



Noise Effects on Emittance Blow-up and Luminosity Degradation in HL-LHC

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LBNL

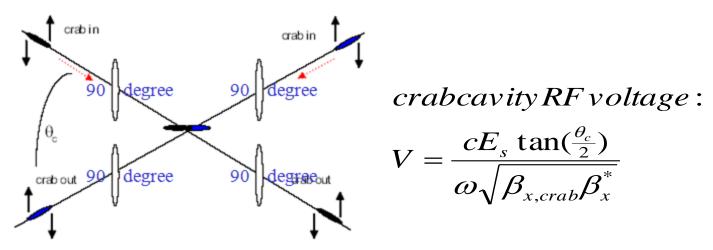
In collaboration with T. Pieloni, J. Barranco, K. Ohmi, T. Mastori, A. Ratti

Joint HiLumi-LARP Annual Meeting, May 11-13, 2015, Fermilab

• High energy collider, LHC, needs large luminosity

$$L(d_x, \phi_y, \sigma_x, \sigma_y, \sigma_s) = L_0 \frac{e^{-\frac{d_x^2}{4\sigma_x^2}}}{\sqrt{1+\zeta^2}}$$
$$L_0 = \frac{N^2 n_b f_0}{4\pi\epsilon\beta^*} \qquad \zeta = \frac{\phi}{2} \frac{\sigma_s}{\sigma_x}$$

- LHC beam collides with an crossing angle to reduce the long-range beam-beam effects
- Crab cavity compensates the luminosity loss due to crossing angle



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RF Noise in the Crab Cavity Causes Emittance Growth and Luminosity Degradation



$$x_i \propto V_{cc} \sin(kz_i + \delta \varphi)$$

0th order error (phase error): $\delta X = -\frac{c}{\omega_{cc}} \tan\left(\frac{\theta}{2}\right) \delta \varphi$

1st order error (voltage error): $\delta x_i \propto \delta V_{cc} \sin(kz_i) \approx \delta V_{cc} kz_i$

white noise offset collision drives emittance growth

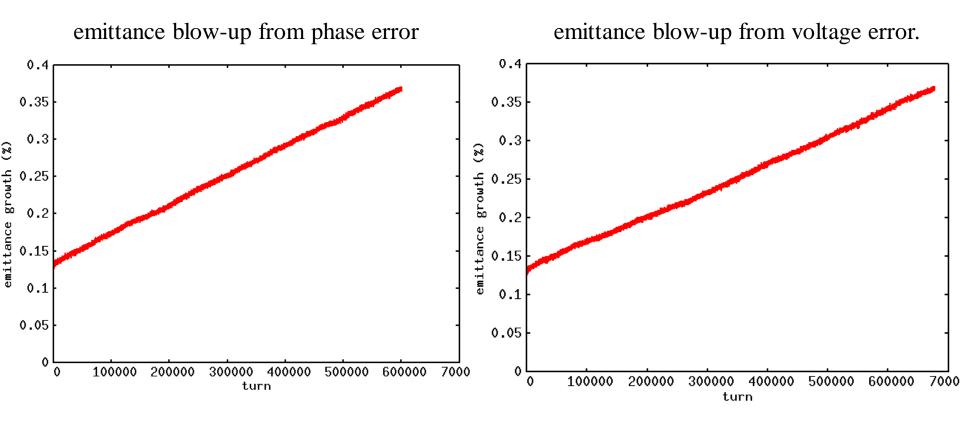
$$\frac{\delta\varepsilon}{\varepsilon} \approx \frac{K}{\left(1 + \frac{G}{2\pi|\xi|}\right)^2} \frac{\delta x^2}{\sigma_x^2}$$

