence m. 457 the Ma 9.32 N/ 9.32 N/ 6.02 N/ 28.11 N/	e, 12 0.096 0.00 172.58 8813.17 mende al [terial (mm2 mm2 mm2 mm2 mm2	Kg d Interfe Max OD St before Shri mm 88.557 of Disc, T	3 K3 = K6 = rence bo 3304 nk ube and rRd2 = rC,d2 = rRd3 = rC,d3 =	0.0991 0.0960 0.0960 SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30 -50.31 122.40	s 7 8 611 tube age N/mm2 N/mm2 N/mm2	$a = \frac{d_2}{E_2} \left[\frac{d_2}{d_2} \right]$ $a = \frac{d_2}{E_2} \left[\frac{d_2}{d_2} \right]$ $F_0 = f_2 \pi d$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{3hP_{S}}{04 \text{ Disc}}$ $\frac{04 \text{ Disc}}{4 \text{ nk}}$	$K_2 =$ $K_3 =$ $K_5 = f_1 \pi a$ is Feas Effecti Cleara mm -0.2	$\frac{d_2}{B_2} \left\{ \frac{d_2}{d_1} + c \\ B_2 \left\{ \frac{d_2}{d_2} + c \\ B_3 \left\{ \frac{d_1}{d_2} + c \\ \frac{d_2}{d_1} + c \\ \frac{d_1}{d_2} + c \\ \frac{d_2}{d_1} + c \\ \frac{d_1}{d_2} + c \\$	$\frac{d_{2}^{2}}{\sigma_{r}} + \mu_{2} = K$ Assembly $Trai $ $\sigma_{r,d_{2},G_{11}} = \sigma_{r,d_{2},G_{11}} = \sigma_{r,d_{2},G_{2},G_{2}} = \sigma_{r,d_{2},G_{2},G_{2},G_{2}} = \sigma_{r,d_{2},G_{2},G_{2},G_{2}} = \sigma_{r,d_{2},G_{2},G_{2},G_{2}} = $	$c_{3} = \frac{d_{2}}{E_{2}} \left[a - \frac{d_{3}}{E_{2}} \right]$ $c_{4} = \frac{d_{3}}{E_{2}} \left[a - \frac{d_{3}}{E_{2}} \right]$ $y \text{ During}$ $= 0$ $= -P_{1}$ $= -P_{1}$ $= -P_{0}$	$\frac{2}{3} \frac{2}{3} \frac{2}{3} - dz$ $\frac{2}{3} \frac{2}{3} - dz$ $\frac{2}{3} \frac{2}{3} - dz$ $g \text{ Shrin}$ $\sigma_{c dz}$ $\sigma_{c dz}$ $\sigma_{c dz}$	k Fitting Disc = - Disc	$\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}+d_{2}^{2})}{d_{2}^{2}-d_{1}^{2}}$ $\frac{d_{3}^{2}-d_{2}^{2}}{d_{3}^{2}-d_{3}^{2}}$ $\frac{P_{1}(d_{2}^{2}-P_{0})}{d_{3}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}-P_{0})}{d_{3}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}-P_{0})}{d_{3}^{2}-d_{1}^{2}}$						
FrietionC K1= K4= Po= Fo= Fi= Now C Min ID C Min ID C Min ID C Calcula Inner E Tube 6	0.00051 0.09961 50.31 50.31 50.32 8636 heck wl 311 1 1 1 1 1 1 1 1 1 1 1 1	1 N/mm2 N/mm2 31.3 N 39.1 N hether F Max Interf min 0 5304 = = -13 = -5 = 1: 5304	K2 = K5 = Recom Diametric erence m. 457 the Ma 9.32 N/ 9.32 N/ 6.02 N/ 28.11 N/	e, f2 0.096 0.00 1172.58 H 8813.17 H 8813.17 H 8813.17 H 10 8813.17 H 10 8815.17 H 10 8813.17 H 10 8813.17 H	×g d Interfe Max OD SS before Shri mm 86.557 of Disc, T	3 K3 = K6 = rence bo 3304 nk ube and rRd2 = rC,d2 = rC,d3 =	0.0991 0.0960 etween (SS shrink upto 800 0.225 1 Ring -56.02 -83.30 -50.31 122.40	s 7 8 11 tube age N/mm2 N/mm2 N/mm2	