$$G = 1/\tau$$

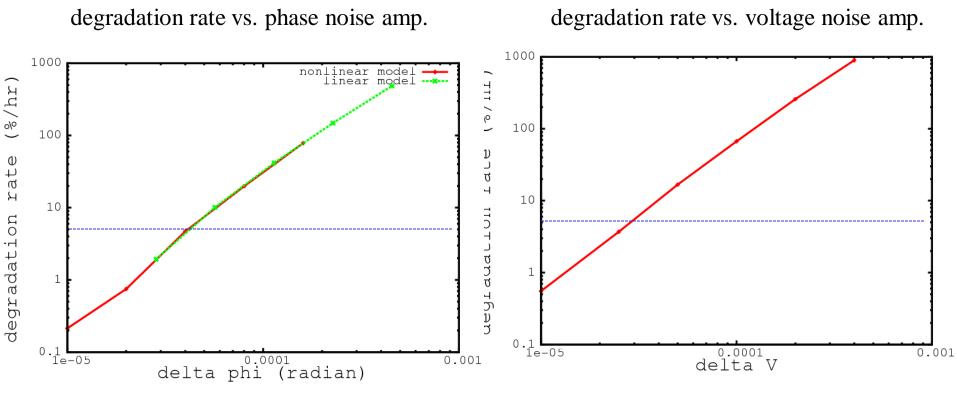
$$\Delta x^2 = \frac{\delta x^2}{2G}$$

$$\frac{\Delta L}{L} = 10.8 \left(\xi \frac{\Delta x}{\sigma}\right)^2$$
G. Stupakov, SSC-560 (1991).
T. Sen and J. Ellison, PRL 77, 1051 Y. Alexahin, NIM A391,73 (1996)
(1996)
K. Ohmi, in Proc. Beam-Beam 2013 workshop.





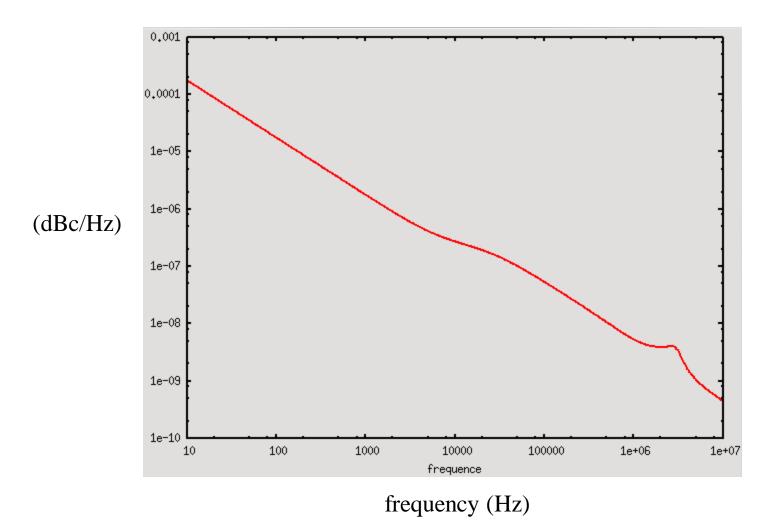




In order to have a good luminosity lifetime ~ 20 hours, the noise amplitude needs to be kept below the level of a few 10^{-5} .

J. Qiang et al., in Proc. IPAC2015.

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Courtesy of T. Mastori

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BeamBeam3D: Parallel Strong-Strong / Strong-Weak Simulation

- Multiple-slice model for finite bunch length effects
- New algorithm -- shifted Green function -- efficiently models long-range parasitic collisions
- Parallel particle-based decomposition to achieve perfect load balance
- Lorentz boost to handle crossing angle collisions
- Arbitrary closed-orbit separation (static or time-dep)
- Independent beam parameters for the 2 beams
- Multiple bunches, multiple collision points
- Linear transfer matrix + one turn chromaticity
- Conducting wire, crab cavity, e-lens compensation model



- Strong-Strong beam-beam forces with soft-Gaussian approximation
- Two IPs per turn
- Use both ideal feedback model and a damper feedback model
- Local crab-cavity correction (4 CCs per beam)
- Frequency dependent crab cavity phase errors and voltage errors
- Phase errors amplitude ~ voltage errors amplitude
- 8 slices per beam
- 1 million macroparticles per beam