$\frac{d_2}{d_1} = \frac{d_3}{Z_2} \left[\frac{d_3}{d_3} \right]$ $\frac{d_3}{Z_2} = \frac{d_3}{Z_2} \left[\frac{d_3}{d_3} \right]$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ synPg 04 Disc 4 nk	$K_2 = K_5 $	$\frac{d_2}{d_2} = \frac{d_2}{d_3} = \frac{d_1}{d_4} = $	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{3} = K$ $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3} = K$ Assembly $\sigma_{rd_{2}} \rho_{1s} = \sigma_{rd_{2}} \rho_{1s} =$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{4} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $y \text{ During}$ $= 0$ $= -P_{4}$ $= -P_{4}$ $= -P_{6}$ $= -P_{6}$	$\frac{2}{3} = \frac{d_{z}}{d_{z}}$ $\frac{2}{3} = -\frac{d_{z}}{d_{z}}$ $\frac{2}{3} = \frac{d_{z}}{d_{z}}$ $\frac{2}{3} = -\frac{d_{z}}{d_{z}}$ $\sigma_{c} d_{2} d_{z}$ $\sigma_{c} d_{2} d_{z}$ $\sigma_{c} d_{2} d_{z}$ $\sigma_{c} d_{2} d_{z}$	k Fitting $p_{isc} = -$ $p_{isc} $	$\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}+d_{1}^{2})}{d_{2}^{2}-d}$ $\frac{(d_{3}^{2}+d_{2}^{2})}{d_{3}^{2}-d}$ $\frac{(d_{4}^{2}+d_{2}^{2})}{d_{3}^{2}-d}$	$ \frac{d_1}{d_2} \\ \frac{d_2}{d_3} \\ \frac{d_4}{d_4} \\ \frac{d_1^2}{d_2^2} \\ \frac{d_2^2}{d_2^2} \\ d$					
FrietionC K1 = K4 = Po = Po = Fi = Now C Min ID C mm 86 Calcula Inner E Tube 6 Outer I	0.00061 0.09861 50.31 56.02 8003 8636 heck wl att att att σF,d1: σC,d1: σC,d2 Ring SS att σF,d2 σC,d2 αtt αtt αtt αtt αtt αtt αtt αt	N/mm2 N/mm2 N/mm2 31.3 N 39.1 N hether I Max Interf min 0 sses in iso4 = 10	K2 = K5 = = 8 = 8 Recom Diametri erence m 457 the Ma 0 N/ 9.32 N/ 6.02 N/ 28.11 N/	e, f2 0.096 0.00 172.58 8813.17 mende al f terial (mm2 mm2 mm2 mm2 mm2 mm2 mm2 mm	<pre>s73 s73 s73 s73 s73 s73 s73 s73 s73 s73</pre>	3 K3 = K6 = rence b 3304 nk ube and rRd2 = rC,d2 = rC,d3 = rC,d3 =	0.0991 0.0960 0.0960 SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30 -50.31 122.40	s S S S S S S S S S S S S S S S S S S S	$\frac{d_2}{d_1} = \frac{d_2}{d_2} \begin{bmatrix} \frac{d_2}{d_2} \\ \frac{d_1}{d_2} \end{bmatrix}$ $\frac{d_2}{d_2} = \frac{d_2}{d_1} \begin{bmatrix} \frac{d_1}{d_2} \\ \frac{d_2}{d_2} \end{bmatrix}$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{s_{PB}}{s_{PB}}$ 04 Disc 4 nk	$K_2 = K_3 = K_5 $	$\frac{d_2}{E_2} \left(\frac{d_2}{d_3} + c \\ \frac{d_3}{d_4} + c \\ \frac{d_4}{E_3} + c \\ \frac{d_4}{d_4} + \frac{d_4}{E_3} + c \\ \frac{d_4}{d_4} + c \\$	$\frac{d_{2}^{2}}{d_{3}^{2} + \mu_{2}} = K$ $\frac{d_{1}^{2}}{d_{3}^{2} + \mu_{3}} = K$ Assembly $Tral ssembly \sigma_{rd_{2} \text{ Disc}} \sigma_{rd_{2} \text{ Disc}} \sigma_{rd_{2} \text{ Cis}} \sigma_{rd_{3} \text{ Cis}} \sigma_{rd_{3} \text{ Ring}}$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{e_{1}} \right]$ $c_{4} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{e_{1}} \right]$ $y \text{ During}$ $= 0$ $= -P_{i}$ $= -P_{i}$ $= -P_{o}$ $= -P_{o}$	$\frac{2 \ d_{2}}{d_{1}^{2} - d_{2}^{2}}$ $\frac{2 \ d_{1}^{2}}{d_{1}^{2} - d_{2}^{2}}$ $g \ Shrin$ $\sigma_{c \ d_{2}}$ $\sigma_{c \ d_{2}}$ $\sigma_{c \ d_{2}}$ $\sigma_{c \ d_{2}}$	k Fittin $p_{isc} = -$ $p_{isc} =$	$\frac{2P_{i}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}+d_{1}^{2})}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}+d_{2}^{2})}{d_{3}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}-P_{0})}{d_{3}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}-P_{0})}{d_{3}^{2}-d_{1}^{2}}$ $\frac{P_{i}(d_{2}^{2}-H_{0})}{d_{3}^{2}-d_{1}^{2}}$	d1 d2 d3 d4 d4 (d3 d4 (d3 d4 (d3 d4 (d4 (d3 d4 (d4 (d3 (d4 (d4 (d4 (d4 (d4 (d5 (d4 (d5 (d4 (d5 (d5))))))))))))))))))))))))))))))))))))					
FrietionC K1 = K4 = Po = Po = Fi = Now C Min ID C mm 86 Calcula Inner E Tube 6 Outer I	0.00061 0.09661 50.31 50.31 50.32 8636 heck with 311 1 1 1 1 1 1 1 1 1 0 1 0 7 C,d1 3 1 σ C,d1 3 1 σ C,d1 3 1 0 7 C,d1 3 1 0 0 C,d1 3 1 0 0 0 0 0 0 0 0 0 0 0 0 0	1 N/mm2 N/mm2 31.3 N 39.1 N hether f Max Interf Max interf 304 = -13 = -13 = 1.3 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	K2 = K5 = = K = Recom Diametri erence m 457 the Ma 0 N/ 9.32 N/ 6.02 N/ 28.11 N/ 50.31 N/	mm2 mm2 mm2 mm2 mm2	Kg d Interfe Max OD S before Shri mm 86.557 of Disc, T	<pre>3 K3 = K6 = K</pre>	0.0991 0.0960 2tween (SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30 -50.31 122.40	s S S S S S S S S S S S S S S S S S S S	and SS3 $DD SS30$ $after Shrimmer 86.332$	$\frac{+d_z^2}{-d_z^2} - \mu$ $\frac{+d_z^2}{-d_z^2} - \mu$ synRs 04 Disc 4 nk	K2 = K5 =	$\frac{d_2}{d_2} = \frac{d_2}{d_3} + \frac{d_1}{d_4} + $	$\frac{d_{2}^{2}}{d_{3}^{2}} + \mu_{2} = K$ $\frac{d_{3}^{2}}{d_{3}^{2}} + \mu_{3} = K$ Assembly $\sigma_{rd_{2}} D_{10} c$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{8} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $p \text{During}$ $= 0$ $= -P_{1}$ $= -P_{1}$ $= -P_{0}$ $= -P_{0}$	$\frac{2}{3} = dz$ $\frac{2}{3} = -dz$ $\frac{2}{3} = -dz$ $\frac{2}{3} = -dz$ $\sigma_{c} dz$ $\sigma_{c} dz$ $\sigma_{c} dz$ $\sigma_{c} dz$	k Fitting $p_{1sc} = -$ $p_{1sc} $	$\frac{2P_1d_2^2}{d_2^2 - d_1^2}$ $\frac{d_2^2 - d_1^2}{d_2^2 - d_1^2}$ $\frac{d_2^2 - d_1^2}{d_2^2 - d_2^2}$ $\frac{d_2^2 - P_1(d_2^2 - P_2)}{d_3^2 - d_1^2}$ $\frac{d_1d_2^2 - P_2}{d_1^2 - d_2^2}$						
FrietionC k1 = K4 = Po = Pi - Fo = Fi = Now C Min ID C mm 86 Calcula Inner C Tube C	0.00051 0.09561 50.31 50.32 8009 8636 heck with atternation of the strength or R,d1 or R,d1 or R,d1 or R,d1 or R,d1 or R,d1 or R,d1 or R,d1 or R,d1 or R,d2 or R,d1 or R,d2 or R,d1 or R,d2 or R,d1 or R,d2 or R,d1 or R,d2 or R,d1 or R,d2 or R,d2 or R,d3 or R,d3	N/mm2 N/mm2 31.3 N 39.1 N Max Interf Max Interf 0 0 sses in 304 = = -13 = -5 = 12 5304	K2 = K5 = E Recom Diamete erence M 457 the Ma 9.32 N/ 8.32 N/ 8.32 N/ 8.32 N/ 8.32 N/ 9.33 N/	mm2 mm2 mm2	<pre>s73 s73 s73 s73 s73 s73 s73 s73 s73 s73</pre>	3 K3 = K6 = rence b 3304 nk ube and rRd2 = rC,d2 = rC,d3 = rC,d3 = rRd4 =	0.0991 0.0960 0.0960 SS shrink upto 80K mm 0.225 1 Ring -56.02 -83.30 -50.31 122.40 0	s 7 8 311 tube age N/mm2 N/mm2 N/mm2 N/mm2	$\frac{d_2}{E_1} \begin{bmatrix} d_2 \\ d_3 \end{bmatrix}$ $\frac{d_2}{E_2} \begin{bmatrix} d_3 \\ d_4 \end{bmatrix}$ $\frac{d_2}{E_2} \begin{bmatrix} d_4 \\ d_4 \end{bmatrix}$ and SS3 OD SS30 after Shri mm 86.332	$\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $\frac{+d_{z}^{2}}{-d_{z}^{2}} - \mu$ $a_{z}^{n}AP_{s}$ 04 Disc 4 nk	$K_2 = K_3 = K_4 = K_5 $	$\frac{d_2}{E_2} \left(\frac{d_2}{d_1} + c \\ \frac{d_2}{E_3} + c \\ \frac{d_3}{d_4} + \frac{d_4}{E_3} + c \\ \frac{d_4}{d_4} + \frac{d_4}{E_3} + \frac{d_4}{d_4} + c \\ \frac{d_4}{d_4} + \frac{d_4}{d_4}$	$\frac{d_{12}^{2}}{d_{13}^{2} + \mu_{2}} = K$ $\frac{d_{12}^{2}}{d_{13}^{2} + \mu_{3}} = K$ Assembly $Tral ssembly \sigma_{r} d_{1} Disc \sigma_{r} d_{2} Disc \sigma_{r} d_{2} Ci1 \sigma_{r} d_{3} Ring$	$c_{3} = \frac{d_{2}}{E_{2}} \left[\frac{d_{3}}{d_{1}} \right]$ $c_{6} = \frac{d_{3}}{E_{2}} \left[\frac{d_{3}}{d_{2}} \right]$ $y \text{ During}$ $= 0$ $= -P_{i}$ $= -P_{i}$ $= -P_{o}$ $= -P_{o}$	$\frac{2 \ d_2}{g_1^2} - \frac{d_2}{d_2}$ $\frac{2 \ d_2}{g_2^2} - \frac{d_2}{d_2}$ $g \ Shrin $ $\sigma_c \ d_2 t$ $\sigma_c \ d_2 t$ $\sigma_c \ d_2 t$	k Fittin $p_{isc} = -$ $p_{isc} =$	$\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{2P_{1}d_{2}^{2}}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}-d_{1}^{2})}{d_{2}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}-d_{1}^{2})}{d_{3}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}-P_{0})}{d_{3}^{2}-d_{1}^{2}}$ $\frac{P_{1}(d_{2}^{2}-H_{0}^{2})}{d_{3}^{2}-d_{1}^{2}}$	$ \frac{d_1}{d_2} \\ \frac{d_2}{d_3} \\ \frac{d_4}{d_4} \\ \frac{d_4}{d_2} \\ \frac{d_4}{d_2} \\ \frac{d_2}{d_2} \\ \frac{d_2}{d_2} \\ \frac{d_3}{d_2} \\ \frac{d_4}{d_2} \\ \frac{d_4}{d_4} \\ \frac{d_4}{d_4} \\ \frac{d_4}{d_4} \\ \frac{d_4}{d_4} \\ \frac{d_4}{d_4} \\$					