Physical parameters	
Е	0.335 nm
pick-up gain	0.05
Tunes	62.31/60.32
Chromaticity	0 – 4
β*	15-60 cm
Θ	0.59 mrad
ξ	0.011 - 0.022
N	$1.1 - 2.2 \times 10^{11}$
IPs	2

Procedure to Generate Turn-Dependent Noise Used in the Simulation Using Frequency-Dependent Noise Spectrum

1) noise errors in each crab cavity are independent of each other;

2) to get the noise error vs. turn, assume 256 samplings per turn (to reach MHz in frequency domain), and for 131072 turns, generate a random white Gaussian noise by sampling a random Gaussian distribution (0,1) using 131072 x 256 data points;

3)FFT the random Gaussian sampling data and extract the frequency dependent data;

4)multiply that frequency dependent data with the spectral data after taking $(Sqrt(10^{(data/10)}));$

5) take an inverse FFT of the signal and back to time domain;

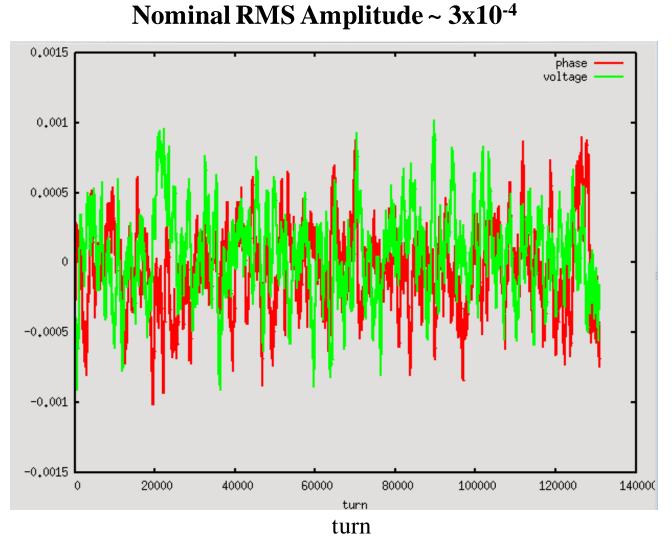
6) for every 256 data points, select only 1 point to obtain the turn-dependent signal to be used in the crab cavity beam-beam simulation.

7)scale the turn-dependent noise to the nominal rms noise amplitude $\sim 3x10^{-4}$.

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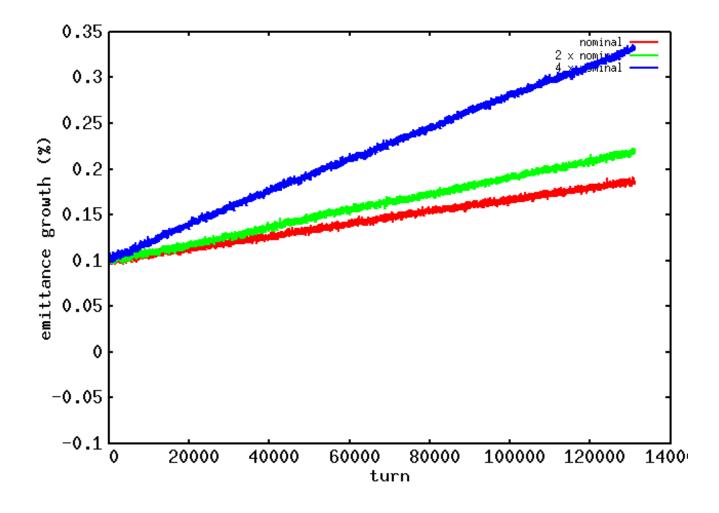
Crab Cavity Noise in Time Domain