Remarks on Cryomodule Development



- Many very good ideas and much work have already gone into cryomodule design by various laboratories around the world.
- Fermilab and RRCAT are building upon the experience from these laboratories as well as continuing our own analysis & design work in developing a cryomodule design for the unique requirements of 650 MHz, CW section of the Project X linac.
- Tesla type of cryomodule has been taken as the baseline and this design is being modified to accommodate the requirements of the project.
- A major value engineering exercise has been taken up.
- Very close interaction through fortnightly WEBEX meetings has resulted in covering a lot of ground.





String Assembly







MP9 Clean Room









Final Assembly



1st U.S. built ILC/PX Cryomodule



1st Dressed Cavity



Fermilab Vertical Test Stand











MAGNETIC

- Indian Institutions have provided engineering resources to design an upgraded Vertical Test Stand for Fermilab.
 - It is being fabricated by a US vendor using ARRA funds
 - RRCAT also purchased one
- RRCAT has carried out design of the following:
- Liquid Helium Vessel Shell
- Liquid Helium Vessel Top Flange
- Vacuum Vessel Shell
- Vacuum Vessel Flange
- Top Insert Plate
- RRCAT has also verified the design of following by Analysis
- Assembly of LHe Vessel Top Flange, Weld Rim
- Top Insert Plate
- Assembly of Vacuum Vessel Flange, LHe Vessel Flange, Top Plate, Support Pads
- Magnetic Shield design 300K & 2K



3-D MODELS OF VTS-2 VESSELS



Horizontal Test Stand (HTS)







- Purpose: high power tests of dressed cavities
 - "high power" = tens to hundreds of kW of input power
 - "dressed" = LHe vessel, high power input coupler, mechanical tuners, HOM couplers
- Test goal 1: qualify cavities for CM assembly based on Q₀, E_{acc}, field emission
- Test goal 2: verify functionality of auxiliary components



HTS data: examples











- HTS-2 is a facility similar to HTS but with expanded capabilities
 - Cool down of two cavities simultaneously
 - Doubles the number of tests that can be done per thermal cycle
 - Testing of either 650 or 1300 MHz cavities
 - CW testing as well as pulsed
 - Testing a cavity + magnet package
- An IIFC project
 - India will design and procure the cryostat and its cryogenic feed box, including J-T heat exchanger
 - Fermilab will assemble RF system and other test infrastructure
 - Similar facility to be built in India based on HTS-2 experience

HTS-2 cryostat design at RRCAT







325 MHz Spoke Cavity Processing at ANL





- Chemical polishing, high-pressure rinsing in G150 by Argonne and Fermilab SRF staff
- Cold testing performed at Fermilab
- Both cavities have achieved world leading performance



41111 43510

• Extensive infrastructure completed for CM assembly



String Assembly in Class 10 area of MP9 Clean Room



Exterior of MP9 Clean Room



SRF Infrastructure at ANL



 Joint facility built by ANL/FNAL collaboration

EP processing of 1300 MHz 9-cells
Together with Jlab, ANL/FNAL facility represents state-of-the-art cavity processing facilities for ILC or Project X
Adding 650 MHz processing infrastructure



Electropolishing





High-pressure rinse



SRF Infrastructure at Fermilab



- KEK/Kyoto optical inspection system, commissioned in 2009
- In routine use examining cavities after each step of processing

- Automated Cavity tuning machine
- DESY/FNAL/KEK collaboration
- 2 machines at DESY, one at KEK
- FNAL machine in routine use





SRF Infrastructure at Fermilab



Vacuum Oven 1 of 2



- Removes H₂ introduced during surface treatment
- Key to high Q operation at high gradient

Fermilab is helping RRCAT purchase this from US vendor

Infrastructure for Cavity Development



Infrastructure installed at RRCAT in Collaboration with Fermilab

- Electro-polishing setup
- Centrifugal barrel polishing machine
- High pressure rinsing
- Cavity forming facility



Cavity forming facility







Centrifugal barrel polishing machine



High pressure rinsing Set up





Large scale SRF Infrastructure being set up at RRCAT in collaboration with Fermilab.

- Clean room (class 10000 to 10)
 - Fermilab Design
- Electron beam welding machine
 - US Vendor
- High vacuum annealing furnace
- Cavity machining facilities
- CMM, SIMS etc
- Building under construction (area 70m x 20m)



Building expected to be ready by mid - 2011

SRF Test Linac Project Overview



Overall Goals

- Build a RF Unit Test Facility at the New Muon Lab (NML)
 - ILC RF Unit = 3 cryomodules
 - 10-MW RF system
 - Beam with ILC parameters (3.2 nC/bunch @3 MHz, Up to 3000 bunches @ 5Hz, 300-µm rms bunch length)
- Build a RF Unit for Project X (like ILC but 4 cryomodules @25 MV/M)
- Build Test facilities for Project-X cryomodules
- Phase-1 (FY07 FY10) (Completed Dec. 2010)
 - Prepare facility for testing first cryomodule (CM1) without beam
 - Infrastructure, RF power, cryogenics (Tevatron satellite refrigerators #1 & #2)
 - Install first cryomodule (CM1) and Capture Cavity-2 (CC2), cooldown, and begin RF testing
 - New tunnel civil construction (capability for 2 RF units)

SRF Test Linac Project Overview



• Phase-2 (FY11 – FY12)

- Prepare for First Beam
 - Civil construction for new cryoplant and test stands
 - Move parts from FNPL photo-injector to NML
 - Install new gun, injector, Test beamlines, and beam dump
 - Swap CM1 with second cryomodule (CM2) (S1)
 - Commission gun generate first beam
 - Accelerate beam through single cryomodule

Phase-3 (FY12 – FY14)

- Complete RF Unit
 - Upgrade RF system to 10 MW
 - Install RF Unit (3 cryomodules)
 - Commission new Cryogenic Plant
 - Operate full RF Unit with beam (S2)



Phase-1 Layout of SRF Test Linac










Phase-2 Layout of SRF Test Linac







Phase-2 Civil Construction





Phase-3 of SRF Test Linac and CMTF







Future NML Complex







Cryomodule-1 (CM1)







Cool down of CM1





Cool down to 2 Kelvin (~2 hours)

Cool down to 4.5 Kelvin (2+ days)





Cavity #1 Performance





Fast Thermometry response during a possible quench

BARC: Cryomodule Test Stand



 Conceptual Arrangement of Feed Box, Feed Cap, End Cap & Transfer Lines.



- Status: Design & Drawing of all three subassemblies is taken up.
- CMTF (FY15):Test Stands for Project X
 - Install shielding, RF, cryo for PX test stands
 - 1300 MHz (pulsed) CM test stand (with India)
 - 650 MHz (CW) CM test stand (with India)





- Injector
 - Detailed Lattice designed
 - New gun system being installed
 - Collaboration with DESY, KEK & INFN
 - CC2 (single 9-cell cavity) operational 10/09
- Accelerator
 - CM1 installed, aligned, and under vacuum
 - Cooled, Under RF Power