there are additional 14 turn-dependent noise similar to the above ones

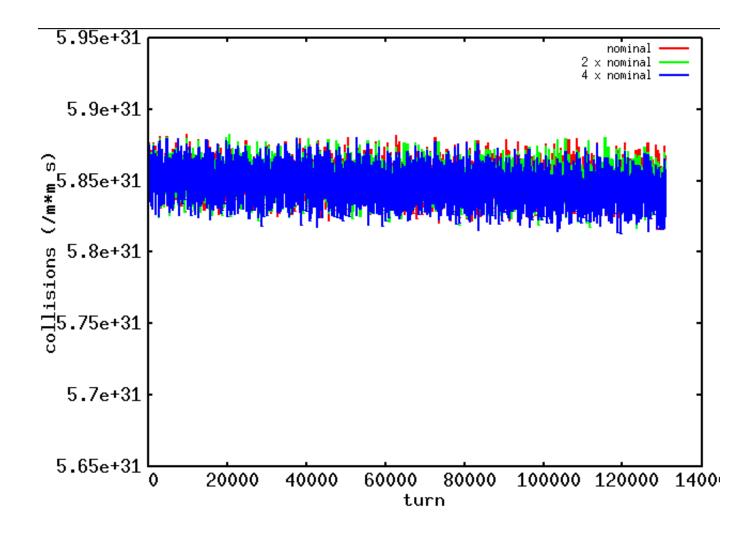
RMS Emittance Evolution with Different Noise Amplitudes



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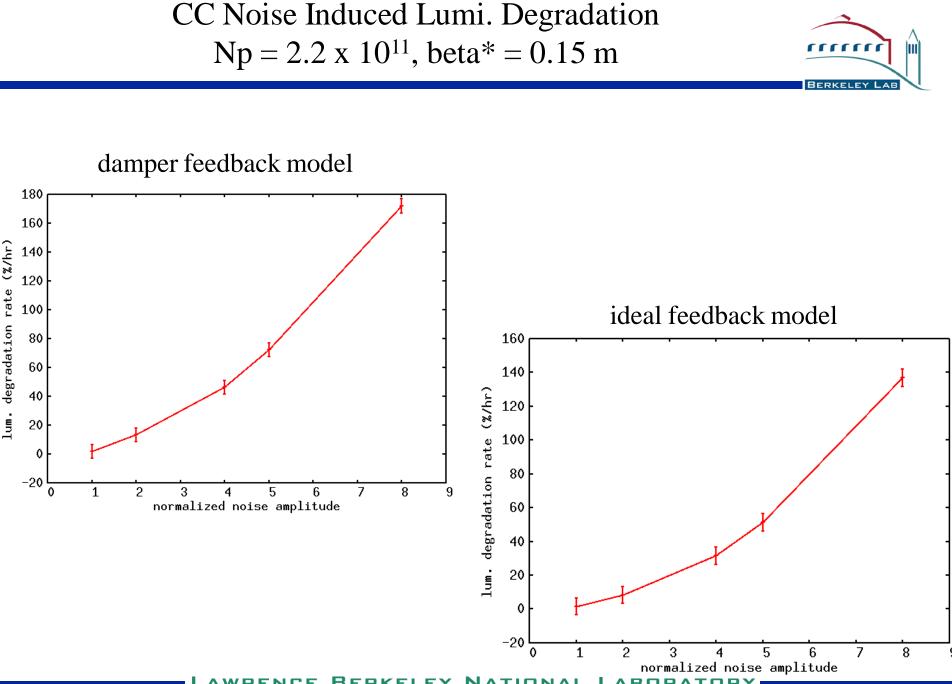
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Peak Luminosity Evolution with Different Noise Amplitudes



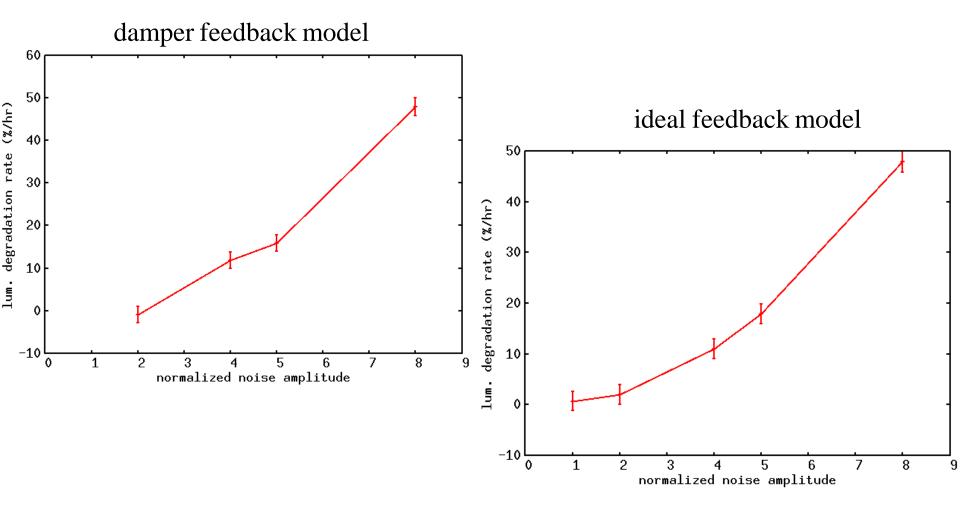
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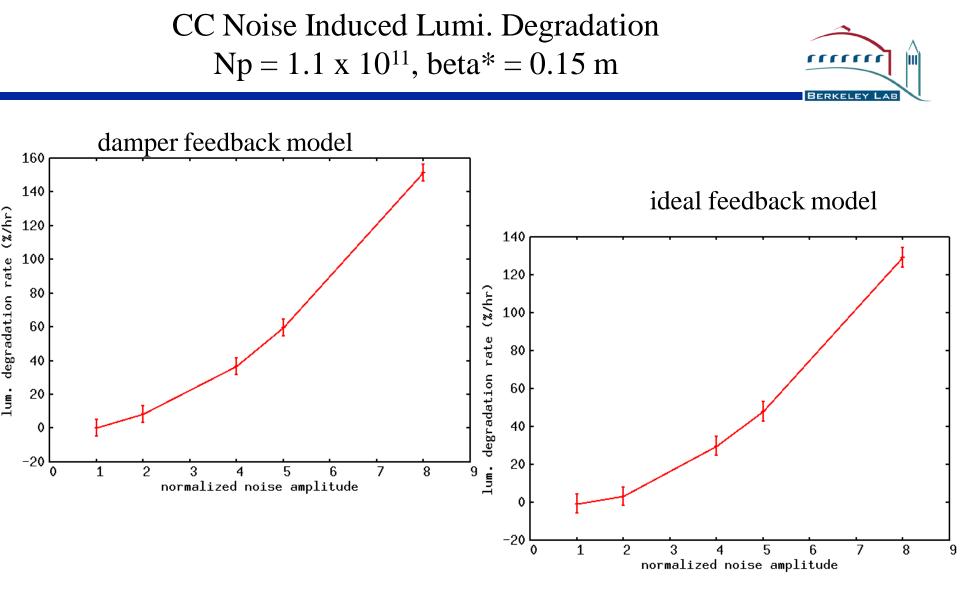
CC Noise Induced Lumi. Degradation Np = 2.2×10^{11} , beta* = 0.49