- The Phase II of this collaboration would expand the present R&D collaboration to all non SRF areas of Project-X
- Elements of Phase II: R&D
 - Front End: Source and RFQ
 - 325 MHz RF Power
 - 650 MHz RF Power
 - Power Coupler
 - Instrumentations and Controls
 - Superconducting Magnet
 - Cryogenics
- The technical discussions have already started
 - This meeting will outline these areas of collaboration

BARC: Solid State Amplifiers at 325 MHz



1 kW (2 nos.) and 5 kW (1 No.) Solid-state amplifiers

Specifications from Fermilab:

- Center frequency : 325 MHz
- Bandwidth (3 dB) : 10 MHz
- Power output (1 dB), CW : 1 kW and 5 kW
- Gain (1 dB), minimum : 50 dB
- Gain Stability : +/-0.5 dB
- Stability : Un conditionally Stable
- Cooling : Water Cooled
- Harmonics & Spurious : <30 dBc
- Efficiency (Total) : > 50%
- Gain Stabilization with in +/- 0.5 dB



1 kW solid state module under testing at BARC

Solid State Amplifier Development 650 MHz

- प्रजवि प्रजवि
- RRCAT has taken up development of 30 kW CW 650 MHz solid state amplifiers for energizing SCRF cavities

8kW Amplifier Scheme

30kW Amplifier Scheme



 32 Nos. of 270 W RF modules are used with suitable combiners and dividers to make a 8 kW RF amplifier module. Four such modules will be combined to obtain 30 kW RF power output.



Input coupler





Coaxial design, adjustable, 76.9 mm outer/33.4 mm inner, two disk-type ceramic windows.



3 couplers are in-house and tested. One currently installed in test cryostat. Design modifications in-process to reduce weight.





- Fermilab and DAE accelerator laboratories have proposed to jointly work
 - On the construction and commissioning of the Project-X accelerator at Fermilab
 - Development of Indian capabilities and industrial infrastructure that could lead the construction of HIPA in India.
- India is expected to make significant In-Kind contributions
 US will share accelerator technology and knowledge
- The Accelerator collaboration started in 2006 and has now gone into the 3rd stage
 - 1. Component level \rightarrow Scientists to Scientists
 - 2. System Level \rightarrow Laboratories to Laboratories
 - 3. Facility Level \rightarrow Agency to Agency
 - i. Fermilab has worked with US DOE in developing a DOE-DAE agreement based on IIFC discussion to date)
 - ii. At present the US-DOE and DAE are working to negotiate the language and high level details of DOE-DAE agreement.

Collaboration on High Energy Physics



- Indian institutions have been collaborating on Fermilab based High Energy Physics experiments since 1986.
 - Several students have received PhD from Indian universities while working on Fermilab experiments.
- Recently we have established a Neutrino Physics collaboration with India
 - Indian Institutions have joined MINOS, MIPP and LBNE
 - Students and faculties are contributing to the analysis
 - Several PhD thesis
 - Faculty and engineering staff are getting involved in design of future experiments.
- We held a joint workshop in Jan 2011 to discuss collaboration on all aspect of High Energy Physics, Nuclear Physics and Energy
 - Support is overwhelming
 - We are developing a set of proposal for XII plan.



Colleagues at Fermilab under IIFC





Accelerator: 5+1 (1 Student), HEP: 6+2 (5+2 Students)

IIFC Developing Indian Technical Expertise



Summary



- Indian Institutions and Fermilab have established an excellent working relationship and are collaborating on SRF part of the High Power Linac for HIPA.
 - Progress is being made on several fronts.
- We are proceeding to expand this R&D collaboration to all non-SRF aspect of the accelerator.
- Fermilab has proposed to build a 3 GeV CW, ~3 MW SRF linac (followed by 3-8 GeV Pulsed SRF Linac) for its High Energy Physics program.
 - The design of this SRF linac is aligned with Indian 3rd Stage Nuclear program.
- This is an unprecedented opportunity for both Indian and US Institutions, and agencies to collaborate on jointly developing accelerators for its domestic program.
 - Total Project Collaboration
- During this meeting
 - we need to make significant technical progress on Phase I and II
 - Discuss steps that could be taken to make a plan for Phase III