rrrr

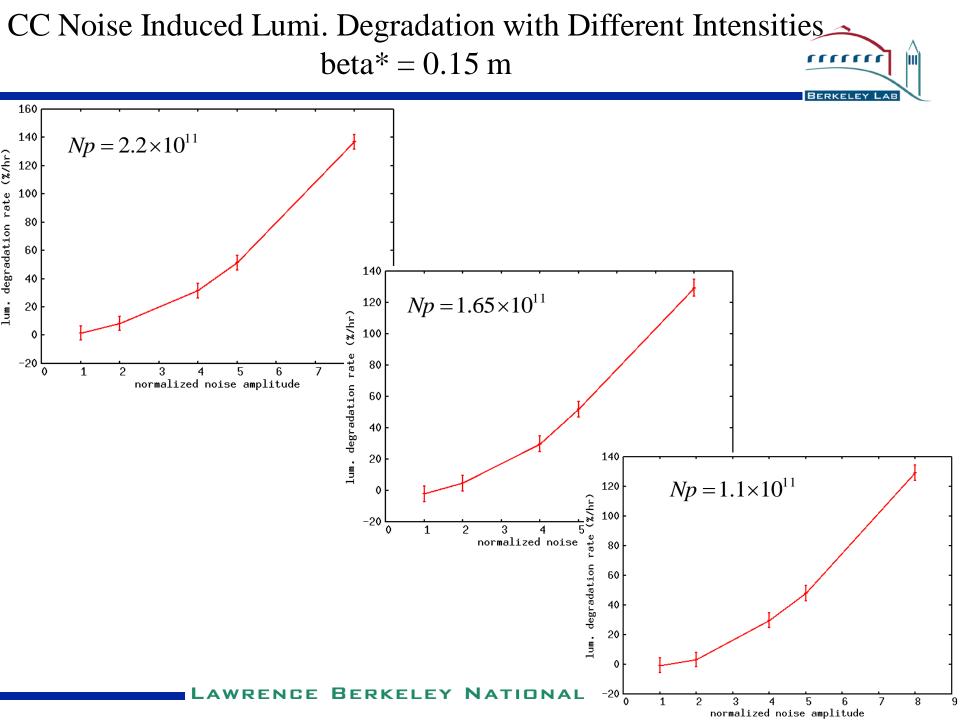
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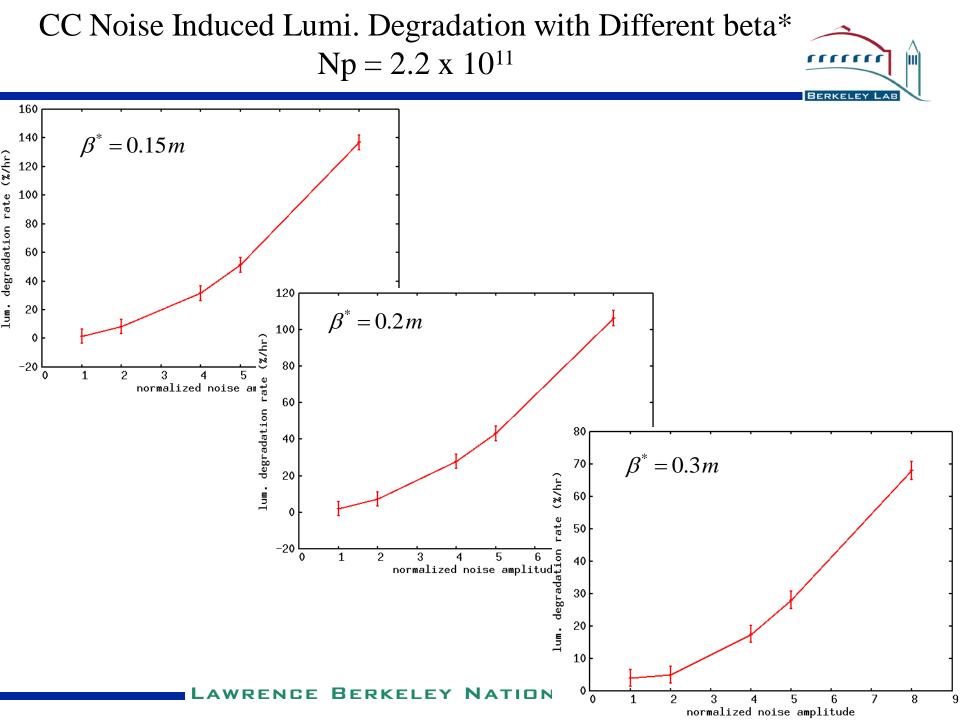
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- Damper feedback model and ideal feedback model show similar degradation rate
- A factor of two of the nominal noise amplitude might be acceptable for good luminosity lifetime

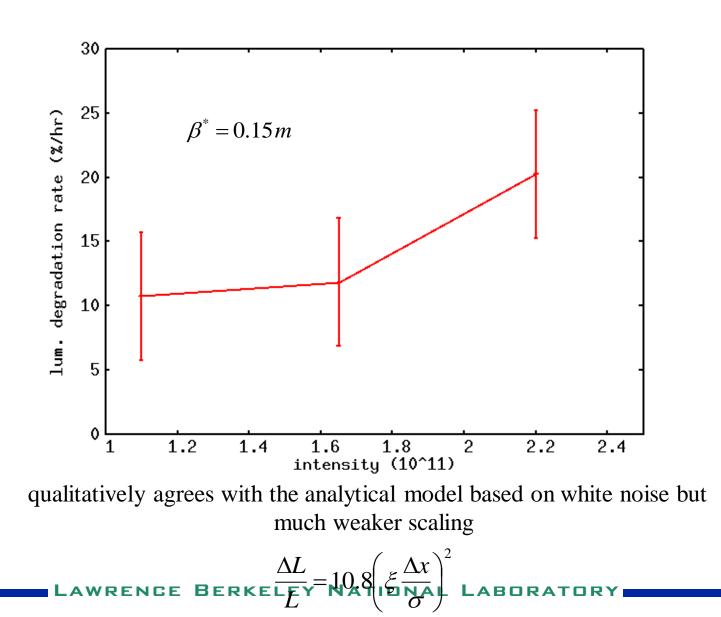
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CC Noise Induced Lumi. Degradation with Different beta* $Np = 2.2 \times 10^{11}$ **rrrr** AE $\beta^* = 0.4 m$ lum. degradation rate (%/hr) $\beta^* = 0.49 m$ rate (%/hr) -10 $\beta^* = 0.6m$ (%/hr) Imm. degradation -10 -56 AWRENCE BERKELEY NATION normalized noise amplitude

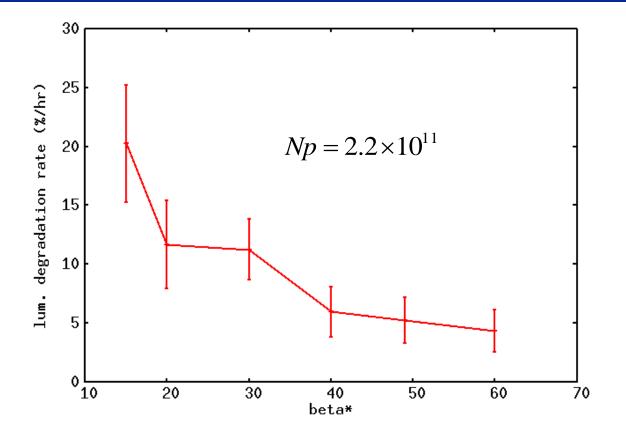
CC Noise Induced Lumi. Degradation with vs. Intensity (with nominal noise amplitude)



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CC Noise Induced Lumi. Degradation with vs. beta*

(with nominal noise amplitude)



qualitatively agrees with the analytical model based on white noise

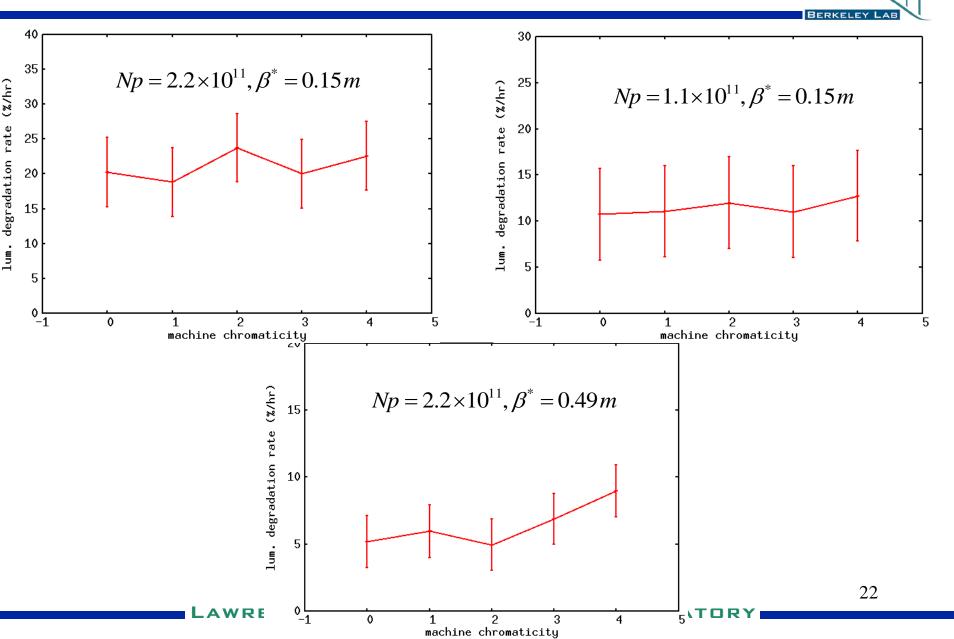
$$\frac{\Delta L}{L} = 10.8 \left(\xi \frac{\Delta x}{\sigma}\right)^2$$

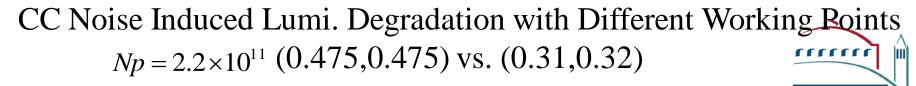
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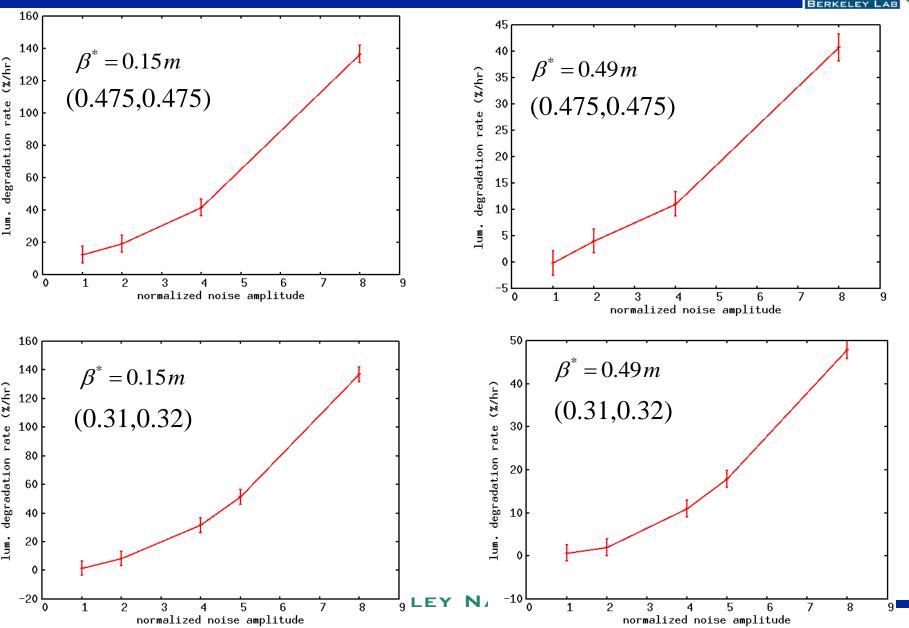
Lumi. Degradation with Different Chromaticities (and with nominal CC noise amplitude)

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Conclusions



- Frequency-dependent noise error shows larger error tolerance than the white noise error for luminosity lifetime.
- Nominal 3x10⁻⁴ frequency-dependent phase and voltage noise rms amplitude will not cause significant luminosity lifetime degradation during beta* leveling.
- Luminosity degradation rate decreases with the increase of the beta*.
- Luminosity degradation rate increases with the increase of the bunch intensity.
- Luminosity degradation rate is not sensitive to the machine chromaticity and tune working point.